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Bridge 1-159 on James St. over Christina River

Contract T201207101

Foundation Report

Final – November 2014



Prepared for: Delaware Department of Transportation



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FINAL FOUNDATION REPORT (REV. November 2014)

**BR 1-159 - Newport Bridge
James Street Over Christina River
New Castle County, Delaware**

EXECUTIVE SUMMARY

This report summarizes the results of the subsurface exploration program, laboratory test data and geotechnical analyses for the proposed 393'-11 7/8", 5-span bridge on James Street over Christina River in New Castle County, Delaware. The report was prepared in accordance with the DelDOT Bridge Design Manual ⁽¹⁾, AASHTO LRFD Bridge Design Specifications⁽²⁾ and Drilled Shafts: Construction Procedures and LRFD Design Methods – Publication No. FHWA-NHI-10-016 - May 2010⁽³⁾.

The recommendations for foundation design include:

1. Recommended Foundation Design Features

Recommended Drilled Shaft Foundations at Abutments A&B

	Abutment A	Abutment B
Recommended Foundation Type	48" Diameter Cased Drilled Shafts	48" Diameter Cased Drilled Shafts
Applicable Boring	JS-2	JS-9
Bottom of Drilled Shaft Cap Elevation, ft.	+1.5/+4.5	+4.0
Top of Casing Elevation, ft.	+1.5/+4.5	+4.0
Load Carrying Mechanism	Friction and End bearing in Rock	Friction and End bearing in Rock
Min. Bottom of Drilled Shaft Elevation, ft.	-94.0	-46.0
Assumed Top of Rock Elevation, ft.	-109.5	-92.5
Estimated Bottom of Drilled Shaft Elevation, ft.	-111.5	-94.5
Estimated Shaft Length, ft.*	113.0/116.0	98.5
Factored Axial Resistance (R _R), Kips	516	415
Factored Lateral Resistance, Kips	105.6	229.3
Factored Service Lateral Resistance, Kips	67.40	146.9
Service Limit State Lateral Deflection, inches	0.69	0.19
Service Limit State Allowable Deflection, inches	1.0	1.0
Minimum Shaft spacing, ft.	12	12

**Drilled Shaft Length measured from the top of permanent casing to estimated bottom of drilled shaft.*

Recommended Drilled Shaft Foundations at Piers 1, 2, 3 & 4

	Pier 1	Pier 2	Pier 3	Pier 4
Recommended Foundation Type	48" Diameter Cased Drilled Shafts	48" Diameter Cased Drilled Shafts	48" Diameter Cased Drilled Shafts	48" Diameter Cased Drilled Shafts
Applicable Boring	JS-3 & JS-4	JS-5	JS-6	JS-7 & JS-8
Bottom of Pier Cap Elevation, ft.	+7.25	+9.22	+8.83	+6.29
Top of Casing Elevation, ft.	0.0	-12.0	-1.0	+3.0
Load Carrying Mechanism	Friction and End bearing in Rock	Friction and End bearing in Rock	Friction and End bearing in Rock	Friction and End bearing in Rock
Min. Bottom of Drilled Shaft Elevation, ft.	-104.0	-103.0	-99.0	-93.0

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Recommended Drilled Shaft Foundations at Piers 1, 2, 3 & 4

	Pier 1	Pier 2	Pier 3	Pier 4
Assumed Top of Rock Elevation, ft.	-107.0	-107.0	-107.0	-100.5
Estimated Bottom of Drilled Shaft Elevation, ft.	-109.0	-109.0	-109.0	-102.5
Estimated Shaft Length, ft.*	109.0	97.0	108.0	105.5
Factored Axial Resistance (R_R), Kips	778	703	695	1044
Factored Lateral Resistance, Kips	67.79	30.73	22.81	81.31
Factored Service Lateral Resistance, Kips	52.67	19.25	15.79	46.59
Service Limit State Lateral Deflection, inches	0.08	0.42	0.70	0.23
Service Limit State Allowable Deflection, inches	1.0	1.0	1.0	1.0
Minimum Shaft spacing, ft.	12	12	12	12

**Drilled Shaft Length measured from the top of permanent casing to estimated bottom of drilled shaft.*

2. The drilled shafts will be installed using a permanent steel casing and using the rotating or oscillating methods to minimize vibration. The minimum steel casing thickness is ½ inch at the abutments and Piers 1, 2 and 4 and ¾ inch at Pier 3. After the casing has been filled with concrete, fill all void space occurring between the casing and drilled shaft excavation with a material which approximates the geotechnical properties of the in-situ soils. Testing using crosshole sonic log is recommended. Access tubes for crosshole sonic log testing shall be steel pipe of 0.145 inches minimum wall thickness and at least 1-1/2 inch inside diameter. A minimum of four tubes per shaft are recommended. One Bi-Directional Load cell Test at a technique shaft located at Wing A is recommended.
3. The effects of construction activity on the 72-inch forced sewer main should be minimized. The area in the immediate vicinity of the pipe should be delineated to restrict construction activity around the pipe. Vibration Monitoring is recommended at the 72-inch forced sewer main. A threshold value of 0.2 inches/sec should not be exceeded. Installation of drilled shafts should proceed from Abutment B, towards Abutment A.
4. The contractor is responsible for stability of excavated slopes. The contractor is also responsible for providing dewatering of the excavation to allow for inspection and construction. Any dewatering sumps or wells should be located at least three feet away from the footing excavation.

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1.0 INTRODUCTION

The existing bridge BR1-159 carries James Street over Christina River, in New Castle County. This report summarizes the results of the subsurface exploration program, laboratory test data and geotechnical analyses. The report also specifies the foundation design and construction recommendations. The foundation design requirements for the structure include recommendations for bottom of Drilled Shaft elevations, axial and lateral capacities for Drilled Shafts and approach embankment treatment to mitigate settlement. The conclusions and recommendations are based on soil and groundwater information gathered during the geotechnical exploration program and subsequent laboratory analysis of samples. The report was prepared in accordance with the DelDOT Bridge Design Manual⁽¹⁾, AASHTO LRFD Bridge Design Specifications⁽²⁾ and Drilled Shafts: Construction Procedures and LRFD Design Methods – Publication No. FHWA-NHI-10-016 - May 2010⁽³⁾.

The following tasks were performed for the preparation of this report:

- Drafting of the Subsurface Profile.
- Interpretation of the subsurface exploration and the laboratory test data.

2.0 SITE AND PROJECT DESCRIPTION

2.1 *Site Description*

The project site is shown in **Figure 1 – Project Location Map**. The Boring Location Plan- **Figure 2** indicates that the existing ground surface elevations in the vicinity of the proposed structure range from Elev. -25 (channel elevation) to Elev. +11 feet above mean sea level. Industrial and commercial areas are adjacent to the proposed structure.

2.2 *Proposed Structure*

The proposed structure will be constructed just east of the existing bridge alignment and will be 393'-11 7/8" long, with 5 spans. The span lengths varies from 55'-5 1/2" (Span 5) to 88'-1 1/8" (Span 2). The structure will have a curb-to-curb width of 28 feet and a 10-foot wide bike and pedestrian way. The out-to-out width of 42'- 5 1/2" consists of two 12-foot lanes, two 2-foot shoulders, two 1'-8 1/4" parapets and 1'-1" for a handrail. The proposed bridge structure type, size and location are shown on the Boring Location Plan provided in **Figure 2**. The proposed deck elevation at the centerline is 12.76 feet at Abutment A and 12.5 feet at Abutment B. The maximum embankment height is approximately 9 feet at Abutment A and 5.5 feet at Abutment B.

3.0 SUBSURFACE EXPLORATION AND LABORATORY TESTING

The subsurface exploration and laboratory testing data are included in **Appendix B**.

3.1 *Subsurface Exploration*

During the months of May through August 2012 Walton Corporation completed ten (10) Standard Penetration Test (SPT) borings (JS-1 thru JS-10) at the structure and approach roadway. The structure test boring locations are shown on the Boring Location Plan in **Figure 2**. Borings JS-1 and JS-10 were drilled as roadway borings. A summary of the boring program is shown in **Table 3.1**.

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Table 3.1 Summary of Boring Program

Boring No.	Ground Surface Elevation (ft.)	Substructure Unit	Ave. N_{CORR}-Value (bp 1.0 ft.)⁽¹⁾	Groundwater Elevation (ft.)	Remarks on Subsurface Material
JS-1	9.0	Roadway	N/A	Dry	Medium/dense fill over saturated soft silts/clays with alternating layers of medium dense to dense/stiff sands, silts and clays below
JS-2	8.5	Abutment A and Wing A	25	-19.5	Medium/dense fill over saturated soft silts/clays with alternating layers of medium dense to dense/stiff sands, silts and clays below
JS-3	11.0	Pier 1	27	1.0	Medium/dense fill over saturated soft silts/clays with alternating layers of medium dense to dense/stiff sands, silts and clays below
JS-4	4.0		21	-15.8	Medium/dense fill over saturated soft silts/clays with alternating layers of medium dense to dense/stiff sands, silts and clays below
JS-5	11.0	Pier 2	26	*4.6	River mud/saturated clayey silts overlying alternating layers of medium dense to very dense/stiff sands, silts and clays below
JS-6	11.0	Pier 3	20	*4.6	River mud/saturated clayey silts overlying alternating layers of medium dense to very dense/hard sands, silts and clays below
JS-7	11.0	Pier 4	27	-3.8	Medium/dense fill over alternating layers of medium dense to dense/stiff sands and silts
JS-8	1.0		26	-5.5	Medium/dense fill over alternating layers of medium dense to dense/stiff sands and silts
JS-9	4.5	Abutment B and Wing D	27	-1.5	Medium/dense fill over alternating layers of medium dense to dense/stiff sands and silts
JS-10	8.5	Roadway	N/A	Dry	Medium/dense fill over alternating layers of medium dense to dense/stiff sands and silts

⁽¹⁾ *Averaged over the length of the boring*
**Assumed at Mean High Water Elevation*

3.2 Standard Penetration Test Boring

The borings were typically advanced using 3.25-inch O.D. hollow-stem augers. Samples were captured using the Standard Penetration Testing (SPT) procedure. Split-barrel samples, in accordance with ASTM D 1586, were taken at intervals with a 2.0-inch outer-diameter split-barrel sampler. For each 2-foot sampling interval, the number of blows required to drive the sampler six inches using a 140-pound weight dropped 30 inches was recorded. The soil obtained from the sampling sequence was visually classified by type, texture and color. Boring logs, recording blow counts, sample depths and material descriptions were maintained throughout the drilling operation. Graphic interpretations of these logs are presented on the Subsurface Profile in **Appendix A - Figure 3**.

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3.3 Laboratory Testing Program

The Laboratory testing results are shown in **Appendix B**. Testing included: Classification and Index tests, undisturbed soil sample tests and corrosion tests. The soil samples were tested at laboratories of Geo-Technology Associates, Inc. and DelDOT.

Corrosion tests included: pH (ASTM G-51), Earth Resistivity (ASTM G-57), Redox Potential (ASTM D1498), Qualitative Test for Sulfide and Natural Moisture Content.

A summary of the laboratory tests on undisturbed samples is shown in **Table 3.2**

Table 3.2 Summary of Laboratory Tests on Undisturbed Samples

Boring No	Undisturbed Sample Depth (ft.)	Laboratory Testing	Laboratory Test Results
JS-2	16.0	Consolidation Test	$P_c=1.15\text{tsf}$, $C_c=0.65$, $C_r=0.08$, $e_0=1.659$, $C_v=0.1\text{ft}^2/\text{day}$
JS-2	26.0	CU with Pore Pressures	$C=0.346\text{tsf}$, $C'=0.236\text{tsf}$ $\phi=10\text{ deg}$, $\phi'=24.7\text{ deg}$
JS-3	22.0	CU with Pore Pressures	$C=0.056\text{tsf}$, $C'=0.035\text{tsf}$ $\phi=16.1\text{ deg}$, $\phi'=35.3\text{ deg}$

3.4 Groundwater

Groundwater readings were made during the course of the boring operations and after completion of the borings. The groundwater elevations are shown in **Table 3.1**. The groundwater readings are for the times shown on the boring logs and may not be indicative of seasonal or long-term fluctuations in groundwater levels. The Mean High Water elevation of Christina River is 4.64 feet. A design groundwater elevation of 5.0 feet was therefore assumed.

4.0 SUBSURFACE CONDITIONS

4.1 Geology

According to the map of the *Geology of Wilmington Area, Delaware* (1975), prepared by the Delaware Geological Survey (DGS), the area is situated in the Potomac Formation. The Potomac Formation is characterized by variegated red, gray, purple, yellow, and white, frequently lignitic silts and clays containing interbedded white, gray, and rust-brown quartz sands and some gravel. Individual beds usually restricted laterally in northern Delaware.

The Potomac Formation is of the Early to Late Cretaceous age. Potomac sediments are of continental origin and consist mainly of vari-colored clays and silts with some interbedded sands. Encroachment of the sea and marine deposition apparently took place from Late Cretaceous time up to Late Eocene time but no sediment record of these events remains in the map area. Fluvial sands and gravels of the Columbia Formation (Pleistocene age) unconformably overlie the Potomac Formation in most of the map area. In some cases, Pleistocene streams cut deep valleys into the Potomac; the thickness of Holocene fluvial materials may exceed fifty feet.

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4.2 Subsurface Conditions

The surface elevations of the structure borings (JS-2 thru JS-9) range from elevation +4.5 feet to +11.0 feet. The soil profile at the approach to the south abutment (Abutment A) and Pier 1 consisted of medium/dense fill over saturated soft silts/clays with alternating layers of medium dense to dense/stiff sands, silts and clays below. Bedrock was not encountered. The corrected N-values of the soils in borings JS-2 thru JS-4 ranged from 21 to 27, with the N-values generally increasing with depth. The soft silts/clays are susceptible to consolidation.

Pier 4 and the north abutment (Abutment B)/approach soil profile consisted of medium/dense fill over alternating layers of medium dense to dense/stiff sands, silts and clays below. The corrected N-values of the soils in borings JS-7 thru JS-9 ranged from 26 to 27, with the N-values generally increasing with depth. Bedrock was encountered in borings JS-8 and JS-9 at elevations -100.5 feet and -93.5 feet respectively. RQD ranged from 58% to 84.8%.

The soil profile at Pier 2 (Borings JS-5) consisted of river mud/saturated clayey silts overlying alternating layers of medium dense to very dense/stiff sands, silts and clays below. The soil profile at the Pier 3 (Borings JS-6) consisted of River mud/saturated clayey silts overlying alternating layers of medium dense to very dense/hard sands, silts and clays below. Bedrock was not encountered in these borings.

The Subsurface Profile is included in **Appendix A - Figure 3**.

4.3 Soil Parameters for Design (Abutments)

The recommended design soil parameters for the abutments are given in **Appendix C-1**, and are summarized in **Table 4.1**. The parameters are based on SPT blow-count correlations.

Table 4.1 Recommended Foundation Design Features for Abutments

Parameters	Abutment A	Abutment B
Recommended Foundation Type	48" Diameter Cased Drilled Shafts	48" Diameter Cased Drilled Shafts
Applicable Boring	JS-2	JS-9
Bottom of Drilled Shaft Cap Elevation (ft.)	+1.5	+4.0
No. of Soil Layers	7	6
Bearing Stratum	Medium dense to dense/stiff sands, silts and clays	Medium dense to very dense/stiff sands, silts and clays over Schist bedrock
Unit Weight, γ (lb./ft ³)	135/100/130/125/130/125/135	120/135/135/125/135/150
Soil Cohesion, c (psf)	0/400/0/1000/0/1000/0	750/0/0/1000/0/200,000
In-situ Soil Friction Angle, ϕ_f (°)	Layer 1 - 34, Layer 2- N/A, Layer 3-32, Layer 4 - N/A, Layer 5 -32, Layer 6-N/A, Layer 7-34	Layer 1 – N/A, Layer 2- 34, Layer 3-32, Layer 4 - N/A, Layer 5 -34, Layer 6-46
Drilled Shaft Bearing Resistance Factor, (ϕ) Side/End	0.55/0.5 (Sand) and 0.45/0.4 (Clay)	0.55/0.5 (Sand) and 0.45/0.4 (Clay)

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4.4 Soil Parameters for Design (Piers)

The recommended design soil parameters for the piers are given in **Appendix C-2**, and are summarized in **Table 4.2 and Table 4.3**. The parameters are based on SPT blow-count correlations.

Table 4.2 Recommended Foundation Design Features for Piers

Parameters	Pier 1	Pier 2
Recommended Foundation Type	48" Diameter Cased Drilled Shafts	48" Diameter Cased Drilled Shafts
Applicable Boring	JS-3 & JS-4	JS-5
Top of Casing Elevation (ft.)	0.0	-12.0
No. of Soil Layers	4	6
Bearing Stratum	Medium dense to dense/stiff sands, silts and clays	Medium dense to dense/stiff sands, silts and clays
Unit Weight, γ (lb./ft ³)	100/130/125/135	110/120/130/125/135/150
Soil Cohesion, c (psf)	300/0/1000/0	0/0/0/2000/0/0
In-situ Soil Friction Angle, ϕ_r (°)	Layer 1 - 0, Layer 2- 32, Layer 3-0, Layer 4 -35	Layer 1 – 30, Layer 2-32, Layer 3-32, Layer 4-N/A, Layer 5-36, Layer 6-46
Drilled Shaft Bearing Resistance Factor, (ϕ) Side/End	0.55/0.5 (Sand) and 0.45/0.4 (Clay)	0.55/0.5 (Sand) and 0.45/0.4 (Clay)

Parameters	Pier 3	Pier 4
Recommended Foundation Type	48" Diameter Cased Drilled Shafts	48" Diameter Cased Drilled Shafts
Applicable Boring	JS-6	JS-7 & JS-8
Top of Casing Elevation (ft.)	-1.0	+3.0
No. of Soil Layers	4	7
Bearing Stratum	Medium dense to very dense/hard sands, silts and clays below	Medium dense to dense/stiff sands, silts and clays over Schist bedrock
Unit Weight, γ (lb./ft ³)	105/120/125/135	120/135/115/135/125/135/150
Soil Cohesion, c (psf)	600/0/2000/0	750/0/750/0/1000/0/200,000
In-situ Soil Friction Angle, ϕ_r (°)	Layer 1 – N/A, Layer 2 – 32, Layer 3- N/A, Layer 4- 36	Layer 1 – N/A, Layer 2-34, Layer 3-N/A, Layer 4 -34, Layer 5- N/A, Layer 6 -34, Layer 7-46
Drilled Shaft Bearing Resistance Factor, (ϕ) Side/End	0.55/0.5 (Sand) and 0.45/0.4 (Clay)	0.55/0.5 (Sand) and 0.45/0.4 (Clay)

5.0 EVALUATION AND RECOMMENDATIONS – ABUTMENTS

5.1 Abutment Foundation Alternative Analysis

Deep and shallow foundation alternatives were considered. A shallow foundation was not recommended because of the presence of soft soils just below the anticipated bottom of footing elevation. A cast-in-place reinforced concrete cantilever abutment on driven piles was also ruled out in order to minimize vibration, which could affect the nearby 72-inch diameter forced sewer main. As indicated in the Boring Location Plan, **Figure 2**, the abutments will consist of stub abutments on 48-inch diameter cased drilled shafts. The drilled shafts will be installed using a permanent 49" OD minimum steel casing, using the rotating or oscillating methods, where necessary, to minimize vibration.

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5.2 Summary of Analysis and Recommendations – Abutments

The abutments will consist of stub abutments on 48-inch diameter cased drilled shafts. The Bottom of Drilled Shaft Cap Elevation (BDSCE) was determined based the superstructure depth and the drilled shaft cap thickness. The minimum bottom of drilled shaft elevation (MBDSE) was determined based on the required penetration depth needed to support the factored applied axial loads. In order to insure that the axial capacities of the shafts are achieved during construction, all drilled shafts will be terminated two feet into rock. The estimated bottoms of drilled shaft elevations (EBDSE) are shown in **Table 5.1** and on the boring profile in **Figure 3**.

The Factored Geotechnical Resistance (R_R) of a single drilled shaft was determined using the Ensoft computer program SHAFT. The resistance factors outlined in AASHTO Table 10.5.5.2.3-1 were used. The strength axial capacity calculations are included in **Appendix C-1** and the results are shown in **Table 5.1**. A resistance factor of 0.45 and 0.4 for side and end respectively was used for clay soils and 0.55 and 0.5 for side and end respectively, in sand. The lateral capacities at the strength and service limit states were determined using the Ensoft computer program LPILE. The calculations are included in **Appendix C-1** and the results are shown in **Table 5.1**. The minimum spacing of the shafts should be 3 diameters, or 12 feet.

5.3 Abutment Foundation Recommendations

The drilled shaft foundation recommendations at the abutments are shown in **Table 5.1**.

Table 5.1 Recommended Drilled Shaft Foundations at Abutments A&B

	Abutment A	Abutment B
Recommended Foundation Type	48" Diameter Cased Drilled Shafts	48" Diameter Cased Drilled Shafts
Applicable Boring	JS-2	JS-9
Bottom of Drilled Shaft Cap Elevation, ft.	+1.5/+4.5	+4.0
Top of Casing Elevation, ft.	+1.5/+4.5	+4.0
Load Carrying Mechanism	Friction and End bearing in Rock	Friction and End bearing in Rock
Min. Bottom of Drilled Shaft Elevation, ft.	-94.0	-46.0
Assumed Top of Rock Elevation, ft.	-109.5	-92.5
Estimated Bottom of Drilled Shaft Elevation, ft.	-111.5	-94.5
Estimated Shaft Length, ft.*	113.0/116.0	98.5
Factored Axial Resistance (R_R), Kips	516	415
Factored Lateral Resistance, Kips	105.6	229.3
Factored Service Lateral Resistance, Kips	67.40	146.9
Service Limit State Lateral Deflection, inches	0.69	0.19
Service Limit State Allowable Deflection, inches	1.0	1.0
Minimum Shaft spacing, ft.	12	12

*Drilled Shaft Length measured from the top of permanent casing to estimated bottom of drilled shaft.

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6.0 EVALUATION AND RECOMMENDATIONS – PIERS

6.1 Pier Foundation Alternative Analysis

Deep and shallow foundation alternatives were considered. A shallow foundation was ruled out because of the potential for scour and/or because of the presence of soft soils immediately below the anticipated bottom of footing elevation. Steel H-piles driven to very stiff/hard sandy clay were ruled out in order to minimize vibration, which could affect the nearby 72-inch diameter forced sewer main. Also the use of cofferdams in the river was not permitted. Drilled shafts continuous with the pier columns were therefore chosen.

6.2 Summary of Analysis and Recommendations – Piers

The piers will be supported on 48-inch diameter cased drilled shafts. The MBDSEs were determined based on the required penetration depth needed to support the factored applied axial loads, with the 100-year design flood scour taken into account. In order to insure that the axial capacities of the shafts are achieved during construction, all drilled shafts will be terminated two feet into rock. The EBDSEs are shown in **Table 6.1** and on the boring profile in **Figure 3**.

The Factored Geotechnical Resistance (R_R) of a single drilled shaft was determined using the Ensoft computer program SHAFT. The resistance factors outlined in AASHTO Table 10.5.5.2.3-1 were used. The strength axial capacity calculations are included in **Appendix C-2** and the results are shown in **Table 6.1**. A resistance factor of 0.45 and 0.4 for side and end respectively was used for clay soils and 0.55 and 0.5 for side and end respectively, in sand. The lateral capacities at the strength and service limit states were determined using the Ensoft computer program LPILE. The calculations are included in **Appendix C-2** and the results are shown in **Table 6.1**. The minimum spacing of the shafts is 3 diameters or 12 feet.

6.3 Pier Foundation Recommendations

The foundation recommendations at the piers are shown in **Table 6.1**.

Table 6.1 Recommended Drilled Shaft Foundations at Piers 1, 2, 3 & 4

	Pier 1	Pier 2	Pier 3	Pier 4
Recommended Foundation Type	48" Diameter Cased Drilled Shafts	48" Diameter Cased Drilled Shafts	48" Diameter Cased Drilled Shafts	48" Diameter Cased Drilled Shafts
Applicable Boring	JS-3 & JS-4	JS-5	JS-6	JS-7 & JS-8
Bottom of Pier Cap Elevation, ft.	+7.25	+9.22	+8.83	+6.29
Top of Casing Elevation, ft.	0.0	-12.0	-1.0	+3.0
Load Carrying Mechanism	Friction and End bearing in Rock	Friction and End bearing in Rock	Friction and End bearing in Rock	Friction and End bearing in Rock
Min. Bottom of Drilled Shaft Elevation, ft.	-104.0	-103.0	-99.0	-93.0
Assumed Top of Rock Elevation, ft.	-107.0	-107.0	-107.0	-100.5
Estimated Bottom of Drilled Shaft Elevation, ft.	-109.0	-109.0	-109.0	-102.5
Estimated Shaft Length, ft.*	109.0	97.0	108.0	105.5
Factored Axial Resistance (R_R), Kips	778	703	695	1044

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James Street Over Christina River
New Castle County, Delaware

Table 6.1 Recommended Drilled Shaft Foundations at Piers 1, 2, 3 & 4

	Pier 1	Pier 2	Pier 3	Pier 4
Factored Lateral Resistance, Kips	67.79	30.73	22.81	81.31
Factored Service Lateral Resistance, Kips	52.67	19.25	15.79	46.59
Service Limit State Lateral Deflection, inches	0.08	0.42	0.70	0.23
Service Limit State Allowable Deflection, inches	1.0	1.0	1.0	1.0
Minimum Shaft spacing, ft.	12	12	12	12

**Drilled Shaft Length measured from the top of permanent casing to estimated bottom of drilled shaft.*

7.0 DRILLED SHAFT GROUP RESISTANCE

No reduction in resistance for group efficiency is anticipated, since the permanent casing will be advanced in front of the excavation heading, and the drilled shaft spacing will be three diameters, or 12 feet. The drilled shafts will also penetrate a layer of stiff or hard cohesive material, at the piers.

8.0 DRILLED SHAFT SETTLEMENT

Short-term settlement was computed using the computer program SHAFT. The program computes settlement of the top and base of the shaft as a function of axial loading. The drilled shafts were within tolerable settlement limits (1 inch) for the predicted service loads. Long-term settlement is not anticipated, since the drilled shafts will be terminated in bedrock.

9.0 EVALUATION AND RECOMMENDATIONS - WINGS

Wing A and Wing D will be Cast-in-Place Reinforced Concrete Cantilever Walls with spread footing on soil. The soil parameters for Wing A will be the same as for Abutment A and the soil parameters for Wing D will be the same as for Abutment B. The bottom of footing elevations for Wings A and D should be a minimum of 3 feet below finished grade to prevent damage due to frost heave.

10.0 APPROACH EMBANKMENT SETTLEMENT

In order to mitigate embankment settlement which may affect the 72-inch forced sewer main at the south approach, lightweight aggregate fill will be used. The lightweight aggregate fill producer shall submit verification of a compacted density of less than 60 pcf when measured by a one-point compaction ("Proctor") test conducted in accordance with ASTM D698. A special Provision is provided in **Appendix D**. At the north approach, approximately 5 feet of fill will be placed. Based on the soil profile at borings JS-9 and JS-10, long-term settlement is not anticipated.

11.0 SPECIAL CONSIDERATIONS

11.1 Drilled Shaft Construction and Testing

The drilled shafts will be installed using a minimum 49" OD permanent steel casing and by the rotating or oscillating method to minimize vibration. After the casing has been filled with concrete, fill all void space

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BR 1-159 - Newport Bridge James Street Over Christina River New Castle County, Delaware

occurring between the casing and drilled shaft excavation with a material which approximates the geotechnical properties of the in-situ soils. Testing using crosshole sonic log is recommended. Access tubes for crosshole sonic log testing shall be steel pipe of 0.145 inches minimum wall thickness and at least 1-1/2 inch inside diameter. A minimum of four tubes are recommended. One Bi-Directional Load cell Test at a technique shaft is recommended. The technique should be abandoned after testing. Other requirements for testing are included in the drilled shaft special provisions in **Appendix D**.

11.2 Seismic Design Considerations

Based on the SPT blow counts and the soil profile and in accordance with AASHTO Table 3.10.3.1-1, a Site Class E should be used for seismic design.

11.3 Corrosion Protection

Based on the AASHTO Section 10.7.5, the results of the laboratory chemical testing which is included in **Appendix B** indicate the absence of a corrosive environment. Protection against corrosion is therefore not necessary.

11.4 Temporary Cut Slope and Support of Excavation

Excavation for the foundations should be carried out in a manner that will ensure the stability of the sides of the excavations. The sides of the excavations may have to be sloped to prevent slope failure. Where there is inadequate room to accommodate the necessary sloping of the excavation sides, temporary shoring should be installed. All excavation safety measures, including sloping and shoring should conform to current OSHA and local standards. Care should be exercised when excavating at the toe or on the side of existing fill or cut slopes so that the stability of the slope is not affected. A qualified engineer registered in the state of Delaware should design all temporary sheeting and shoring.

11.5 Scour Analysis

Results of the scour analysis are included in **Appendix C-3**. It is anticipated that scour will not affect the abutments. The anticipated total scour for the 100-Year flood at Piers 1 and 2 is 0 feet and 7.28 feet, respectively. The anticipated total scour for the 100-Year flood at Piers 3 and 4 is 7.3 feet and 6.63 feet, respectively.

11.6 Environmental Concerns

Because of the proximity of the proposed structure to a Superfund Site care should be taken to avoid disturbance of the landfill cap, during construction of the south abutment.

11.7 Dewatering and Drainage

Groundwater may be encountered during excavation at the abutments. Any groundwater that flows into the excavation can be removed using a sump and pump. The contractor is responsible for maintaining dry conditions during construction.

11.8 Protection of Existing Utilities

Overhead utilities were observed at east side of the existing structure, along the relocated alignment. Underground utilities in the vicinity of the proposed structure should be located by calling Miss Utility prior to excavation. The effects of construction activity on the 72-inch forced sewer main should be

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minimized. The area in the immediate vicinity of the pipe should be delineated to restrict construction activity around the pipe.

11.9 *Preconstruction Survey for adjacent structures*

Vibration Monitoring is recommended at the 72-inch forced sewer main.

12.0 BASIS FOR RECOMMENDATIONS

The recommendations are based on the information available at the time of writing this report. The report should be revised as new information becomes available. Stub abutments and piers on drilled shafts were the most suitable substructure options, given the concerns about vibration affecting the 72-inch forced sewer main.

13.0 REFERENCES

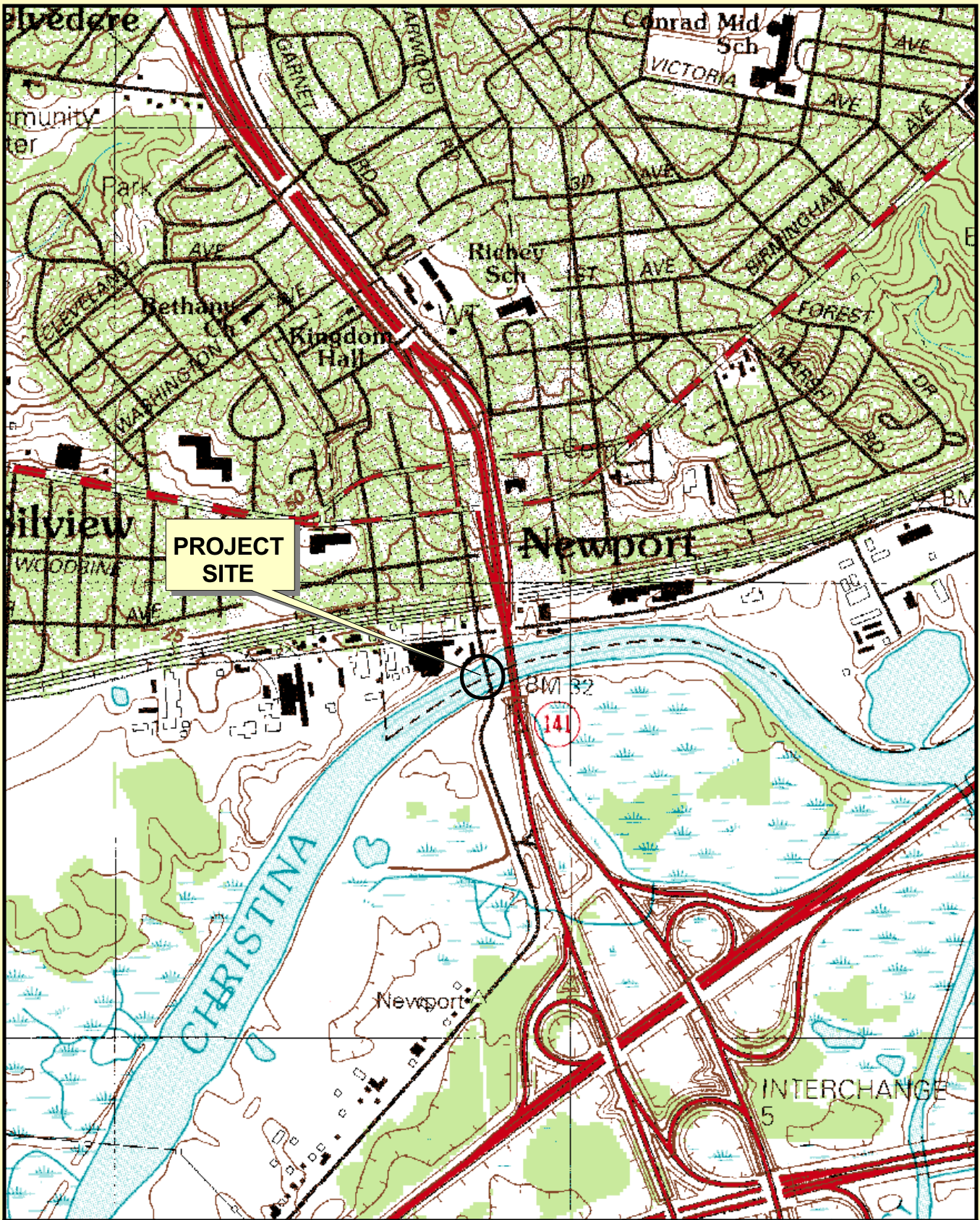
1. DelDOT Bridge Design Manual.
2. AASHTO LRFD Bridge Design Specifications, 5th edition, 2010.
3. Drilled Shafts: Construction Procedures and LRFD Design Methods – Publication No. FHWA-NHI-10-016 - May 2010.
4. Final Foundation Report for Bridge 1-159, James Street over Christina River, by McCormick Taylor, Inc. dated November, 2012.

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BR 1-159 - Newport Bridge
James Street Over Christina River
New Castle County, Delaware

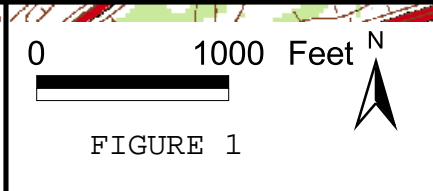
APPENDIX A

Figures

Figure 1	Project Location Map
Figure 2	Boring Location Plan
Figure 3	Subsurface Profile

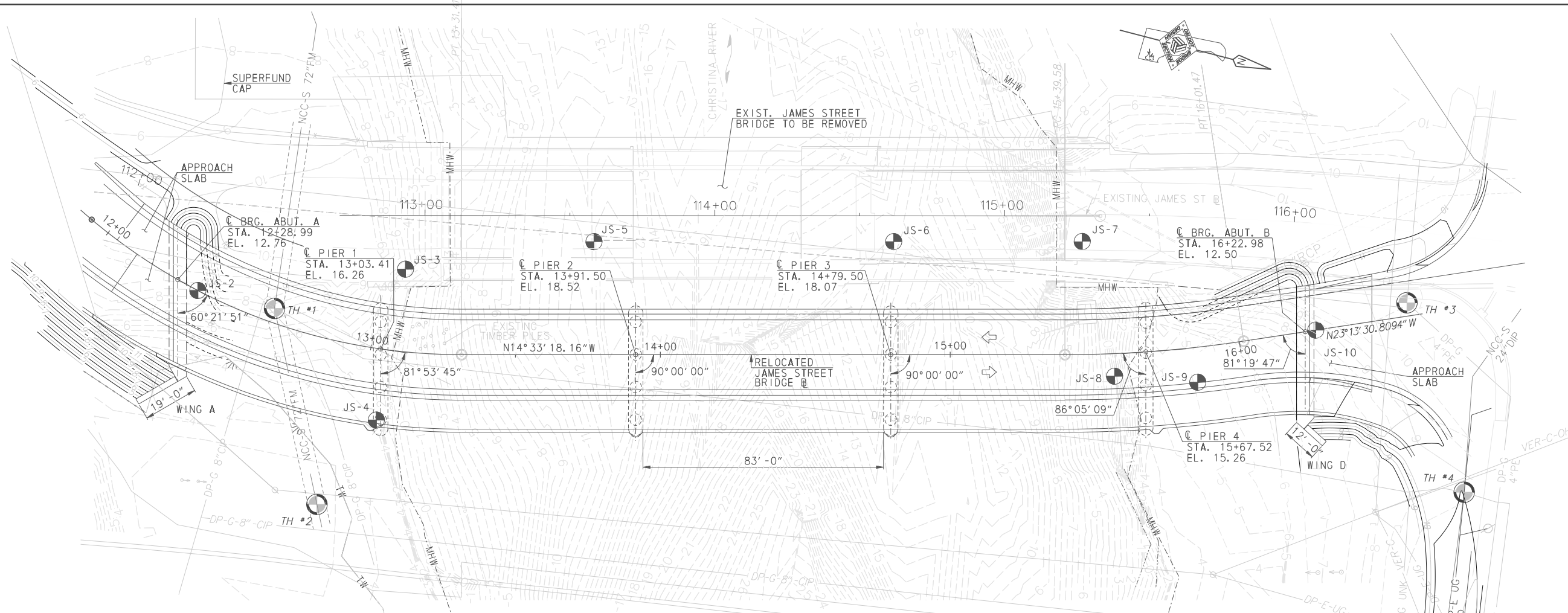


**McCormick
Taylor**
Engineers & Planners
Since 1946



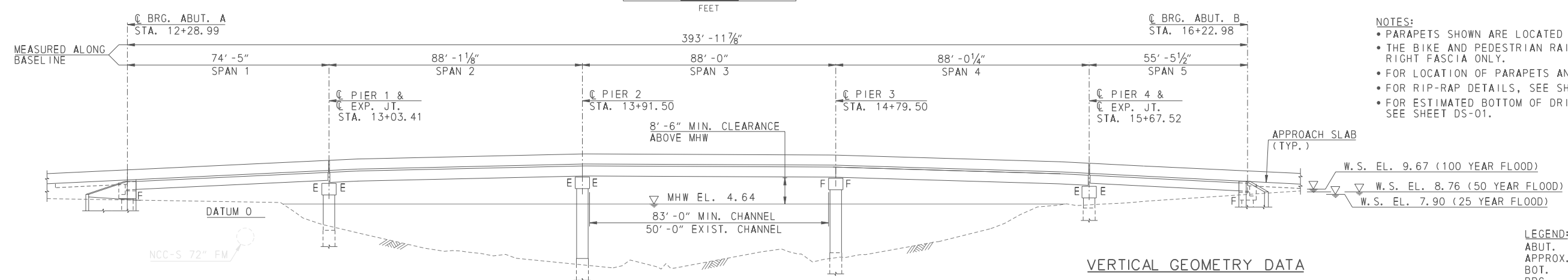
PROJECT LOCATION MAP
BRIDGE NO. 1-159
Newport, New Castle County, Del

10/28/2014 3:27:33 PM
 Y:\BRIDGES\DELDOT\BR1-159_JAMES ST BRIDGE\SEED FILES & BDRS\159_NEWPORTGPE_BORDER.DGN
 USER NAME: bfg.bo
 REV. DATE: 10/28/2014



CORE BORINGS		
BORING	STATION	OFFSET
JS-2	12+36.88	0.00
JS-3	13+08.78	28.40' L
JS-4	13+05.16	24.51' R
JS-5	13+77.10	39.00' L
JS-6	14+80.50	39.00' L
JS-7	15+46.19	39.00' L
JS-8	15+56.40	7.78' R
JS-9	15+84.19	12.00' R
JS-10	16+26.25	0.00

PLAN
 SCALE
 0 20 40 60
 FEET

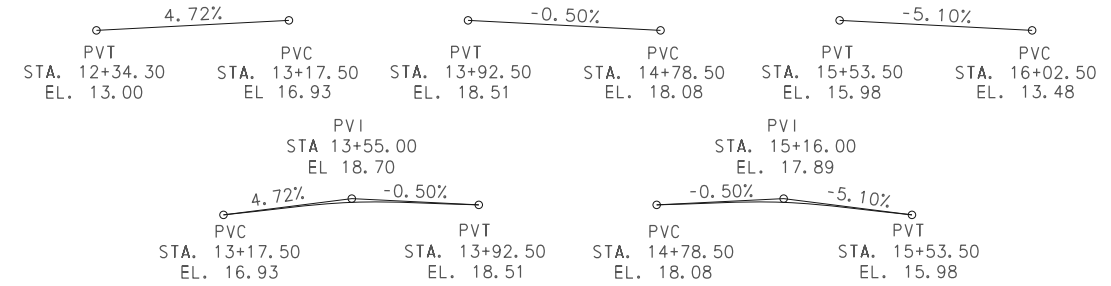


NOTES:

- PARAPETS SHOWN ARE LOCATED ADJACENT TO THE ROADWAY.
- THE BIKE AND PEDESTRIAN RAILING IS LOCATED AT THE RIGHT FASCIA ONLY.
- FOR LOCATION OF PARAPETS AND RAILING, SEE SHEET PE-02.
- FOR RIP-RAP DETAILS, SEE SHEETS EC-01 AND EC-02.
- FOR ESTIMATED BOTTOM OF DRILLED SHAFT ELEVATIONS, SEE SHEET DS-01.

HORIZONTAL GEOMETRY DATA	
P. I. STA. 12+65.05	P. I. STA. 15+70.59
Δ = 40° 07' 44.3396" LT.	Δ = 8° 40' 12.6464" LT.
D = 28° 56' 14.1446"	D = 14° 00' 31.4930"
T = 72.3186'	T = 31.0048'
L = 138.6758'	L = 61.8912'
R = 198.0000'	R = 409.0000'
E = 12.7937'	E = 1.1735'

ELEVATION
 SCALE
 0 20 40 60
 FEET



LEGEND:

- ABUT. = ABUTMENT
- APPROX. = APPROXIMATE
- BOT. = BOTTOM
- BRG. = BEARING
- BSPW = BOTTOM SHEET PILE WALL
- DIA. = DIAMETER
- E = EXPANSION
- EL. = ELEVATION
- EXIST. = EXISTING
- EXP. = EXPANSION
- F = FIXED
- JT. = JOINT
- MHW = MEAN HIGH WATER
- MIN. = MINIMUM
- MPT E = MINIMUM PILE TIP ELEVATION
- STA. = STATION
- TYP. = TYPICAL
- W. S. = WATER SURFACE
- ⊙ = SOIL BORING

FIGURE 2

ADDENDUMS / REVISIONS

SCALE: AS NOTED

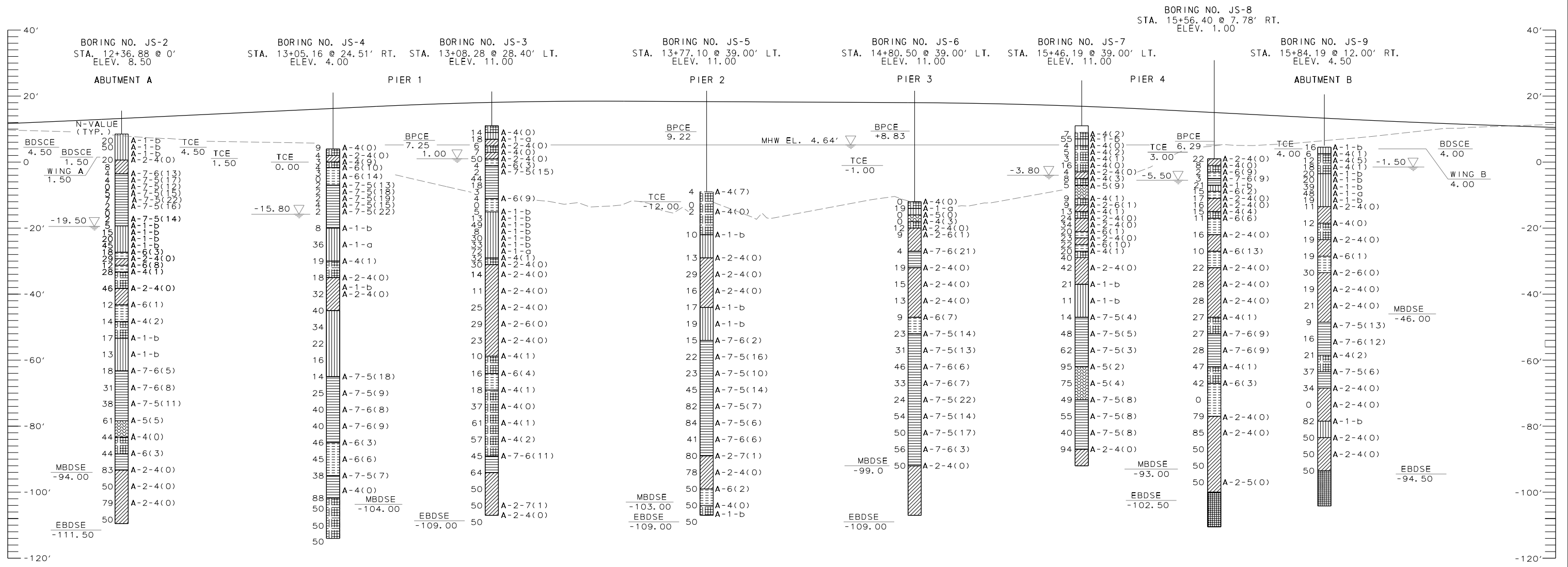
BR 1-159 ON JAMES STREET OVER CHRISTINA RIVER

CONTRACT T201207101	BRIDGE NO. 1-159
COUNTY NEW CASTLE	DESIGNED BY: ZME
	CHECKED BY: BUH

BORING LOCATION PLAN

SHEET NO.	
TOTAL SHTS.	

11/5/2014
 Y:\BRIDGES\DELDOT\BR1-159_JAMES ST BRIDGE\SEED FILES & BDRS\159_NEWPORT\PE_BORDER.DGN
 bfg.bo
 11/5/2014 1:58:39 PM



LEGEND

- | | | | | |
|--|---|--|---------------|---|
| | WELL GRADED GRAVELS AND SANDS | | PLASTIC CLAYS | BDSCE - BOTTOM OF DRILLED SHAFT CAP ELEVATION |
| | POORLY GRADED, SILTY OR CLAYEY SANDS AND GRAVEL | | SILTY SOILS | BPCE - BOTTOM OF PIER CAP ELEVATION |
| | EXPANSIVE PLASTIC CLAYS | | ELASTIC SILTS | EBDSE - ESTIMATED BOTTOM OF DRILLED SHAFT ELEVATION |
| | PLASTIC CLAYS | | SCHIST | MBDSE - MINIMUM BOTTOM OF DRILLED SHAFT ELEVATION |
| | | | | N-VALUE - SAMPLE BLOWS PER FOOT |
| | | | | TCE - TOP OF CASING ELEVATION |
| | | | | TYP. - TYPICAL |
| | | | | ▽ - GROUND WATER ELEVATION AT ZERO HOURS |

FIGURE 3

ADDENDUMS / REVISIONS

NOT TO SCALE

CONTRACT	BRIDGE NO.	1-159
T201207101	DESIGNED BY:	SJM
COUNTY	CHECKED BY:	XXX
NEW CASTLE		

SHEET NO.	
TOTAL SHTS.	

FINAL FOUNDATION REPORT (REV. November 2014)

**BR 1-159 - Newport Bridge
James Street Over Christina River
New Castle County, Delaware**

APPENDIX B

**Geotechnical Data
Boring Logs and Laboratory Testing Summary**

**STATE OF DELAWARE
DEPARTMENT OF TRANSPORTATION
MATERIALS AND RESEARCH**

BORING JS-2

Project Name: James Street Bridge

Location: Newport, DE

State Contract #: T201207101

Federal Contract #:

Station/Offset:

Northing:

Easting:

Boring Surface Elev.:

Reference:

Date Started: 5/31/12

Date Completed: 6/5/12

Wt. of Sample Hammer: 140
Type of: D-Sampler: Split Barrel
S-Sampler:
U-Sampler:
Core Bit:

Lbs.
O.D.
O.D.
O.D.
O.D.

Average Fall: 30
O.D. of Sampler: 2
O.D. of Samp. Tube:
O.D. of Samp. Tube:
O.D. of Rock Core:

IN.
IN.
IN.
IN.
IN.

Hollow Stem Auger Diameter: 3 1/4" **Inches**
Mud Rotary:

From Depth of: 0.0 **To:** 28.0
From Depth of: 28.0 **To:** 118.2

Water Level Readings
Date
5/31/12

Depth to Water (ft)
28.0

Caved Depth (ft)

Boring Contractor: Walton Corporation

Equipment/Rig Type: CME 55 ATV

Driller: Jason Truver

Logged By: Meghan Lester and Chris Costanzi

Depth (ft.)	Water Level	No.	Sample Depth	Blows/6"	Sample Description	AASHTO Class.	Remarks
2.53		1	2.0'	6 10 10 9	Moist loose brown coarse sandy fine gravel w/ some fine sand, trace of silt. 6" RECOVERY	A-1-b	6" hot-mix and 18" crushed stone. Fill
5.06		2	4.0'	7 50	Moist very dense gray coarse to fine sand w/some fine gravel and silt. 3" RECOVERY	A-1-b	Fill
7.59		3	6.0'	2 4 8 7	Moist medium dense grayish tan silty fine to coarse sand and fine gravel. 16" RECOVERY	A-1-b	Fill
10.12		4	8.0'	6 11 9 6	Moist medium dense black silty fine gravel and coarse sand w/some fine sand, trace of clay. 15" RECOVERY	A-2-4(0)	Fill
12.65		5	10.0'	4 4 4 8	No sieve analysis - Indication of moist loose gray clayey sand, trace of fine gravel. 7" RECOVERY		Fill
15.18		6	12.0'	3 2 2 3	Saturated soft gray clay w/trace of coarse to fine sand, fine gravel and silt. 20" RECOVERY	A-7-6(13)	
		7	14.0'	2 2 2 2	Saturated soft tan organic clay w/some coarse sand, trace of fine sand and silt. 18" RECOVERY	A-7-5(17)	Casing set @ 15'
			16.0'				

Remarks: Concrete slab @ 4' +/-

Reviewed By: Hany Fekry

Soils Supervisor: Aaron Wieczorek

**STATE OF DELAWARE
DEPARTMENT OF TRANSPORTATION
MATERIALS AND RESEARCH**

Project Name: James Street Bridge
State Contract: T201207101

Boring No.: JS-2

Depth (ft.)	Water Level	No.	Sample Depth	Blows/6"	Sample Description	AASHTO Class.	Remarks
		U-1	16.0'		Saturated dark gray organic clay w/some fine gravel, trace of fine to coarse sand and silt.	A-7-5(12)	Shelby Tube - Press Sample
17.71			18.0'		24" RECOVERY		
		9	18.0'	1 2 3	Saturated firm dark gray organic clay w/some coarse to fine sand, trace of silt.	A-7-5(15)	
			20.0'		24" RECOVERY		
20.24		10	20.0'	4 3 4 3	Saturated firm gray organic clay w/trace of coarse to fine sand and silt.	A-7-5(22)	
			22.0'		24" RECOVERY		
22.77		11	22.0'	1 1 1 2	Saturated soft gray organic coarse sandy clay w/ trace of fine sand and silt.	A-7-5(16)	
			24.0'		24" RECOVERY		
25.3		U-2	24.0'				Shelby Tube - Press Sample
			26.0'		24" RECOVERY		
		12	26.0'	1 1 1 2	Saturated soft gray organic coarse sandy clay w/ trace of fine sand and silt.	A-7-5(14)	
			28.0'		24" RECOVERY		
27.83	▽	13	28.0'	1 2 3 7	Saturated soft tannish gray coarse sand w/some fine sand and silt, trace of fine gravel.	A-1-b	
			30.0'		20" RECOVERY		
30.36		14	30.0'	7 9 6 8	Saturated medium dense tannish gray fine gravelly coarse to fine sand w/trace of silt.	A-1-b	
			32.0'		20" RECOVERY		
32.89		15	32.0'	9 8 12 10	Saturated medium dense gray coarse to fine sand w/some fine gravel, trace of silt.	A-1-b	
			34.0'		14" RECOVERY		
35.42		16	34.0'	9 15 30 40	Saturated dense gray coarse sandy fine gravel w/ some fine sand, trace of silt.	A-1-b	
			36.0'		12" RECOVERY		
37.95		17	36.0'	1 3 15 19	Saturated very stiff tan fine sandy clay w/some silt, trace of coarse sand and fine gravel.	A-6(3)	Potomac Formation at 37'
			38.0'		21" RECOVERY		
		18	38.0'	16 13 16 15	Saturated medium dense tan fine to coarse sand w/ some silt, trace of fine gravel.	A-2-4(0)	
			40.0'		12" RECOVERY		

**STATE OF DELAWARE
DEPARTMENT OF TRANSPORTATION
MATERIALS AND RESEARCH**

Project Name: James Street Bridge
State Contract: T201207101

Boring No.: JS-2

Depth (ft.)	Water Level	No.	Sample Depth	Blows/6"	Sample Description	AASHTO Class.	Remarks
40.48		19	40.0'	3 5 7 10	Saturated stiff red silty fine sandy clay w/trace of coarse sand.	A-6(8)	
			42.0'			19" RECOVERY	
43.01		20	42.0'	16 14 14 15	Saturated very stiff red clayey fine sandy silt w/ some coarse sand and fine gravel.	A-4(1)	4" Casing set @ 42'
			44.0'				
45.54							
48.07		21	48.0'	4 16 30 21	Saturated dense brown clayey fine sand w/some fine gravel and silt, trace of coarse sand.	A-2-4(0)	
			50.0'			20" RECOVERY	
50.6							
53.13		22	53.0'	7 7 5 4	Saturated stiff brown fine to coarse sandy clay w/ trace of fine gravel and silt.	A-6(1)	
			55.0'			24" RECOVERY	
55.66							
58.19		23	58.0'	5 6 8 8	Saturated stiff brown clayey fine sandy silt w/some fine gravel, trace of coarse sand.	A-4(2)	
			60.0'			20" RECOVERY	
60.72							
63.25		24	63.0'	4 5 12 15	Saturated medium dense brown silty coarse to fine sand and fine gravel.	A-1-b	

**STATE OF DELAWARE
DEPARTMENT OF TRANSPORTATION
MATERIALS AND RESEARCH**

Project Name: James Street Bridge
State Contract: T201207101

Boring No.: JS-2

Depth (ft.)	Water Level	No.	Sample Depth	Blows/6"	Sample Description	AASHTO Class.	Remarks
			65.0'		18" RECOVERY		
65.78							
68.31		25	68.0'	2 3 10 5	Saturated medium dense brown coarse to fine sand w/some silt, trace of fine gravel.	A-1-b	
			70.0'		20" RECOVERY		
70.84							
73.37		26	73.0'	5 8 10 11	Saturated very stiff brown fine sandy clay w/trace of coarse sand, fine gravel and silt.	A-7-6(5)	
			75.0'		24" RECOVERY		
75.9							
78.43		27	78.0'	12 11 20 28	Saturated hard brown fine sandy clay w/trace of coarse san, fine gravel and silt.	A-7-6(8)	
			80.0'		24" RECOVERY		
80.96							
83.49		28	83.0'	9 15 23 28	Saturated hard brown clay w/some fine sand, trace of coarse sand, fine gravel and silt.	A-7-5(11)	
			85.0'		24" RECOVERY		
86.02							

**STATE OF DELAWARE
DEPARTMENT OF TRANSPORTATION
MATERIALS AND RESEARCH**

Project Name: James Street Bridge
State Contract: T201207101

Boring No.: JS-2

Depth (ft.)	Water Level	No.	Sample Depth	Blows/6"	Sample Description	AASHTO Class.	Remarks
88.55		29	88.0'	11 23 38 45	Saturated hard grayish red clayey fine sandy silt w/ trace of coarse sand and fine gravel. Weathered Rock. 24" RECOVERY	A-5(5)	
			90.0'				
91.08							
		30	93.0'	10 17 27 50	Saturated hard grayish red fine sandy silt w/trace of coarse sand. Weathered Rock. 21" RECOVERY	A-4(0)	
			95.0'				
93.61							
		31	98.0'	18 20 24 29	Saturated hard grayish brown fine sandy clay w/ some silt, trace of coarse sand and fine gravel. Weathered Rock. 24" RECOVERY	A-6(3)	
			100.0'				
96.14							
		32	103.0'	26 33 50	Saturated very dense grayish brown silty fine sand w/some coarse sand and fine gravel. Weathered Rock. 15" RECOVERY	A-2-4(0)	
			105.0'				
98.67							
		33	108.0'	37 50	Saturated very dense gray silty fine sand w/some coarse sand and fine gravel. Weathered Rock. 7" RECOVERY	A-2-4(0)	
			110.0'				
101.2							
103.73							
106.26							
108.79							
111.32							

**STATE OF DELAWARE
DEPARTMENT OF TRANSPORTATION
MATERIALS AND RESEARCH**

Project Name: James Street Bridge
State Contract: T201207101

Boring No.: JS-2

Depth (ft.)	Water Level	No.	Sample Depth	Blows/6"	Sample Description	AASHTO Class.	Remarks
113.85		34	113.0'	18 34 45 50	Saturated very dense gray silty fine gravelly fine sand w/trace of coarse sand. Weathered Rock. 21" RECOVERY	A-2-4(0)	
			115.0'				
116.38					No sieve analysis - Indication of saturated hard gray weathered rock. End Boring		
118.91		35	118.0'	50			
			120.0'		2" RECOVERY		
121.44							
123.97							
126.5							
129.03							
131.56							
134.09							

KEY TO SYMBOLS

Symbol Description

Strata symbols



Well graded gravels and sands



Poorly graded, silty or clayey sands and gravel



Expansive plastic clays



Plastic clays



Silty soils



Elastic Silts

Misc. Symbols



Water table during drilling

Notes:

1. Exploratory borings were drilled using a 3 1/4 - inch diameter hollow stem auger.
2. No free water was encountered at the time of drilling or when re-checked the following day, unless recorded on 1st page.
3. Boring locations were taped from existing features and elevations extrapolated from survey unless otherwise reported.
4. These logs are subject to the limitations, conclusions, and recommendations in this report.
5. Results of tests conducted on samples recovered are reported on the logs.
6. All blow counts are uncorrected.

**STATE OF DELAWARE
DEPARTMENT OF TRANSPORTATION
MATERIALS AND RESEARCH**

BORING JS-3

Project Name: James Street Bridge

Location: Newport, DE

State Contract #: T201207101

Federal Contract #:

Station/Offset:

Northing:

Easting:

Boring Surface Elev.:

Reference:

Date Started: 5/31/12

Date Completed: 6/6/12

Wt. of Sample Hammer: 140
Type of: D-Sampler: Split Barrel
S-Sampler:
U-Sampler:
Core Bit:

Lbs.
O.D.
O.D.
O.D.
O.D.

Average Fall: 30
O.D. of Sampler: 2
O.D. of Samp. Tube:
O.D. of Samp. Tube:
O.D. of Rock Core:

IN.
IN.
IN.
IN.
IN.

Hollow Stem Auger Diameter: 3 1/4" **Inches**
Mud Rotary:

From Depth of: 0.0 **To:** 36.0
From Depth of: 36.0 **To:** 118.0

Water Level Readings

Date
5/31/12

Depth to Water (ft)
10.0

Caved Depth (ft)

Boring Contractor: Walton Corporation

Equipment/Rig Type: CME 55 Truck

Driller: Bill Holden

Logged By: Chris Costanzi

Depth (ft.)	Water Level	No.	Sample Depth	Blows/6"	Sample Description	AASHTO Class.	Remarks
		1	0.0'	4 7 7 23	Moist very stiff brown coarse sandy silt w/some fine sand, trace of fine gravel and clay.	A-4(0)	4" hot-mix. Fill
			2.0'		18" RECOVERY		
2.53		2	2.0'	20 11 7 9	Moist medium dense gray fine gravel w/trace of fine to coarse sand and silt.	A-1-a	Fill
			4.0'		10" RECOVERY		
		3	4.0'	3 3 3 4	Moist loose brown clayey fine gravel w/some coarse to fine sand and silt.	A-2-4(0)	Fill
5.06			6.0'		20" RECOVERY		
		4	6.0'	3 4 3 3	Wet firm grayish brown coarse to fine sandy silt w/ some clay, trace of fine gravel.	A-4(0)	
7.59			8.0'		20" RECOVERY		
		5	8.0'	3 9 41 3	Wet dense gray silty fine gravel w/some coarse to fine sand and clay.	A-2-4(0)	
			10.0'		6" RECOVERY		
10.12	▽	6	10.0'	2 2 2 2	Saturated soft grayish brown fine gravelly clay w/ some silt and fine sand, trace of coarse sand.	A-6(3)	
			12.0'		6" RECOVERY		
		7	12.0'	WH 1 1 2	Saturated soft gray clay w/some coarse sand and silt, trace of fine sand.	A-7-5(15)	
12.65			14.0'		24" RECOVERY		

Remarks:

Reviewed By: Hany Fekry

Soils Supervisor: Aaron Wieczorek

**STATE OF DELAWARE
DEPARTMENT OF TRANSPORTATION
MATERIALS AND RESEARCH**

Project Name: James Street Bridge
State Contract: T201207101

Boring No.: JS-3

Depth (ft.)	Water Level	No.	Sample Depth	Blows/6"	Sample Description	AASHTO Class.	Remarks
15.18		8	14.0'	32 32 12	No sieve analysis - Indication of saturated hard gray wet very stiff silt.		
			16.0'		4" RECOVERY		
17.71		9	16.0'	8 11 7 5	No sieve analysis - Indication of saturated hard gray organic wet very stiff silt.		
			18.0'		6" RECOVERY		
20.24		10	18.0'	5 2 1 1	No sieve analysis - Indication of saturated hard gray organic wet very stiff silt.		
			20.0'		2" RECOVERY		
		11	20.0'	2 2 2 1	Saturated soft gray organic silty clay w/some fine to coarse sand.	A-6(9)	
			22.0'		24" RECOVERY		
22.77		U-1	22.0'				Shelby Tube - Press Sample
			24.0'		24" RECOVERY		
25.3		13	24.0'	WR 3 2 8	Saturated loose gray coarse to fine sand w/trace of silt and fine gravel.	A-1-b	
			26.0'		24" RECOVERY		
27.83		14	26.0'	1 5 8 16	Saturated medium dense gray coarse to fine sand w/trace of fine gravel and silt.	A-1-b	
			28.0'		24" RECOVERY		
		15	28.0'	23 28 21 25	Saturated dense gray coarse sand w/some fine gravel, trace of fine sand and silt.	A-1-b	
			30.0'		24" RECOVERY		
30.36		16	30.0'	4 3 5 12	Saturated loose gray coarse to fine sand w/trace of fine gravel and silt.	A-1-b	
			32.0'		24" RECOVERY		
32.89		17	32.0'	10 15 15 17	Saturated medium dense gray fine gravelly coarse to fine sand w/trace of silt.	A-1-b	
			34.0'		20" RECOVERY		
35.42		18	34.0'	14 17 16 15	Saturated dense grayish brown coarse sandy fine gravel w/some fine sand, trace of silt.	A-1-b	
			36.0'		18" RECOVERY		
		19	36.0'	16 22 50	Saturated medium dense grayish brown coarse sandy fine gravel w/some fine sand, trace of silt.	A-1-a	
37.95			38.0'		16" RECOVERY		

**STATE OF DELAWARE
DEPARTMENT OF TRANSPORTATION
MATERIALS AND RESEARCH**

Project Name: James Street Bridge
State Contract: T201207101

Boring No.: JS-3

Depth (ft.)	Water Level	No.	Sample Depth	Blows/6"	Sample Description	AASHTO Class.	Remarks
		20	38.0'	7 12 20 16	Saturated hard reddish brown clayey fine to coarse sandy silt w/trace of fine gravel.	A-4(1)	
			40.0'		24" RECOVERY		
40.48		21	40.0'	9 12 18 22	Saturated medium dense reddish brown clayey fine sand w/some coarse sand, fine gravel and silt.	A-2-4(0)	
			42.0'		10" RECOVERY		
43.01		22	43.0'	5 6 8 10	Saturated medium dense brown clayey fine to coarse sand w/some silt, trace of fine gravel.	A-2-4(0)	
			45.0'		15" RECOVERY		
45.54							
48.07		23	48.0'	6 7 4 6	Saturated medium dense brown silty fine to coarse sand.	A-2-4(0)	
			50.0'		20" RECOVERY		
50.6							
53.13		24	53.0'	19 14 11 17	Saturated medium dense brown silty fine sand w/ some coarse sand, trace of fine gravel.	A-2-4(0)	
			55.0'		20" RECOVERY		
55.66							
58.19		25	58.0'	11 12 17 9	Saturated medium dense brown clayey fine to coarse sand and fine gravel w/some silt.	A-2-6(0)	
			60.0'		20" RECOVERY		
60.72							

**STATE OF DELAWARE
DEPARTMENT OF TRANSPORTATION
MATERIALS AND RESEARCH**

Project Name: James Street Bridge
State Contract: T201207101

Boring No.: JS-3

Depth (ft.)	Water Level	No.	Sample Depth	Blows/6"	Sample Description	AASHTO Class.	Remarks
63.25		26	63.0'	10 10 13 11	Saturated medium dense brown silty fine to coarse sand w/trace of fine gravel. 18" RECOVERY	A-2-4(0)	
65.78	65.0'						
68.31		27	68.0'	4 5 5	Saturated stiff grayish brown clayey fine sandy silt w/some coarse sand, trace of fine gravel. 20" RECOVERY	A-4(1)	
70.84	70.0'						
73.37		28	73.0'	5 6 10 9	Saturated very stiff grayish brown fine to coarse sandy clay w/some silt. 24" RECOVERY	A-6(4)	
75.9	75.0'						
78.43		29	78.0'	11 7 11 20	Saturated very stiff gray clayey fine to coarse sandy silt. 24" RECOVERY	A-4(1)	
80.96	80.0'						
83.49		30	83.0'	15 20 17 27	Saturated hard gray fine sandy silt w/some coarse sand, trace of fine gravel. 24" RECOVERY	A-4(0)	
	85.0'						

**STATE OF DELAWARE
DEPARTMENT OF TRANSPORTATION
MATERIALS AND RESEARCH**

Project Name: James Street Bridge
State Contract: T201207101

Boring No.: JS-3

Depth (ft.)	Water Level	No.	Sample Depth	Blows/6"	Sample Description	AASHTO Class.	Remarks
88.55		31	88.0'	13 23 38 50	Saturated hard gray clayey coarse to fine sandy silt w/trace of fine gravel. (Weathered Rock) 24" RECOVERY	A-4(1)	
			90.0'				
91.08							
93.61		32	93.0'	15 23 34 50	Saturated hard gray clayey fine sandy silt w/some coarse sand. (Weathered Rock) 24" RECOVERY	A-4(2)	
			95.0'				
96.14							
98.67		33	98.0'	14 22 23 34	Saturated hard grayish brown fine sandy clay w/ some coarse sand and silt, trace of fine gravel. (Weathered Rock) 24" RECOVERY	A-7-6(11)	
			100.0'				
101.2							
103.73		34	103.0'	23 24 40 50	Saturated very dense bluish gray clayey fine to coarse sand w/some silt, trace of fine gravel. (Weathered Rock) 23" RECOVERY	A-2-7(1)	
			105.0'				
106.26							
108.79		35	108.0'	33 50	Saturated very dense bluish gray clayey fine sand w/some coarse sand and silt, trace of fine gravel.	A-2-4(0)	

KEY TO SYMBOLS

Symbol Description

Strata symbols



Silty soils



Well graded gravels and sands



Poorly graded, silty or clayey
sands and gravel



Plastic clays



Expansive plastic clays

Misc. Symbols



Water table during
drilling

Notes:

1. Exploratory borings were drilled using a 3 1/4 - inch diameter hollow stem auger.
2. No free water was encountered at the time of drilling or when re-checked the following day, unless recorded on 1st page.
3. Boring locations were taped from existing features and elevations extrapolated from survey unless otherwise reported.
4. These logs are subject to the limitations, conclusions, and recommendations in this report.
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6. All blow counts are uncorrected.

**STATE OF DELAWARE
DEPARTMENT OF TRANSPORTATION
MATERIALS AND RESEARCH**

BORING JS-4

Project Name: James Street Bridge

Location: Newport, DE

State Contract #: T201207101

Federal Contract #:

Station/Offset:

Northing:

Easting:

Boring Surface Elev.:

Reference:

Date Started: 8/21/12

Date Completed: 8/23/12

Wt. of Sample Hammer: 140
Type of: D-Sampler: Split Barrel
S-Sampler:
U-Sampler:
Core Bit:

Lbs.
O.D.
O.D.
O.D.
O.D.

Average Fall: 30
O.D. of Sampler: 2
O.D. of Samp. Tube:
O.D. of Samp. Tube:
O.D. of Rock Core:

IN.
IN.
IN.
IN.
IN.

Hollow Stem Auger Diameter: 3 1/4" **Inches**
Mud Rotary:

From Depth of: 0.0 **To:** 23.0
From Depth of: 23.0 **To:** 118.1

Water Level Readings

Date
8/21/12

Depth to Water (ft)
19.8

Caved Depth (ft)

Boring Contractor: Walton Corporation

Equipment/Rig Type: CME 55 Truck

Driller: Bill Holden

Logged By: Kat Kershaw

Depth (ft.)	Water Level	No.	Sample Depth	Blows/6"	Sample Description	AASHTO Class.	Remarks
		1	0.0'	4 4 5	Wet stiff brown fine to coarse sandy silt w/trace of fine gravel.	A-4(0)	
			2.0'		18" RECOVERY		
2.53		2A	2.0'	4 4	Wet loose brown silty fine to coarse sand w/some fine gravel.	A-2-4(0)	
			3.0'		6" RECOVERY		
		2B	3.0'	5 3	Saturated firm gray clayey silt w/trace of fine to coarse sand and fine gravel.	A-4(9)	
			4.0'		12" RECOVERY		
5.06		3	4.0'	1 2 2 2	Saturated soft gray silty clay w/trace of fine to coarse sand and fine gravel.	A-6(10)	
			6.0'		6" RECOVERY		
		4	6.0'	2 1 2 2	Saturated soft gray silty clay w/trace of fine to coarse sand.	A-6(14)	
7.59			8.0'		14" RECOVERY		
		U-1	8.0'				Shelby Tube - Press Sample
			10.0'		24" RECOVERY		
10.12		5	10.0'	WH 1 1 1	Saturated soft gray organic clay w/some silt, trace of fine to coarse sand.	A-7-5(13)	
			12.0'		24" RECOVERY		
12.65		6	12.0'	WH 1 1 1	Saturated soft gray organic clay w/some silt, trace of fine to coarse sand.	A-7-5(18)	
			14.0'		24" RECOVERY		

Remarks: 5' of 8" casing set, 48' of 4" casing set.

Reviewed By: _____

Soils Supervisor: _____

**STATE OF DELAWARE
DEPARTMENT OF TRANSPORTATION
MATERIALS AND RESEARCH**

Project Name: James Street Bridge
State Contract: T201207101

Boring No.: JS-4

Depth (ft.)	Water Level	No.	Sample Depth	Blows/6"	Sample Description	AASHTO Class.	Remarks
15.18	▽	7	14.0'	1 1 1 2	Saturated soft gray organic clay w/some silt, trace of fine to coarse sand.	A-7-5(19)	
					24" RECOVERY		
17.71		8	16.0'	1 2 2 2	Saturated soft gray organic clay w/some silt, trace of fine to coarse sand.	A-7-5(15)	
					24" RECOVERY		
20.24		9	18.0'	1 1 1 1	Saturated soft gray clay w/some silt, trace of coarse to fine sand.	A-7-5(22)	
					24" RECOVERY		
22.77							
25.3		10	23.0'	1 3 5 8	Saturated loose gray coarse sand w/some fine sand and fine gravel, trace of silt.	A-1-b	
					24" RECOVERY		
27.83							
30.36		11	28.0'	22 28 8 8	Saturated dense orange fine gravel w/some coarse to fine sand and silt.	A-1-a	
					12" RECOVERY		
32.89							
35.42	12	33.0'	7 8 11 23	Saturated very stiff yellow clayey fine sandy silt w/ trace of coarse sand and fine gravel.	A-4(1)		
				24" RECOVERY			
37.95							

**STATE OF DELAWARE
DEPARTMENT OF TRANSPORTATION
MATERIALS AND RESEARCH**

Project Name: James Street Bridge
State Contract: T201207101

Boring No.: JS-4

Depth (ft.)	Water Level	No.	Sample Depth	Blows/6"	Sample Description	AASHTO Class.	Remarks
		13	38.0'	8 9 9 9	Saturated medium dense tan silty fine to coarse sand w/trace of fine gravel. 22" RECOVERY	A-2-4(0)	
40.48			40.0'				
		14	43.0'	11 14 18 19	Saturated dense tan silty fine to coarse sand w/trace of fine gravel. 24" RECOVERY	A-2-4(0)	
43.01			45.0'				
		15	48.0'	28 20 20 20	Saturated dense tan coarse to fine sand w/some fine gravel and silt. 24" RECOVERY	A-1-b	
45.54			50.0'				
		16	53.0'	18 19 15 12	No Recovery NR" RECOVERY		
48.07			55.0'				
		17	58.0'	8 10 12 14	No Recovery NR" RECOVERY		
50.6			60.0'				
53.13							
55.66							
58.19							
60.72							

**STATE OF DELAWARE
DEPARTMENT OF TRANSPORTATION
MATERIALS AND RESEARCH**

Project Name: James Street Bridge
State Contract: T201207101

Boring No.: JS-4

Depth (ft.)	Water Level	No.	Sample Depth	Blows/6"	Sample Description	AASHTO Class.	Remarks
63.25		18	63.0'	5 7 9 9	No Recovery		
			65.0'		NR" RECOVERY		
65.78							
68.31		19	68.0'	6 6 8 12	Saturated stiff yellow clay w/some silt and fine sand, trace of coarse sand.	A-7-5(18)	
			70.0'		24" RECOVERY		
70.84							
73.37		20	73.0'	6 10 15 40	Saturated very stiff gray clay w/some fine to coarse sand and fine gravel, trace of silt.	A-7-5(9)	
			75.0'		24" RECOVERY		
75.9							
78.43		21	78.0'	10 15 25 29	Saturated hard gray fine sandy clay w/trace of coarse sand and silt.	A-7-6(8)	
			80.0'		24" RECOVERY		
80.96							
83.49		22	83.0'	13 20 20 26	Saturated hard gray fine sandy clay w/trace of coarse sand and silt.	A-7-6(9)	
			85.0'		24" RECOVERY		

**STATE OF DELAWARE
DEPARTMENT OF TRANSPORTATION
MATERIALS AND RESEARCH**

Project Name: James Street Bridge
State Contract: T201207101

Boring No.: JS-4

Depth (ft.)	Water Level	No.	Sample Depth	Blows/6"	Sample Description	AASHTO Class.	Remarks
88.55		23	88.0'	15 18 28 36	Saturated hard gray fine sandy clay w/some silt, trace of coarse sand.	A-6(3)	
			90.0'		24" RECOVERY		
91.08							
93.61		24	93.0'	15 17 28 29	Saturated hard gray silty fine sandy clay w/trace of coarse sand.	A-6(6)	
			95.0'		24" RECOVERY		
96.14							
98.67		25	98.0'	12 13 25 48	Saturated hard green fine sandy clay w/some coarse sand, trace of silt.	A-7-5(7)	
			100.0'		24" RECOVERY		
101.2							
103.73							
106.26		26	104.7'	19 40 48 50	Saturated hard greenish brown fine sandy silt w/ some coarse sand and clay.	A-4(0)	
			106.7'		21" RECOVERY		
108.79		27	108.0'	50	No sieve analysis - Indication of saturated dense gray silty sand.		

**STATE OF DELAWARE
DEPARTMENT OF TRANSPORTATION
MATERIALS AND RESEARCH**

Project Name: James Street Bridge
State Contract: T201207101

Boring No.: JS-4

Depth (ft.)	Water Level	No.	Sample Depth	Blows/6"	Sample Description	AASHTO Class.	Remarks
			110.0'		<p style="text-align: center;">2" RECOVERY</p> <p style="text-align: center;">No sieve analysis - Indication of saturated dense gray silty sand. (Weathered Rock)</p> <p style="text-align: center;">2" RECOVERY</p>		
111.32							
		28	113.2'	50			
113.85			115.2'				
116.38							
		29	118.0'	50			
118.91			120.0'				
121.44							
					<p style="text-align: center;">No Recovery</p> <p style="text-align: center;">NR" RECOVERY</p>		
123.97							
126.5							
129.03							
131.56							

KEY TO SYMBOLS

Symbol Description

Strata symbols



Silty soils



Poorly graded, silty or clayey
sands and gravel



Plastic clays



Expansive plastic clays



Well graded gravels and sands

Misc. Symbols



Water table during
drilling

Notes:

1. Exploratory borings were drilled using a 3 1/4 - inch diameter hollow stem auger.
2. No free water was encountered at the time of drilling or when re-checked the following day, unless recorded on 1st page.
3. Boring locations were taped from existing features and elevations extrapolated from survey unless otherwise reported.
4. These logs are subject to the limitations, conclusions, and recommendations in this report.
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**STATE OF DELAWARE
DEPARTMENT OF TRANSPORTATION
MATERIALS AND RESEARCH**

BORING JS-5

Project Name: James Street Bridge

Location: Newport, DE

State Contract #: T201207101

Federal Contract #:

Station/Offset:

Northing:

Easting:

Boring Surface Elev.:

Reference:

Date Started: 8/7/12

Date Completed:

Wt. of Sample Hammer: 140
Type of: D-Sampler: Split Barrel
S-Sampler:
U-Sampler:
Core Bit:

Lbs.
O.D.
O.D.
O.D.
O.D.

Average Fall: 30
O.D. of Sampler: 2
O.D. of Samp. Tube:
O.D. of Samp. Tube:
O.D. of Rock Core:

IN.
IN.
IN.
IN.
IN.

Hollow Stem Auger Diameter: 3 1/4" **Inches**
Mud Rotary:

From Depth of: 0.0 **To:** 28.0
From Depth of: 28.0 **To:** 120.0

Water Level Readings
Date

Depth to Water (ft)

Caved Depth (ft)

Boring Contractor: Walton Corporation

Equipment/Rig Type: CME 55 Truck

Driller: Bill Holden

Logged By: Meghan Lester

Depth (ft.)	Water Level	No.	Sample Depth	Blows/6"	Sample Description	AASHTO Class.	Remarks	
20.24		1	20.0'	1 2 2	Saturated soft gray clayey silt w/some fine sand, trace of coarse sand and fine gravel.	A-4(7)	River Mud	
		2	22.0'	6 WH	4" RECOVERY		River Mud	
			22.0'		No Sample			
22.77			3	24.0'	WH	NR" RECOVERY		River Mud
				24.0'		No Sample		
				26.0'		NR" RECOVERY		
25.3			4	26.0'	1 2	Saturated soft gray clayey fine sandy silt w/some coarse sand and fine gravel.	A-4(0)	
				26.0'		WH" RECOVERY		
27.83				28.0'				
30.36			5	33.0'	8 6 4 6	Saturated loose tan fine gravelly coarse to fine sand w/trace of silt.	A-1-b	
32.89								

Remarks: Mudline @ 20'

Reviewed By: Hany Fekry

Soils Supervisor: Aaron Wieczorek

**STATE OF DELAWARE
DEPARTMENT OF TRANSPORTATION
MATERIALS AND RESEARCH**

Project Name: James Street Bridge
State Contract: T201207101

Boring No.: JS-5

Depth (ft.)	Water Level	No.	Sample Depth	Blows/6"	Sample Description	AASHTO Class.	Remarks
35.42			35.0'		14" RECOVERY		
37.95							
40.48		6	38.0'	7 6 7 7	Saturated medium dense red silty coarse to fine sand w/trace of fine gravel. 11" RECOVERY	A-2-4(0)	
43.01			40.0'				
45.54		7	43.0'	7 14 15 15	Saturated medium dense tan fine to coarse sand w/ some silt. 20" RECOVERY	A-2-4(0)	
48.07			45.0'				
50.6		8	48.0'	9 8 8 8	Saturated medium dense tan silty fine to coarse sand w/trace of fine gravel. 15" RECOVERY	A-2-4(0)	
53.13			50.0'				
55.66		9	53.0'	9 8 9 15	Saturated medium dense yellow coarse to fine sand w/some silt, trace of fine gravel. 20" RECOVERY	A-1-b	
			55.0'				

**STATE OF DELAWARE
DEPARTMENT OF TRANSPORTATION
MATERIALS AND RESEARCH**

Project Name: James Street Bridge
State Contract: T201207101

Boring No.: JS-5

Depth (ft.)	Water Level	No.	Sample Depth	Blows/6"	Sample Description	AASHTO Class.	Remarks
		10	58.0'	12 11 8 11	Saturated medium dense yellows coarse to fine sand and fine gravel w/some silt. 12" RECOVERY	A-1-b	
60.72			60.0'				
63.25		11	63.0'	13 6 9 14	Saturated stiff yellow coarse sandy clay w/some fine sand and fine gravel, trace of silt. 18" RECOVERY	A-7-6(2)	
65.78			65.0'				
68.31		12	68.0'	6 9 13 17	Saturated very stiff grayish tan fine sandy clay w/ some silt, trace of coarse sand. 21" RECOVERY	A-7-5(16)	
70.84			70.0'				
73.37		13	73.0'	5 12 11 15	Saturated very stiff grayish brown fine sandy clay w/some coarse sand and silt. 24" RECOVERY	A-7-5(10)	
75.9			75.0'				
78.43		14	78.0'	9 19 26 37	Saturated hard reddish brown fine sandy clay w/ some coarse sand and silt. 24" RECOVERY	A-7-5(14)	
80.96			80.0'				

**STATE OF DELAWARE
DEPARTMENT OF TRANSPORTATION
MATERIALS AND RESEARCH**

Project Name: James Street Bridge
State Contract: T201207101

Boring No.: JS-5

Depth (ft.)	Water Level	No.	Sample Depth	Blows/6"	Sample Description	AASHTO Class.	Remarks
83.49		15	83.0'	21 32 50	Saturated hard grayish fine sandy clay w/some coarse sand and silt.	A-7-5(7)	
			85.0'		18" RECOVERY		
86.02							
88.55		16	88.0'	15 34 50	Saturated hard grayish brown fine sandy clay w/ some coarse sand and silt.	A-7-5(6)	
			90.0'		24" RECOVERY		
91.08							
93.61		17	93.0'	16 19 22 30	Saturated hard reddish brown fine sandy clay w/ some silt, trace of coarse sand.	A-7-6(6)	
			95.0'		24" RECOVERY		
96.14							
98.67		18	98.0'	18 28 52	Saturated very dense grayish brown clayey fine to coarse sand w/trace of silt and fine gravel. (Weathered Rock)	A-2-7(1)	
			100.0'		18" RECOVERY		
101.2							
103.73		19	103.0'	26 28 50	Saturated very dense grayish brown silty fine sand w/some coarse sand, trace of fine gravel. (Weathered Rock)	A-2-4(0)	
			105.0'		16" RECOVERY		

**STATE OF DELAWARE
DEPARTMENT OF TRANSPORTATION
MATERIALS AND RESEARCH**

Project Name: James Street Bridge
State Contract: T201207101

Boring No.: JS-5

Depth (ft.)	Water Level	No.	Sample Depth	Blows/6"	Sample Description	AASHTO Class.	Remarks
106.26							
108.79		20	108.0'	50	Saturated hard green fine to coarse sandy clay w/ some silt, trace of fine gravel. (Highly Weathered Rock) 2" RECOVERY	A-6(2)	
			110.0'				
111.32							
113.85		21	113.0'	50	Saturated hard green clayey fine sandy silt w/trace of coarse sand. (Highly Weathered Rock) 2" RECOVERY	A-4(0)	
			115.0'				
116.38							
118.91		22	118.0'	50	Saturated dense green silty coarse to fine sand w/ some fine gravel. (Highly Weathered Rock) 2" RECOVERY	A-1-b	
			120.0'				
121.44							
123.97							
126.5							
129.03							

KEY TO SYMBOLS

Symbol Description

Strata symbols



Silty soils



Well graded gravels and sands



Poorly graded, silty or clayey
sands and gravel



Expansive plastic clays



Plastic clays

Notes:

1. Exploratory borings were drilled using a 3 1/4 - inch diameter hollow stem auger.
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**STATE OF DELAWARE
DEPARTMENT OF TRANSPORTATION
MATERIALS AND RESEARCH**

BORING JS-6

Project Name: James Street Bridge

Location: Newport, DE

State Contract #: T201207101

Federal Contract #:

Station/Offset:

Northing:

Easting:

Boring Surface Elev.:

Reference:

Date Started: 8/16/12

Date Completed: 8/20/12

Wt. of Sample Hammer: 140
Type of: D-Sampler: Split Barrel
S-Sampler:
U-Sampler:
Core Bit:

Lbs.
O.D.
O.D.
O.D.
O.D.

Average Fall: 30
O.D. of Sampler: 2
O.D. of Samp. Tube:
O.D. of Samp. Tube:
O.D. of Rock Core:

IN.
IN.
IN.
IN.
IN.

Hollow Stem Auger Diameter: 3 1/4" **Inches**
Mud Rotary:

From Depth of: 23.0 **To:** 118.0
From Depth of: **To:**

Water Level Readings
Date

Depth to Water (ft)

Caved Depth (ft)

Boring Contractor: Walton Corporation

Equipment/Rig Type: CME 55 Truck

Driller: Bill Holden

Logged By: KK, JL and CC

Depth (ft.)	Water Level	No.	Sample Depth	Blows/6"	Sample Description	AASHTO Class.	Remarks
		1	23.0'	WH	River Mud.	A-4(0)	River Mud
			25.0'		4" RECOVERY		
25.3		2	25.0'	17 13 6 WH	Saturated medium dense gray coarse sandy fine gravel w/some silt, trace of fine sand.	A-1-a	
			27.0'		24" RECOVERY		
27.83		3	27.0'	WH	Saturated soft dark gray organic fine sandy silt w/ some coarse sand.	A-5(0)	
			29.0'		24" RECOVERY		
30.36		4	29.0'	WH	Saturated soft dark gray clayey fine sandy silt w/ trace of coarse sand.	A-4(3)	
			31.0'		24" RECOVERY		
32.89		5	31.0'	7 5 7 6	Saturated medium dense orange fine to coarse sand w/some silt, trace of fine gravel.	A-2-4(0)	
			33.0'		13" RECOVERY		
35.42		6	33.0'	3 3 6 7	Saturated loose orange clayey coarse to fine sand w/some silt, trace of fine gravel.	A-2-6(1)	
			35.0'		14" RECOVERY		

Remarks: Boring performed through bridge deck. 8" casing set to 20', 4" casing set to 40'.

Reviewed By: Hany Fekry

Soils Supervisor: Aaron Wieczorek

**STATE OF DELAWARE
DEPARTMENT OF TRANSPORTATION
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Project Name: James Street Bridge
State Contract: T201207101

Boring No.: JS-6

Depth (ft.)	Water Level	No.	Sample Depth	Blows/6"	Sample Description	AASHTO Class.	Remarks
37.95							
		7	38.0'	WH 1 3 8	Saturated soft pinkish white clay w/some silt and fine sand, trace of coarse sand.	A-7-6(21)	
			40.0'		16" RECOVERY		
40.48							
43.01		8	43.0'	12 11 8 7	Saturated medium dense orangish tan coarse to fine sand w/some silt, trace of fine gravel.	A-2-4(0)	Hole Caved up to 40'. Rewash
			45.0'		17" RECOVERY		
45.54							
48.07		9	48.0'	7 8 7 7	Saturated medium dense orange organic silty fine sand w/some coarse sand, fine gravel and clay.	A-2-4(0)	
			50.0'		20" RECOVERY		
50.6							
53.13		10	53.0'	6 6 7 10	Saturated medium dense tannish orange silty coarse to fine sand w/some fine gravel.	A-2-4(0)	
			55.0'		16" RECOVERY		
55.66							
58.19		11	58.0'	4 4 5 7	Saturated stiff gray silty fine sandy clay w/trace of coarse sand and fine gravel.	A-6(7)	Boring Advanced using roller bit. Quick gel/soda ash water mud mix.
			60.0'		17" RECOVERY		
60.72							

**STATE OF DELAWARE
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MATERIALS AND RESEARCH**

Project Name: James Street Bridge
State Contract: T201207101

Boring No.: JS-6

Depth (ft.)	Water Level	No.	Sample Depth	Blows/6"	Sample Description	AASHTO Class.	Remarks
63.25		12	63.0'	7 10 13 13	Saturated very stiff green fine sandy clay w/some silt, trace of coarse sand.	A-7-5(14)	
			65.0'		21" RECOVERY		
65.78							
68.31		13	68.0'	10 13 18 19	Saturated hard green fine sandy clay w/some silt, trace of coarse sand.	A-7-5(13)	
			70.0'		20" RECOVERY		
70.84							
73.37		14	73.0'	11 22 24 28	Saturated hard green fine sandy clay w/some silt, trace of coarse sand.	A-7-6(6)	
			75.0'		24" RECOVERY		
75.9							
78.43		15	78.0'	11 17 16 19	Saturated hard grayish brown fine sandy clay w/ some silt, trace of coarse sand.	A-7-6(7)	
			80.0'		24" RECOVERY		
80.96							
83.49		16	83.0'	8 9 15 15	Saturated very stiff green clay w/some fine sand and silt, trace of coarse sand.	A-7-5(22)	

**STATE OF DELAWARE
DEPARTMENT OF TRANSPORTATION
MATERIALS AND RESEARCH**

Project Name: James Street Bridge
State Contract: T201207101

Boring No.: JS-6

Depth (ft.)	Water Level	No.	Sample Depth	Blows/6"	Sample Description	AASHTO Class.	Remarks
			85.0'		24" RECOVERY		
86.02							
88.55		17	88.0'	13 22 32 40	Saturated hard green fine sandy clay w/some silt, trace of coarse sand.	A-7-5(14)	
			90.0'		24" RECOVERY		
91.08							
93.61		18	93.0'	22 26 24 32	Saturated hard reddish brown clay w/some coarse to fine sand and silt.	A-7-5(17)	
			95.0'		24" RECOVERY		
96.14							
98.67		19	98.0'	22 28 28 22	Saturated hard bluish gray fine sandy clay w/trace of coarse sand and silt.	A-7-6(3)	
			100.0'		24" RECOVERY		
101.2							
103.73		20	103.0'	50	Saturated dense bluish gray silty fine to coarse sand.	A-2-4(0)	
			105.0'		5" RECOVERY		
106.26							
108.79		21	108.0'		No Sample		

**STATE OF DELAWARE
DEPARTMENT OF TRANSPORTATION
MATERIALS AND RESEARCH**

Project Name: James Street Bridge

Boring No.: JS-6

State Contract: T201207101

Depth (ft.)	Water Level	No.	Sample Depth	Blows/6"	Sample Description	AASHTO Class.	Remarks
111.32					No Sample		
113.85		22	113.0'			50" RECOVERY	
116.38					End Boring.		
118.91		23	118.0'			50" RECOVERY	
121.44							
123.97							
126.5							
129.03							
131.56							

KEY TO SYMBOLS

Symbol Description

Strata symbols



Silty soils



Well graded gravels and sands



Elastic Silts



Poorly graded, silty or clayey
sands and gravel



Expansive plastic clays



Plastic clays

Notes:

1. Exploratory borings were drilled using a 3 1/4 - inch diameter hollow stem auger.
2. No free water was encountered at the time of drilling or when re-checked the following day, unless recorded on 1st page.
3. Boring locations were taped from existing features and elevations extrapolated from survey unless otherwise reported.
4. These logs are subject to the limitations, conclusions, and recommendations in this report.
5. Results of tests conducted on samples recovered are reported on the logs.
6. All blow counts are uncorrected.

**STATE OF DELAWARE
DEPARTMENT OF TRANSPORTATION
MATERIALS AND RESEARCH**

BORING JS-7

Project Name: James Street Bridge

Location: Newport, DE

State Contract #: T201207101

Federal Contract #:

Station/Offset:

Northing:

Easting:

Boring Surface Elev.:

Reference:

Date Started: 6/7/12

Date Completed: 6/14/12

Wt. of Sample Hammer: 140
Type of: D-Sampler: Split Barrell
S-Sampler:
U-Sampler:
Core Bit:

Lbs.
O.D.
O.D.
O.D.
O.D.

Average Fall: 30
O.D. of Sampler: 2
O.D. of Samp. Tube:
O.D. of Samp. Tube:
O.D. of Rock Core:

IN.
IN.
IN.
IN.
IN.

Hollow Stem Auger Diameter: 3 1/4" **Inches**
Mud Rotary:

From Depth of: 0.0 **To:** 42.0
From Depth of: 42.0 **To:** 103.0

Water Level Readings

Date
6/8/12

Depth to Water (ft)
14.8

Caved Depth (ft)

Boring Contractor: Walton Corporation

Equipment/Rig Type: CME 55 Truck

Driller: Jason Truver

Logged By: Chris Costanzi

Depth (ft.)	Water Level	No.	Sample Depth	Blows/6"	Sample Description	AASHTO Class.	Remarks
		1	2.5'	2 4 3	Wet firm brown clayey silt w/some coarse to fine sand, trace of fine gravel.	A-4(2)	6" hot-mix, 2' GABC. Fill
			4.0'		12" RECOVERY		
5.06		2	4.0'	2 5 50	Wet very dense brown fine gravel w/some fine to coarse sand and silt.	A-1-b	Fill
			6.0'		10" RECOVERY		
		3	6.0'	3 2 3	Wet soft brown clayey coarse sandy fine gravelly silt w/some fine sand.	A-4(0)	Fill
7.59			8.0'		16" RECOVERY		
		4	8.0'	2 2 3 4	Wet firm brown clayey silt w/some fine to coarse sand, trace of fine gravel.	A-4(2)	Fill
10.12			10.0'		24" RECOVERY		
		5	10.0'	3 2 1 1	Saturated soft gray clayey silt w/some coarse to fine sand and fine gravel.	A-4(1)	Fill
			12.0'		20" RECOVERY		
12.65		6	12.0'	17 9 7 6	Saturated very stiff gray clayey fine gravelly silt w/ some fine to coarse sand.	A-4(0)	Fill
			14.0'		16" RECOVERY		
		7	14.0'	3 2 2 1	Saturated loose gray clayey fine gravel w/some fine to coarse sand and silt.	A-2-4(0)	Fill
15.18	▽		16.0'		15" RECOVERY		
		8	16.0'	3 5 3	Saturated firm gray clayey fine gravelly silt w/	A-4(3)	Fill

Remarks:

Reviewed By: Hany Fekry

Soils Supervisor: Aaron Wieczorek

**STATE OF DELAWARE
DEPARTMENT OF TRANSPORTATION
MATERIALS AND RESEARCH**

Project Name: James Street Bridge
State Contract: T201207101

Boring No.: JS-7

Depth (ft.)	Water Level	No.	Sample Depth	Blows/6"	Sample Description	AASHTO Class.	Remarks
17.71			18.0'	2	some fine sand, trace of coarse sand. 20" RECOVERY		
20.24		9	18.0'	3 2 3 2	Saturated firm gray clayey silt w/trace of fine to coarse sand and fine gravel. 20" RECOVERY	A-5(9)	Shelby Tube - Press Sample
		U-1	20.0'		24" RECOVERY		
22.77		11	22.0'	2 3 6 10	Saturated firm brown clayey fine sandy silt w/some coarse sand, trace of fine gravel. 14" RECOVERY	A-4(1)	
25.3		12	24.0'	2 3 6 10	Saturated loose tan clayey fine sand w/some coarse sand, fine gravel and silt. 20" RECOVERY	A-2-6(1)	
27.83		13	26.0'	6 7 6 7	Saturated stiff reddish brown clayey fine sandy silt w/trace of coarse sand and fine gravel. 24" RECOVERY	A-4(1)	
30.36		14	28.0'	5 10 14 13	Saturated medium dense reddish brown silty fine sand w/some coarse sand and fine gravel. 24" RECOVERY	A-2-4(0)	
32.89		15	30.0'	9 14 20 22	Saturated dense brown clayey fine sand w/some coarse sand and silt, trace of fine gravel. 24" RECOVERY	A-2-4(0)	
35.42		16	32.0'	3 8 12 17	Saturated very stiff brown fine sand clay w/some coarse sand and silt, trace of fine gravel. 20" RECOVERY	A-6(1)	
37.95		17	34.0'	8 10 13 15	Saturated medium dense brown clayey coarse to fine sand w/some silt, trace of fine gravel. 24" RECOVERY	A-2-4(0)	
40.48		18	36.0'	11 13 9 8	Saturated very stiff brown silty clay w/some fine sand, trace of coarse sand and fine gravel. 24" RECOVERY	A-6(10)	
		19	38.0'	8 10 10 13	Saturated very stiff reddish brown clayey fine sandy silt w/trace of coarse sand and fine gravel. 20" RECOVERY	A-4(1)	
		20	40.0'	8 15	No sieve analysis - Indication of saturated dense		

**STATE OF DELAWARE
DEPARTMENT OF TRANSPORTATION
MATERIALS AND RESEARCH**

Project Name: James Street Bridge
State Contract: T201207101

Boring No.: JS-7

Depth (ft.)	Water Level	No.	Sample Depth	Blows/6"	Sample Description	AASHTO Class.	Remarks
				25 20	brown sand.		
			42.0'		24" RECOVERY		
43.01		21	43.0'	15 20 22 16	Saturated dense brown silty fine to coarse sand w/ some fine gravel.	A-2-4(0)	
			45.0'		20" RECOVERY		
45.54							
48.07		22	48.0'	7 8 13 20	Saturated medium dense gray coarse to fine sand w/some fine gravel and silt.	A-1-b	
			50.0'		20" RECOVERY		
50.6							
53.13		23	53.0'	10 6 5 11	Saturated medium dense tan fine gravel and coarse to fine sand w/some silt.	A-1-b	
			55.0'		20" RECOVERY		
55.66							
58.19		24	58.0'	5 7 7 13	Saturated stiff tan fine sandy clay w/some coarse sand, trace of silt and fine gravel.	A-7-5(4)	
			60.0'		24" RECOVERY		
60.72							
63.25		25	63.0'	15 24 24 28	Saturated hard grayish brown fine sandy clay w/ some silt, trace of coarse sand. (Weathered Rock)	A-7-5(5)	

**STATE OF DELAWARE
DEPARTMENT OF TRANSPORTATION
MATERIALS AND RESEARCH**

Project Name: James Street Bridge
State Contract: T201207101

Boring No.: JS-7

Depth (ft.)	Water Level	No.	Sample Depth	Blows/6"	Sample Description	AASHTO Class.	Remarks
			65.0'		24" RECOVERY		
65.78							
68.31		26	68.0'	14 23 39 37	Saturated hard grayish brown fine sandy clay w/ some coarse sand, trace of silt. (Weathered Rock)	A-7-5(3)	
			70.0'		24" RECOVERY		
70.84							
73.37		27	73.0'	27 45 50	Saturated hard bluish gray clayey fine to coarse sandy silt. (Weathered Rock)	A-5(2)	
			75.0'		15" RECOVERY		
75.9							
78.43		28	78.0'	24 25 50	Saturated hard bluish gray clayey fine sandy silt w/ trace of coarse sand. (Weathered Rock)	A-5(4)	
			80.0'		18" RECOVERY		
80.96							
83.49		29	83.0'	19 25 24 50	Saturated hard bluish gray clay w/some fine to coarse sand and silt. (Weathered Rock)	A-7-5(8)	
			85.0'		23" RECOVERY		
86.02							
		30	88.0'	21			

**STATE OF DELAWARE
DEPARTMENT OF TRANSPORTATION
MATERIALS AND RESEARCH**

Project Name: James Street Bridge
State Contract: T201207101

Boring No.: JS-7

Depth (ft.)	Water Level	No.	Sample Depth	Blows/6"	Sample Description	AASHTO Class.	Remarks
88.55				27 28 41	Saturated hard bluish gray fine sandy clay w/some silt, trace of coarse sand. (Weathered Rock) 24" RECOVERY	A-7-5(8)	
			90.0'				
91.08							
93.61		31	93.0'	15 20 20 25	Saturated hard bluish gray fine sandy clay w/some silt, trace of coarse sand and fine gravel. (Weathered Rock) 24" RECOVERY	A-7-5(8)	
			95.0'				
96.14							
98.67		32	98.0'	23 44 50	Saturated very dense bluish gray silty fine sand w/ some coarse sand.(Weathered Rock) 16" RECOVERY	A-2-4(0)	
			100.0'				
101.2							
103.73		33	103.0'		End Boring. NR" RECOVERY		
			105.0'				
106.26							
108.79							
111.32							

KEY TO SYMBOLS

Symbol Description

Strata symbols



Silty soils



Well graded gravels and sands



Poorly graded, silty or clayey
sands and gravel



Elastic Silts



Plastic clays



Expansive plastic clays

Misc. Symbols



Water table during
drilling

Notes:

1. Exploratory borings were drilled using a 3 1/4 - inch diameter hollow stem auger.
2. No free water was encountered at the time of drilling or when re-checked the following day, unless recorded on 1st page.
3. Boring locations were taped from existing features and elevations extrapolated from survey unless otherwise reported.
4. These logs are subject to the limitations, conclusions, and recommendations in this report.
5. Results of tests conducted on samples recovered are reported on the logs.
6. All blow counts are uncorrected.

**STATE OF DELAWARE
DEPARTMENT OF TRANSPORTATION
MATERIALS AND RESEARCH**

BORING JS-8

Project Name: James Street Bridge

Location: Newport, DE

State Contract #: T201207101

Federal Contract #:

Station/Offset:

Northing:

Easting:

Boring Surface Elev.:

Reference:

Date Started: 5/21/12

Date Completed: 5/29/12

Wt. of Sample Hammer: 140
Type of: D-Sampler: Split Barrel
S-Sampler:
U-Sampler:
Core Bit:

Lbs.
O.D.
O.D.
O.D.
O.D.

Average Fall: 30
O.D. of Sampler: 2
O.D. of Samp. Tube:
O.D. of Samp. Tube:
O.D. of Rock Core:

IN.
IN.
IN.
IN.
IN.

Hollow Stem Auger Diameter: 3 1/4" **Inches**
Mud Rotary:

From Depth of: 0.0 **To:** 28.0
From Depth of: 28.0 **To:** 98.0

Water Level Readings
Date
5/21/12

Depth to Water (ft)
6.5

Caved Depth (ft)

Boring Contractor: Walton Corporation

Equipment/Rig Type: CME 55 ATV

Driller: Bill Holden and Truver

Logged By: Tom Kane

Depth (ft.)	Water Level	No.	Sample Depth	Blows/6"	Sample Description	AASHTO Class.	Remarks
		1	0.0'	10 10 12 12	Moist medium dense brown silty coarse sandy fine gravel w/some fine sand.	A-2-4(0)	Topsoil 2". Fill
			2.0'		12" RECOVERY		
2.53		2	2.0'	5 4 4 3	Saturated firm black coarse sandy fine gravelly silt w/some fine sand.	A-4(0)	
			4.0'		14" RECOVERY		
		3	4.0'	2 1 1 3	Saturated soft gray silty clay w/some fine gravel, trace of fine to coarse sand.	A-6(9)	
5.06			6.0'		10" RECOVERY		
	▽	4	6.0'	2 2 1 2	Saturated soft gray clay w/some coarse to fine sand and silt, trace of fine gravel.	A-7-6(9)	
7.59			8.0'		14" RECOVERY		
		5	8.0'	5 10 11 12	Saturated medium dense brown fine gravelly coarse sand w/some fine sand and silt.	A-1-b	
			10.0'		14" RECOVERY		
10.12		6	10.0'	7 8 7 10	Saturated stiff brownish red fine to coarse sandy clay w/some silt, trace of fine gravel.	A-6(2)	
			12.0'		18" RECOVERY		
		7	12.0'	5 8 9 9	Saturated medium dense orange silty fine sand w/ some coarse sand.	A-2-4(0)	
12.65			14.0'		15" RECOVERY		

Remarks: 8" casing set @ 18', 4" casing set at 23'.

Reviewed By: Hany Fekry

Soils Supervisor: Aaron Wieczorek

**STATE OF DELAWARE
DEPARTMENT OF TRANSPORTATION
MATERIALS AND RESEARCH**

Project Name: James Street Bridge
State Contract: T201207101

Boring No.: JS-8

Depth (ft.)	Water Level	No.	Sample Depth	Blows/6"	Sample Description	AASHTO Class.	Remarks
15.18		8	14.0'	5 8 8 8	Saturated medium dense orangish brown silty fine to coarse sand w/trace of fine gravel.	A-2-4(0)	
			16.0'		12" RECOVERY		
17.71		9	16.0'	5 7 8 9	Saturated stiff reddish orange clayey fine sandy silt w/trace of coarse sand and fine gravel.	A-4(4)	
			18.0'		12" RECOVERY		
20.24		10	18.0'	3 4 7 8	Saturated stiff red silty fine sandy clay w/trace of coarse sand.	A-6(6)	
			20.0'		20" RECOVERY		
22.77							
25.3		11	23.0'	7 6 10 8	Saturated medium dense brownish orange silty fine to coarse sand w/trace of fine gravel.	A-2-4(0)	
			25.0'		16" RECOVERY		
27.83							
30.36		12	28.0'	3 4 6 6	Saturated firm red silty clay w/some fine sand, trace of coarse sand.	A-6(13)	
			30.0'		24" RECOVERY		
32.89							
35.42		13	33.0'	6 10 12 16	Saturated medium dense orange silty fine to coarse sand w/some fine gravel.	A-2-4(0)	
			35.0'		16" RECOVERY		
37.95							

**STATE OF DELAWARE
DEPARTMENT OF TRANSPORTATION
MATERIALS AND RESEARCH**

Project Name: James Street Bridge
State Contract: T201207101

Boring No.: JS-8

Depth (ft.)	Water Level	No.	Sample Depth	Blows/6"	Sample Description	AASHTO Class.	Remarks																																																																																																												
		14	38.0'	14 15 13 16	Saturated medium dense brown silty fine sand w/ some coarse sand and fine gravel. 18" RECOVERY	A-2-4(0)																																																																																																													
40.48			40.0'							15	43.0'	7 14 14 15	Saturated medium dense gray clayey fine to coarse sand w/some silt and fine gravel. 21" RECOVERY	A-2-4(0)		43.01		45.0'				16	48.0'	10 12 15 17	Saturated very stiff brownish tan fine sandy silt w/ some clay, trace of coarse sand. 22" RECOVERY	A-4(1)		45.54		50.0'				17	53.0'	6 8 19 24	Saturated very stiff brownish gray fine sandy clay w/trace of coarse sand, fine gravel and silt. 22" RECOVERY	A-7-6(9)		48.07		55.0'				18	58.0'	8 10 18 19	Saturated very stiff brown fine sandy clay w/some silt, trace of coarse sand. 24" RECOVERY	A-7-6(9)		50.6		60.0'										53.13																55.66																58.19																60.72			
		15	43.0'	7 14 14 15	Saturated medium dense gray clayey fine to coarse sand w/some silt and fine gravel. 21" RECOVERY	A-2-4(0)																																																																																																													
43.01			45.0'							16	48.0'	10 12 15 17	Saturated very stiff brownish tan fine sandy silt w/ some clay, trace of coarse sand. 22" RECOVERY	A-4(1)		45.54		50.0'				17	53.0'	6 8 19 24	Saturated very stiff brownish gray fine sandy clay w/trace of coarse sand, fine gravel and silt. 22" RECOVERY	A-7-6(9)		48.07		55.0'				18	58.0'	8 10 18 19	Saturated very stiff brown fine sandy clay w/some silt, trace of coarse sand. 24" RECOVERY	A-7-6(9)		50.6		60.0'										53.13																55.66																58.19																60.72															
		16	48.0'	10 12 15 17	Saturated very stiff brownish tan fine sandy silt w/ some clay, trace of coarse sand. 22" RECOVERY	A-4(1)																																																																																																													
45.54			50.0'							17	53.0'	6 8 19 24	Saturated very stiff brownish gray fine sandy clay w/trace of coarse sand, fine gravel and silt. 22" RECOVERY	A-7-6(9)		48.07		55.0'				18	58.0'	8 10 18 19	Saturated very stiff brown fine sandy clay w/some silt, trace of coarse sand. 24" RECOVERY	A-7-6(9)		50.6		60.0'										53.13																55.66																58.19																60.72																											
		17	53.0'	6 8 19 24	Saturated very stiff brownish gray fine sandy clay w/trace of coarse sand, fine gravel and silt. 22" RECOVERY	A-7-6(9)																																																																																																													
48.07			55.0'							18	58.0'	8 10 18 19	Saturated very stiff brown fine sandy clay w/some silt, trace of coarse sand. 24" RECOVERY	A-7-6(9)		50.6		60.0'										53.13																55.66																58.19																60.72																																							
		18	58.0'	8 10 18 19	Saturated very stiff brown fine sandy clay w/some silt, trace of coarse sand. 24" RECOVERY	A-7-6(9)																																																																																																													
50.6			60.0'													53.13																55.66																58.19																60.72																																																			
53.13																																																																																																																			
55.66																																																																																																																			
58.19																																																																																																																			
60.72																																																																																																																			

**STATE OF DELAWARE
DEPARTMENT OF TRANSPORTATION
MATERIALS AND RESEARCH**

Project Name: James Street Bridge
State Contract: T201207101

Boring No.: JS-8

Depth (ft.)	Water Level	No.	Sample Depth	Blows/6"	Sample Description	AASHTO Class.	Remarks
63.25		19	63.0'	12 19 28 27	Saturated hard brownish gray clayey fine sandy silt w/some coarse sand. 24" RECOVERY	A-4(1)	
			65.0'				
65.78							
68.31		20	68.0'	12 18 24 18	Saturated hard grayish green fine sandy clay w/ some silt, trace of coarse sand. 24" RECOVERY	A-6(3)	
			70.0'				
70.84							
73.37		21	73.0'	50	No Sample		
			75.0'		NR" RECOVERY		
75.9							
78.43		22	78.0'	17 36 43 50	Saturated very dense greenish gray silty fine to coarse sand. 20" RECOVERY	A-2-4(0)	
			80.0'				
80.96							
83.49		23	83.0'	23 35 50	Saturated very dense greenish gray silty fine to coarse sand w/trace of fine gravel. 16" RECOVERY	A-2-4(0)	
			85.0'				

**STATE OF DELAWARE
DEPARTMENT OF TRANSPORTATION
MATERIALS AND RESEARCH**

Project Name: James Street Bridge
State Contract: T201207101

Boring No.: JS-8

Depth (ft.)	Water Level	No.	Sample Depth	Blows/6"	Sample Description	AASHTO Class.	Remarks
88.55		24	88.0'	50	No sieve analysis - Indication of saturated dense greenish gray highly weathered rock. 2" RECOVERY		
91.08			90.0'				
93.61		25	93.0'	50	No sieve analysis - Indication of saturated dense greenish gray highly weathered rock. 3" RECOVERY		
96.14			95.0'				
98.67		26	98.0'	25 50	Saturated very dense greenish gray clayey fine to coarse sand w/some silt, trace of fine gravel. 7" RECOVERY	A-2-5(0)	
101.2			100.0'				
103.73		CR-1	101.5'		Schist, gray fine grained, thin bedded, slightly weathered, hard.		RQD - 58
106.26			106.5'		44" RECOVERY		
108.79		CR-2	106.5'		Schist, gray fine grained, thin bedded, slightly weathered, hard.		RQD - 68

**STATE OF DELAWARE
DEPARTMENT OF TRANSPORTATION
MATERIALS AND RESEARCH**

Project Name: James Street Bridge

Boring No.: JS-8

State Contract: T201207101

Depth (ft.)	Water Level	No.	Sample Depth	Blows/6"	Sample Description	AASHTO Class.	Remarks
111.32			111.5'		51" RECOVERY		
					End Boring.		
113.85							
116.38							
118.91							
121.44							
123.97							
126.5							
129.03							
131.56							

KEY TO SYMBOLS

Symbol Description

Strata symbols



Poorly graded, silty or clayey sands and gravel



Silty soils



Plastic clays



Expansive plastic clays



Well graded gravels and sands



Schist

Misc. Symbols



Water table during drilling

Notes:

1. Exploratory borings were drilled using a 3 1/4 - inch diameter hollow stem auger.
2. No free water was encountered at the time of drilling or when re-checked the following day, unless recorded on 1st page.
3. Boring locations were taped from existing features and elevations extrapolated from survey unless otherwise reported.
4. These logs are subject to the limitations, conclusions, and recommendations in this report.
5. Results of tests conducted on samples recovered are reported on the logs.
6. All blow counts are uncorrected.

**STATE OF DELAWARE
DEPARTMENT OF TRANSPORTATION
MATERIALS AND RESEARCH**

BORING JS-9

Project Name: James Street Bridge

Location: Newport, DE

State Contract #: T201207101

Federal Contract #:

Station/Offset:

Northing:

Easting:

Boring Surface Elev.:

Reference:

Date Started: 5/21/12

Date Completed: 5/29/12

Wt. of Sample Hammer: 140
Type of: D-Sampler: Split Barrel
S-Sampler:
U-Sampler:
Core Bit:

Lbs.
O.D.
O.D.
O.D.
O.D.

Average Fall: 30
O.D. of Sampler: 2
O.D. of Samp. Tube:
O.D. of Samp. Tube:
O.D. of Rock Core:

IN.
IN.
IN.
IN.
IN.

Hollow Stem Auger Diameter: 3 1/4" **Inches**
Mud Rotary:

From Depth of: 0.0 **To:** 42.0
From Depth of: 42.0 **To:** 98.0

Water Level Readings

Date
5/21/12

Depth to Water (ft)
6.0

Caved Depth (ft)

Boring Contractor: Walton Corporation

Equipment/Rig Type: CME 55 ATV

Driller: Bill Holden

Logged By: Tom Kane/Chris Costanzi

Depth (ft.)	Water Level	No.	Sample Depth	Blows/6"	Sample Description	AASHTO Class.	Remarks	
	▽	1	0.0'	15 8 8 12	Moist medium dense brown coarse to fine sand and fine gravel w/some silt.	A-1-b	Topsoil 2". Fill	
					10" RECOVERY			
2.53		2	2.0'	3 3 3 2	Wet firm brownish gray silt w/some fine to coarse sand, trace of fine gravel and clay.	A-4(1)	Fill	
					18" RECOVERY			
5.06		3	4.0'	4.0'	6 6 6 5	Wet stiff tan clayey silt w/trace of fine to coarse sand and fine gravel.	A-4(5)	
					13" RECOVERY			
7.59		4	6.0'	6.0'	6 7 11 9	Wet very stiff tan silt w/some fine sand and clay, trace of coarse sand and fine gravel.	A-4(1)	
					18" RECOVERY			
10.12		5	8.0'	8.0'	6 8 12 12	Wet medium dense brown coarse to fine sand w/some fine gravel and silt.	A-1-b	
					14" RECOVERY			
		6	10.0'	10.0'	8 11 9 6	Wet medium dense brown fine gravelly coarse to fine sand w/some silt.	A-1-b	
					14" RECOVERY			
12.65		7	12.0'	12.0'	9 19 20 20	Wet dense brown coarse sandy fine gravel w/some fine sand, trace of silt.	A-1-b	
					16" RECOVERY			

Remarks:

Reviewed By: Hany Fekry

Soils Supervisor: Aaron Wieczorek

**STATE OF DELAWARE
DEPARTMENT OF TRANSPORTATION
MATERIALS AND RESEARCH**

Project Name: James Street Bridge
State Contract: T201207101

Boring No.: JS-9

Depth (ft.)	Water Level	No.	Sample Depth	Blows/6"	Sample Description	AASHTO Class.	Remarks
15.18		8	14.0'	25 29 19 27	Wet dense orange coarse sandy fine gravel w/some fine sand and silt. 10" RECOVERY	A-1-a	
17.71		9	16.0'	25 8 11 10	Wet medium dense orange silty fine sand and fine gravel w/some coarse sand. 12" RECOVERY	A-1-b	
20.24		10	18.0'	12 3 8 9	Wet medium dense orange silty fine sand w/some coarse sand, trace of fine gravel. 10" RECOVERY	A-2-4(0)	
22.77			20.0'				
25.3		11	23.0'	5 5 7 12	Wet stiff brown clayey fine sandy silt w/some coarse sand, trace of fine gravel. 16" RECOVERY	A-4(0)	
27.83			25.0'				
30.36		12	28.0'	10 11 8 10	Wet medium dense brownish orange silty coarse to fine sand w/trace of fine gravel. 21" RECOVERY	A-2-4(0)	
32.89			30.0'				
35.42		13	33.0'	2 6 13 12	Wet very stiff reddish brown fine sandy clay w/ some coarse sand and silt, trace of fine gravel. 16" RECOVERY	A-6(1)	
37.95		14	37.0'	6 16 14 16	Wet medium dense brownish gray clayey fine to coarse sand w/some fine gravel, trace of silt	A-2-6(0)	

**STATE OF DELAWARE
DEPARTMENT OF TRANSPORTATION
MATERIALS AND RESEARCH**

Project Name: James Street Bridge
State Contract: T201207101

Boring No.: JS-9

Depth (ft.)	Water Level	No.	Sample Depth	Blows/6"	Sample Description	AASHTO Class.	Remarks
			39.0'		24" RECOVERY		
40.48							
		15	42.0'	4 7 12 19	Wet medium dense reddish brown silty fine sand w/some fine gravel and clay, trace of coarse sand.	A-2-4(0)	
43.01			44.0'		18" RECOVERY		
45.54							
		16	47.0'	8 11 10 14	Wet medium dense gray silty fine sand w/some coarse sand and fine gravel.	A-2-4(0)	
48.07			49.0'		24" RECOVERY		
50.6							
		17	52.0'	2 3 6 5	Saturated firm grayish brown fine sandy clay w/ some silt, trace of coarse sand and fine gravel.	A-7-5(13)	
53.13			54.0'		24" RECOVERY		
55.66							
		18	57.0'	7 7 9 13	Saturated very stiff grayish brown fine sandy clay w/some silt, trace of coarse sand and fine gravel.	A-7-6(12)	
58.19			59.0'		24" RECOVERY		
60.72							

**STATE OF DELAWARE
DEPARTMENT OF TRANSPORTATION
MATERIALS AND RESEARCH**

Project Name: James Street Bridge
State Contract: T201207101

Boring No.: JS-9

Depth (ft.)	Water Level	No.	Sample Depth	Blows/6"	Sample Description	AASHTO Class.	Remarks
63.25		19	62.0'	9 10 11 23	Saturated very stiff grayish brown clayey fine sandy silt w/trace of coarse sand and fine gravel. 24" RECOVERY	A-4(2)	
			64.0'				
65.78		20	67.0'	10 17 20 22	Saturated hard bluish gray fine sandy clay w/some coarse sand, trace of silt and fine gravel. 24" RECOVERY	A-7-5(6)	
			69.0'				
70.84		21	72.0'	18 16 18 50	Saturated medium dense bluish gray silty fine to coarse sand w/trace of fine gravel. 18" RECOVERY	A-2-4(0)	
			74.0'				
73.37		22	77.0'	50	Saturated very dense bluish gray silty fine sand w/ some coarse sand, trace of fine gravel. 5" RECOVERY	A-2-4(0)	
			79.0'				
75.9		23	82.0'	28 38 44 50	Saturated very dense bluish gray coarse to fine sand and fine gravel w/some silt. 18" RECOVERY	A-1-b	
			84.0'				
78.43							
80.96							
83.49							

**STATE OF DELAWARE
DEPARTMENT OF TRANSPORTATION
MATERIALS AND RESEARCH**

Project Name: James Street Bridge
State Contract: T201207101

Boring No.: JS-9

Depth (ft.)	Water Level	No.	Sample Depth	Blows/6"	Sample Description	AASHTO Class.	Remarks
					4" RECOVERY		
88.55		24	87.0'	50	Saturated dense gray silty fine sand w/some coarse sand, trace of fine gravel. (Weathered Rock)	A-2-4(0)	
			89.0'		4" RECOVERY		
91.08							
		25	92.0'	50	Saturated dense gray silty fine sand w/some coarse sand, trace of fine gravel. (Weathered Rock)	A-2-4(0)	
93.61			94.0'		4" RECOVERY		
96.14							
		26	97.0'	50	Schist, wet, very dense weathered rock.		No Recovery
98.67		CR-1	98.0'		Schist gray fine grained thin bedded, mod-slightly weathered rock.		REC - 81.7%. RQD - 46.3%
			99.0'		NR" RECOVERY		
101.2							
103.73							
			104.8'		67" RECOVERY		
106.26		CR-2	104.9'		Schist gray fine grained thin bedded, slightly weathered rock.		REC - 93.4%. RQD - 84.8%
108.79							
			108.7'		End Boring.		
					43" RECOVERY		

KEY TO SYMBOLS

Symbol Description

Strata symbols



Well graded gravels and sands



Silty soils



Poorly graded, silty or clayey
sands and gravel



Plastic clays



Expansive plastic clays



Schist

Misc. Symbols



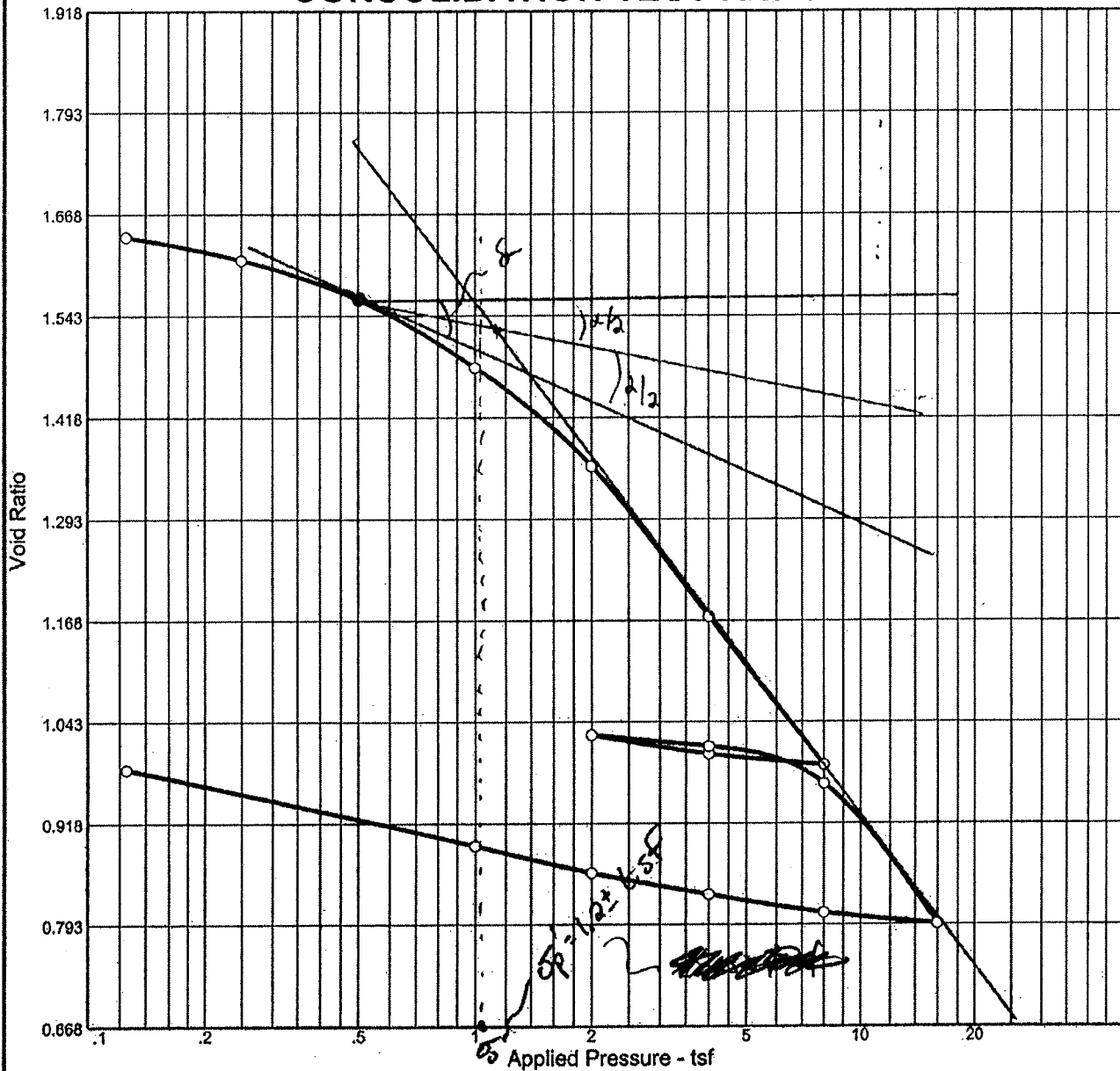
Water table during
drilling

Notes:

1. Exploratory borings were drilled using a 3 1/4 - inch diameter hollow stem auger.
2. No free water was encountered at the time of drilling or when re-checked the following day, unless recorded on 1st page.
3. Boring locations were taped from existing features and elevations extrapolated from survey unless otherwise reported.
4. These logs are subject to the limitations, conclusions, and recommendations in this report.
5. Results of tests conducted on samples recovered are reported on the logs.
6. All blow counts are uncorrected.

Boring/Trench/Test Pit number	SAMP_NUM	Depth (ft. or m.)	Material description	Liquid limit	Plasticity index	Natural moisture %	USCS	AASHTO classification	Percent < than the #10 sieve	Percent < than the #200 sieve	Blow count #1	Blow count #2	Blow count #3	Blow count #4
JS-3														
	1	0	Moist very stiff brown coarse sandy silt w/some fine sand, trace of fine gravel and clay.	19.3	1.5	10.4	SM	A-4(0)	85.9	42.1	4	7	7	23
	2	2	Moist medium dense gray fine gravel w/trace of fine to coarse sand and silt.	NV	NP	3.1	GP-GM	A-1-a	18.1	5.1	20	11	7	9
	3	4	Moist loose brown clayey fine gravel w/some coarse to fine sand and silt.	26	8.1	10.7	SC	A-2-4(0)	53.2	21	3	3	3	4
	4	6	Wet firm grayish brown coarse to fine sandy silt w/some clay, trace of fine gravel.	22.4	3.7	16.1	ML	A-4(0)	98	51.8	3	4	3	3
	5	8	Wet dense gray silty fine gravel w/some coarse to fine sand and clay.	26.3	4.3	24.1	SC-SM	A-2-4(0)	66.4	28.4	3	9	41	3
	6	10	Saturated soft grayish brown fine gravelly clay w/some silt and fine sand, trace of coarse sand.	40.2	11.2	43.1	SM	A-6(3)	66.7	48.1	2	2	2	2
	7	12	Saturated soft gray clay w/some coarse sand and silt, trace of fine sand.	50.4	18.1	68.3	MH	A-7-5(15)	100	77.4	WH	1	1	2
	8	14	No sieve analysis - Indication of saturated hard gray wet very stiff silt.	33.3	9.6	135.9					32	32	12	
	9	16	No sieve analysis - Indication of saturated hard gray organic wet very stiff silt.	37.8	8.5	66.4					8	11	7	5
	10	18	No sieve analysis - Indication of saturated hard gray organic wet very stiff silt.	NV	NP	96.9					5	2	1	1
	11	20	Saturated soft gray organic silty clay w/some fine to coarse sand.	40	11.4	64	ML	A-6(9)	100	75.8	2	2	2	1
	U-1	22												
	13	24	Saturated loose gray coarse to fine sand w/trace of silt and fine gravel.	NV	NP	23.6	SP-SM	A-1-b	91.9	6.6	WR	3	2	8
	14	26	Saturated medium dense gray coarse to fine sand w/trace of fine gravel and silt.	NV	NP	17.5	SW	A-1-b	90.9	4.6	1	5	8	16
	15	28	Saturated dense gray coarse sand w/some fine gravel, trace of fine sand and silt.	NV	NP	15.8	SP	A-1-b	80.6	3.3	23	28	21	25
	16	30	Saturated loose gray coarse to fine sand w/trace of fine gravel and silt.	NV	NP	20.8	SW-SM	A-1-b	92.2	6.5	4	3	5	12
	17	32	Saturated medium dense gray fine gravelly coarse to fine sand w/trace of silt.	NV	NP	15.8	SW-SM	A-1-b	74.9	8.3	10	15	15	17
	18	34	Saturated dense grayish brown coarse sandy fine gravel w/some fine sand, trace of silt.	NV	NP	9.1	SP-SM	A-1-b	51.1	8.3	14	17	16	15
	19	36	Saturated medium dense grayish brown coarse sandy fine gravel w/some fine sand, trace of silt.	NV	NP	10	SP	A-1-a	43.7	3.5	16	22	50	
	20	38	Saturated hard reddish brown clayey fine to coarse sandy silt w/trace of fine gravel.	25.5	9.8	16.5	SC	A-4(1)	98.1	39.4	7	12	20	16
	21	40	Saturated medium dense reddish brown clayey fine sand w/some coarse sand, fine gravel and silt.	22	6.4	13.7	SC-SM	A-2-4(0)	86.1	31.4	9	12	18	22
	22	43	Saturated medium dense brown clayey fine to coarse sand w/some silt, trace of fine gravel.	20.9	6.8	14.2	SC-SM	A-2-4(0)	96.6	30.4	5	6	8	10
	23	48	Saturated medium dense brown silty fine to coarse sand.	19.7	NP	16.9	SM	A-2-4(0)	99.6	26	6	7	4	6
	24	53	Saturated medium dense brown silty fine sand w/some coarse sand, trace of fine gravel.	NV	NP	15	SM	A-2-4(0)	98.6	26.4	19	14	11	17
	25	58	Saturated medium dense brown clayey fine to coarse sand and fine gravel w/some silt.	34.3	17.9	13.9	SC	A-2-6(0)	76.5	19.7	11	12	17	9
	26	63	Saturated medium dense brown silty fine to coarse sand w/trace of fine gravel.	NV	NP	21.1	SM	A-2-4(0)	91.9	21.6	10	10	13	11
	27	68	Saturated stiff grayish brown clayey fine sandy silt w/some coarse sand, trace of fine gravel.	28.3	9.5	23.5	SC	A-4(1)	94.4	41	4	5	5	5
	28	73	Saturated very stiff grayish brown fine to coarse sandy clay w/some silt.	37.4	13.9	17.9	SC	A-6(4)	99.9	49.6	5	6	10	9
	29	78	Saturated very stiff gray clayey fine to coarse sandy silt.	34.8	8.8	28.4	SM	A-4(1)	100	43.6	11	7	11	20
	30	83	Saturated hard gray fine sandy silt w/some coarse sand, trace of fine gravel.	15.1	NP	25.9	SM	A-4(0)	99.4	47.2	15	20	17	27
	31	88	Saturated hard gray clayey coarse to fine sandy silt w/trace of fine gravel. (Weathered Rock)	39.4	8.1	19.1	SM	A-4(1)	98.7	42.1	13	23	38	50
	32	93	Saturated hard gray clayey fine sandy silt w/some coarse sand. (Weathered Rock)	33.3	9.6	34.3	CL	A-4(2)	100	50.2	15	23	34	50
	33	98	Saturated hard grayish brown fine sandy clay w/some coarse sand and silt, trace of fine gravel. (Weathered Rock)	52.4	30.7	17	CH	A-7-6(11)	96.8	50.6	14	22	23	34
	34	103	Saturated very dense bluish gray clayey fine to coarse sand w/some silt, trace of fine gravel. (Weathered Rock)	53.3	17	19.6	SM	A-2-7(1)	95.1	28.5	23	24	40	50
	35	108	Saturated very dense bluish gray clayey fine sand w/some coarse sand and silt, trace of fine gravel.	40.3	6	26.5	SM	A-2-4(0)	96.1	27.3	33	50		
	36	113	No sieve analysis - Indication of blue grey weathered rock.	34.8	NP	31.7					50			
	37	118	End Boring.								50			

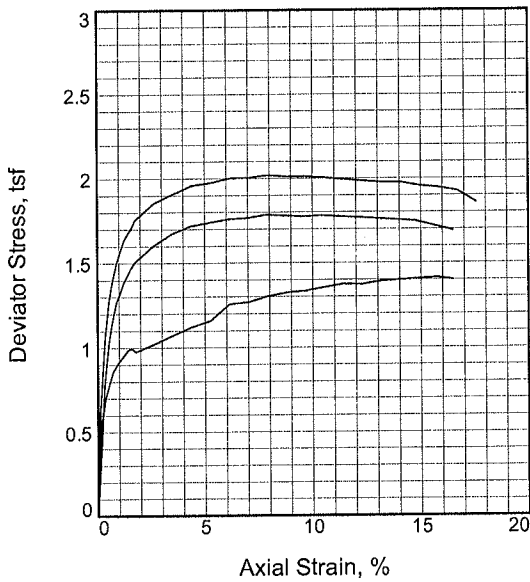
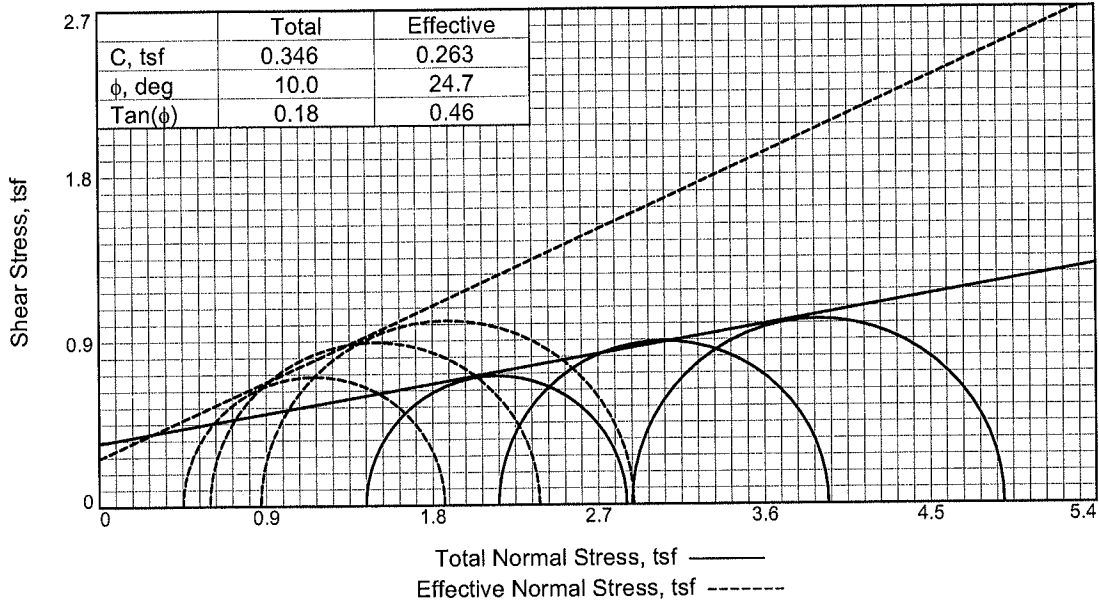
CONSOLIDATION TEST REPORT



Natural		Dry Dens. (pcf)	LL	PI	Sp. Gr.	Overburden (tsf)	P _c (tsf)	C _c	C _r	Swell Press. (tsf)	Swell %	e ₀
Sat.	Moist.											
102.8 %	70.5 %	56.8	48.1	13.1	2.420	1.02	1.15	0.65	0.08			1.659

MATERIAL DESCRIPTION	USCS	AASHTO
Saturated dark gray organic clay w/some fine gravel, trace of fine to coarse sand and silt.	ML	A-7-5(12)

Project No. T201207101	Client:	Remarks:
Project: James Street Bridge		
Source: JS-2	Sample No.: U-1 Elev./Depth: 16.0	
CONSOLIDATION TEST REPORT Delaware Department of Transportation Materials and Research Laboratory		Figure



Sample No.	1	2	3	
Initial	Water Content, %	80.1	71.0	73.1
	Dry Density, pcf	54.4	57.7	56.7
	Saturation, %	103.9	100.6	100.9
	Void Ratio	2.0433	1.8692	1.9184
	Diameter, in.	2.85	2.85	2.85
	Height, in.	6.09	5.98	6.07
At Test	Water Content, %	59.8	55.0	60.1
	Dry Density, pcf	64.0	67.3	63.8
	Saturation, %	100.0	100.0	100.0
	Void Ratio	1.5848	1.4568	1.5930
	Diameter, in.	2.71	2.69	2.77
	Height, in.	5.71	5.76	5.69
Strain rate, in./min.	0.00	0.00	0.00	
Back Pressure, psi	90.00	90.00	90.00	
Cell Pressure, psi	110.00	120.00	130.00	
Fail. Stress, tsf	1.41	1.78	2.02	
Total Pore Pr., tsf	7.47	8.04	8.49	
Ult. Stress, tsf				
Total Pore Pr., tsf				
$\bar{\sigma}_1$ Failure, tsf	1.86	2.38	2.89	
$\bar{\sigma}_3$ Failure, tsf	0.45	0.60	0.87	

Type of Test:
CU with Pore Pressures

Sample Type: Undisturbed

Description: Elastic SILT

LL= 66 PL= 36 PI= 30

Assumed Specific Gravity= 2.65

Remarks:

Client: Delaware Department of Transportation

Project: Replacement of BR1-159 James Street Bridge

Source of Sample: JS-2 **Depth:** 26.0

Sample Number: U-2

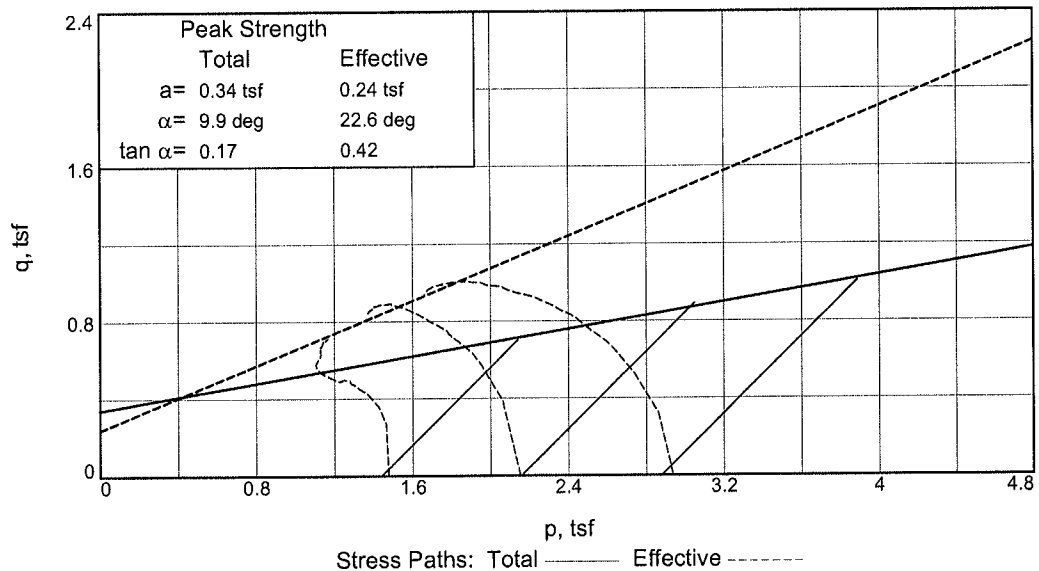
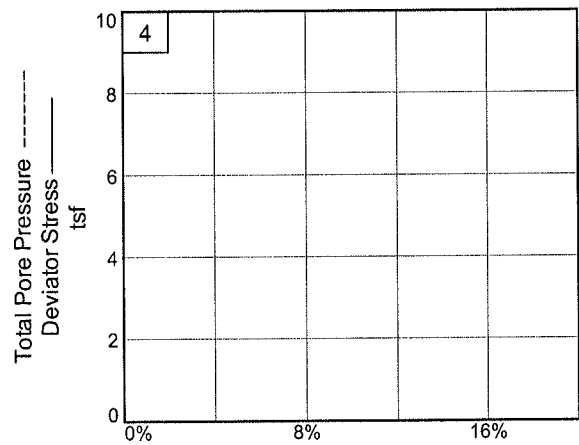
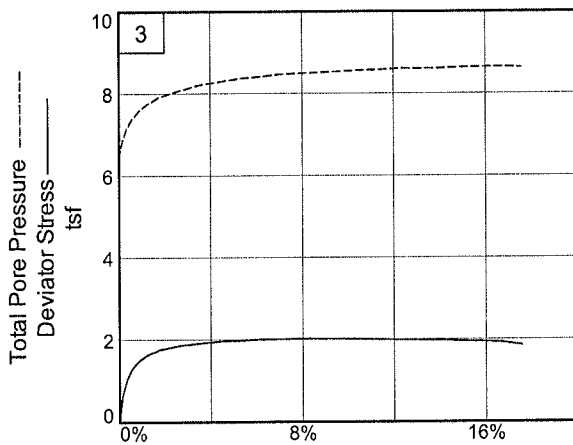
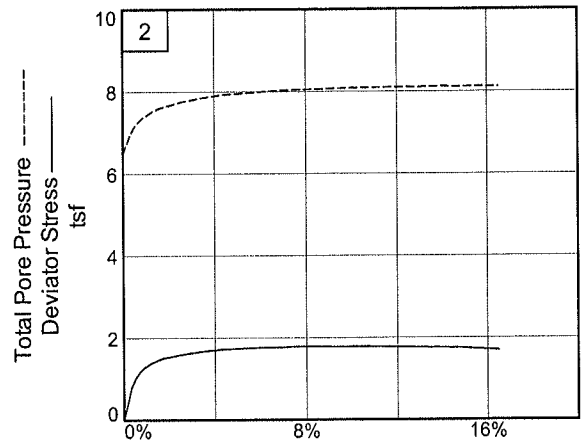
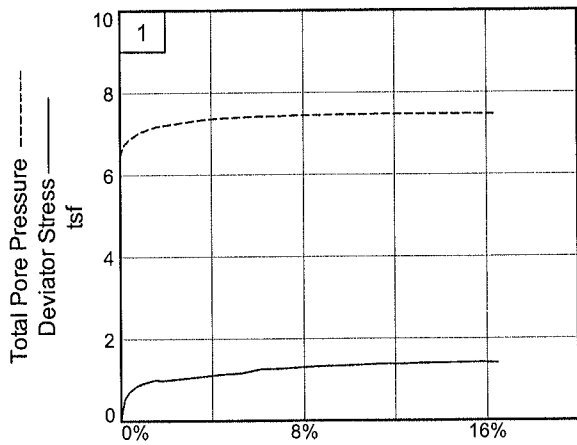
Proj. No.: AGR 1550, Task 15 **Date Sampled:**



GEO-TECHNOLOGY
ASSOCIATES, INC.
18 Boulden Circle, Suite 36
New Castle, DE 19720

Figure 1

Tested By: K. Kershaw Checked By: M. Lester



Client: Delaware Department of Transportation

Project: Replacement of BR1-159 James Street Bridge

Source of Sample: JS-2

Depth: 26.0

Sample Number: U-2

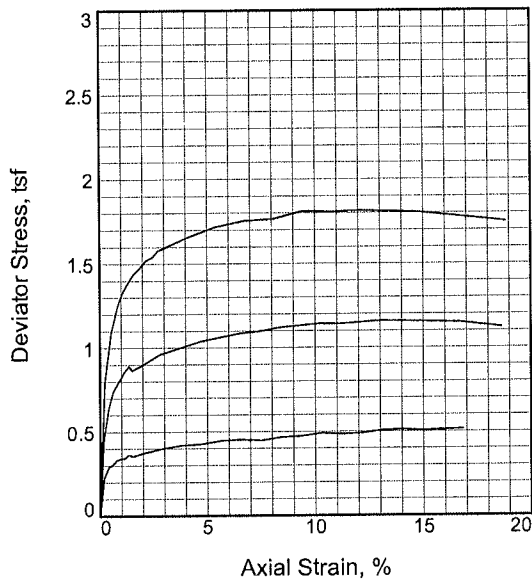
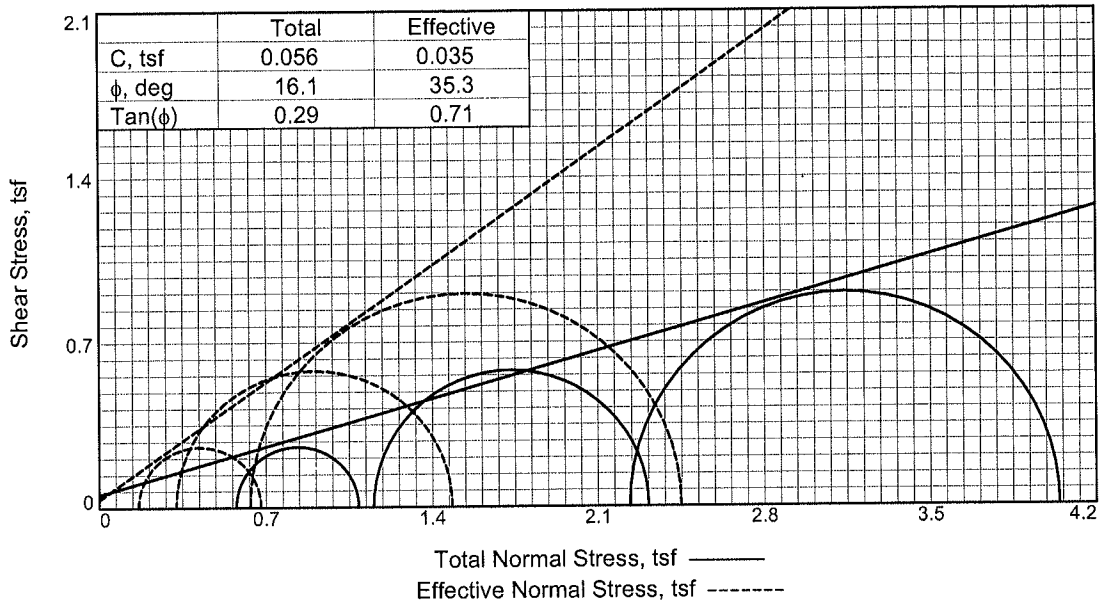
Project No.: AGR 1550, Task 15

Figure _____

Geo-Technology Associates, Inc.

Tested By: K. Kershaw

Checked By: M. Lester



Sample No.	1	2	3	
Initial	Water Content, %	74.4	74.4	74.4
	Dry Density, pcf	49.3	55.5	53.4
	Saturation, %	83.7	99.6	94.0
	Void Ratio	2.3570	1.9808	2.0984
	Diameter, in.	2.88	2.88	2.88
	Height, in.	5.63	5.63	4.05
At Test	Water Content, %	66.1	57.2	53.4
	Dry Density, pcf	60.1	65.7	68.5
	Saturation, %	100.0	100.0	100.0
	Void Ratio	1.7523	1.5162	1.4139
	Diameter, in.	2.67	2.70	2.65
	Height, in.	5.34	5.37	3.71
Strain rate, in./min.	0.00	0.00	0.00	
Back Pressure, psi	90.00	90.00	91.00	
Cell Pressure, psi	98.00	106.00	122.00	
Fail. Stress, tsf	0.51	1.16	1.81	
	Total Pore Pr., tsf	6.89	7.31	8.15
Ult. Stress, tsf				
	Total Pore Pr., tsf			
$\bar{\sigma}_1$ Failure, tsf	0.68	1.48	2.45	
$\bar{\sigma}_3$ Failure, tsf	0.17	0.32	0.63	

Type of Test:
 CU with Pore Pressures
Sample Type: Undisturbed
Description: Elastic SILT

 LL= 55 PL= 35 PI= 20
 Assumed Specific Gravity= 2.65
Remarks:

Client: Delaware Department of Transportation
Project: Replacement of BR1-159 James Street Bridge
Source of Sample: JS-3 **Depth:** 22.0
Sample Number: U-1
 Proj. No.: AGR 1550, Task 15 **Date Sampled:**

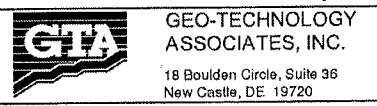
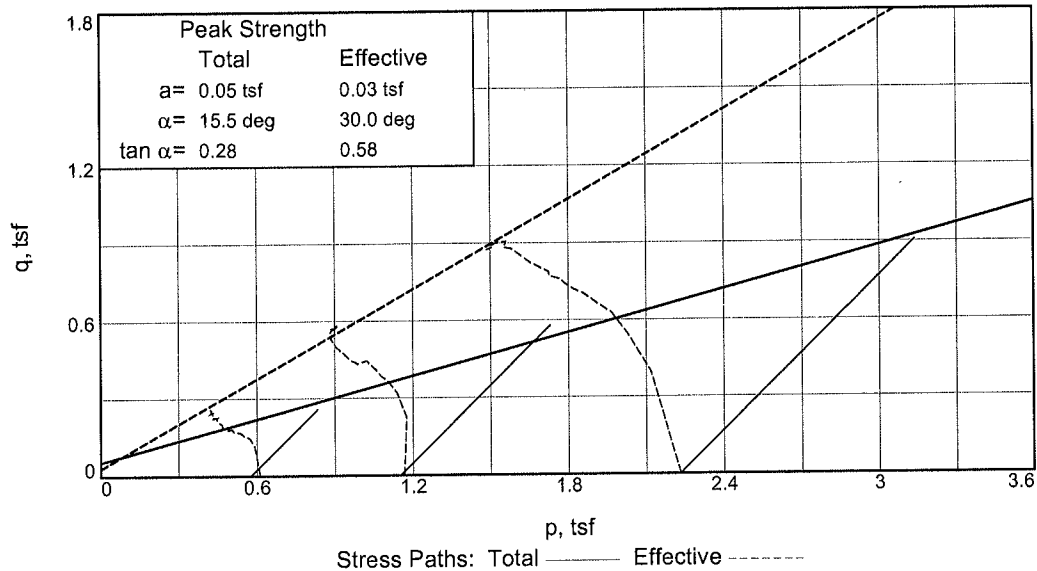
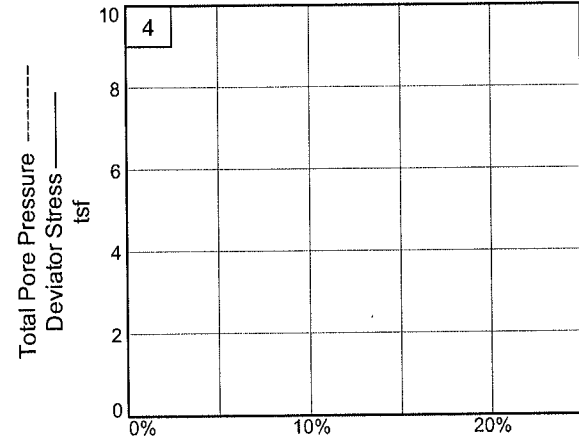
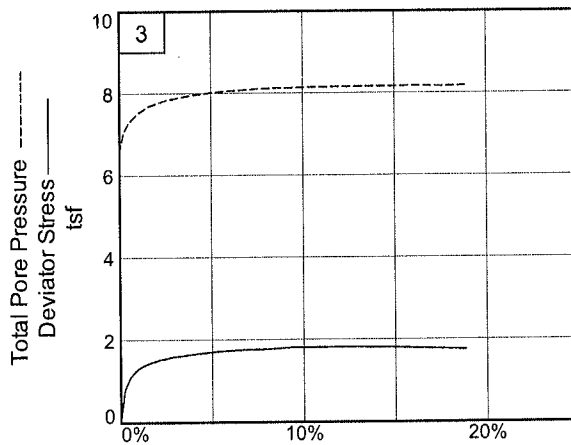
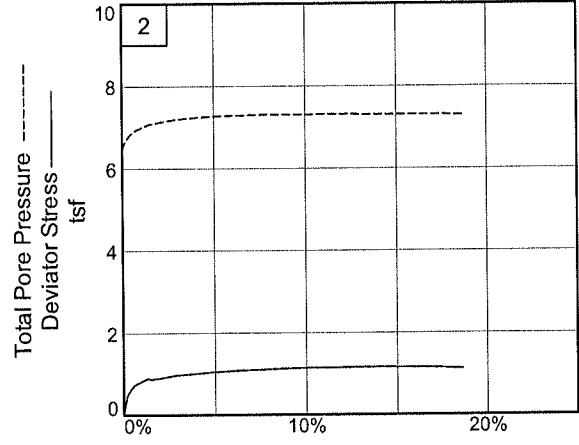
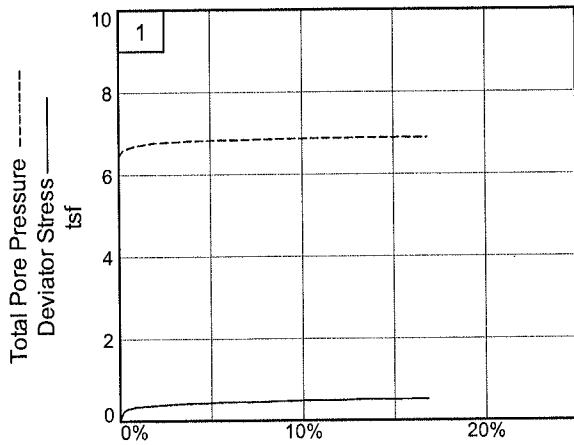


Figure 2



Client: Delaware Department of Transportation

Project: Replacement of BR1-159 James Street Bridge

Source of Sample: JS-3

Depth: 22.0

Sample Number: U-1

Project No.: AGR 1550, Task 15

Figure _____

Geo-Technology Associates, Inc.

Tested By: C. Reith

Checked By: M. Lester

Preliminary Subsurface Exploration
 AGR 1550, Task 15, Replacement of BR1-159 James Street Bridge

TABLE
 SUMMARY OF CORROSION POTENTIAL TESTING

Corrosion Potential Test	Sample ID		
	JS-7 38-42 feet	JS-3 32-38 feet	JS-3 38-55 feet
Resistivity -ohm-cm (ASTM G-57)			
< 1,500			
≥ 1,500-1,800			
> 1,800-2,100			
> 2,100-2,500			
> 2,500-3,000			
> 3,000	18,000	21,000	27,000
pH (ASTM G-51)			
0-2			
2-4			
4-6.5	6.00		6.46
6.5-7.5		6.89	
7.5-8.5			
> 8.5			
pH (Retested six weeks from original test date)	---	---	---
Redox potential (ASTM D1498)			
> 100 mV	380.8	396.1	400.0
50 to 100 mV			
0 to 50 mV			
Negative			
Sulfides			
Positive			
Trace			
Negative	Negative	Negative	Negative
Moisture (ASTM D-2216)			
Poor drainage, continuously wet	Wet	Wet	Wet
Fair Drainage, generally moist			
Good drainage, generally dry			

FINAL FOUNDATION REPORT (REV. November 2014)

**BR 1-159 - Newport Bridge
James Street Over Christina River
New Castle County, Delaware**

APPENDIX C

Design Calculations

- C-1 – Abutment Design Calculations**
- C-2 – Piers Design Calculations**
- C-3 – Scour Analysis Summary**

FINAL FOUNDATION REPORT (REV. November 2014)
BR 1-159 - Newport Bridge
James Street Over Christina River
New Castle County, Delaware

APPENDIX C-1

Abutment Design Calculations

ABUTMENT A

Layer

Boring No. JS-2

By: SJM

Chk: AT
OG Elev. =

~~5.06~~ 8.5

Sample No.	Depth of SS run (ft)	N-Values Field	q' (ksf)	C _N	N _{CORR}
1	2	20	0.095	2.020	40
2	4	50	0.190	1.788	89
3	6	12	0.286	1.653	20
4	8	20	0.381	1.556	31
5	10	8	0.476	1.482	12
6	12	4	0.571	1.421	6
7	14	4	0.666	1.369	5
9	18	5	0.857	1.285	6
10	20	7	0.952	1.250	9
11	22	2	1.047	1.218	2
12	26	2	1.238	1.162	2
13	28	5	1.333	1.138	6
14	30	15	1.428	1.114	17
15	32	20	1.523	1.093	22
16	34	45	1.618	1.073	48
17	36	18	1.714	1.053	19
18	38	29	1.809	1.035	30
19	40	12	1.904	1.018	12
20	42	28	1.999	1.002	28
21	48	46	2.285	0.957	44
22	53	12	2.523	0.924	11
23	58	14	2.761	0.894	13
24	63	17	2.999	0.866	15
25	68	13	3.237	0.841	11
26	73	18	3.475	0.817	15
27	78	31	3.713	0.795	25
28	83	38	3.951	0.774	29
29	88	61	4.189	0.755	46
30	93	44	4.427	0.736	32
31	98	44	4.665	0.719	32
32	103	83	4.903	0.702	58
33	108	50	5.141	0.686	34
34	113	79	5.379	0.671	53
35	118	50	5.617	0.656	33

GWT = -23.0
γ = 110 lb/ft³
γ' = 47.6 lb/ft³

1
2
3
4
5
6
7

N_{avg} (Below BPCE) = 25
(Ref. AASHTO Eqn 10.4.6.2.4-1)

C_N = 0.77 × log (40/q')

N_{CORR} = N_{Field} × C_N

PROJECT BR 1-159 JOB NO. _____ SHEET NO. 1 OF 1
 LOCATION ABUTMENT A
 SUBJECT SOIL PROFILE (JS-2)
 DESIGNED BY SJM DATE 7/24/14 CHECKED BY AT DATE 8/14
 REVISED BY _____ DATE _____ BACK CHECKED BY _____ DATE _____

BORING JS-2

REF./REM.

DEPTH BELOW OG X=0	LAYER THICKNESS (ft)	ELEVATION	SOIL TYPE	SCOUR: NONE
X=0		8.5		
	X_1 DEPTH BELOW BDS E			
LAYER ① X=10	(10)	$X_1=0$ $X_2=3.0 - 1.5$	$N_{CORR} = 20-89$ MED SAND WITH SILT + GRAVEL (FIN) DENSE $\gamma_s = 135$ pcf $\phi = 34^\circ$ MHW E 4.64	TOP OF DS + 2.5 BDS CE + 1.5
	② (16)	$X_1=19 - 17.5$	$N_{CORR} 2-12$ SOFT CLAY WITH SAND $\gamma_s = 100$ pcf $C = 400$ psf $\phi = 0^\circ$	
X=26	③ (12)	$X_1=31 - 29.5$	$N_{CORR} 6-48$ MED SAND WITH SOME GRAVEL $\gamma_s = 130$ pcf $\phi = 32^\circ$ $C = 0$ psf	
X=38	④ (20)	$X_1=51 - 49.5$	$N_{CORR} 11-44$ CLAY + F SAND $\phi = 0^\circ$ $\gamma_s = 125$ pcf $C = 1000$ psf	
X=58	⑤ (10)	$X_1=61 - 59.5$	$N_{CORR} 13-15$ MED SAND WITH GRAVEL $\gamma_s = 130$ pcf $\phi = 32^\circ$ $C = 0$ psf	
X=68	⑥ (25)	$X_1=86 - 84.5$	$N_{CORR} = 15-46$ SILT/CLAY + F SAND $\gamma_s = 125$ pcf $C = 1000$ psf $\phi = 0^\circ$	
X=93	⑦ (25)	$X_1=111 - 109.5$	$N_{CORR} = 32-58$ VERY DENSE SAND + GRAVEL $\gamma_s = 135$ pcf $\phi = 34^\circ$	TIP @ $X_1 = 95'$ EL. - 93.5 SAY - 94.0
X=118				

Ref: FHWA HI-88-009, July 1993

a. Granular Soil (Sand)

Description	Very Loose	Loose	Medium	Dense	Very Dense
Standard Penetration no. N' *	0	4	10	30	50
Approx. angle of internal friction, (ϕ) degrees**	25-30	27-32	30-35	35-40	38-43
Approx. range of moist unit weight, (γ) pcf**	70-100	90-115	110-130	120-140	130-150

* N' is SPT value corrected for overburden pressure.

** Use larger values for granular material with 5% or less fine sand and silt.

b. Cohesive soils (Clay) - (Rather unreliable, use only for preliminary estimate purposes).

Consistency	Very Soft	Soft	Medium	Stiff	Very Stiff	Hard
q_u , ksf	0	0.5	1.0	2.0	4.0	8.0
N , standard penetration resistance	0	2	4	8	16	32
γ (moist) pcf	100-120		110-130		120-140	

4. Use the appropriate equation on figures 14 thru 17 to compute the ultimate bearing capacity. The continuous footing general case may be used when the footing length is 9 or more times the footing width. Also the bearing capacity factor N_q will usually be determined for a rough base condition since most footings are poured concrete. If soil test data was used, apply a minimum safety factor of 2.5 to find the allowable bearing capacity. A safety factor of 3 should be used for bearing capacity computed using standard penetration values.

File Analysis Mult Option

Help Topics

Mult MENU		
Mult - Shape and Axial Loads		Edit - Computation Control
Mult - Rebar & Concrete Strength		Edit - Output Tables
Mult - Section Dimension		FILE MENU
Mult - Rebar Arrangement		File - Read
EDIT MENU		File - New
Edit - Title		File - Save
Edit - Pile Properties		File - Write
Edit - Soil Properties		File - Directory
Edit - Soil - p-y Criteria		File - Change Directory
Edit - Soil - k for Clays		File - Exit to DOS
Edit - Soil - k for Sands		MAIN MENU
Edit - Soil - E50 ←		Main - Pull-down Menus
Edit - Soil - p-y Multipliers		Main - Hot Keys
Edit - Soil - Unit Weights		OPTIONS MENU
Edit - Lat. Load Trans.		Options - Units
Edit - Data for Loading		Options - File Property Library
		Options - Save Config. File
		Options - Auto-backup

F1-Help Alt-X-Exit

Move the cursor to the "E50", then press <Enter>.

File Analysis Mult Option

EXAMPLE.ING

Soil Strain Parameter E50

Soft Clay,	c = 1.74 to 3.47 psi 250 to 500 psf 12 to 24 KPa	E50 = 0.02	
Medium Clay,	c = 3.47 to 6.94 psi 500 to 1000 psf 24 to 48 KPa	E50 = 0.01	←
Stiff Clay,	c = 6.94 to 13.9 psi 1000 to 2000 psf 48 to 96 KPa	E50 = 0.007	←
Very Stiff Clay,	c = 13.9 to 27.8 psi 2000 to 4000 psf 96 to 192 KPa	E50 = 0.005	

F1 : Help Index PageUp PageDown F8 : Return

F1-Help Alt-X-Exit

Press Command Key [F8] to return.

Recommended k	Relative Density		
	Loose	Medium	Dense
MN/m ³ (lb/in. ³)	5.4 (20.0)	16.3 (60.0)	34 (125.0)

Table 3.6 Representative Values of k for Submerged Sand

Recommended k	Relative Density		
	Loose	Medium	Dense
MN/m ³ (lb/in. ³)	6.8 (25.0)	24.4 (90.0)	61.0 (225.0)

Table 3.7 Representative Values of k for Sand Above the Water Table (Static and Cyclic Loading)

9. Establish the parabolic section of the p - y curve,

$$p = \bar{C}y^{1/n} \dots\dots\dots (3.53)$$

- Fit the parabola between points k and m as follows:

- a. Get the slope of the line between points m and u by,

$$m = \frac{P_u - P_m}{y_u - y_m} \dots\dots\dots (3.54)$$

- b. Obtain the power of the parabolic section by,

$$n = \frac{P_m}{m y_m} \dots\dots\dots (3.55)$$

- c. Obtain the coefficient \bar{C} as follows:

$$\bar{C} = \frac{P_m}{y_m^{1/n}} \dots\dots\dots (3.56)$$

Table 10.5.5.2.4-1—Resistance Factors for Geotechnical Resistance of Drilled Shafts

	Method/Soil/Condition		Resistance Factor
Nominal Axial Compressive Resistance of Single-Drilled Shafts, ϕ_{stat}	Side resistance in clay	α -method (O'Neill and Reese, 1999)	0.45
	Tip resistance in clay	Total Stress (O'Neill and Reese, 1999)	0.40
	Side resistance in sand	β -method (O'Neill and Reese, 1999)	0.55
	Tip resistance in sand	O'Neill and Reese (1999)	0.50
	Side resistance in IGMs	O'Neill and Reese (1999)	0.60
	Tip resistance in IGMs	O'Neill and Reese (1999)	0.55
	Side resistance in rock	Horvath and Kenney (1979) O'Neill and Reese (1999)	0.55
	Side resistance in rock	Carter and Kulhawy (1988)	0.50
	Tip resistance in rock	Canadian Geotechnical Society (1985) Pressuremeter Method (Canadian Geotechnical Society, 1985) O'Neill and Reese (1999)	0.50
Block Failure, ϕ_{bl}	Clay		0.55
Uplift Resistance of Single-Drilled Shafts, ϕ_{up}	Clay	α -method (O'Neill and Reese, 1999)	0.35
	Sand	β -method (O'Neill and Reese, 1999)	0.45
	Rock	Horvath and Kenney (1979) Carter and Kulhawy (1988)	0.40
Group Uplift Resistance, ϕ_{ug}	Sand and clay		0.45
Horizontal Geotechnical Resistance of Single Shaft or Shaft Group	All materials		1.0
Static Load Test (compression), ϕ_{load}	All Materials		Values in Table 10.5.5.2.3-2, but no greater than 0.70
Static Load Test (uplift), ϕ_{upload}	All Materials		0.60

10.5.5.2.5—Micropiles

C10.5.5.2.5

Resistance factors shall be selected from Table 10.5.5.2.5-1 based on the method used for determining the nominal axial pile resistance. If the resistance factors provided in Table 10.5.5.2.5-1 are to be applied to piles in potentially creeping soils, highly plastic soils, weak rock, or other marginal ground type, the resistance factor values in the Table should be reduced by 20 percent to reflect greater design uncertainty.

The resistance factors in Table 10.5.5.2.5-1 were calibrated by fitting to ASD procedures tempered with engineering judgment. The resistance factors in Table 10.5.5.2.5-2 for structural resistance were calibrated by fitting to ASD procedures and are equal to or slightly more conservative than corresponding resistance factors from Section 5 of the AASHTO LRFD Specifications for reinforced concrete column design.

where:

E_m = Elastic modulus of the rock mass (ksi)

E_m/E_i = Reduction factor determined from Table 10.4.6.5-1 (dim)

E_i = Elastic modulus of intact rock from tests (ksi)

For critical or large structures, determination of rock mass modulus (E_m) using in-situ tests may be warranted. Refer to Sabatini et al. (2002) for descriptions of suitable in-situ tests.

Table 10.4.6.5-1—Estimation of E_m Based on RQD (after O'Neill and Reese, 1999)

RQD (percent)	E_m/E_i	
	Closed Joints	Open Joints
100	1.00	0.60
70	0.70	0.10
50	0.15	0.10
20	0.05	0.05

Table C10.4.6.5-1—Summary of Elastic Moduli for Intact Rock (modified after Kulhawy, 1978)

Rock Type	No. of Values	No. of Rock Types	Elastic Modulus, E_i (ksi $\times 10^3$)			Standard Deviation (ksi $\times 10^3$)
			Maximum	Minimum	Mean	
Granite	26	26	14.5	0.93	7.64	3.55
Diorite	3	3	16.2	2.48	7.45	6.19
Gabbro	3	3	12.2	9.8	11.0	0.97
Diabase	7	7	15.1	10.0	12.8	1.78
Basalt	12	12	12.2	4.20	8.14	2.60
Quartzite	7	7	12.8	5.29	9.59	2.32
Marble	14	13	10.7	0.58	6.18	2.49
Gneiss	13	13	11.9	4.13	8.86	2.31
Slate	11	2	3.79	0.35	1.39	0.96
Schist	13	12	10.0	0.86	4.97	3.18
Phyllite	3	3	2.51	1.25	1.71	0.57
Sandstone	27	19	5.68	0.09	2.13	1.19
Siltstone	5	5	4.76	0.38	2.39	1.65
Shale	30	14	5.60	0.001	1.42	1.45
Limestone	30	30	13.0	0.65	5.7	3.73
Dolostone	17	16	11.4	0.83	4.22	3.44

Poisson's ratio for rock should be determined from tests on intact rock core.

Where tests on rock core are not practical, Poisson's ratio may be estimated from Table C10.4.6.5-2.

SPECIFICATIONS

COMMENTARY

Table 10.6.3.2.2-2 - Typical Range of Uniaxial Compressive Strength (Co) as a Function of Rock Category and Rock Type

ROCK CATEGORY	GENERAL DESCRIPTION	ROCK TYPE	Co ⁽¹⁾	
			MPa	ksf
A	Carbonate rocks with well-developed crystal cleavage	Dolostone	30-310	600-6,400
		Limestone	20-290	600-6,000
		Carbonatite	40-70	800-1,400
		Marble	40-240	800-5,000
		Tactite-Skarn	130-330	2,800-6,800
B	Lithified argillaceous rock	Argillite	30-150	600-3,000
		Claystone	1-8	30-170
		Marlstone	50-190	1,000-4,000
		Phyllite	20-240	600-5,000
		Siltstone	10-120	200-2,400
		Shale ⁽²⁾	10-35	150-740
		Slate	140-210	3,000-4,400
C	Arenaceous rocks with strong crystals and poor cleavage	Conglomerate	30-220	600-4,600
		Sandstone	70-170	1,400-3,600
		Quartzite	60-380	1,200-8,000
D	Fine-grained igneous crystalline rock	Andesite	100-180	2,000-3,800
		Diabase	20-575	450-12,000
E	Coarse-grained igneous and metamorphic crystalline rock	Amphibolite	120-280	2,400-5,800
		Gabbro	125-310	2,600-6,400
		Gneiss	20-310	500-6,400
		Granite	10-330	300-6,800
		Quartzdiorite	10-100	200-2,000
		Quartzmonzonite	130-160	2,800-3,400
		Schist	10-140	200-3,000
Syenite	180-430	3,800-9,000		

⁽¹⁾Range of Uniaxial Compressive Strength values reported by various investigations

⁽²⁾Not including oil shale

10.6.3.2.3 Analytic Method

The nominal bearing resistance of foundations on rock shall be determined using established rock mechanics principles based on the rock mass strength parameters determined in accordance with D10.4.6.4. The influence of discontinuities on the failure mode shall also be considered.

C10.6.3.2.3

Depending upon the relative spacing of joints and rock layering, bearing capacity failures for foundations on rock may take several forms. Except for the case of a rock mass with closed joints, the failure modes are different from those in soil. Procedures for estimating bearing resistance for each of the failure modes can be found in Kulhawy and Goodman (1980), Kulhawy and Goodman (1987), Goodman (1989),

AXIAL CAPACITY

Abut A.sfo
 UNDRAINED SHEAR STRENGTH, LB/SQ FT = 0.000E+00
 INTERNAL FRICTION ANGLE, DEG. = 0.340E+02
 BLOWS PER FOOT FROM STANDARD PENETRATION TEST = 0.000E+00
 SOIL UNIT WEIGHT, LB/CU FT = 0.135E+03
 MAXIMUM LOAD TRANSFER FOR SOIL, LB/SQ FT = 0.100E+11
 DEPTH, FT = 0.300E+01

LRFD RESISTANCE FACTOR (SIDE FRICTION) = 0.550E+00
 LRFD RESISTANCE FACTOR (TIP RESISTANCE) = 0.500E+00

LAYER NO 2-----CLAY
 AT THE TOP
 STRENGTH REDUCTION FACTOR-ALPHA = 0.550E+00
 END BEARING COEFFICIENT-NC = 0.800E+01
 UNDRAINED SHEAR STRENGTH, LB/SQ FT = 0.400E+03
 INTERNAL FRICTION ANGLE, DEG. = 0.000E+00
 BLOWS PER FOOT FROM STANDARD PENETRATION TEST = 0.000E+00
 SOIL UNIT WEIGHT, LB/CU FT = 0.100E+03
 MAXIMUM LOAD TRANSFER FOR SOIL, LB/SQ FT = 0.100E+11
 DEPTH, FT = 0.300E+01

AT THE BOTTOM
 STRENGTH REDUCTION FACTOR-ALPHA = 0.550E+00
 END BEARING COEFFICIENT-NC = 0.800E+01
 UNDRAINED SHEAR STRENGTH, LB/SQ FT = 0.400E+03
 INTERNAL FRICTION ANGLE, DEG. = 0.000E+00
 BLOWS PER FOOT FROM STANDARD PENETRATION TEST = 0.000E+00
 SOIL UNIT WEIGHT, LB/CU FT = 0.100E+03
 MAXIMUM LOAD TRANSFER FOR SOIL, LB/SQ FT = 0.190E+02

LRFD RESISTANCE FACTOR (SIDE FRICTION) = 0.450E+00
 LRFD RESISTANCE FACTOR (TIP RESISTANCE) = 0.400E+00

LAYER NO 3-----SAND
 AT THE TOP
 SKIN FRICTION COEFFICIENT- BETA = 0.912E+00
 UNDRAINED SHEAR STRENGTH, LB/SQ FT = 0.000E+00
 INTERNAL FRICTION ANGLE, DEG. = 0.370E+02
 BLOWS PER FOOT FROM STANDARD PENETRATION TEST = 0.000E+00
 SOIL UNIT WEIGHT, LB/CU FT = 0.130E+03
 MAXIMUM LOAD TRANSFER FOR SOIL, LB/SQ FT = 0.100E+11
 DEPTH, FT = 0.190E+02

AT THE BOTTOM
 SKIN FRICTION COEFFICIENT- BETA = 0.748E+00
 UNDRAINED SHEAR STRENGTH, LB/SQ FT = 0.000E+00
 INTERNAL FRICTION ANGLE, DEG. = 0.370E+02
 BLOWS PER FOOT FROM STANDARD PENETRATION TEST = 0.000E+00
 SOIL UNIT WEIGHT, LB/CU FT = 0.130E+03
 MAXIMUM LOAD TRANSFER FOR SOIL, LB/SQ FT = 0.100E+11

Abut A.sfo
 SHAFT for Windows, Version 2012.7.11
 Serial Number : 228741384
 VERTICALLY LOADED DRILLED SHAFT ANALYSIS
 (C) Copyright ENSOFT, Inc., 1987-2012
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Path to file locations : Y:\Bridges\DELDOT\BRI-159_JAMES ST
 BRIDGE\FOUNDATION REPORT\SHAFT Output\
 Name of input data file : Abut A.sfd
 Name of output file : Abut A.sfo
 Name of plot output file : Abut A.sfp
 Name of runtime file : Abut A.sfr

Time and Date of Analysis

Date: July 30, 2014 Time: 11:42:25

BRI-159 Amutment A

PROPOSED DEPTH = 103.0 FT

NUMBER OF LAYERS = 7

WATER TABLE DEPTH = 0.0 FT.

SOIL INFORMATION

LAYER NO 1-----SAND

AT THE TOP

SKIN FRICTION COEFFICIENT- BETA = 0.120E+01
 UNDRAINED SHEAR STRENGTH, LB/SQ FT = 0.000E+00
 INTERNAL FRICTION ANGLE, DEG. = 0.340E+02
 BLOWS PER FOOT FROM STANDARD PENETRATION TEST = 0.000E+00
 SOIL UNIT WEIGHT, LB/CU FT = 0.135E+03
 MAXIMUM LOAD TRANSFER FOR SOIL, LB/SQ FT = 0.100E+11
 DEPTH, FT = 0.000E+00

AT THE BOTTOM

SKIN FRICTION COEFFICIENT- BETA = 0.120E+01

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 DIAMETER OF STEM = 4.000 FT.
 DIAMETER OF BASE = 4.000 FT.
 END OF STEM TO BASE = 0.000 FT.
 ANGLE OF BELL = 0.000 DEG.
 IGNORED TOP PORTION = 5.000 FT.
 IGNORED BOTTOM PORTION = 4.000 FT.
 AREA OF ONE PERCENT STEEL = 18.098 LB/SQ IN.
 ELASTIC MODULUS, EC = 0.312E+07 LB/SQ IN.
 VOLUME OF UNDERREAM = 0.000 CU.YDS.

PREDICTED RESULTS

 QS = ULTIMATE SIDE RESISTANCE;
 QB = ULTIMATE BASE RESISTANCE;
 WT = WEIGHT OF DRILLED SHAFT (UPLIFT CAPACITY ONLY);
 QU = TOTAL ULTIMATE RESISTANCE;
 LRFD QS = TOTAL SIDE FRICTION USING LRFD RESISTANCE FACTOR
 TO THE ULTIMATE SIDE RESISTANCE;
 LRFD QB = TOTAL BASE BEARING USING LRFD RESISTANCE FACTOR
 TO THE ULTIMATE BASE RESISTANCE
 LRFD QU = TOTAL CAPACITY WITH LRFD RESISTANCE FACTOR.

LENGTH (FEET)	VOLUME (CU.YDS)	QS (TONS)	QB (TONS)	QU (TONS)	LRFD QS (TONS)	LRFD QB (TONS)	LRFD QU (TONS)
10.0	4.65	1.38	20.11	21.49	0.62	8.04	8.67
11.0	5.12	2.76	20.11	22.87	1.24	8.04	9.29
12.0	5.59	4.15	27.15	31.30	1.87	10.86	12.73
13.0	6.05	5.53	34.97	40.50	2.49	13.99	16.48
14.0	6.52	6.91	43.57	50.49	3.11	17.43	20.54
15.0	6.98	8.29	52.96	61.25	3.73	21.18	24.92
16.0	7.45	9.68	60.00	69.68	4.35	24.00	28.35
17.0	7.91	11.06	64.69	75.75	4.98	25.88	30.85
18.0	8.38	12.44	67.04	80.86	5.60	26.82	32.41
19.0	8.84	13.82	67.04	82.24	6.22	33.52	39.74
20.0	9.31	15.21	67.04	83.63	6.84	33.52	40.36
21.0	9.78	16.59	67.04	85.01	7.47	33.52	41.61
22.0	10.24	17.97	67.04	86.39	8.09	33.52	42.85
23.0	10.71	19.35	67.04	87.78	8.71	33.52	44.09
24.0	11.17	20.73	61.73	89.16	9.34	29.33	45.23
25.0	11.64	22.11	61.73	90.54	9.96	29.33	46.37
26.0	12.10	23.50	55.30	91.92	10.58	27.65	47.51
27.0	12.57	24.88	55.30	93.30	11.20	27.65	48.65
28.0	13.03	26.26	51.11	94.68	11.82	26.39	49.80
29.0	13.50	27.64	51.11	96.06	12.44	26.39	50.94
30.0	13.96	29.02	50.27	97.44	13.06	25.14	52.08
31.0	14.43	30.40	50.27	98.82	13.68	25.14	53.22
32.0	14.90	31.78	50.27	100.20	14.30	20.11	54.36
33.0	15.36	33.16	50.27	101.58	14.92	20.11	55.50
34.0	15.83	34.54	50.27	102.96	15.54	20.11	56.64
35.0	16.29	35.92	50.27	104.34	16.16	20.11	57.78
36.0	16.76	37.30	50.27	105.72	16.78	20.11	58.92
37.0	17.22	38.68	50.27	107.10	17.40	20.11	60.06
38.0	17.69	40.06	50.27	108.48	18.02	20.11	61.20
39.0	18.15	41.44	50.27	109.86	18.64	20.11	62.34
40.0	18.62	42.82	50.27	111.24	19.26	20.11	63.48
41.0	19.08	44.20	50.27	112.62	19.88	20.11	64.62
42.0	19.55	45.58	50.27	114.00	20.50	20.11	65.76

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43.0	20.02	115.43	50.27	165.70	58.79	20.11	78.90
44.0	20.48	118.89	52.79	171.67	60.34	21.11	81.19
45.0	20.95	122.34	55.38	177.93	61.90	22.12	83.48
46.0	21.41	125.80	58.05	184.46	63.45	23.13	85.77
47.0	21.88	129.26	62.01	191.26	65.01	24.14	88.06
48.0	22.34	132.71	64.52	197.24	66.56	25.15	90.35
49.0	22.81	136.17	66.20	202.37	68.12	26.16	92.64
50.0	23.27	139.63	67.04	206.66	69.67	27.17	94.93
51.0	23.74	143.08	67.04	210.12	71.23	28.18	97.22
52.0	24.21	146.54	67.04	213.58	72.78	29.19	99.51
53.0	24.67	149.99	67.04	217.03	74.34	30.20	101.80
54.0	25.14	153.45	65.47	218.92	75.90	31.21	104.09
55.0	25.60	156.91	63.80	220.62	77.45	32.22	106.38
56.0	26.07	160.21	61.80	222.00	79.01	33.23	108.67
57.0	26.53	163.56	59.13	223.10	80.56	34.24	110.96
58.0	27.00	166.97	56.36	224.00	82.11	35.25	113.25
59.0	27.46	170.42	53.59	224.75	83.66	36.26	115.54
60.0	27.93	173.90	50.82	225.40	85.21	37.27	117.83
61.0	28.39	177.42	48.05	225.95	86.76	38.28	120.12
62.0	28.86	180.96	45.28	226.45	88.31	39.29	122.41
63.0	29.33	184.51	42.51	226.90	89.86	40.30	124.70
64.0	29.79	188.08	39.74	227.30	91.41	41.31	126.99
65.0	30.25	191.66	36.97	227.65	92.96	42.32	129.28
66.0	30.72	195.22	34.20	227.95	94.51	43.33	131.57
67.0	31.19	198.77	31.43	228.20	96.06	44.34	133.86
68.0	31.65	202.33	28.66	228.40	97.61	45.35	136.15
69.0	32.12	205.89	25.89	228.55	99.16	46.36	138.44
70.0	32.58	209.44	23.12	228.65	100.71	47.37	140.73
71.0	33.05	212.99	20.35	228.70	102.26	48.38	143.02
72.0	33.51	216.54	17.58	228.75	103.81	49.39	145.31
73.0	33.98	220.09	14.81	228.80	105.36	50.40	147.60
74.0	34.45	223.64	12.04	228.85	106.91	51.41	149.89
75.0	34.91	227.19	9.27	228.90	108.46	52.42	152.18
76.0	35.38	230.74	6.50	228.95	110.01	53.43	154.47
77.0	35.85	234.29	3.73	229.00	111.56	54.44	156.76
78.0	36.31	237.84	0.96	229.05	113.11	55.45	159.05
79.0	36.78	241.39	0.00	229.10	114.66	56.46	161.34
80.0	37.24	244.94	0.00	229.15	116.21	57.47	163.63
81.0	37.71	248.49	0.00	229.20	117.76	58.48	165.92
82.0	38.17	252.04	0.00	229.25	119.31	59.49	168.21
83.0	38.64	255.59	0.00	229.30	120.86	60.50	170.50
84.0	39.10	259.14	0.00	229.35	122.41	61.51	172.79
85.0	39.57	262.69	0.00	229.40	123.96	62.52	175.08
86.0	40.03	266.24	0.00	229.45	125.51	63.53	177.37
87.0	40.50	269.79	0.00	229.50	127.06	64.54	179.66
88.0	40.96	273.34	0.00	229.55	128.61	65.55	181.95
89.0	41.43	276.89	0.00	229.60	130.16	66.56	184.24
90.0	41.89	280.44	0.00	229.65	131.71	67.57	186.53
91.0	42.36	283.99	0.00	229.70	133.26	68.58	188.82
92.0	42.82	287.54	0.00	229.75	134.81	69.59	191.11
93.0	43.29	291.09	0.00	229.80	136.36	70.60	193.40
94.0	43.75	294.64	0.00	229.85	137.91	71.61	195.69
95.0	44.22	298.19	0.00	229.90	139.46	72.62	197.98
96.0	44.69	301.74	0.00	229.95	141.01	73.63	200.27
97.0	45.15	305.29	0.00	229.99	142.56	74.64	202.56
98.0	45.62	308.84	0.00	230.04	144.11	75.65	204.85
99.0	46.08	312.39	0.00	230.09	145.66	76.66	207.14
100.0	46.55	315.94	0.00	230.14	147.21	77.67	209.43
101.0	47.01	319.49	0.00	230.19	148.76	78.68	211.72
102.0	47.48	323.04	0.00	230.24	150.31	79.69	214.01

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Abut A.sfo

RESULT FROM TREND (AVERAGED) LINE		
TOP LOAD	TOP MOVEMENT	TIP LOAD
ton	IN.	ton
0.4451E-01	0.2041E-04	0.9776E-03
0.2226E+00	0.1020E-03	0.4888E-02
0.4451E+00	0.2041E-03	0.9776E-02
0.2226E+02	0.1020E-01	0.4888E+00
0.3339E+02	0.1530E-01	0.7332E+00
0.4452E+02	0.2041E-01	0.9776E+00
0.1116E+03	0.5107E-01	0.2444E+01
0.1990E+03	0.9816E-01	0.4888E+01
0.2535E+03	0.1370E+00	0.7332E+01
0.2986E+03	0.1741E+00	0.9776E+01
0.3912E+03	0.3519E+00	0.2441E+02
0.4271E+03	0.6160E+00	0.4782E+02
0.4336E+03	0.7445E+00	0.5760E+02
0.4451E+03	0.1328E+01	0.8581E+02
0.4948E+03	0.2549E+01	0.1361E+03

TIP MOVEMENT		
IN.	ton	IN.
0.1000E-04	0.5000E-04	0.1000E-04
0.5000E-04	0.5000E-04	0.5000E-04
0.1000E-03	0.5000E-03	0.1000E-03
0.5000E-02	0.5000E-02	0.5000E-02
0.7500E-02	0.7500E-02	0.7500E-02
0.1000E-01	0.1000E-01	0.1000E-01
0.2500E-01	0.2500E-01	0.2500E-01
0.5000E-01	0.5000E-01	0.5000E-01
0.7500E-01	0.7500E-01	0.7500E-01
0.1000E+00	0.1000E+00	0.1000E+00
0.2500E+00	0.2500E+00	0.2500E+00
0.5000E+00	0.5000E+00	0.5000E+00
0.6250E+00	0.6250E+00	0.6250E+00
0.1200E+01	0.1200E+01	0.1200E+01
0.2400E+01	0.2400E+01	0.2400E+01

RESULT FROM UPPER-BOUND LINE

TOP LOAD	TOP MOVEMENT	TIP LOAD	TIP MOVEMENT
ton	IN.	ton	IN.
0.6785E-01	0.2540E-04	0.1397E-02	0.1000E-04
0.3393E+00	0.1270E-03	0.6983E-02	0.5000E-04
0.6785E+00	0.2540E-03	0.1397E-01	0.1000E-03
0.3393E+00	0.1270E-01	0.6983E+00	0.5000E-02
0.5095E+02	0.1905E-01	0.1047E+01	0.7500E-02
0.6803E+02	0.2542E-01	0.1397E+01	0.1000E-01
0.1689E+03	0.6357E-01	0.3492E+01	0.2500E-01
0.2801E+03	0.1176E+00	0.6983E+01	0.5000E-01
0.3342E+03	0.1576E+00	0.1047E+02	0.7500E-01
0.3696E+03	0.1933E+00	0.1397E+02	0.1000E+00
0.4375E+03	0.3658E+00	0.3480E+02	0.2500E+00
0.4679E+03	0.6295E+00	0.6648E+02	0.5000E+00
0.4767E+03	0.7593E+00	0.7975E+02	0.6250E+00
0.4865E+03	0.1341E+01	0.1019E+03	0.1200E+01
0.5294E+03	0.2560E+01	0.1448E+03	0.2400E+01

RESULT FROM LOWER-BOUND LINE

TOP LOAD	TOP MOVEMENT	TIP LOAD	TIP MOVEMENT
ton	IN.	ton	IN.
0.2479E-01	0.1598E-04	0.5586E-03	0.1000E-04
0.1239E+00	0.7992E-04	0.2793E-02	0.5000E-04
0.2479E+00	0.1598E-03	0.5586E-02	0.1000E-03
0.1239E+02	0.7992E-02	0.2793E+00	0.5000E-02
0.1859E+02	0.1199E-01	0.4190E+00	0.7500E-02
0.2479E+02	0.1598E-01	0.5586E+00	0.1000E-01
0.6204E+02	0.3997E-01	0.1397E+01	0.2500E-01
0.1202E+03	0.7927E-01	0.2793E+01	0.5000E-01
0.1690E+03	0.1163E+00	0.4190E+01	0.1000E+00
0.2120E+03	0.1521E+00	0.5586E+01	0.2500E+00
0.3439E+03	0.3439E+00	0.1019E+02	0.5000E+00
0.3861E+03	0.6204E+00	0.2077E+02	0.6250E+00
0.3871E+03	0.7290E+00	0.2871E+02	0.7500E+00
0.4037E+03	0.1215E+01	0.2871E+02	0.1200E+01
0.4602E+03	0.2535E+01	0.1274E+03	0.2400E+01

LATERAL CAPACITY ABUTMENT A.

Abut A.lp7o
Description: Abutment A Lateral Pile Capacity

Abut A.lp7o
LPile Plus for Windows, Version 2013-07.007
Analysis of Individual Piles and Drilled shafts
Subjected to Lateral Loading using the p-y Method
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Files used for Analysis
Y:\Bridges\DELDOT\BRI-159_JAMES ST BRIDGE\FOUNDATION
Path to file locations:
REPORT\LPile Output
Name of input data file: Abut A.lp7d
Name of output report file: Abut A.lp7o
Name of plot output file: Abut A.lp/p
Name of runtime message file: Abut A.lp/r

Date and Time of Analysis
Date: October 15, 2014 Time: 16:10:38

Problem Title
Project Name: BRI-159 Abutment A

Job Number:
Client: DelDOT
Engineer: SJM

Program Options and Settings

Engineering Units of Input data and Computations:
- Engineering units are US Customary Units (pounds, feet, inches)

Analysis Control Options:
- Maximum number of iterations allowed = 100
- Deflection tolerance for convergence = 1.0000E-05 in
- Maximum allowable deflection = 100.0000 in
- Number of pile increments = 100

Loading Type and Number of Cycles of Loading:
- Static loading specified

Computational Options:
- Use unfactored loads in computations (conventional analysis)
- Compute pile response under loading and nonlinear bending properties of pile (only if nonlinear pile properties are input)
- Use of p-y modification factors for p-y curves: not selected
- Loading by lateral soil movements acting on pile: not selected
- Input of shear resistance at the pile tip: not selected
- Computation of pile-head foundation stiffness matrix: not selected
- Push-over analysis of pile: not selected
- Buckling analysis of pile: not selected

Output Options:
- No p-y curves to be computed and reported for user-specified depths
- Values of pile-head deflection, bending moment, shear force, and soil reaction are printed for full length of pile.
- Printing Increment (nodal spacing of output points) = 1

Pile Structural Properties and Geometry

Total number of pile sections = 1
Total length of pile = 95.00 ft
Depth of ground surface below top of pile = 1.00 ft
Pile diameter values used for p-y curve computations are defined using 2 points.
p-y curves are computed using pile diameter values interpolated with depth over the length of the pile.

Point	Depth X ft	Pile Diameter in
1	0.000000	49.00000000
2	95.00000000	49.00000000

Input Structural Properties:

File Section No. 1:

Section Type = Drilled Shaft with
Permanent Casing
Section Length = 95.00000 ft
Section Diameter = 49.00000 in

Ground Slope and Pile Batter Angles

Ground Slope Angle = 0.000 degrees
= 0.000 radians
Pile Batter Angle = 0.000 degrees
= 0.000 radians

Soil and Rock Layering Information

The soil profile is modelled using 7 layers

Layer 1 is sand, p-y criteria by Reese et al., 1974

Distance from top of pile to top of layer = 1.00000 ft
Distance from top of pile to bottom of layer = 4.00000 ft
Effective unit weight at top of layer = 72.60000 pcf
Effective unit weight at bottom of layer = 72.60000 pcf
Friction angle at top of layer = 34.00000 deg.
Friction angle at bottom of layer = 34.00000 deg.
Epsilon-50 at top of layer = 60.00000 pci
Epsilon-50 at bottom of layer = 60.00000 pci

Layer 2 is soft clay, p-y criteria by Matlock, 1970

Distance from top of pile to top of layer = 4.00000 ft
Distance from top of pile to bottom of layer = 20.00000 ft
Effective unit weight at top of layer = 37.60000 pcf
Effective unit weight at bottom of layer = 37.60000 pcf
Undrained cohesion at top of layer = 400.00000 psf
Undrained cohesion at bottom of layer = 400.00000 psf
Epsilon-50 at top of layer = 0.02000
Epsilon-50 at bottom of layer = 0.02000

Layer 3 is sand, p-y criteria by Reese et al., 1974

Distance from top of pile to top of layer = 20.00000 ft
Distance from top of pile to bottom of layer = 32.00000 ft
Effective unit weight at top of layer = 67.60000 pcf
Effective unit weight at bottom of layer = 67.60000 pcf
Friction angle at top of layer = 32.00000 deg.
Friction angle at bottom of layer = 32.00000 deg.
Epsilon-50 at top of layer = 60.00000 pci
Epsilon-50 at bottom of layer = 60.00000 pci

Layer 4 is stiff clay with water-induced erosion

Distance from top of pile to top of layer = 32.00000 ft
Distance from top of pile to bottom of layer = 52.00000 ft
Effective unit weight at top of layer = 62.60000 pcf
Effective unit weight at bottom of layer = 62.60000 pcf
Undrained cohesion at top of layer = 1000.00000 psf
Undrained cohesion at bottom of layer = 1000.00000 psf
Epsilon-50 at top of layer = 0.00700
Epsilon-50 at bottom of layer = 0.00700
Subgrade k at top of layer = 200.00000 pci
Subgrade k at bottom of layer = 200.00000 pci

Layer 5 is sand, p-y criteria by Reese et al., 1974

Distance from top of pile to top of layer = 52.00000 ft
Distance from top of pile to bottom of layer = 62.00000 ft
Effective unit weight at top of layer = 67.20000 pcf
Effective unit weight at bottom of layer = 67.20000 pcf
Friction angle at top of layer = 32.00000 deg.
Friction angle at bottom of layer = 32.00000 deg.
Epsilon-50 at top of layer = 60.00000 pci
Epsilon-50 at bottom of layer = 60.00000 pci

Layer 6 is stiff clay with water-induced erosion

Distance from top of pile to top of layer = 62.00000 ft
Distance from top of pile to bottom of layer = 87.00000 ft
Effective unit weight at top of layer = 62.60000 pcf
Effective unit weight at bottom of layer = 62.60000 pcf
Undrained cohesion at top of layer = 1000.00000 psf
Undrained cohesion at bottom of layer = 1000.00000 psf
Epsilon-50 at top of layer = 0.00700
Epsilon-50 at bottom of layer = 0.00700
Subgrade k at top of layer = 200.00000 pci
Subgrade k at bottom of layer = 200.00000 pci

Layer 7 is sand, p-y criteria by Reese et al., 1974

Distance from top of pile to top of layer = 87.00000 ft
Distance from top of pile to bottom of layer = 112.00000 ft
Effective unit weight at top of layer = 72.60000 pcf
Effective unit weight at bottom of layer = 72.60000 pcf
Friction angle at top of layer = 34.00000 deg.
Friction angle at bottom of layer = 34.00000 deg.
Epsilon-50 at top of layer = 123.00000 pci
Epsilon-50 at bottom of layer = 123.00000 pci

(Depth of lowest soil layer extends 17.00 ft below pile tip)

Summary of Soil Properties

Layer Page 4 Effective Undrained

Abut A.1p7o

Angle of Friction deg.	Strain Factor (p-y Curve Criteria) Epsilon 50	Soil Type kpcy	Depth ft	Unit wt. pcf	Cohesion psf
1	Sand (Reese, et al.)	60.000	1.000	72.600	--
34.000	--	60.000	4.000	72.600	--
2	Soft clay	0.02000	4.000	37.600	400.000
3	Sand (Reese, et al.)	60.000	20.000	37.600	400.000
32.000	--	60.000	20.000	67.600	--
4	Stiff Clay with Free Water	60.000	32.000	67.600	--
32.000	0.00700	200.000	32.000	62.600	1000.000
5	Sand (Reese, et al.)	60.000	52.000	62.600	1000.000
32.000	--	60.000	52.000	67.200	--
6	Stiff Clay with Free Water	60.000	62.000	67.200	--
32.000	0.00700	200.000	62.000	62.600	1000.000
7	Sand (Reese, et al.)	125.000	87.000	62.600	1000.000
34.000	--	125.000	87.000	72.600	--
34.000	--	125.000	112.000	72.300	--

Static loading criteria were used when computing p-y curves for all analyses.

Pile-head Loading and Pile-head Fixity Conditions

Load Compute Top y vs. Pile Length	Condition	Condition	Axial Thrust Force, lbs
1	1	2	
1	1	2	
Yes	V = 68000. lbs	M = 5342000. in-lbs	504400.
2	1	M = 53000. lbs	M = 4038000. in-lbs
Yes	V = 53000. lbs	M = 4038000. in-lbs	410100.
3	4	M = 1.00000 in	M = 5342000. in-lbs
			504400.

Abut A.1p7o

Yes	4	Y =	M =	5342000. in-lbs	504400.
Yes	4	Y = 1.50000 in	M = 5342000. in-lbs	504400.	
No	4	Y = 2.00000 in	M = 5342000. in-lbs	504400.	
Yes	4	Y = 0.50000 in	M = 4038000. in-lbs	410100.	
Yes	4	Y = 1.00000 in	M = 4038000. in-lbs	410100.	
Yes	4	Y = 1.50000 in	M = 4038000. in-lbs	410100.	

V = perpendicular shear force applied to pile head
M = bending moment applied to pile head
Y = lateral deflection relative to pile axis
S = pile slope relative to original pile batter angle
R = rotational stiffness applied to pile head
Axial thrust is assumed to be acting axially for all pile batter angles.

Computations of Nominal Moment Capacity and Nonlinear Bending Stiffness

Axial thrust force values were determined from pile-head loading conditions

Number of Pile Sections Analyzed = 1

Pile Section No. 1:

Dimensions and Properties of Drilled Shaft (Bored Pile) with Permanent Casing:

Length of Section	=	95.00000 ft
Outer Diameter of Casing	=	49.00000 in
Concrete Thickness Inside Casing	=	4.00000 in
Casing Wall Thickness	=	0.25000 in
Welding of Inertial of Steel Casing	=	2.24000 in#4
Yield Stress of Casing	=	36000. psi
Elastic Modulus of Casing	=	290000000. psi
Number of Reinforcing Bars	=	12
Area of Single Reinforcing Bar	=	0.79000 sq. in.
Edge-to-Edge Bar Spacing	=	9.09394 in
Maximum Concrete Aggregate Size	=	0.50000 in
Ratio of Bar Spacing to Aggregate Size	=	18.19
Offset of Center of Rebar Cage from Center of Pile	=	0.0000 in
Yield Stress of Reinforcing Bars	=	60000. psi
Modulus of Elasticity of Reinforcing Bars	=	290000000. psi
Gross Area of Pile	=	1885.24099 sq. in.
Area of Concrete	=	1800.07737 sq. in.
Cross-sectional Area of Steel Casing	=	76.18362 sq. in.
Area of All Steel (Casing and Bars)	=	85.66362 sq. in.
Area Ratio of All Steel to Gross Area of Pile	=	4.54 percent

Axial Structural Capacities:

Nom. Axial Structural Capacity = 0.85 FC AC + FY AS	=	7901.608 kips
Tensile Load for Cracking of Concrete	=	-939.735 kips
Nominal Axial Tensile Capacity	=	-3311.410 kips

Reinforcing Bar Dimensions and Positions Used in Computations:

Bar Number	Bar Diam. inches	Bar Area sq. in.	X inches	Y inches
1	1.00000	0.79000	19.50000	0.00000
2	1.00000	0.79000	16.88750	9.75000
3	1.00000	0.79000	9.75000	16.88750
4	1.00000	0.79000	0.00000	19.50000
5	1.00000	0.79000	-9.75000	16.88750
6	1.00000	0.79000	-19.50000	9.75000
7	1.00000	0.79000	-16.88750	-9.75000
8	1.00000	0.79000	-9.75000	-16.88750
9	1.00000	0.79000	0.00000	-19.50000
10	1.00000	0.79000	9.75000	-16.88750
11	1.00000	0.79000	16.88750	-9.75000
12	1.00000	0.79000	16.88750	-9.75000

NOTE: The positions of the above rebars were computed by LPTile

Minimum spacing between any two bars not equal to zero = 9.09394 inches between Bars 7 and 8

Concrete Properties:

Compressive Strength of Concrete	= 3000.00000 psi
Modulus of Elasticity of Concrete	= 312019. psi
Modulus of Rupture of Concrete	= -410.79191 psi
Compression Strain at Peak Stress	= 0.00163
Tensile Strain at Fracture of Concrete	= -0.0001160
Maximum Coarse Aggregate Size	= 0.00000 in

Number of Axial Thrust Force values Determined from Pile-head Loadings = 2

Number	Axial Thrust Force kips
1	410.100
2	504.400

Definitions of Run Messages and Notes:

- C = concrete in section has cracked in tension.
- Y = stress in reinforcing steel has reached yield stress.
- T = ACI 318-08 criteria for tension-controlled section met, tensile strain in reinforcement exceeds 0.005 while simultaneously compressive strain in concrete more than 0.003. See ACI 318-08, Section 10.3.4.
- Z = depth of tensile zone in concrete section is less than 10 percent of section depth.

Bending Stiffness (EI) = Computed Bending Moment / Curvature.
Position of neutral axis is measured from edge of compression side of pile.
Compressive stresses and strains are positive in sign.
Tensile stresses and strains are negative in sign.

Axial Thrust Force = 410.100 kips

Abut A.1p7o

Run	Depth to N Axis		Bending Moment in-kip	Max Casing Stress kip-in ²	Bending Curvature rad/in.	Max Concrete Stress ksi	Max Steel Stress in-kip	Max Casing Stress ksi	Depth to N Axis in	Max Comp Strain in/in	Max Tens Strain in/in
	Msg	in									
97	3972510		1016.283287	162605.3262	0.00000625	0.00000625	1016.283287	162605.3262	97.3972510	0.0000609	0.0000302
98	3972510		1.7608846	1.7608846	0.00001250	0.00001250	1.7608846	1.7608846	60.9792541	0.0000762	0.0000150
99	3972510		2.2016167	2.2016167	0.00001875	0.00001875	2.2016167	2.2016167	48.8535267	0.0000916	-0.000000275
100	3972510		2.6430886	2.6430886	0.00002500	0.00002500	2.6430886	2.6430886	42.8002900	0.0001070	-0.0000155
101	3972510		3.0852585	3.0852585	0.00003125	0.00003125	3.0852585	3.0852585	39.1734655	0.0001224	-0.0000307
102	3972510		3.5278922	3.5278922	0.00003750	0.00003750	3.5278922	3.5278922	36.7580676	0.0001378	-0.0000459
103	3972510		3.9707961	3.9707961	0.00004375	0.00004375	3.9707961	3.9707961	35.0341260	0.0001533	-0.0000611
104	3972510		4.4138704	4.4138704	0.00005000	0.00005000	4.4138704	4.4138704	33.7419764	0.0001687	-0.0000763
105	3972510		4.8570616	4.8570616	0.00005625	0.00005625	4.8570616	4.8570616	32.7375035	0.0001841	-0.0000915
106	3972510		5.3003396	5.3003396	0.00006250	0.00006250	5.3003396	5.3003396	31.9343018	0.0001996	-0.0001067
107	3972510		5.7438860	5.7438860	0.00006875	0.00006875	5.7438860	5.7438860	28.9963893	0.0001994	-0.0001375
108	3972510		6.1874917	6.1874917	0.00007500	0.00007500	6.1874917	6.1874917	28.2317503	0.0002117	-0.0001558
109	3972510		6.6310974	6.6310974	0.00008125	0.00008125	6.6310974	6.6310974	27.5723971	0.0002240	-0.0001741
110	3972510		7.0747031	7.0747031	0.00008750	0.00008750	7.0747031	7.0747031	26.9982941	0.0002362	-0.0001925
111	3972510		7.5183088	7.5183088	0.00009375	0.00009375	7.5183088	7.5183088	26.4940382	0.0002484	-0.0002110
112	3972510		7.9619145	7.9619145	0.00010000	0.00010000	7.9619145	7.9619145	26.0475634	0.0002605	-0.0002295
113	3972510		8.4055202	8.4055202	0.00010625	0.00010625	8.4055202	8.4055202	25.6497162	0.0002725	-0.0002481
114	3972510		8.8491259	8.8491259	0.00011250	0.00011250	8.8491259	8.8491259	25.2925644	0.0002845	-0.0002667
115	3972510		9.2927316	9.2927316	0.00011875	0.00011875	9.2927316	9.2927316	24.9697585	0.0002965	-0.0002854
116	3972510		9.7363373	9.7363373	0.00012500	0.00012500	9.7363373	9.7363373	24.6781673	0.0003085	-0.0003040
117	3972510		10.1799430	10.1799430	0.00013125	0.00013125	10.1799430	10.1799430	24.4119664	0.0003204	-0.0003227
118	3972510		10.6235487	10.6235487	0.00013750	0.00013750	10.6235487	10.6235487	24.1693238	0.0003323	-0.0003414
119	3972510		11.0671544	11.0671544	0.00014375	0.00014375	11.0671544	11.0671544	23.9462060	0.0003442	-0.0003601
120	3972510		11.5107601	11.5107601	0.00015000	0.00015000	11.5107601	11.5107601	23.7419139	0.0003561	-0.0003789
121	3972510		11.9543658	11.9543658	0.00015625	0.00015625	11.9543658	11.9543658	23.5518472	0.0003680	-0.0003976
122	3972510		12.3979715	12.3979715	0.00016250	0.00016250	12.3979715	12.3979715	23.3769558	0.0003799	-0.0004164
123	3972510		12.8415772	12.8415772	0.00016875	0.00016875	12.8415772	12.8415772	23.2145744	0.0003917	-0.0004351
124	3972510		13.2851829	13.2851829	0.00017500	0.00017500	13.2851829	13.2851829			

Abut. A. 1p7o		Abut. A. 1p7o		Abut. A. 1p7o		Abut. A. 1p7o		Abut. A. 1p7o		Abut. A. 1p7o		Abut. A. 1p7o		Abut. A. 1p7o		Abut. A. 1p7o		Abut. A. 1p7o		Abut. A. 1p7o		Abut. A. 1p7o	
Bending Concrete Curvature Stress ksi	Bending Steel Moment in-kip	Bending Max Steel Stress ksi	Bending Max Casing Stiffness kip-in2	Depth to Run N Axis in	Max Comp Strain in/in	Max Tens Strain in/in	0.0023028	-0.0042816	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000
0.0001344	62681.	60.0000000	466460224.	17.1372542	0.0023028	-0.0042816	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000
2.9954509	62847.	60.0000000	450917991.	17.0499805	0.0023763	-0.0044530	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000
2.9979602	62998.	60.0000000	436351819.	16.9707310	0.0024501	-0.0046242	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000
2.9993690	63139.	60.0000000	422691045.	16.8969414	0.0025240	-0.0047954	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000
2.9993252	63265.	60.0000000	409813844.	16.8261188	0.0025975	-0.0049668	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000
2.9963195	63383.	60.0000000	397697401.	16.7598874	0.0026711	-0.0051383	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000
2.9996857	63494.	60.0000000	386275042.	16.6995376	0.0027450	-0.0053094	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000
2.9964167	63595.	60.0000000	375466307.	16.6427963	0.0028189	-0.0054805	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000
2.9996199	63691.	60.0000000	365250462.	16.5908913	0.0028930	-0.0056513	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000
2.9957328	63775.	60.0000000	355242555.	16.5436355	0.0029675	-0.0058219	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000
2.9990934	63853.	60.0000000	346321345.	16.5024143	0.0030426	-0.0059917	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000
2.9981833	63921.	60.0000000	337538060.	16.4642481	0.0031179	-0.0061615	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000
2.9975442	63988.	60.0000000	329197349.	16.4293559	0.0031935	-0.0063309	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000
2.9980194	64046.	60.0000000	321233071.	16.3964161	0.0032690	-0.0065003	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000
2.9951123	64102.	60.0000000	313646693.	16.3649161	0.0033446	-0.0066698	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000
2.9960643	64155.	60.0000000	305400058.	16.3355157	0.0034202	-0.0068391	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000
2.9998149	64205.	60.0000000	299497358.	16.3069573	0.0034958	-0.0070086	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000
2.9950194	64251.	60.0000000	292883848.	16.2821537	0.0035719	-0.0071775	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000
2.9971161	64297.	60.0000000	286558333.	16.2594319	0.0036482	-0.0073462	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000
2.9955809	64336.	60.0000000	280483661.	16.2378083	0.0037245	-0.0075148	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000
2.9975688	64373.	60.0000000	274658466.	16.2186902	0.0038013	-0.0076831	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000
2.9942114	64437.	60.0000000	264584666.	16.2000000	0.0038813	-0.0078514	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000

Axial Thrust Force = 504.400 kips

Load No.	Axial Thrust kips	Nominal Moment in-kip	Max. Comp. Strain	Abut. A. 1p7o
1	410.100	63808.984	0.00300000	0.70
2	504.400	64612.939	0.00300000	0.70

Summary of Results for Nominal (Unfactored) Moment Capacity for Section 1
 Moment values interpolated at maximum compressive strain = 0.003
 or maximum developed moment if pile fails at smaller strains.

Note note that the values of moment capacity in the table above are not factored by a strength reduction factor (ϕ -factor).
 In ACI 318-08, the value of the strength reduction factor depends on whether the transverse reinforcing steel bars are tied hoops (0.65) or spirals (0.70).
 The above values should be multiplied by the appropriate strength reduction factor to compute ultimate moment capacity according to ACI 318-08 Section 9.3.2.2 or the value required by the design standard being followed.
 The following table presents factored moment capacities and corresponding bending stiffnesses computed for common resistance factor values used for reinforced concrete sections.

Load No.	Axial Thrust kips	Nominal Moment Capacity in-kip	Ultimate (Factored) Axial Thrust kips	Ultimate Moment
1	410.100	63808.984	266.565	63808.984
2	504.400	64612.939	327.860	64612.939

Res. X	Depth of Soil	Deflect. Spr.	Bending Moment	Shear Force	Slope	Total Stress	Bending Stiffness
feet	lb/inch	inches	in-lbs	lbs	radians	psi*	lb-in ²
0.000	0.00	1.0886	5342000.	68000.	-0.004463	0.000	1.619E+12
0.000	0.950	1.0379	6142754.	68000.	-0.004422	0.000	1.619E+12
0.000	1.900	0.9877	6943360.	66966.	-0.004376	0.000	1.618E+12
-181.3208	2092.7159	719970.	719970.	63669.	-0.004325	0.000	1.617E+12
-397.16730	4826.5681	844648.	844648.	57839.	-0.004268	0.000	1.616E+12
-625.5380	8020.7800	9087239.	9087239.	53204.	-0.004206	0.000	1.615E+12
-187.7271	2545.7254	9706064.	9706064.	51028.	-0.004139	0.000	1.613E+12
-194.0364	2788.5625	10298777.	10298777.	48783.	-0.004069	0.000	1.612E+12
-199.7611	3050.8277	10865111.	10865111.	46476.	-0.003994	0.000	1.611E+12
-204.9330	3335.2066	11404369.	11404369.	44114.	-0.003905	0.000	1.280E+12
-209.5575	3645.1157	11915809.	11915809.	41701.	-0.003800	0.000	1.264E+12
-213.6550	3983.4173	12398865.	12398865.	39245.	-0.003690	0.000	1.250E+12
-217.2215	4354.0315	12853040.	12853040.	36752.	-0.003574	0.000	1.238E+12
-220.2499	4761.4984	13277912.	13277912.	34227.	-0.003453	0.000	1.228E+12
-222.7314	5211.1300	13673128.	13673128.	31677.	-0.003328	0.000	1.218E+12
-224.6556	5709.1921	0.000	0.000				

Computed values of Pile Loading and Deflection for Lateral Loading for Load Case Number 1

Pile-head conditions are Shear and Moment (Loading Type 1)
 Shear force at pile head = 68000.0 lbs
 Applied moment at pile head = 5342000.0 in-lbs
 Axial thrust load on pile head = 504400.0 lbs

Abut A. 1p7o		Abut A. 1p7o		Abut A. 1p7o	
14.250	0.4114	14038412.	0.000	1.210E+12	0.000
-226.0118	6263.1282	0.000	0.000	1.203E+12	0.000
15.200	0.3757	14373563.	0.000	1.197E+12	0.000
-226.7883	6881.8404	0.000	0.000	1.192E+12	0.000
16.150	0.3415	14678458.	0.000	1.187E+12	0.000
-226.9731	7576.0509	0.000	0.000	1.183E+12	0.000
17.100	0.3090	14953051.	0.000	1.180E+12	0.000
-226.5541	8358.7637	0.000	0.000	1.177E+12	0.000
18.050	0.2781	15197379.	0.000	1.176E+12	0.000
-225.5188	9245.8685	0.000	0.000	1.175E+12	0.000
19.000	0.2488	15411560.	0.000	1.175E+12	0.000
-223.8550	10257.0000	0.000	0.000	1.175E+12	0.000
19.950	0.2212	15595795.	0.000	1.175E+12	0.000
-221.5508	11416.0000	0.000	0.000	1.175E+12	0.000
20.900	0.1954	15750370.	0.000	1.175E+12	0.000
-746.5634	43676.0000	0.000	0.000	1.175E+12	0.000
21.850	0.1713	15806783.	0.000	1.175E+12	0.000
-727.1280	48064.0000	0.000	0.000	1.175E+12	0.000
22.800	0.1489	15768467.	0.000	1.175E+12	0.000
-671.9015	54357.0000	0.000	0.000	1.175E+12	0.000
23.750	0.1283	15641952.	0.000	1.175E+12	0.000
-599.6978	53289.0000	0.000	0.000	1.175E+12	0.000
24.700	0.1094	15436632.	0.000	1.175E+12	0.000
-589.7720	61409.0000	0.000	0.000	1.175E+12	0.000
25.650	0.0922	15153874.	0.000	1.175E+12	0.000
-574.9580	71097.0000	0.000	0.000	1.175E+12	0.000
26.600	0.0766	14794550.	0.000	1.175E+12	0.000
-550.6720	81907.0000	0.000	0.000	1.175E+12	0.000
27.550	0.0627	14364865.	0.000	1.175E+12	0.000
-516.8971	93963.0000	0.000	0.000	1.175E+12	0.000
28.500	0.0503	13866214.	0.000	1.175E+12	0.000
-488.9836	110764.0000	0.000	0.000	1.175E+12	0.000
29.450	0.0394	13303266.	0.000	1.175E+12	0.000
-461.6119	133471.0000	0.000	0.000	1.175E+12	0.000
30.400	0.0299	12679615.	0.000	1.175E+12	0.000
-425.8890	162181.0000	0.000	0.000	1.175E+12	0.000
31.350	0.0218	11999948.	0.000	1.175E+12	0.000
-374.0546	195859.0000	0.000	0.000	1.175E+12	0.000
32.300	0.0148	11271045.	0.000	1.175E+12	0.000
-389.3336	299011.0000	0.000	0.000	1.175E+12	0.000
33.250	0.009056	10490968.	0.000	1.175E+12	0.000
-304.1029	382816.0000	0.000	0.000	1.175E+12	0.000
34.200	0.004114	9670944.	0.000	1.175E+12	0.000
-204.9768	567952.0000	0.000	0.000	1.175E+12	0.000
35.150	-4.829E-05	8823888.	0.000	1.175E+12	0.000
21.0409	4967632.	0.000	0.000	1.175E+12	0.000
189.0734	615697.	0.000	0.000	1.175E+12	0.000
253.8781	458540.	0.000	0.000	1.175E+12	0.000
295.4425	394032.	0.000	0.000	1.175E+12	0.000
323.8741	359442.	0.000	0.000	1.175E+12	0.000
343.3585	339045.	0.000	0.000	1.175E+12	0.000
356.1870	326834.	0.000	0.000	1.175E+12	0.000
363.8142	319883.	0.000	0.000	1.175E+12	0.000
367.2541	316986.	0.000	0.000	1.175E+12	0.000
43.700	-0.0132	2340749.	0.000	1.175E+12	0.000

Abut A. 1p7o

Abut A. 1p7o

Abut A. 1p7o

367.2611	316980.	0.000	0.000	1.620E+12	0.000
44.650	-0.0130	2065930.	0.000	1.620E+12	0.000
364.4232	319448.	0.000	0.000	1.620E+12	0.000
45.600	-0.0126	1638387.	0.000	1.620E+12	0.000
359.2147	324081.	0.000	0.000	1.620E+12	0.000
46.550	-0.0121	1257461.	0.000	1.620E+12	0.000
352.0282	330697.	0.000	0.000	1.620E+12	0.000
47.500	-0.0115	922235.	0.000	1.620E+12	0.000
343.1942	339209.	0.000	0.000	1.620E+12	0.000
48.450	-0.0109	631572.	0.000	1.620E+12	0.000
332.9942	349600.	0.000	0.000	1.620E+12	0.000
49.400	-0.0101	384160.	0.000	1.620E+12	0.000
321.6684	361909.	0.000	0.000	1.620E+12	0.000
50.350	-0.009376	178536.	0.000	1.620E+12	0.000
309.4208	376234.	0.000	0.000	1.620E+12	0.000
51.300	-0.008604	13118.	0.000	1.620E+12	0.000
296.4213	392734.	0.000	0.000	1.620E+12	0.000
52.250	-0.007832	-113779.	0.000	1.620E+12	0.000
134.8419	196271.	0.000	0.000	1.620E+12	0.000
53.200	-0.007069	-223146.	0.000	1.620E+12	0.000
126.3380	204088.	0.000	0.000	1.620E+12	0.000
54.150	-0.006324	-316060.	0.000	1.620E+12	0.000
117.3228	211866.	0.000	0.000	1.620E+12	0.000
55.100	-0.005604	-393888.	0.000	1.620E+12	0.000
107.6767	219684.	0.000	0.000	1.620E+12	0.000
56.050	-0.004915	-457267.	0.000	1.620E+12	0.000
98.0791	227461.	0.000	0.000	1.620E+12	0.000
57.000	-0.004264	-540740.	0.000	1.620E+12	0.000
87.9809	235350.	0.000	0.000	1.620E+12	0.000
57.950	-0.003653	-624740.	0.000	1.620E+12	0.000
77.8333	243050.	0.000	0.000	1.620E+12	0.000
58.900	-0.003086	-716855.	0.000	1.620E+12	0.000
67.9066	250855.	0.000	0.000	1.620E+12	0.000
59.850	-0.002565	-817021.	0.000	1.620E+12	0.000
58.2039	258653.	0.000	0.000	1.620E+12	0.000
60.800	-0.002093	-929799.	0.000	1.620E+12	0.000
48.9085	266449.	0.000	0.000	1.620E+12	0.000
61.750	-0.001669	-1043196.	0.000	1.620E+12	0.000
40.1433	274247.	0.000	0.000	1.620E+12	0.000
62.700	-0.001294	-117352.	0.000	1.620E+12	0.000
114.9650	1012614.	0.000	0.000	1.620E+12	0.000
63.650	-0.000969	-1303541.	0.000	1.620E+12	0.000
99.4950	1170062.	0.000	0.000	1.620E+12	0.000
64.600	-0.000693	-1439555.	0.000	1.620E+12	0.000
84.1190	1383936.	0.000	0.000	1.620E+12	0.000
65.550	-0.000463	-1590555.	0.000	1.620E+12	0.000
68.7408	1693538.	0.000	0.000	1.620E+12	0.000
66.500	-0.000276	-1792379.	0.000	1.620E+12	0.000
53.0682	2193687.	0.000	0.000	1.620E+12	0.000
67.450	-0.000128	-1938786.	0.000	1.620E+12	0.000
36.2017	3215717.	0.000	0.000	1.620E+12	0.000
68.400	-0.000105	-208470.	0.000	1.620E+12	0.000
12.8213	9079193.	0.000	0.000	1.620E+12	0.000
69.350	-0.000085	-223473.	0.000	1.620E+12	0.000
25.8859	4497339.	0.000	0.000	1.620E+12	0.000
70.300	-0.000062	-238828.	0.000	1.620E+12	0.000
35.2419	3303367.	0.000	0.000	1.620E+12	0.000
71.250	-0.000046	-253751.	0.000	1.620E+12	0.000
39.9719	2912466.	0.000	0.000	1.620E+12	0.000
72.200	-0.000034	-268681.	0.000	1.620E+12	0.000
42.1903	2759319.	0.000	0.000	1.620E+12	0.000
73.150	-0.0000179	-283447.	0.000	1.620E+12	0.000
42.7461	2723442.	0.000	0.000	1.620E+12	0.000

MOMENT
FIXITY

ELEVATION = 15-69.35 = -67.85
AND ELEVATION = 4.5-69.35 = -64.85

Maximum shear force = 21.850000 lbs
 Depth of maximum bending moment = 35.150000 feet below pile head
 Depth of maximum shear force = 29
 Number of iterations = 3
 Number of zero deflection points = 3

Abut A.1p7o = -74367. lbs
 Abut A.1p7o = 21.850000 lbs
 Abut A.1p7o = 35.150000 feet below pile head

Pile-head Deflection vs. Pile Length for Load Case 1

 Boundary Condition Type 1, Shear and Moment

Shear = 68000. lb
 Moment = 5342000. in-lb
 Axial Load = 504400. lb

Pile Length feet	Pile Head Deflection inches	Maximum Moment in-lbs	Maximum Shear lbs
95.0000	1.0885729	15806783.	-74367.
95.2000	1.1983304	16925896.	-72003.
95.4000	1.3103308	16252502.	-76044.
95.6000	1.4248824	15849393.	-76599.
95.8000	1.5423868	16137173.	-76263.
96.0000	1.6629132	15570426.	-73593.
96.2000	1.7865600	16008341.	-74765.
96.4000	1.9133183	15724912.	-73563.
96.6000	2.0431851	16094306.	-77931.
96.8000	2.1761440	15823352.	-87647.
97.0000	2.3121639	15326522.	-101070.
97.2000	2.4511637	14348897.	-116689.
97.4000	2.5931428	13839465.	-151447.

Computed Values of Pile Loading and Deflection for Lateral Loading for Load Case Number 2

 Pile-head conditions are Shear and Moment (Loading Type 1)

Shear force at pile head = 53000.0 lbs
 Applied moment at pile head = 4038000.0 in-lbs
 Axial thrust load on pile head = 410100.0 lbs

Res. X	Soil Spr.	Depth	Deflect. y	Bending Moment	Shear Force	Slope	Total Stress	Bending Stiffness
		ft	inches	in-lbs	lbs	radians	psi*	lb-in ²
0.000	0.000	0.00	0.6893	4038000.	53000.	-0.002922	0.000	1.626E+12
0.000	0.000	0.00	0.000	0.000	0.000	0.000	0.000	1.626E+12
0.000	0.950	0.950	0.6562	4655793.	53000.	-0.002891	0.000	1.626E+12
0.000	1.900	0.6234	0.6234	5273433.	52090.	-0.002856	0.000	1.625E+12

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Abut A.1p7o = 2905.6722 -7.715E-07
 2434.2747 -1.281E-06
 1983.9896 -1.595E-06
 1561.4411 -1.750E-06
 1171.5624 -1.779E-06
 817.9654 -1.715E-06
 503.2494 -1.584E-06
 229.3130 -1.414E-06
 -2.2445 -1.225E-06
 -189.4291 -1.036E-06
 -328.0957 -8.617E-07
 -389.5066 -7.141E-07
 -348.4321 -5.977E-07
 -236.9678 -5.093E-07
 -166.5070 -4.398E-07
 -155.0199 -3.837E-07
 -140.6952 -3.400E-07
 -123.6834 -3.076E-07
 -104.0816 -2.851E-07
 -81.9348 -2.710E-07
 -57.2401 -2.634E-07
 -29.9534 -2.604E-07
 0.000 -2.597E-07
 0.000

74.100 0.000174
 -42.1105 2764547.
 75.050 0.000161
 -40.5908 2868056.
 76.000 0.000144
 -38.4066 3031161.
 76.950 0.000125
 -35.7247 3258716.
 77.900 0.000105
 -32.6751 3562857.
 78.850 8.441E-05
 -29.3595 3965213.
 79.800 6.545E-05
 -25.8538 4502873.
 80.750 4.828E-05
 -22.2052 5242761.
 81.700 3.322E-05
 -18.4899 6320463.
 82.650 2.056E-05
 -14.8204 8072968.
 83.600 1.068E-06
 -9.9750 1170683E-06
 84.550 7.917E-07
 -0.8668 13772567E-06
 85.500 6.670E-06
 8.0779 13798559.
 86.450 1.201E-05
 11.4833 10139000.
 87.400 1.838E-05
 0.8793 548318.
 88.350 2.294E-05
 1.1360 564563.
 89.300 2.703E-05
 1.3771 580608.
 90.250 3.069E-05
 1.6074 597053.
 91.200 3.404E-05
 1.8315 613298.
 92.150 3.719E-05
 2.0539 629543.
 93.100 4.022E-05
 2.2785 645788.
 94.050 4.320E-05
 2.5086 662033.
 95.000 4.616E-05
 2.7464 339139.

* This analysis computed pile response using nonlinear moment-curvature relationships.
 Values of total stress due to combined axial and bending stresses are computed only for elastic sections only and do not equal the actual stresses in concrete and steel.
 Stresses in concrete and steel may be interpolated from the output for nonlinear bending properties relative to the magnitude of bending moment developed in the pile.

Output Summary for Load Case No. 1:
 Pile-head deflection = 1.0885729 inches
 Computed slope at pile head = -0.0044629 radians
 Maximum bending moment = 15806783. inch-lbs
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Abut A.1p7o

15.8766	274247.	0.000	0.000	1143.0775	1.423E-05	0.000	1.626E+12	92.150	-7.503E-06	266.1992	Abut A.1p7o	0.000	1.626E+12	
62.700	-0.000484	-356070.	0.000	1877.2492	1.179E-05	0.000	1.626E+12	0.4144	629543.	0.000	-15.1704	-1.458E-08	0.000	1.626E+12
70.2675	1656718.	0.000	0.000	2477.7255	9.510E-06	0.000	1.626E+12	93.100	-7.659E-06	120.2448	-10.3356	-1.322E-08	0.000	1.626E+12
63.650	-0.000336	-338534.	0.000	2943.0114	7.422E-06	0.000	1.626E+12	0.4339	645788.	0.000	-5.2791	-1.270E-08	0.000	1.626E+12
58.5346	1988794.	0.000	0.000	3264.1615	5.569E-06	0.000	1.626E+12	94.050	-7.805E-06	30.6708	0.000	-1.259E-08	0.000	1.626E+12
64.600	-0.000215	-313339.	0.000	3334.4581	3.978E-06	0.000	1.626E+12	0.4532	662033.	0.000	0.000	0.000	0.000	1.626E+12
46.8121	2486811.	0.000	0.000	3159.4429	2.652E-06	0.000	1.626E+12	95.000	-7.948E-06	0.000	0.000	-1.259E-08	0.000	1.626E+12
34.8170	3343554.	0.000	0.000	2885.8020	1.579E-06	0.000	1.626E+12	0.4729	339139.	0.000	0.000	0.000	0.000	1.626E+12
66.500	-4.537E-05	-246348.	0.000	2570.5220	7.367E-07	0.000	1.626E+12	* This analysis computed pile response using nonlinear moment-curvature relationships.						
21.5251	5408132.	0.000	0.000	2237.7999	9.965E-08	0.000	1.626E+12	Values of total stress due to combined axial and bending stresses are computed only for elastic sections only and do not equal the actual stresses in concrete and steel.						
-9.1924	12665638.	0.000	0.000	1902.7993	-3.585E-07	0.000	1.626E+12	Stresses in concrete and steel may be interpolated from the output for nonlinear bending properties relative to the magnitude of bending moment developed in the pile.						
68.400	4.532E-05	-170359.	0.000	1576.0505	-6.646E-07	0.000	1.626E+12	Output Summary for Load Case No. 2:						
-21.5120	5411663.	0.000	0.000	1265.1503	-8.447E-07	0.000	1.626E+12	Pile-head deflection = 0.6893235 inches						
69.350	6.874E-05	-135749.	0.000	975.6171	-9.237E-07	0.000	1.626E+12	Computed slope at pile head = -0.0029216 radians						
-26.4852	4393814.	0.000	0.000	711.3939	-9.246E-07	0.000	1.626E+12	Maximum bending moment = 11451693. inch-lbs						
73.050	5.811E-05	-4907.7425	0.000	475.1844	-8.687E-07	0.000	1.626E+12	Maximum shear force = -55069. lbs						
-24.3589	4779090.	0.000	0.000	268.7061	-7.747E-07	0.000	1.626E+12	Depth of maximum bending moment = 20.9000000 feet below pile head						
76.000	4.738E-05	4635.8484	0.000	92.9155	-6.593E-07	0.000	1.626E+12	Number of iterations = 42						
-29.5552	3958874.	0.000	0.000	-51.7334	-5.364E-07	0.000	1.626E+12	Number of zero deflection points = 3						
72.200	8.359E-05	-53557.	0.000	-164.8730	-4.176E-07	0.000	1.626E+12	Pile-head Deflection vs. Pile Length for Load Case 2						
-29.2169	3984477.	0.000	0.000	-234.1795	-3.120E-07	0.000	1.626E+12	Boundary Condition Type 1, Shear and Moment						
-28.1075	4141735.	0.000	0.000	-254.9547	-2.251E-07	0.000	1.626E+12	Shear = 53000. lb						
74.100	6.844E-05	-17617.	0.000	-240.5279	-1.586E-07	0.000	1.626E+12	Moment = 4038000. in-lb						
-26.4364	4403536.	0.000	0.000	-201.2007	-1.113E-07	0.000	1.626E+12	Axial Load = 410100. lb						
-21.5960	5292467.	0.000	0.000	-144.3136	-8.004E-08	0.000	1.626E+12	Pile Length Deflection Maximum Moment Maximum Shear						
-19.4442	5967026.	0.000	0.000	-74.7182	-6.034E-08	0.000	1.626E+12	95.0000 0.6893235 11451693. -55069.						
-16.7800	6957674.	0.000	0.000	-35.5607	-4.660E-08	0.000	1.626E+12	Computed Values of Pile Loading and Deflection for Lateral Loading for Load Case Number 3						
14.06830	877824E-05	17034.	0.000	-32.0768	-3.570E-08	0.000	1.626E+12	Pile-head conditions are Displacement and Moment (Loading Type 4)						
-11.3168	10366335.	0.000	0.000	-28.2586	-2.737E-08	0.000	1.626E+12	Displacement of pile head = 1.000000 inches						
-8.5750	13643335E-06	16280.	0.000	-24.1488	-2.129E-08	0.000	1.626E+12	Moment at pile head = 5342000.0 in-lbs						
-3.6266	13684591E-06	13848.	0.000	-19.7789	-1.715E-08	0.000	1.626E+12	Axial load at pile head = 504400.0 lbs						
82.650	1.512E-08	10944.	0.000	0.000	0.000	0.000	1.626E+12	depth Deflect. Bending Shear Slope Total Bending Soil						
83.600	-2.114E-06	8036.7509	0.000	0.000	0.000	0.000	1.626E+12	Res. Soil Spr. Distrib. Page 24						
2.5492	13746575.	0.000	0.000	0.000	0.000	0.000	1.626E+12							
84.550	-3.601E-06	5460.9895	0.000	0.000	0.000	0.000	1.626E+12							
4.3503	13772567.	0.000	0.000	0.000	0.000	0.000	1.626E+12							
85.500	-4.651E-06	3450.4147	0.000	0.000	0.000	0.000	1.626E+12							
5.6299	13798559.	0.000	0.000	0.000	0.000	0.000	1.626E+12							
86.450	-5.426E-06	2171.3871	0.000	0.000	0.000	0.000	1.626E+12							
6.5798	13824551.	0.000	0.000	0.000	0.000	0.000	1.626E+12							
87.400	-6.077E-06	1747.4050	0.000	0.000	0.000	0.000	1.626E+12							
0.2899	548318.	0.000	0.000	0.000	0.000	0.000	1.626E+12							
88.350	-6.488E-06	1361.0389	0.000	0.000	0.000	0.000	1.626E+12							
0.3213	564563.	0.000	0.000	0.000	0.000	0.000	1.626E+12							
89.300	-6.841E-06	1016.3872	0.000	0.000	0.000	0.000	1.626E+12							
0.3485	580808.	0.000	0.000	0.000	0.000	0.000	1.626E+12							
90.250	-7.112E-06	716.9977	0.000	0.000	0.000	0.000	1.626E+12							
0.3725	597053.	0.000	0.000	0.000	0.000	0.000	1.626E+12							
91.200	-7.326E-06	465.9943	0.000	0.000	0.000	0.000	1.626E+12							
0.3941	613298.	0.000	0.000	0.000	0.000	0.000	1.626E+12							

Abut A. 1p7o		Abut A. 1p7o	
57.0000	-0.003722	-4807.16	-3179.1278
76.8000	235259.	0.0000	4.956E-05
57.9500	-0.003176	-512243.	-2355.4192
67.7103	243056.	0.0000	4.607E-05
58.7800	-0.002671	-534949.	-1634.4344
58.7800	250854.	0.0000	4.238E-05
50.1297	-0.002209	-549995.	-1013.6588
50.1297	258652.	0.0000	3.857E-05
41.8809	-0.001792	-558504.	-489.1984
41.8809	266449.	0.0000	3.467E-05
34.1387	-0.001419	-561548.	-55.8868
34.1387	274247.	0.0000	3.072E-05
62.7000	-0.001091	-560132.	740.4522
105.5699	1102744.	0.0000	2.678E-05
63.6500	-0.000809	-544973.	1860.1554
90.8693	1281149.	0.0000	2.289E-05
64.6000	-0.000570	-517983.	2812.8048
76.2622	1526547.	0.0000	1.915E-05
65.5500	-0.000372	-481061.	3598.8242
61.6360	1888814.	0.0000	1.563E-05
66.5000	-0.000213	-436110.	4216.0516
46.6495	2495646.	0.0000	1.241E-05
30.1720	8.5917E-05	-385078.	4653.9639
67.4500	-0.000154	0.0000	9.516E-06
65.4000	3838087.	-350109.	4800.2338
-4.5268	13330703.	275713.	4621.6585
-26.8132	424.074E-05	676713.	4621.6585
74.7200	0.000115	-22791.	4273.6337
34.7438	3399509.	0.0000	3.106E-06
-37.9758	3065479.	178310.	3861.9820
72.2000	0.001153	-136757.	3419.9847
-39.5676	2942184.	0.0000	5.790E-07
-39.7113	2931562.	-100341.	2968.0953
74.1000	0.000147	0.0000	-2.553E-07
-38.8093	2999713.	-69082.	2520.5281
-37.1314	3135284.	0.0000	-8.515E-07
76.0000	0.000119	-21469.	2087.6660
-34.8741	3338247.	0.0000	-1.245E-06
76.9500	0.000101	-4605.4517	1677.2347
-32.1880	3616843.	0.0000	-1.472E-06
77.9000	8.344E-05	8074.8320	1294.9806
-29.1918	3988101.	0.0000	-1.551E-06
-25.9783	4481478.	0.0000	945.1153
-22.6158	5147841.	0.0000	-1.463E-06
-19.1437	6081570.	0.0000	630.6456
82.6500	1.352E-05	0.0000	353.6597
-11.7520	9907261.	0.0000	-1.324E-06
-6.2808	13746575.	0.0000	115.6306
1.8416	13772567.	0.0000	-1.157E-06
8.4667	13748892.	0.0000	-82.1611
86.4500	-1.160E-05	8421.4167	-237.8201
			-8.109E-07
			-340.6074
			-365.9111
			-307.1538
			-196.8453
			-3.724E-07

Abut A. 1p7o		Abut A. 1p7o	
10.8856	10694332.	0.0000	0.0000
87.4000	-1.551E-05	6886.7007	-130.5444
0.7461	548318.	0.0000	-3.186E-07
88.3500	-1.887E-05	5448.6688	-120.9657
0.9344	564563.	0.0000	-2.752E-07
89.3000	-2.179E-05	4131.8482	-109.3130
1.1100	580808.	0.0000	-2.415E-07
90.2500	-2.437E-05	2959.1097	-95.7103
1.2765	597053.	0.0000	-2.165E-07
91.2000	-1.672E-05	1952.1429	-80.2400
1.4376	613298.	0.0000	-1.992E-07
92.1500	-2.892E-05	1131.9291	-62.9439
1.5968	629543.	0.0000	-1.884E-07
93.1000	-3.102E-05	519.1880	-43.8269
1.7571	645788.	0.0000	-1.826E-07
94.0500	-3.308E-05	134.7750	-22.8623
1.9209	662033.	0.0000	-1.803E-07
95.0000	-3.513E-05	0.0000	0.0000
2.0900	339139.	0.0000	-1.798E-07

* This analysis computed pile response using nonlinear moment-curvature relationships. Values of total stress due to combined axial and bending stresses are computed only for elastic sections only and do not equal the actual stresses in concrete and steel. Stresses in concrete and steel may be interpolated from the output for nonlinear bending properties relative to the magnitude of bending moment developed in the pile.

Output Summary for Load Case No. 3:

Pile-head deflection	=	1.0000000 inches
Computed slope at pile head	=	-0.0041421 radians
Maximum bending moment	=	14953248. lb-ft
Maximum shear force	=	14953248. lb
Depth of maximum bending moment	=	21.8500000 feet below pile head
Depth of maximum shear force	=	35.1500000 feet below pile head
Number of iterations	=	42
Number of zero deflection points	=	3

----- Pile-head Deflection vs. Pile Length for Load Case 3 -----

Boundary Condition Type 4, Deflection and Moment

Deflection =	1.000000 in	Maximum Moment	14953248. lb-ft
Moment =	5342000. in-lb	Maximum Shear	15006913. lb
Axial Load =	504400. lb		

Pile Length feet	Pile Head Deflection inches	Maximum Moment in-lbs	Maximum Shear lbs
95.0000	1.0000000	14953248.	-70507.
90.2500	1.0000000	15006913.	-70577.
85.5000	1.0000000	15060170.	-70767.
80.7500	1.0000000	15140081.	-71104.

76.0000	1.0000000	15034710.	-70581.	14.250	0.5910	16803268.	42180.	-0.004372	0.000	1.160E+12
71.2500	1.0000000	14976702.	-70911.	-255.0273	4918.9887	0.000	39265.	-0.004204	0.000	1.153E+12
66.5000	1.0000000	14984909.	-70395.	15.2000	0.5421	17292211.	36340.	-0.004031	0.000	1.147E+12
61.7500	1.0000000	15063200.	-70598.	-256.2800	5389.0500	0.000	33412.	-0.003852	0.000	1.142E+12
57.0000	1.0000000	14999825.	-70295.	16.1500	0.4952	17746866.	30488.	-0.003668	0.000	1.137E+12
52.2500	1.0000000	14983188.	-72217.	-256.8908	5914.1248	0.000	27576.	-0.003480	0.000	1.132E+12
47.5000	1.0000000	14436485.	-78794.	17.1000	0.4502	18167120.	24684.	-0.003288	0.000	1.129E+12
42.7500	1.0000000	14034685.	-83139.	-256.8456	6503.3532	0.000	18171.	-0.003092	0.000	1.126E+12
38.0000	1.0000000	13023097.	-78816.	18.0500	0.4074	18552952.	8117.9746	-0.002893	0.000	1.124E+12
33.2500	1.0000000	10521778.	-63547.	-256.1301	7167.8308	0.000	-1592.3965	-0.002693	0.000	1.123E+12
28.5000	1.0000000	6109165.	-46782.	-254.7299	7921.1248	0.000	-10648.	-0.002493	0.000	1.124E+12
23.7500	1.0000000	5448267.	-38521.	19.9500	0.3280	19221703.	-19273.	-0.002295	0.000	1.125E+12
19.0000	1.0000000	5342000.	-44514.	-252.6309	8779.9463	0.000	-27812.	-0.002099	0.000	1.128E+12
				20.9000	0.2916	19505031.	-36165.	-0.001906	0.000	1.133E+12
				-889.9777	34788.	0.000	-44189.	-0.001719	0.000	1.138E+12
				21.8500	0.2575	19671562.	-51846.	-0.001537	0.000	1.145E+12
				-873.7369	38678.	0.000	-59165.	-0.001363	0.000	1.153E+12
				22.8000	0.2257	19723394.	-66085.	-0.001196	0.000	1.164E+12
				-829.8369	41918.	0.000	-72480.	-0.001038	0.000	1.177E+12
				23.7500	0.1961	19666229.	-78526.	-0.000890	0.000	1.192E+12
				-758.8711	44112.	0.000	-83944.	-0.000753	0.000	1.211E+12
				24.7000	0.1688	19509295.	-88177.	-0.000627	0.000	1.234E+12
				-754.1985	50926.	0.000	-91050.	-0.000512	0.000	1.261E+12
				25.6500	0.1438	19233208.	-91337.	-0.000419	0.000	1.611E+12
				-744.0413	58987.	0.000	-89133.	-0.000345	0.000	1.613E+12
				26.6000	0.1210	18899307.	-85911.	-0.000279	0.000	1.615E+12
				-721.3467	67975.	0.000	-82080.	-0.000219	0.000	1.616E+12
				27.5500	0.1003	18450566.	-77836.	-0.000166	0.000	1.618E+12
				-686.3673	77991.	0.000	-73303.	-0.000119	0.000	1.619E+12
				28.5000	0.0818	17911562.	-68574.	-7.854E-05	0.000	1.619E+12
				-656.9089	91367.	0.000	-63721.	-4.322E-05	0.000	1.620E+12
				-627.1933	109536.	0.000	-58801.	-1.301E-05	0.000	1.620E+12
				-586.7950	131009.	0.000				
				-535.1118	1605280	1579370.				
				-525.4661	221548.	0.000				
				-425.1640	273817.	14013036				
				-317.4484	34200.	0.000				
				-186.5543	35150.	0.000				
				36.1000	0.003408	12009808.				
				136.1289	854980	0.000				
				250.6633	464394	0.000				
				314.5798	370048	8934100.				
				357.4161	325701	0.000				
				387.2765	300591.	0.000				
				407.9510	285358.	0.000				
				421.6382	276096.	0.000				
				429.7811	270865.	0.000				
				43.7000	-0.0184	3942913.				

Computed Values of Pile Loading and Deflection
for Lateral Loading for Load Case Number 4

Pile-head conditions are Displacement and Moment (Loading Type 4)
 Displacement of pile head = 1.500000 inches
 Moment at pile head = 5342000.0 in-lbs
 Axial load at pile head = 504400.0 lbs

Res. X	Depth	Deflect.	Bending	Shear	Slope	Total	Bending	Soil
ft	ft	inches	in-lbs	lbs	radians	psi*	lb-inn2	lb/in
0.000	0.00	0.00	0.00	85768.	-0.005908	0.000	1.619E+12	0.000
0.000	0.950	0.00	0.00	85768.	-0.005867	0.000	1.619E+12	0.000
-202.	1.900	1691.1891	7364974.	84612.	-0.005819	0.000	1.617E+12	0.000
-444.	2.850	3899.3930	8349693.	80922.	-0.005763	0.000	1.616E+12	0.000
-699.	3.800	6461.7290	9276276.	74398.	-0.005701	0.000	1.614E+12	0.000
-209.	4.750	2041.8243	10111520.	69213.	-0.005633	0.000	1.612E+12	0.000
-216.	5.700	1064.8243	10919114.	66783.	-0.005558	0.000	1.611E+12	0.000
-223.	6.650	2233.7786	11698089.	64274.	-0.005467	0.000	1.271E+12	0.000
-229.	7.600	2440.1876	12447432.	61694.	-0.005358	0.000	1.249E+12	0.000
-234.	8.550	2663.0511	13166317.	59048.	-0.005240	0.000	1.230E+12	0.000
-239.	9.500	2904.6691	13853992.	56344.	-0.005114	0.000	1.214E+12	0.000
-243.	10.450	3167.5665	14509781.	53589.	-0.004980	0.000	1.200E+12	0.000
-247.	11.400	3454.6048	15133086.	50788.	-0.004838	0.000	1.188E+12	0.000
-250.	12.350	3769.0803	15723384.	47948.	-0.004690	0.000	1.178E+12	0.000
-253.	13.300	4114.8305	16280232.	45076.	-0.004534	0.000	1.169E+12	0.000

Abut A. 1p70		Abut A. 1p70		Abut A. 1p70	
433.4072	268599.	0.000	0.000	-191687.	4690.9739
44.650	-0.0184	3300741.	0.000	0.000	3.640E-07
433.2912	268672.	0.000	0.000	-141718.	4077.2149
45.600	-0.0181	2714745.	0.000	0.000	-8.092E-07
430.0423	270702.	0.000	0.000	-98717.	3473.5613
46.550	-0.0176	2184528.	0.000	0.000	-1.655E-06
424.1549	274460.	0.000	0.000	-62501.	2891.1043
47.500	-0.0169	1709346.	0.000	0.000	-2.222E-06
416.0392	279814.	0.000	0.000	-32775.	2338.3627
48.450	-0.0161	1288163.	0.000	0.000	-2.558E-06
406.0411	286704.	0.000	0.000	-9157.3773	1821.9095
49.400	-0.0152	919697.	0.000	0.000	-2.705E-06
394.4550	295126.	0.000	0.000	8795.9323	1346.8264
50.350	-0.0143	602457.	0.000	0.000	-2.600E-06
381.5319	305122.	0.000	0.000	21581.	917.0864
367.4845	316786.	0.000	0.000	29735.	535.9397
209.4798	196271.	0.000	0.000	33829.	206.4023
198.7121	204068.	0.000	0.000	34467.	-67.9431
186.6016	211866.	0.000	0.000	32302.	-281.1241
173.4192	219664.	0.000	0.000	28077.	-414.7112
159.4334	227461.	0.000	0.000	22864.	-400.9888
144.5068	235259.	0.000	0.000	18950.	-337.4163
130.0239	243056.	0.000	0.000	13584.	-320.4648
115.2338	250854.	0.000	0.000	0.000	-296.0964
100.5788	258652.	0.000	0.000	0.000	-264.5512
86.2801	266449.	0.000	0.000	0.000	-225.9579
72.6015	274247.	0.000	0.000	0.000	-180.3347
62.700	-0.002413	873700.	0.000	0.000	-127.5958
56.9626	741588.	0.000	0.000	0.000	-67.5655
63.650	-0.001879	867982.	0.000	0.000	0.000
138.5077	840508.	0.000	0.000	0.000	0.000
64.600	-0.001414	-844229.	0.000	0.000	0.000
120.1515	968823.	0.000	0.000	0.000	0.000
65.550	-0.001016	-804826.	0.000	0.000	0.000
101.8823	1142676.	0.000	0.000	0.000	0.000
66.500	-0.000684	-752151.	0.000	0.000	0.000
83.5644	1393175.	0.000	0.000	0.000	0.000
67.450	-0.000411	-688585.	0.000	0.000	0.000
64.8245	1795962.	0.000	0.000	0.000	0.000
68.400	-0.000194	-616566.	0.000	0.000	0.000
44.5598	2612873.	0.000	0.000	0.000	0.000
69.350	-2.662E-05	-538732.	0.000	0.000	0.000
16.5549	7037397.	0.000	0.000	0.000	0.000
70.300	9.756E-05	-458724.	0.000	0.000	0.000
-31.5607	3687966.	0.000	0.000	0.000	0.000
71.250	0.000185	-382799.	0.000	0.000	0.000
-43.4786	2677323.	0.000	0.000	0.000	0.000
72.200	0.000242	-312510.	0.000	0.000	0.000
-49.7100	2341779.	0.000	0.000	0.000	0.000
73.150	0.000274	-248668.	0.000	0.000	0.000
-52.8748	2201648.	0.000	0.000	0.000	0.000

* This analysis computed pile response using nonlinear moment-curvature relationships. Values of total stress due to combined axial and bending stresses are computed only for elastic sections only and do not equal the actual stresses in concrete and steel. Stresses in concrete and steel may be interpolated from the output for nonlinear bending properties relative to the magnitude of bending moment developed in the pile.

Output Summary for Load Case No. 4:

Pile-head deflection = 1.5000000 inches
Computed slope at pile head = -0.0059081 radians
Maximum bending moment = 19723394. inch-lbs

Maximum shear force = -91337 lbs
 Depth of maximum bending moment = 22.800000 feet below pile head
 Moment at pile head = 36.1000000 feet below pile head
 Number of iterations = 22
 Number of zero deflection points = 3

Abut A.1p7o
 Pile-head Deflection vs. Pile Length for Load Case 4

Boundary Condition Type 4, Deflection and Moment

Deflection = 1.50000 in
 Moment = 5342000.0 in-lb
 Axial Load = 504400.0 lb

Pile Length feet	Pile Head Deflection inches	Maximum Moment in-lb	Maximum Shear lbs
95.0000	1.500000	19723394.	-91337.
90.2500	1.500000	19751686.	-91392.
85.5000	1.500000	19799223.	-91670.
80.7500	1.500000	19859304.	-92161.
76.0000	1.500000	19787069.	-91782.
71.2500	1.500000	19728736.	-91827.
66.5000	1.500000	19751693.	-91536.
61.7500	1.500000	19751693.	-91331.
57.0000	1.500000	19751693.	-91331.
52.2500	1.500000	19751693.	-91331.
47.5000	1.500000	1829426.	-10478.
42.7500	1.500000	1817098.	-107709.
38.0000	1.500000	12348109.	-96737.
33.2500	1.500000	8818748.	-77409.
28.5000	1.500000	6516878.	-54913.
23.7500	1.500000	5593769.	-42906.
19.0000	1.500000	5342000.	-48904.

Pile Length feet	0.000	1.900	0.000	0.000	1.8270	0.000	7837778.	0.000	1.617E+12
95.0000	-228.6856	1426.9558	0.000	0.000	1.7414	9055496.	0.000	1.00164.	0.000
90.2500	-502.6712	3290.7891	0.000	0.000	1.6565	10207520.	0.000	92792.	0.000
85.5000	-790.6579	5441.3800	0.000	0.000	1.5724	11256374.	0.000	86967.	0.000
80.7500	-231.2840	1676.8148	0.000	0.000	1.4895	12274596.	0.000	84284.	0.000
76.0000	-239.3819	1832.1498	0.000	0.000	1.4078	13261066.	0.000	81513.	0.000
71.2500	-246.8086	1998.5518	0.000	0.000	1.3276	14214753.	0.000	78660.	0.000
66.5000	-253.6098	2177.7640	0.000	0.000	1.2489	15134709.	0.000	75734.	0.000
61.7500	-259.8010	2371.5504	0.000	0.000	1.1718	16020066.	0.000	72740.	0.000
57.0000	-265.3842	2581.8341	0.000	0.000	1.0965	16870039.	0.000	69687.	0.000
52.2500	-270.3544	2810.7821	0.000	0.000	1.0231	17689322.	0.000	66580.	0.000
47.5000	-274.7027	3060.8794	0.000	0.000	0.9517	18461095.	0.000	63427.	0.000
42.7500	-278.4182	3335.0060	0.000	0.000	0.8824	19201021.	0.000	60236.	0.000
38.0000	-281.4881	3636.5264	0.000	0.000	0.8153	19903250.	0.000	57013.	0.000
33.2500	-283.18986	3969.3984	0.000	0.000	0.7506	20567420.	0.000	53767.	0.000
28.5000	-285.16353	4336.3069	0.000	0.000	0.6882	21193239.	0.000	50504.	0.000
23.7500	-286.18278	4748.8356	0.000	0.000	0.6283	21780988.	0.000	47234.	0.000
19.0000	-287.10250	5207.6663	0.000	0.000	0.5710	22329370.	0.000	43964.	0.000
14.2500	-286.6478	5722.8914	0.000	0.000	0.5163	22839466.	0.000	40703.	0.000
9.5000	-285.5333	6304.3132	0.000	0.000	0.4644	23311133.	0.000	37458.	0.000
4.7500	-283.6660	6963.9424	0.000	0.000	0.4152	23745338.	0.000	29933.	0.000
0.0000	-1036.6431	78464.	0.000	0.000	0.3688	24041786.	0.000	18133.	0.000
0.0000	-1033.4383	319423	0.000	0.000	0.3254	24203273.	0.000	6546.9353	0.000
0.0000	-999.2484	350114	0.000	0.000	0.2848	24233438.	0.000	4468.8713	0.000
0.0000	-933.3492	37359.	0.000	0.000	0.2472	24140836.	0.000	-15128.	0.000
0.0000	-936.7242	43206.	0.000	0.000	0.2124	23925038.	0.000	-25785.	0.000
0.0000	-932.9209	50073.	0.000	0.000	0.1805	23586552.	0.000	-36313.	0.000
0.0000	-913.9996	57726.	0.000	0.000	0.1514	23127862.	0.000	-46538.	0.000
0.0000	-879.9276	66245.	0.000	0.000	0.1251	22553427.	0.000	-56402.	0.000
0.0000	-850.6295	77514.	0.000	0.000	0.1015	21867096.	0.000	-65925.	0.000
0.0000	-820.0606	92149.	0.000	0.000	0.0804	21072889.	0.000	-75025.	0.000
0.0000	-776.4390	110118.	0.000	0.000			0.000		

Computed Values of Pile Loading and Deflection for Lateral Loading for Load Case Number 5

Pile-head conditions are Displacement and Moment (Loading Type 4)
 Displacement of pile head = 2.000000 inches
 Moment at pile head = 5342000.0 in-lb
 Axial load at pile head = 504400.0 lbs

Depth X feet	Deflect. Y inches	Bending Moment in-lb	Shear Force lbs	slope S radians	Total Stress psi*	Bending Stiffness lb-in ²	Soil p lb/in
0.000	2.0000	5342000.	105636.	0.007631	0.000	1.619E+12	
0.950	1.9132	6590023.	105636.	-0.007589	0.000	1.619E+12	

STRL CAPACITY
 @ 2" DEFLECTION

Abut A. 1p7o		Abut A. 1p7o	
-719.0811	0.0618	20176532.	0.000
31.350	132692.	0.000	1.118E+12
-719.0811	0.0455	19185539.	0.000
32.300	170754.	0.000	1.129E+12
-681.8282	0.0315	18104823.	0.000
33.250	203366.	0.000	1.142E+12
-566.3365	0.0195	16949388.	0.000
34.200	261033.	0.000	1.158E+12
-446.0694	0.009393	15735024.	0.000
35.150	379966.	0.000	1.178E+12
-309.7719	0.001041	14479525.	0.000
36.100	1131122.	0.000	1.201E+12
-103.3054	-0.005744	13209810.	0.000
37.050	480525.	0.000	1.229E+12
242.1061	-0.0111	11970855.	0.000
38.000	345221.	0.000	1.262E+12
337.1071	294599.	0.000	1.161E+12
395.0722	267274.	0.000	1.129E+12
39.900	-0.0186	9630228.	0.000
435.4844	8541572.	0.000	1.613E+12
40.850	-0.0211	8541572.	0.000
463.9935	250859.	0.000	1.615E+12
41.800	-0.0229	7512869.	0.000
483.6488	240669.	0.000	1.617E+12
42.750	-0.0241	6546717.	0.000
496.3634	234507.	0.000	1.618E+12
43.700	-0.0248	5644807.	0.000
503.4363	231205.	0.000	1.619E+12
44.650	-0.0251	4808096.	0.000
505.8287	2309549.	0.000	1.620E+12
504.4391	23058245	0.000	1.620E+12
499.6764	232959.	0.000	1.620E+12
47.500	236546.	0.000	1.620E+12
492.1027	214140.	0.000	1.620E+12
48.450	-0.0228	2113100.	0.000
482.1301	241440.	0.000	1.620E+12
49.400	-0.0216	1598556.	0.000
470.1091	247614.	0.000	1.620E+12
50.350	-0.0204	1145043.	0.000
456.3397	255087.	0.000	1.620E+12
51.300	-0.0191	750790.	0.000
441.0796	263913.	0.000	1.620E+12
52.250	-0.0177	413828.	0.000
303.9001	196271.	0.000	1.620E+12
290.2920	204068.	0.000	1.620E+12
54.150	-0.0148	143416.	0.000
274.5479	211866.	0.000	1.620E+12
55.100	-0.0133	367491.	0.000
257.0500	219664.	0.000	1.620E+12
56.050	-0.0119	558146.	0.000
238.1807	227461.	0.000	1.620E+12
218.3162	235259.	0.000	1.620E+12
57.950	-0.009278	849100.	0.000
197.8215	243056.	0.000	1.620E+12
58.900	-0.008046	954633.	0.000
177.0465	250854.	0.000	1.620E+12
59.850	-0.006890	1037118.	0.000
156.3231	258652.	0.000	1.620E+12
60.800	-0.005817	1099246.	0.000
135.9632	266449.	0.000	1.620E+12
61.750	-0.004833	0.000	1.620E+12
116.2573	274247.	0.000	1.620E+12
62.700	-0.003940	0.000	1.620E+12
200.5809	580384.	0.000	1.620E+12
63.650	-0.003141	0.000	1.620E+12
179.1009	649998.	0.000	1.620E+12
64.600	-0.002437	0.000	1.620E+12
157.7498	737986.	0.000	1.620E+12
65.550	-0.001825	0.000	1.620E+12
136.5275	852718.	0.000	1.620E+12
115.3605	1009208.	0.000	1.620E+12
94.0315	1238179.	0.000	1.620E+12
71.9802	1617627.	0.000	1.620E+12
47.4914	2452298.	0.000	1.620E+12
-1.6142	13382687.	0.000	1.620E+12
-71.250	0.000167	-599440.	0.000
-41.3265	2815862.	0.000	1.620E+12
-53.9561	2157163.	0.000	1.620E+12
-60.8485	1913072.	0.000	1.620E+12
-74.100	0.000407	-333679.	0.000
-64.4508	1806273.	0.000	1.620E+12
-65.5173	1768887.	0.000	1.620E+12
-65.5244	176305.	-396955.	0.000
-64.0929	18690401	-141375.	0.000
-61.5792	1892637	94110.	0.000
-58.2727	1998853	54837.	0.000
-54.4117	2140819.	-23136.	0.000
-50.0656	2327147.	14957949	0.000
-45.3178	2571700.	18621.	0.000
-40.2103	2899548.	31855.	0.000
-34.7289	3359329.	38863.	0.000
-28.7595	4061060.	41355.	0.000
-21.9537	5333001.	40109.	0.000
-13.0250	9085320.	36007.	0.000
0.5461	548318.	30212.	0.000
88.350	-3.663E-05	24486.	0.000
89.300	-5.993E-05	18995.	0.000
3.0536	580808.	0.000	1.620E+12
90.250	-8.172E-05	13900.	0.000
4.2799	597053.	0.000	1.620E+12

Abut. A.1p7c

91.200	-0.000102	9360.1433	-367.7089	-1.780E-06	0.000	1.620E+12	0.000	1.623E+12
5.5083	613298.	0.000						0.000
92.150	-0.000122	5536.2403	-297.8125	-1.728E-06	0.000	1.620E+12	0.000	1.623E+12
6.7542	629543.	0.000						0.000
93.100	-0.000142	2589.8885	-213.5330	-1.699E-06	0.000	1.620E+12	0.000	1.622E+12
8.0317	645788.	0.000						0.000
94.050	-0.000161	687.2277	-114.4428	-1.688E-06	0.000	1.620E+12	0.000	1.622E+12
9.3526	662033.	0.000						0.000
95.000	-0.000180	0.000	0.000	-1.685E-06	0.000	1.620E+12	0.000	1.621E+12
10.7251	339139.	0.000						0.000

* This analysis computed pile response using nonlinear moment-curvature relationships. Values of total stress due to combined axial and bending stresses are computed only for elastic sections only and do not equal the actual stresses in concrete and steel. Stresses in concrete and steel may be interpolated from the output for nonlinear bending properties relative to the magnitude of bending moment developed in the pile.

Output Summary for Load Case No. 5:

Pile-head deflection = 2.0000000 inches
 Computed slope at pile head = -0.0076307 radians
 Maximum bending moment = 24233438. inch-lbs
 Maximum shear force = -111090. lbs
 Depth of maximum bending moment = 23.7500000 feet below pile head
 Depth of maximum shear force = 36.1000000 feet below pile head
 Number of iterations = 12
 Number of zero deflection points = 3

Computed values of Pile Loading and Deflection for Lateral Loading for Load Case Number 6

Res. X	Depth	Deflect.	Bending	Shear	Slope	Total	Bending	Soil
feet	feet	inches	in-lbs	lbs	radians	psi*	lb-in^2	lb/in
Es*H	Lat. Load	Distri.	Moment	Force	S	Stress	Stiffness	p
lb/inch	lb/inch	lb/inch	in-lbs	lbs	radians	psi*	lb-in^2	lb/in
0.000	0.000	0.5000	4038000.	44561.	-0.002194	0.000	1.626E+12	
0.000	0.950	0.4751	4556190.	44561.	-0.002164	0.000	1.626E+12	
	1.900	0.4507	5074231.	43727.	-0.002130	0.000	1.625E+12	
	2.850	3701.8125	0.000	41083.	-0.002093	0.000	1.625E+12	
	3.800	0.4029	6030490.	36436.	-0.002052	0.000	1.624E+12	
	-497.6121	14079.	0.000					

Abut. A.1p7c

32779.	-0.002009	6423024.	4.750	0.3798	0.000	1.618E+12	0.000	1.618E+12
31110.	-0.001962	6796628.	-144.0357	4323.5389	0.000	1.618E+12	0.000	1.618E+12
29391.	-0.001913	7150682.	5.700	0.3571	0.000	1.618E+12	0.000	1.618E+12
27625.	-0.001862	7484623.	-148.7174	4747.0612	0.000	1.618E+12	0.000	1.618E+12
25819.	-0.001808	7797946.	6.650	0.3350	0.000	1.618E+12	0.000	1.618E+12
23976.	-0.001752	8090198.	-152.9492	5204.1159	0.000	1.618E+12	0.000	1.618E+12
22101.	-0.001694	8360979.	7.600	0.3135	0.000	1.618E+12	0.000	1.618E+12
20199.	-0.001634	8609945.	-156.7610	5699.9787	0.000	1.618E+12	0.000	1.618E+12
18275.	-0.001573	8836805.	8.550	0.2926	0.000	1.618E+12	0.000	1.618E+12
16333.	-0.001510	9041324.	-160.1635	6240.1428	0.000	1.618E+12	0.000	1.618E+12
14379.	-0.001446	9223322.	9.500	0.2723	0.000	1.618E+12	0.000	1.618E+12
12417.	-0.001380	9382678.	-163.1590	6830.7074	0.000	1.618E+12	0.000	1.618E+12
10452.	-0.001314	9519328.	10.450	0.2527	0.000	1.618E+12	0.000	1.618E+12
8490.0923	-0.001246	9633268.	-165.7452	7478.6416	0.000	1.618E+12	0.000	1.618E+12
6336.0958	-0.001178	9724553.	11.400	0.2337	0.000	1.618E+12	0.000	1.618E+12
4595.4934	-0.001109	9793304.	-167.9177	8192.0309	0.000	1.618E+12	0.000	1.618E+12
2673.8267	-0.001040	9839700.	12.350	0.2154	0.000	1.618E+12	0.000	1.618E+12
1249.9108	-0.000970	9863889.	-169.6705	8980.3535	0.000	1.618E+12	0.000	1.618E+12
6993.3241	-0.000901	9820273.	13.300	0.1978	0.000	1.618E+12	0.000	1.618E+12
12239.	-0.000832	972866.	-170.9966	9854.8108	0.000	1.618E+12	0.000	1.618E+12
16879.	-0.000764	9548559.	14.250	0.1810	0.000	1.618E+12	0.000	1.618E+12
21071.	-0.000698	9355264.	-171.8882	10829.	0.000	1.618E+12	0.000	1.618E+12
25117.	-0.000633	9074854.	15.200	0.1648	0.000	1.618E+12	0.000	1.618E+12
28971.	-0.000570	8768514.	-172.3370	11918.	0.000	1.618E+12	0.000	1.618E+12
32565.	-0.000509	8419442.	16.150	0.1495	0.000	1.618E+12	0.000	1.618E+12
35896.	-0.000452	8030787.	-172.3342	13142.	0.000	1.618E+12	0.000	1.618E+12
38899.	-0.000397	7605245.	17.100	0.1349	0.000	1.618E+12	0.000	1.618E+12
41357.	-0.000345	7147597.	-171.8704	14525.	0.000	1.618E+12	0.000	1.618E+12
43167.	-0.000296	6665517.	18.050	0.1211	0.000	1.618E+12	0.000	1.618E+12
45142.	-0.000251	6166155.	-170.9360	16095.	0.000	1.618E+12	0.000	1.618E+12
47168.	-0.000210	5638617.	19.000	0.1080	0.000	1.618E+12	0.000	1.618E+12
47681.	-0.000172	5092695.	-169.5206	17887.	0.000	1.618E+12	0.000	1.618E+12
			167.6139	19948.	0.000	1.618E+12	0.000	1.618E+12
			-20.100	20843	0.000	1.618E+12	0.000	1.618E+12
			-320.7611	70396.	0.000	1.618E+12	0.000	1.618E+12
			-486.5583	75407	0.000	1.618E+12	0.000	1.618E+12
			-436.6680	7807638	0.000	1.618E+12	0.000	1.618E+12
			-373.7565	77899.	0.000	1.618E+12	0.000	1.618E+12
			-361.7071	88927.	0.000	1.618E+12	0.000	1.618E+12
			-348.0336	102281.	0.000	1.618E+12	0.000	1.618E+12
			-328.1378	117111.	0.000	1.618E+12	0.000	1.618E+12
			-302.4361	133650.	0.000	1.618E+12	0.000	1.618E+12
			-281.8062	158042.	0.000	1.618E+12	0.000	1.618E+12
			-245.1250	180264.	0.000	1.618E+12	0.000	1.618E+12
			-186.1802	188061.	0.000	1.618E+12	0.000	1.618E+12
			-131.3059	195859.	0.000	1.618E+12	0.000	1.618E+12
			-215.2399	541288.	0.000	1.618E+12	0.000	1.618E+12
			-140.0396	832739.	0.000	1.618E+12	0.000	1.618E+12
			34.200	-0.000248	0.000	1.618E+12	0.000	1.618E+12

Abut A. 1p70			Abut A. 1p70		
50.0009	2300097.	0.000	64.600	-8.512E-05	-211170.
35.150	-0.002005	4553104.	29.5875	3962594.	0.000
143.0101	812924.	0.000	65.550	-3.238E-05	-183652.
36.100	-0.003399	4031949.	18.3296	6452539.	0.000
186.2438	624623.	0.000	66.500	5.675E-06	-153746.
37.050	-0.004470	3534866.	-6.6100	13278719.	0.000
213.6132	544725.	0.000	67.450	3.145E-05	-124694.
38.000	-0.005259	3065428.	-17.8243	6461911.	0.000
231.7094	502250.	0.000	68.400	4.725E-05	-97954.
243.4048	478159.	0.000	-21.9052	5285075.	0.000
250.3183	464984.	0.000	-23.7057	4893486.	0.000
253.4998	459174.	0.000	-24.1572	4807640.	0.000
253.6946	458844.	0.000	-23.6992	4904719.	0.000
251.4661	462932.	0.000	-22.5970	5147662.	0.000
247.2601	470828.	0.000	-21.0335	5534151.	0.000
241.4416	482196.	0.000	-19.1447	6084387.	0.000
234.3170	496680.	0.000	-17.0520	2.838E-05	6082.4725
226.1620	514852.	0.000	-17.0369	6843060.	0.000
217.1620	536184.	0.000	-14.7943	7888134.	10312.
207.3538	561038.	0.000	-12.4834	9360135.	12619.
197.4215	5860649.	0.000	-10.1309	11351078.	0.000
187.1030	62373427	0.000	-7.0834	13616613.	12667.
176.5496	659677.	0.000	-3.3857	1366596E-07	0.000
176.57250	659677.	0.000	-0.7585	1366596E-07	9111.9773
46.3563250	196271.	0.000	81.700	8.439E-07	7014.7312
42.1463200	204068.	0.000	1.0138	13694591	5049.0085
54.150	-0.002038	-286005.	2.1181	13720583	3358.3897
55.100	-0.001744	-295110.	2.7400	13746575	0.000
33.6127	219664.	0.000	3.0399	13772567	2023.7508
37.8757	211866	0.000	84.550	-2.516E-06	1084.1167
56.050	-0.001474	-299838.	85.500	-2.599E-06	0.000
29.4186	227461	0.000	3.1452	13798559	533.2008
25.3497	235259	0.000	3.1458	13824551.	0.000
57.000	-0.001228	-300733.	3.1458	13824551.	0.000
21.4567	243056.	0.000	0.1224	400.2.545E-06	431.0963
17.7846	250854.	0.000	88.350	-2.462E-06	324.8891
59.850	-0.000633	-285587.	0.1219	564563.	0.000
60.800	-0.000482	-276181.	0.1199	580808.	234.5193
11.2558	266449.	0.000	0.1166	597053.	0.000
61.750	-0.000352	-265303.	0.1122	613298.	0.000
8.4619	274247.	0.000	92.150	-1.936E-06	54.9940
62.700	-0.000243	-253316.	0.1069	629543.	0.000
49.9071	2340191.	0.000	93.100	-1.784E-06	23.8122
63.650	-0.000155	-234836.	0.1010	645788.	0.000
39.8402	2935215.	0.000	94.050	-1.629E-06	5.7601

Abut A. 1p70			Abut A. 1p70		
2247.1046	5.366E-06	0.000	2247.1046	5.366E-06	0.000
2520.2317	3.982E-06	0.000	2520.2317	3.982E-06	0.000
2587.0336	2.800E-06	0.000	2587.0336	2.800E-06	0.000
2447.7585	1.823E-06	0.000	2447.7585	1.823E-06	0.000
2221.3007	1.043E-06	0.000	2221.3007	1.043E-06	0.000
1961.3186	4.400E-07	0.000	1961.3186	4.400E-07	0.000
1688.4996	-6.214E-09	0.000	1688.4996	-6.214E-09	0.000
1415.7180	-3.175E-07	0.000	1415.7180	-3.175E-07	0.000
1151.8295	-5.156E-07	0.000	1151.8295	-5.156E-07	0.000
903.1353	-6.217E-07	0.000	903.1353	-6.217E-07	0.000
674.1191	-6.555E-07	0.000	674.1191	-6.555E-07	0.000
467.8840	-6.355E-07	0.000	467.8840	-6.355E-07	0.000
286.4462	-5.780E-07	0.000	286.4462	-5.780E-07	0.000
130.9628	-4.976E-07	0.000	130.9628	-4.976E-07	0.000
1.9470	-4.067E-07	0.000	1.9470	-4.067E-07	0.000
-96.2886	-3.157E-07	0.000	-96.2886	-3.157E-07	0.000
-156.0193	-2.324E-07	0.000	-156.0193	-2.324E-07	0.000
-179.6984	-1.615E-07	0.000	-179.6984	-1.615E-07	0.000
-178.2434	-1.049E-07	0.000	-178.2434	-1.049E-07	0.000
-160.3915	-6.265E-08	0.000	-160.3915	-6.265E-08	0.000
-132.7003	-3.318E-08	0.000	-132.7003	-3.318E-08	0.000
-99.7547	-1.431E-08	0.000	-99.7547	-1.431E-08	0.000
-64.4992	-3.414E-09	0.000	-64.4992	-3.414E-09	0.000
-28.6403	2.326E-09	0.000	-28.6403	2.326E-09	0.000
-10.0113	5.776E-09	0.000	-10.0113	5.776E-09	0.000
-8.6183	8.426E-09	0.000	-8.6183	8.426E-09	0.000
-7.2398	1.039E-08	0.000	-7.2398	1.039E-08	0.000
-5.8920	1.177E-08	0.000	-5.8920	1.177E-08	0.000
-4.5882	1.268E-08	0.000	-4.5882	1.268E-08	0.000
-3.3393	1.322E-08	0.000	-3.3393	1.322E-08	0.000
-2.1538	1.350E-08	0.000	-2.1538	1.350E-08	0.000
-1.0388	1.360E-08	0.000	-1.0388	1.360E-08	0.000

0.0946 662033. 0.000 0.000 1.362E-08 0.000 1.626E+12
 95.000 -1.473E-06 0.000
 0.0877 339139. 0.000

Abut A.1p7o
 Computed Values of Pile Loading and Deflection
 for Lateral Loading for Load Case Number 7

* This analysis computed pile response using nonlinear moment-curvature relationships.
 Values of total stress due to combined axial and bending stresses are computed only for elastic sections only and do not equal the actual stresses in concrete and steel.
 Stresses in concrete and steel may be interpolated from the output for nonlinear bending properties relative to the magnitude of bending moment developed in the pile.

Output Summary for Load Case No. 6:

Pile-head deflection. = 0.500000 inches
 Computed slope at pile head = -0.0021942 radians
 Maximum bending moment = 9863989. inch-lbs
 Maximum shear force = -47681. lbs
 Depth of maximum bending moment = 20.900000 feet below pile head
 Depth of maximum shear force = 34.200000 feet below pile head
 Number of iterations = 12
 Number of zero deflection points = 3

Pile-head Deflection vs. Pile Length for Load Case 6

Boundary Condition Type 4, Deflection and Moment

Deflection = 0.500000 in
 Moment = 4038000. in-lb
 Axial Load = 410100. lb

Pile Length feet	Pile Head Deflection inches	Maximum Moment in-lb	Maximum Shear lbs
95.0000	0.500000	9863989.	-47681.
90.2500	0.500000	9887865.	-47604.
85.5000	0.500000	9932187.	-47748.
80.7500	0.500000	10005723.	-48120.
76.0000	0.500000	9937141.	-47608.
71.2500	0.500000	9887895.	-48000.
66.5000	0.500000	9904124.	-47633.
61.7500	0.500000	9948097.	-47859.
57.0000	0.500000	9913982.	-47188.
52.2500	0.500000	9923089.	-47515.
47.5000	0.500000	9680496.	-50415.
42.7500	0.500000	8899378.	-53478.
38.0000	0.500000	7372369.	-50875.
33.2500	0.500000	5772002.	-43372.
28.5000	0.500000	4624257.	-32728.
23.7500	0.500000	4147399.	-28561.
19.0000	0.500000	4038000.	-29785.

Abut A.1p7o
 Computed Values of Pile Loading and Deflection
 for Lateral Loading for Load Case Number 7

Pile-head conditions are Displacement and Moment (Loading Type 4)
 Displacement of pile head = 1.000000 inches
 Moment at pile head = 4038000.0 in-lbs
 Axial load at pile head = 410100.0 lbs

SEA V II
 CAPACITY
 @ 1" DEFLECTION

Depth Res. X	Soil Spr. Y	Deflect. Lat. Load	Bending Moment	Shear Force	Slope	Total stress	Bending stiffness
feet	Es*H	inches	in-lbs	lbs	radians	psi*	lb-in ²
0.000	0.000	1.0000	4038000.	67395.	-0.004050	0.000	1.626E+12
0.000	0.950	0.9540	4825167.	67395.	-0.004019	0.000	1.626E+12
0.000	1.900	0.9084	5612175.	66387.	-0.003982	0.000	1.624E+12
-176.8405	2219.3456	0.000	0.000	63171.	-0.003940	0.000	1.623E+12
2.850	5115.8826	0.000	0.000	57484.	-0.003893	0.000	1.622E+12
3.800	8500.4891	0.000	0.000	52964.	-0.003841	0.000	1.621E+12
-610.3420	0.7744	7723052.	8357802.	50847.	-0.003784	0.000	1.620E+12
-182.8495	2688.6920	0.000	8357802.	48662.	-0.003724	0.000	1.619E+12
-188.2181	2944.8081	0.000	8917739.	46417.	-0.003659	0.000	1.617E+12
8.1830	3220.7261	0.000	9477100.	44117.	-0.003590	0.000	1.616E+12
-199.4810	3519.9609	0.000	10010254.	41768.	-0.003507	0.000	1.614E+12
-204.8120	3845.9457	0.000	10516550.	39377.	-0.003407	0.000	1.6227E+12
-208.0026	4202.8280	0.000	10995363.	36950.	-0.003302	0.000	1.215E+12
-211.4723	4593.9558	0.000	11446215.	34492.	-0.003193	0.000	1.204E+12
-214.4145	5024.1730	0.000	11868699.	32010.	-0.003078	0.000	1.195E+12
-216.8195	5499.1542	0.000	12262481.	29509.	-0.002959	0.000	1.187E+12
-218.1672	6025.5993	0.000	12627296.	26997.	-0.002835	0.000	1.180E+12
-219.9767	6611.4768	0.000	12962956.	24480.	-0.002708	0.000	1.174E+12
-220.7062	7266.3303	0.000	13269347.	21965.	-0.002578	0.000	1.168E+12
-220.8538	8001.6681	0.000	13546433.	19459.	-0.002444	0.000	1.164E+12
-220.4073	8831.4691	0.000	13794257.	16967.	-0.002308	0.000	1.160E+12
-219.3542	9772.8378	0.000	14012943.	14499.	-0.002169	0.000	1.156E+12
-219.0000	10847.	0.000	14202694.	9159.5624	-0.002028	0.000	1.154E+12
-217.6823	12087.	0.000	14363800.				
-215.3799	12080.	0.000					
-20.9000	0.1793	14363800.					
-721.3663	45856.	0.000					

Abut A. 1p7o		Abut A. 1p7o	
21.850	0.1570	14430493.	0.000
-693.3942	50341.	1095.4277	-0.001886
22.800	0.1363	-6518.9948	-0.001743
-642.4694	53719.	-13433.	-0.001601
23.750	0.1173	-19874.	-0.001461
-570.5846	55461.	-26167.	-0.001324
24.700	0.0998	-32238.	-0.001190
-559.4119	63879.	-37981.	-0.001060
25.650	0.0840	-43378.	-0.000936
-544.6337	73943.	-48468.	-0.000817
26.600	0.0697	-53210.	-0.000704
-520.3686	85169.	-57387.	-0.000599
27.550	0.0568	-61384.	-0.000501
-487.1332	97700.	-65108.	-0.000421
28.500	0.0455	-67832.	-0.000356
-459.7919	115249.	-68737.	-0.000297
29.450	0.0355	-67522.	-0.000244
-433.1620	139060.	-65125.	-0.000195
30.400	0.0269	-62164.	-0.000153
-398.7075	169227.	-58832.	-0.000115
31.350	0.0194	-55247.	-8.146E-05
-334.1551	195859.	-51493.	-5.269E-05
32.300	0.0132	-47635.	-2.805E-05
-367.1285	317106.	-43721.	-7.208E-06
33.250	0.008016	-39794.	1.014E-05
-286.1152	408903.	-35886.	2.430E-05
34.200	0.003601	-32025.	3.560E-05
-191.7808	607089.	-28235.	4.433E-05
35.150	-0.000107	-24535.	5.081E-05
33.0618	3508624.	-20940.	5.532E-05
36.100	-0.003174	-17464.	5.816E-05
180.0183	646612.	-14117.	5.960E-05
37.050	-0.003661	-10907.	5.991E-05
240.4667	484174.	-18.7544	6208509.
279.4600	41007630		
279.3690	470531		
305.4884	381068139		
323.4375	359935102		
335.0973	347402		
341.8700	340521		
344.7048	33722		
344.3169	338103		
344.4650	341128.		
341.2652	341128.		
45.600	-0.0111		
336.0012	346473.		
328.8992	353955.		
320.2747	363488.		
48.450	-0.009435		
310.3963	375057.		
49.400	-0.008783		
299.4931	388712.		
50.350	-0.008109		
287.7589	404564.		
51.300	-0.007425		
275.3543	422790.		
52.250	-0.006743		
116.0872	196271.		
53.200	-0.006072		
108.6844	204068.		
54.150	-0.005418		
100.6982	211866.		
92.2848	219664.		
83.5967	227461.		
74.7806	235259.		
65.9760	243056.		
57.3144	250854.		
48.9188	258652.		
60.800	-0.001750		
61.750	-0.001387		
33.3729	274247.		
62.700	-0.001068		
104.4393	1114738.		
89.9592	1294181.		
75.5723	1540577.		
61.1737	1903224.		
46.4416	2507042.		
30.3243	3639902.		
-1.1371	13330703.		
-25.7873	4479112.		
-33.4683	347893110		
-37.2156	3128153136		
-38.8520	2986700148		
-38.9875	296100149		
-38.7410	296100142		
-38.1126	3054703		
-36.4672	3192566		
-34.2474	3399348		
-31.6029	3684067		
-28.6517	4063399.		
-25.4860	4566832.		
-22.1738	5250948.		
-18.7544	6208509.		
275.6816	5.935E-05		
-7394.4832	5.809E-05		
-6201.0023	5.623E-05		
-5100.9991	5.389E-05		
-4098.4741	5.113E-05		
-3195.7233	4.804E-05		
-2393.4109	4.469E-05		
-1690.6559	4.116E-05		
-1085.1267	3.748E-05		
-573.1411	3.372E-05		
-149.7669	2.991E-05		
635.7628	2.609E-05		
1743.8343	2.232E-05		
2687.3640	1.868E-05		
3466.8162	1.527E-05		
4080.2234	1.212E-05		
4517.7890	9.306E-06		
4684.0417	6.850E-06		
4529.3161	4.768E-06		
4190.4166	3.048E-06		
3787.5171	1.662E-06		
3354.0958	5.796E-07		
2910.5756	-2.349E-07		
2471.1050	-8.169E-07		
2046.0001	-1.201E-06		
1642.9268	-1.422E-06		
1267.5801	-1.512E-06		
924.1288	-1.500E-06		
615.5437	-1.414E-06		
343.8826	-1.279E-06		
110.5917	-1.116E-06		

Abut A. 1p7o		Abut A. 1p7o	
21.850	0.1570	14430493.	0.000
-693.3942	50341.	1095.4277	-0.001886
22.800	0.1363	-6518.9948	-0.001743
-642.4694	53719.	-13433.	-0.001601
23.750	0.1173	-19874.	-0.001461
-570.5846	55461.	-26167.	-0.001324
24.700	0.0998	-32238.	-0.001190
-559.4119	63879.	-37981.	-0.001060
25.650	0.0840	-43378.	-0.000936
-544.6337	73943.	-48468.	-0.000817
26.600	0.0697	-53210.	-0.000704
-520.3686	85169.	-57387.	-0.000599
27.550	0.0568	-61384.	-0.000501
-487.1332	97700.	-65108.	-0.000421
28.500	0.0455	-67832.	-0.000356
-459.7919	115249.	-68737.	-0.000297
29.450	0.0355	-67522.	-0.000244
-433.1620	139060.	-65125.	-0.000195
30.400	0.0269	-62164.	-0.000153
-398.7075	169227.	-58832.	-0.000115
31.350	0.0194	-55247.	-8.146E-05
-334.1551	195859.	-51493.	-5.269E-05
32.300	0.0132	-47635.	-2.805E-05
-367.1285	317106.	-43721.	-7.208E-06
33.250	0.008016	-39794.	1.014E-05
-286.1152	408903.	-35886.	2.430E-05
34.200	0.003601	-32025.	3.560E-05
-191.7808	607089.	-28235.	4.433E-05
35.150	-0.000107	-24535.	5.081E-05
33.0618	3508624.	-20940.	5.532E-05
36.100	-0.003174	-17464.	5.816E-05
180.0183	646612.	-14117.	5.960E-05
37.050	-0.003661	-10907.	5.991E-05
240.4667	484174.	-18.7544	6208509.
279.4600	41007630		
279.3690	470531		
305.4884	381068139		
323.4375	359935102		
335.0973	347402		
341.8700	340521		
344.7048	33722		
344.3169	338103		
344.4650	341128.		
341.2652	341128.		
45.600	-0.0111		
336.0012	346473.		
328.8992	353955.		
320.2747	363488.		
48.450	-0.009435		
310.3963	375057.		
49.400	-0.008783		
299.4931	388712.		
50.350	-0.008109		
287.7589	404564.		
51.300	-0.007425		

Abut A.1p7o	Abut A.1p7o	Abut A.1p7o	Abut A.1p7o
81.700	2.269E-05	24474.	0.000
-15.2221	7649508.	0.000	1.626E+12
82.650	1.289E-05	22542.	0.000
-11.4748	10148307.	0.000	1.626E+12
83.600	4.896E-06	19118.	0.000
-5.9044	13746575.	0.000	1.626E+12
84.550	1.569E-06	14925.	0.000
1.8958	13772567.	0.000	1.626E+12
85.500	6.842E-06	10979.	0.000
8.2816	13798559.	0.000	1.626E+12
86.450	1.124E-05	8108.8269	0.000
10.7125	10867590.	0.000	1.626E+12
87.400	1.498E-05	6630.4285	0.000
0.7207	548318.	0.000	1.626E+12
88.350	1.820E-05	5245.4784	0.000
0.9014	564563.	0.000	1.626E+12
89.300	2.100E-05	3977.5037	0.000
1.0699	380808.	0.000	1.626E+12
90.250	2.348E-05	2848.4432	0.000
1.2297	397053.	0.000	1.626E+12
91.200	2.573E-05	1879.1039	0.000
1.3844	613298.	0.000	1.626E+12
92.150	2.783E-05	1089.6146	0.000
1.5371	629543.	0.000	1.626E+12
93.100	2.985E-05	499.8544	0.000
1.6909	645788.	0.000	1.626E+12
1.8482	662033.	0.000	1.626E+12
95.000	3.1379E-05	0.000	1.626E+12
2.0105	339139.	0.000	1.626E+12

* This analysis computed pile response using non-linear moment-curvature relationships. Values of total stress due to combined axial and bending stresses are computed only on elastic sections only and do not equal the actual stresses in concrete and steel in concrete and steel may be interpolated from the output for non-linear bending properties relative to the magnitude of bending moment developed in the pile.

Output Summary for Load Case No. 7:

Pile-head deflection	=	1.0000000 inches
Computed slope at pile head	=	-0.0040500 radians
Maximum bending moment	=	14430493. inch-lbs
Maximum shear force	=	-68737. lbs
Depth of maximum bending moment	=	21.8500000 feet below pile head
Depth of maximum shear force	=	35.1500000 feet below pile head
Number of iterations	=	33
Number of zero deflection points	=	3

Pile-head deflection vs. Pile Length for Load Case 7

Boundary Condition Type 4, Deflection and Moment

Deflection =	1.00000 in
Moment =	4038000. in-lb

Axial Load =	410100. lb	Abut A.1p7o
Pile Length feet	95.0000	Maximum Shear lbs
Pile Head Deflection inches	1.0000000	Maximum Moment in-lbs
Res. X _{est} h lb/inch	0.000	14430493.
Deflect. Dist. lb/inch	0.000	14462384.
Soil Spr. Y lb/inch	0.950	14524307.
Bending Moment in-lbs	0.000	14586113.
Shear Force lbs	89002.	14531729.
Slope radians	-0.005780	14475480.
Total Stress psi*	0.000	14482518.
Bending Stiffness lb-in ²	0.000	14524944.
Soil Stiffness lb/in	0.000	14492529.
		14461785.
		13929766.
		12541086.
		10070679.
		7151693.
		5213879.
		4369698.
		4038000.

Computed Values of Pile Loading and Deflection for Lateral Loading for Load Case Number 8

Depth Res. X _{est} h	Deflect. Dist. lb/inch	Bending Moment in-lbs	Shear Force lbs	Slope radians	Total Stress psi*	Bending Stiffness lb-in ²	Soil Stiffness lb/in
0.000	0.000	4038000.	89002.	-0.005812	0.000	1.626E+12	
0.000	0.950	5079726.	89002.	-0.005780	0.000	1.626E+12	
1.900	1.3682	6121286.	87846.	-0.005740	0.000	1.624E+12	
2.850	1.3030	7136290.	84153.	-0.005694	0.000	1.622E+12	
3.800	1.2384	8093213.	77622.	-0.005640	0.000	1.620E+12	
4.750	1.1744	8958808.	72432.	-0.005580	0.000	1.619E+12	
5.700	1.1112	9796837.	69998.	-0.005514	0.000	1.617E+12	
6.650	1.0487	10606327.	67485.	-0.005431	0.000	1.239E+12	
7.600	0.9873	11386285.	64900.	-0.005329	0.000	1.216E+12	
8.550	0.9272	12135882.	62250.	-0.005218	0.000	1.198E+12	

-235.2495	2892.3912	0.000	0.000	0.000	0.000	38.950	-0.0122	7803003.	Abut. A.1p7o	0.000	1.621E+12
9.500	0.8684	12854367.	0.000	0.000	1.182E+12	352.3424	330381.	0.000	-80567.	-0.000213	0.000
-240.1570	3152.7407	0.000	0.000	0.000	1.168E+12	39.900	-0.0143	6908300.	-76383.	-0.000161	0.000
10.450	0.8110	13541061.	0.000	0.000	1.157E+12	381.7764	304914.	0.000	-71914.	-0.000116	0.000
-244.4925	3436.8689	0.000	0.000	0.000	1.147E+12	40.850	-0.0158	6062986.	-67253.	-7.602E-05	0.000
11.400	0.7551	14195363.	0.000	0.000	1.138E+12	402.1329	289481.	0.000	-62470.	-4.165E-05	0.000
-248.2478	3748.0177	0.000	0.000	0.000	1.130E+12	415.5885	280110.	0.000	-57621.	-1.228E-05	0.000
12.350	0.7008	14816748.	0.000	0.000	1.123E+12	423.5713	274833.	0.000	-52753.	1.248E-05	0.000
-251.4123	4089.9600	0.000	0.000	0.000	1.117E+12	423.5713	274833.	0.000	-47905.	3.302E-05	0.000
13.300	0.6481	15404771.	0.000	0.000	1.112E+12	423.5713	274833.	0.000	-43108.	4.973E-05	0.000
-253.9741	4467.1218	0.000	0.000	0.000	1.108E+12	427.0981	272564.	0.000	-38391.	6.299E-05	0.000
14.250	0.5973	15959066.	0.000	0.000	1.104E+12	427.0981	272564.	0.000	-33775.	7.318E-05	0.000
-255.9206	4884.7318	0.000	0.000	0.000	1.100E+12	426.9353	272669.	0.000	-29282.	8.068E-05	0.000
15.200	0.5482	16479349.	0.000	0.000	1.097E+12	426.9353	272669.	0.000	-24926.	8.582E-05	0.000
-257.2381	5349.0080	0.000	0.000	0.000	1.095E+12	45.600	-0.0176	2642911.	-20722.	8.898E-05	0.000
16.150	0.5011	16965420.	0.000	0.000	1.094E+12	423.6852	274762.	0.000	-17503.	9.047E-05	0.000
-257.9125	5867.3942	0.000	0.000	0.000	1.092E+12	417.8367	278609.	0.000	-15248.	9.056E-05	0.000
17.100	0.4560	17417163.	0.000	0.000	1.091E+12	409.7952	284076.	0.000	-13120.	8.943E-05	0.000
-257.9293	6448.8616	0.000	0.000	0.000	1.088E+12	399.9027	291104.	0.000	-11132.	8.725E-05	0.000
18.050	0.4128	17838530.	0.000	0.000	1.086E+12	388.4501	299688.	0.000	-9294.	3.485	8.418E-05
-257.2738	7104.2975	0.000	0.000	0.000	1.085E+12	388.4501	299688.	0.000	-7614.	5.644	8.036E-05
19.000	0.3718	18217644.	0.000	0.000	1.084E+12	375.6851	309871.	0.000	-6097.	1.099	7.593E-05
-257.3000	7847.0098	0.000	0.000	0.000	1.083E+12	361.8173	321749.	0.000	-4743.	7.877	7.101E-05
20.950	0.3329	18566598.	0.000	0.000	1.082E+12	203.0295	196271.	0.000	-3553.	7.991	6.571E-05
-253.8666	8693.5833	0.000	0.000	0.000	1.081E+12	192.3569	204068.	0.000	-2523.	8.938	6.012E-05
21.900	0.2962	18881637.	0.000	0.000	1.080E+12	180.7867	211866.	0.000	-1648.	5.278	5.433E-05
-896.0186	94480.1	0.000	0.000	0.000	1.079E+12	180.7867	211866.	0.000	-369.	3.363	4.841E-05
22.850	0.2618	19079333.	0.000	0.000	1.078E+12	167.3812	219664.	0.000	-1285.	4.769	4.245E-05
-880.1780	3834918	0.000	0.000	0.000	1.077E+12	154.5700	227461.	0.000	-8467.	3.9	3.660E-05
-837.7416	4154296	0.000	0.000	0.000	1.076E+12	140.2986	23356798	0.000	-8234.	2.8	2.564E-05
-766.7250	4374300	0.000	0.000	0.000	1.075E+12	125.9215	24305606	0.000	-7307.	9.0	0.000
23.800	0.2318	19134300.	0.000	0.000	1.074E+12	111.5035	250854.	0.000	-6001.	9.0	0.000
-762.3710	505121	19006369.	0.000	0.000	1.073E+12	97.2665	258652.	0.000	-5737.	9.0	0.000
24.750	0.2021	19006369.	0.000	0.000	1.072E+12	83.4187	266449.	0.000	-5142.	9.0	0.000
-752.25650	58498	0.000	0.000	0.000	1.071E+12	70.1543	274247.	0.000	-4837.	9.0	0.000
25.600	0.1735	18451765.	0.000	0.000	1.070E+12	62.700	-0.002330	0.000	-4378.	9.0	0.000
-730.2573	67401	0.000	0.000	0.000	1.069E+12	54.2653	754674.	0.000	-3786.	9.0	0.000
-695.4174	77323	0.000	0.000	0.000	1.068E+12	54.2653	754674.	0.000	-3234.	9.0	0.000
27.550	0.1025	18029303.	0.000	0.000	1.067E+12	57.900	-0.001813	0.000	-2730.	9.0	0.000
-666.0414	90736	0.000	0.000	0.000	1.066E+12	57.900	-0.001813	0.000	-2240.	9.0	0.000
28.500	0.0837	17515595.	0.000	0.000	1.065E+12	57.900	-0.001813	0.000	-1730.	9.0	0.000
-636.3290	108520	0.000	0.000	0.000	1.064E+12	57.900	-0.001813	0.000	-1240.	9.0	0.000
29.450	0.0668	16914488.	0.000	0.000	1.063E+12	57.900	-0.001813	0.000	-750.	9.0	0.000
-595.7674	130622	0.000	0.000	0.000	1.062E+12	57.900	-0.001813	0.000	-260.	9.0	0.000
30.400	0.0520	16229878.	0.000	0.000	1.061E+12	57.900	-0.001813	0.000	-110.	9.0	0.000
-543.7866	158882.	0.000	0.000	0.000	1.060E+12	57.900	-0.001813	0.000	-60.	9.0	0.000
31.350	0.0390	15467074.	0.000	0.000	1.059E+12	57.900	-0.001813	0.000	-30.	9.0	0.000
-532.8960	218465.	0.000	0.000	0.000	1.058E+12	57.900	-0.001813	0.000	-15.	9.0	0.000
32.300	0.0278	14632874.	0.000	0.000	1.057E+12	57.900	-0.001813	0.000	-7.	9.0	0.000
-431.7411	269656.	0.000	0.000	0.000	1.056E+12	57.900	-0.001813	0.000	-3.	9.0	0.000
33.250	0.0183	13728740.	0.000	0.000	1.055E+12	57.900	-0.001813	0.000	-1.	9.0	0.000
34.200	0.0102	12767870.	0.000	0.000	1.054E+12	57.900	-0.001813	0.000	-0.	9.0	0.000
-323.2091	360221.	0.000	0.000	0.000	1.053E+12	57.900	-0.001813	0.000	-0.	9.0	0.000
35.150	0.003607	11764420.	0.000	0.000	1.052E+12	57.900	-0.001813	0.000	-0.	9.0	0.000
-191.9448	606668.	0.000	0.000	0.000	1.051E+12	57.900	-0.001813	0.000	-0.	9.0	0.000
36.100	-0.001748	10735505.	0.000	0.000	1.050E+12	57.900	-0.001813	0.000	-0.	9.0	0.000
133.5665	871116.	0.000	0.000	0.000	1.049E+12	57.900	-0.001813	0.000	-0.	9.0	0.000
246.9512	-0.005973	9723486.	0.000	0.000	1.048E+12	57.900	-0.001813	0.000	-0.	9.0	0.000
38.000	471337.	0.000	0.000	0.000	1.047E+12	57.900	-0.001813	0.000	-0.	9.0	0.000
310.0783	375403.	0.000	0.000	0.000	1.046E+12	57.900	-0.001813	0.000	-0.	9.0	0.000

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43.3864	2684256.	0.000	6783.3142	1.232E-05	0.000	1.626E+12
69.350	-2.286E-05	-523849.				
15.3000	7630061.	0.000	6691.4817	8.923E-06	0.000	1.626E+12
70.300	9.667E-05	-445574.				
-31.4110	3704045.	0.000	6267.6886	6.060E-06	0.000	1.626E+12
-42.9387	2710472.	0.000	5743.8299	3.697E-06	0.000	1.626E+12
72.200	0.000235	-302728.				
-48.9664	2377038.	0.000	5168.2886	1.793E-06	0.000	1.626E+12
73.150	0.000265	-240442.				
-52.0058	2238218.	0.000	4569.4195	3.017E-07	0.000	1.626E+12
74.100	0.000276	-184907.				
-53.0590	2193856.	0.000	3966.7181	-8.241E-07	0.000	1.626E+12
75.050	0.000272	-136262.				
-52.6781	2209763.	0.000	3374.4985	-1.633E-06	0.000	1.626E+12
76.100	227200257	0.000	2803.5989	-2.172E-06	0.000	1.626E+12
-51.7210	227200257	0.000	2262.3358	-2.487E-06	0.000	1.626E+12
-48.9778	2278232.	0.000	1757.1160	-2.621E-06	0.000	1.626E+12
77.900	0.000207	30316.				
-46.0707	2579544.	0.000	1292.8824	-2.614E-06	0.000	1.626E+12
78.850	0.000178	-7037601				
-42.6144	2731777.	0.000	873.4915	-2.504E-06	0.000	1.626E+12
79.800	0.000148	95706573				
-38.8301	2998055.	0.000	502.0966	-2.324E-06	0.000	1.626E+12
80.750	0.000118	21798.				
-34.7473	3350388.	0.000	181.6378	-2.104E-06	0.000	1.626E+12
81.700	9.055E-05	29510.				
-30.4097	3828358.	0.000	-84.3439	-1.870E-06	0.000	1.626E+12
82.650	6.523E-05	33268.				
-25.8111	4510578.	0.000	-289.8176	-1.642E-06	0.000	1.626E+12
83.600	4.257E-05	33671.				
-20.8524	5583494.	0.000	-411.9233	-1.437E-06	0.000	1.626E+12
84.550	2.261E-05	31362.				
-15.1956	7662944.	0.000	-389.3880	-1.265E-06	0.000	1.626E+12
85.500	5.144E-06	27078.				
-6.2264	13798559.	0.000	-324.8660	-1.124E-06	0.000	1.626E+12
86.450	-1.015E-05	21984.				
10.1800	11429338.	0.000	-308.2698	-1.009E-06	0.000	1.626E+12
87.400	-2.369E-05	18212.				
1.1397	548318.	0.000	-284.6080	-9.186E-07	0.000	1.626E+12
88.350	-3.578E-05	14588.				
1.7719	564563.	0.000	-254.1125	-8.510E-07	0.000	1.626E+12
89.300	-4.670E-05	11193.				
2.3793	580808.	0.000	-216.9088	-8.036E-07	0.000	1.626E+12
90.250	-5.672E-05	8107.0550				
2.9708	597053.	0.000	-173.0165	-7.735E-07	0.000	1.626E+12
91.200	-6.610E-05	5407.0631				
3.5561	613298.	0.000	-122.3557	-7.573E-07	0.000	1.626E+12
92.150	-7.505E-05	3169.0485				
4.1443	629543.	0.000	-64.7605	-7.508E-07	0.000	1.626E+12
93.100	-8.374E-05	1469.5207				
4.7436	645788.	0.000	0.000	-7.494E-07	0.000	1.626E+12
94.050	-9.231E-05	386.4202				
5.3608	662033.	0.000				
95.000	-0.000101	0.000				
6.0007	339139.	0.000				

* This analysis computed pile response using nonlinear moment-curvature relationships. Values of total stress due to combined axial and bending stresses are computed only for elastic sections only and do not equal the actual stresses in concrete and

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steel. Stresses in concrete and steel may be interpolated from the output for nonlinear bending properties relative to the magnitude of bending moment developed in the pile.

Output Summary for Load Case No. 8:

Pile-head deflection = 1.500000 inches
 Computed slope at pile head = -0.0058117 radians
 Maximum bending moment = 19161693. inch-lbs
 Maximum shear force = -89687. lbs
 Depth of maximum bending moment = 22.800000 feet below pile head
 Depth of maximum shear force = 36.100000 feet below pile head
 Number of iterations = 15
 Number of zero deflection points = 3

Pile-head Deflection vs. Pile Length for Load Case 8

Boundary Condition Type 4, Deflection and Moment

Deflection = 1.50000 in
 Moment = 4038000. in-lb
 Axial Load = 410100. lb

Pile Length feet	Pile head Deflection inches	Maximum Moment in-lb	Maximum Shear lbs
95.0000	1.5000000	19161693.	-89687.
90.2500	1.5000000	19185074.	-89742.
85.5000	1.5000000	19259618.	-90070.
80.7500	1.5000000	19342018.	-90517.
76.0000	1.5000000	19236419.	-90147.
71.2500	1.5000000	19180163.	-90165.
66.5000	1.5000000	19182827.	-89909.
61.7500	1.5000000	19248721.	-89675.
57.0000	1.5000000	19189062.	-90090.
52.2500	1.5000000	19037157.	-94171.
47.5000	1.5000000	17980152.	-102750.
42.7500	1.5000000	15643990.	-105179.
38.0000	1.5000000	11884546.	-94537.
33.2500	1.5000000	8206462.	-75042.
28.5000	1.5000000	5681649.	-51829.
23.7500	1.5000000	4547475.	-38334.
19.0000	1.5000000	4038000.	-36275.

Summary of Pile Response(s)

Definitions of Pile-head Loading Conditions:

Load Type 1: Load 1 = Shear, lbs, and Load 2 = Moment, in-lbs
 Load Type 2: Load 1 = Shear, lbs, and Load 2 = Slope, radians
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 Load Type 3: Load 1 = Shear, lbs, and Load 2 = Rotational stiffness, in-lbs/radian
 Load Type 4: Load 1 = Top Deflection, inches, and Load 2 = Moment, in-lbs
 Load Type 5: Load 1 = Top Deflection, inches, and Load 2 = Slope, radians

Case No.	Load No.	Pile-head		Axial Loading lbs	Pile-head Deflection inches	Maximum Moment in-lbs
		Condition 1	Condition 2			
1	1	V = 68000.	M = 5342000.	504400.	1.08857285	
15806783	1	V = -74367.	M = -0.00446290	410100.	0.68932349	
2	1	V = 53000.	M = 4038000.	410100.		
11451693	4	V = -55069.	M = -0.00292165	504400.	1.00000000	
3	4	V = 1.0000	M = 5342000.	504400.		
14953248	4	V = -70507.	M = -0.00414210	504400.	1.50000000	
4	4	V = 1.5000	M = 5342000.	504400.		
19723394	4	V = -91337.	M = -0.00590812	504400.	2.00000000	
5	4	V = 2.0000	M = 5342000.	504400.		
24233438	4	V = -111090.	M = -0.00763070	410100.	0.50000000	
6	4	V = 0.5000	M = 4038000.	410100.		
9863989	4	V = -47681.	M = -0.00219425	410100.	1.00000000	
7	4	V = 1.0000	M = 4038000.	410100.		
14430493	4	V = -68737.	M = -0.00405004	410100.	1.50000000	
8	4	V = 1.5000	M = 4038000.	410100.		
19161693	4	V = -89687.	M = -0.00581171	410100.	1.50000000	

$\Delta = 0.69$ " < 1 " δk
 SER I

LATERAL CAPACITY @ 2.0" DEFLECTION (SER I) = 105.64 k
 LATERAL CAPACITY @ 1.0" DEFLECTION (SER II) = 67.40 k

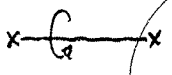
The analysis ended normally.

PROJECT B2-159 JOB NO. _____ SHEET NO. 1 OF 1
 LOCATION JAMES ST OVER CHALWING RIVER
 SUBJECT ABUT A
 DESIGNED BY ZME DATE 10/14/14 CHECKED BY _____ DATE _____
 REVISED BY _____ DATE _____ BACK CHECKED BY _____ DATE _____

REF./REM.

ABUTMENT A

STRENGTH I



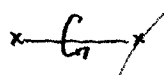
AXIAL = 504.4 K
 LATERAL = 67.9 K
 MOMENT = 5342 K-IN

Actual Deflection = 1.08"

@ 1" Deflection, Lateral = 64.03 K
 1.5" Deflection, Lateral = 85.77 K
 2.0" Deflection, Lateral = 105.64 K

$$\boxed{105.64^k > 67.9^k} \quad \text{OK}$$

SERVICE II



AXIAL = 410.1 K
 LATERAL = 52.6 K
 MOMENT = 4038 K-IN

Actual Deflection = 0.69"

@ 0.5" Deflection, Lateral = 44.56 K
 1.0" Deflection, Lateral = 67.40 K
 1.5" Deflection, Lateral = 89.0 K

$$\boxed{67.40^k > 52.6^k} \quad \text{OK}$$

[4-PILES @ 14'-3" SPACING]

GEOTECHNICAL STRENGTH AXIAL CAPACITY

516^k COMPRESSION > 504.4 k OK

ABSTMENT B

LAYER

Boring No. JS-9

By: SJM

Chk: *AT*

OG Elev. =

4.50 ✓

Sample No.	Depth of SS run (ft)	N-Values Field	q'v (ksf)	C _N	N _{CORR}
2	2	6	0.095	2.020	12
3	4	12	0.190	1.788	21
4	6	18	0.286	1.653	30
5	8	20	0.381	1.556	31
6	10	20	0.476	1.482	30
7	12	39	0.571	1.421	55
8	14	48	0.666	1.369	66
9	16	19	0.762	1.325	25
10	18	11	0.857	1.285	14
11	23	12	1.095	1.203	14
12	28	19	1.333	1.138	22
13	33	19	1.571	1.083	21
14	37	30	1.761	1.044	31
15	42	19	1.999	1.002	19
16	47	21	2.237	0.964	20
17	52	9	2.475	0.931	8
18	57	16	2.713	0.900	14
19	62	21	2.951	0.872	18
20	67	37	3.189	0.846	31
21	72	34	3.427	0.822	28
22	77	0	3.665	0.799	0
23	82	82	3.903	0.778	64
24	87	50	4.141	0.758	38
25	92	50	4.379	0.740	37
26	97	50	4.617	0.722	36

GWT = 4.6
 γ = 110 lb/ft³
 γ' = 48 lb/ft³

②

③

④

⑤

⑥

IGNORE THIS VALUE.

N_{avg} (Below BFE) **27**

(Ref. AASHTO Eqn 10.4.6.2.4-1)

C_N = 0.77 x log (40/q'v)

N_{CORR} = N_{Field} x C_N

PROJECT BRI-159 JOB NO. _____ SHEET NO. 1 OF 1
 LOCATION ABUTMENT B
 SUBJECT SOIL PROFILE (BORING JS-9)
 DESIGNED BY SJM DATE 7/29/14 CHECKED BY AT DATE 8/14
 REVISED BY _____ DATE _____ BACK CHECKED BY _____ DATE _____

DEPTH BELOW OG	DEPTH BELOW BDSF (ft)	LAYER THICKNESS (ft)	ELEVATIONS	SOIL TYPE	OG EL	REF/REM.
			+4.5			
Layer ①	$x_1 = 0$	(6)		SILT WITH SAND + GRAVEL $N_{CORR} = 12-30$ $\gamma'_s = 57.6 \text{ pcf}$ $\gamma_s = 120 \text{ pcf}$ $c = 750 \text{ psf } \phi = 0$ $E_{50} = 0.02$ $\phi = 0^\circ$	OG EL +4.5	$y = 0$ BDSF +4.0 $y = 1.5$
	$x_1 = 5.5$		-1.5			$y = 7.0$
②		(10)		MED DENSE SAND WITH GRAVEL $\gamma'_s = 72.6 \text{ pcf}$ $\gamma_s = 135 \text{ pcf}$ $\phi = 34^\circ$ $K = 60 \text{ pci}$ $N_{CORR} = 25-66$		$y = 17$
	$x_1 = 15.5$		-11.5			
③		(31)		MED FINE SAND WITH SILT + GRAVEL $N_{CORR} = 14-31$ $\gamma'_s = 72.6 \text{ pcf}$ $\gamma_s = 135 \text{ pcf}$ $\phi = 32^\circ$ $K = 60 \text{ pci}$		$y = 48$
	$x_1 = 46.5$		-42.5			
④		(15)		V STIFF SILT/CLAY $N_{CORR} = 8-18$ $\gamma'_s = 62.6 \text{ pcf}$ $\gamma_s = 125 \text{ pcf}$ $c = 1000 \text{ psf } \phi = 0$ $E_{50} = 0.007$ $K = 200 \text{ pci}$		TIP EL -46 $y = 63$
	$x_1 = 61.5$		-57.5			
			EL. -46			
⑤		(30)		VERY DENSE SAND $N_{CORR} = 28-64$ $\gamma'_s = 72.6 \text{ pcf}$ $\gamma_s = 135 \text{ pcf}$ $c = 0$ $K = 125 \text{ pci}$		$y = 93$
	$x_1 = 91.5$		-87.5			
⑥		(16.7)		WEATHERED ROCK $N_{CORR} = 7-36$ $\gamma'_s = 87.6 \text{ pcf}$ $\gamma_s = 150 \text{ pcf}$ $c = 200 \text{ ksf}$ $\phi = 46^\circ$ $K = 580 \text{ pci}$ $= 1398 \text{ ksf}$		$y = 109.7$
	$x_1 = 108.2$		-104.2			
108.7				END BORING		

AXIAL CAPACITY

About B.sfo
 STRENGTH REDUCTION FACTOR-ALPHA = 0.550E+00
 END BEARING COEFFICIENT-NC = 0.800E+01
 UNDRAINED SHEAR STRENGTH, LB/SQ FT = 0.000E+00
 INTERNAL FRICTION ANGLE, DEG. = 0.000E+00
 BLOWS PER FOOT FROM STANDARD PENETRATION TEST = 0.120E+03
 SOIL UNIT WEIGHT, LB/CU FT = 0.100E+11
 MAXIMUM LOAD TRANSFER FOR SOIL, LB/SQ FT = 0.550E+01
 LRFD RESISTANCE FACTOR (SIDE FRICTION) = 0.450E+00
 LRFD RESISTANCE FACTOR (TIP RESISTANCE) = 0.400E+00

LAYER NO 2-----SAND
 AT THE TOP
 SKIN FRICTION COEFFICIENT- BETA = 0.118E+01
 UNDRAINED SHEAR STRENGTH, LB/SQ FT = 0.000E+00
 INTERNAL FRICTION ANGLE, DEG. = 0.340E+02
 BLOWS PER FOOT FROM STANDARD PENETRATION TEST = 0.000E+00
 SOIL UNIT WEIGHT, LB/CU FT = 0.135E+03
 MAXIMUM LOAD TRANSFER FOR SOIL, LB/SQ FT = 0.100E+11
 DEPTH, FT = 0.550E+01

AT THE BOTTOM
 SKIN FRICTION COEFFICIENT- BETA = 0.969E+00
 UNDRAINED SHEAR STRENGTH, LB/SQ FT = 0.000E+00
 INTERNAL FRICTION ANGLE, DEG. = 0.320E+02
 BLOWS PER FOOT FROM STANDARD PENETRATION TEST = 0.000E+00
 SOIL UNIT WEIGHT, LB/CU FT = 0.135E+03
 MAXIMUM LOAD TRANSFER FOR SOIL, LB/SQ FT = 0.100E+11
 DEPTH, FT = 0.155E+02
 LRFD RESISTANCE FACTOR (SIDE FRICTION) = 0.550E+00
 LRFD RESISTANCE FACTOR (TIP RESISTANCE) = 0.500E+00

LAYER NO 3-----SAND
 AT THE TOP
 SKIN FRICTION COEFFICIENT- BETA = 0.969E+00
 UNDRAINED SHEAR STRENGTH, LB/SQ FT = 0.000E+00
 INTERNAL FRICTION ANGLE, DEG. = 0.320E+02
 BLOWS PER FOOT FROM STANDARD PENETRATION TEST = 0.000E+00
 SOIL UNIT WEIGHT, LB/CU FT = 0.135E+03
 MAXIMUM LOAD TRANSFER FOR SOIL, LB/SQ FT = 0.100E+11
 DEPTH, FT = 0.155E+02
 AT THE BOTTOM
 SKIN FRICTION COEFFICIENT- BETA = 0.579E+00
 UNDRAINED SHEAR STRENGTH, LB/SQ FT = 0.000E+00
 INTERNAL FRICTION ANGLE, DEG. = 0.320E+02
 BLOWS PER FOOT FROM STANDARD PENETRATION TEST = 0.000E+00
 SOIL UNIT WEIGHT, LB/CU FT = 0.135E+03
 MAXIMUM LOAD TRANSFER FOR SOIL, LB/SQ FT = 0.100E+11

About B.sfo
 SHAFT for Windows, Version 2012.7.11
 Serial Number : 228741384
 VERTICALLY LOADED DRILLED SHAFT ANALYSIS
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Path to file locations : Y:\bridges\DELDOT\BRI-159_JAMES ST
 BRIDGE\FOUNDATION REPORT\SHAFT output\
 Name of input data file : About B.sfd
 Name of output file : About B.sfo
 Name of plot output file : About B.sfp
 Name of runtime file : About B.sft

 Time and Date of Analysis

Date: July 29, 2014 Time: 11:47:32
 BRI-159 Abutment B
 PROPOSED DEPTH = 100.2 FT
 NUMBER OF LAYERS = 6
 WATER TABLE DEPTH = 0.0 FT.

SOIL INFORMATION
 LAYER NO 1-----CLAY
 AT THE TOP
 STRENGTH REDUCTION FACTOR-ALPHA = 0.550E+00
 END BEARING COEFFICIENT-NC = 0.800E+01
 UNDRAINED SHEAR STRENGTH, LB/SQ FT = 0.750E+03
 INTERNAL FRICTION ANGLE, DEG. = 0.000E+00
 BLOWS PER FOOT FROM STANDARD PENETRATION TEST = 0.000E+00
 SOIL UNIT WEIGHT, LB/CU FT = 0.120E+03
 MAXIMUM LOAD TRANSFER FOR SOIL, LB/SQ FT = 0.100E+11
 DEPTH, FT = 0.000E+00
 AT THE BOTTOM

STRENGTH REDUCTION FACTOR-ALPHA = 0.550E+00
 END BEARING COEFFICIENT-NC = 0.800E+01
 UNDRAINED SHEAR STRENGTH, LB/SQ FT = 0.750E+03
 INTERNAL FRICTION ANGLE, DEG. = 0.000E+00
 BLOWS PER FOOT FROM STANDARD PENETRATION TEST = 0.000E+00
 SOIL UNIT WEIGHT, LB/CU FT = 0.120E+03
 MAXIMUM LOAD TRANSFER FOR SOIL, LB/SQ FT = 0.100E+11
 DEPTH, FT = 0.000E+00
 AT THE BOTTOM

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DEPTH, FT = 0.465E+02

LRFD RESISTANCE FACTOR (SIDE FRICTION) = 0.550E+00
LRFD RESISTANCE FACTOR (TIP RESISTANCE) = 0.500E+00

LAYER NO 4-----CLAY

AT THE TOP
STRENGTH REDUCTION FACTOR-ALPHA = 0.550E+00
END BEARING COEFFICIENT-NC = 0.800E+01
UNDRAINED SHEAR STRENGTH, LB/SQ FT = 0.100E+04
INTERNAL FRICTION ANGLE, DEG. = 0.000E+00
BLOWS PER FOOT FROM STANDARD PENETRATION TEST = 0.000E+00
SOIL UNIT WEIGHT, LB/CU FT = 0.125E+03
MAXIMUM LOAD TRANSFER FOR SOIL, LB/SQ FT = 0.100E+11
DEPTH, FT = 0.465E+02

AT THE BOTTOM

STRENGTH REDUCTION FACTOR-ALPHA = 0.550E+00
END BEARING COEFFICIENT-NC = 0.800E+01
UNDRAINED SHEAR STRENGTH, LB/SQ FT = 0.100E+04
INTERNAL FRICTION ANGLE, DEG. = 0.000E+00
BLOWS PER FOOT FROM STANDARD PENETRATION TEST = 0.000E+00
SOIL UNIT WEIGHT, LB/CU FT = 0.125E+03
MAXIMUM LOAD TRANSFER FOR SOIL, LB/SQ FT = 0.100E+11
DEPTH, FT = 0.615E+02

LRFD RESISTANCE FACTOR (SIDE FRICTION) = 0.450E+00
LRFD RESISTANCE FACTOR (TIP RESISTANCE) = 0.400E+00

LAYER NO 5-----SAND

AT THE TOP
SKIN FRICTION COEFFICIENT- BETA = 0.441E+00
UNDRAINED SHEAR STRENGTH, LB/SQ FT = 0.000E+00
INTERNAL FRICTION ANGLE, DEG. = 0.340E+02
BLOWS PER FOOT FROM STANDARD PENETRATION TEST = 0.000E+00
SOIL UNIT WEIGHT, LB/CU FT = 0.135E+03
MAXIMUM LOAD TRANSFER FOR SOIL, LB/SQ FT = 0.100E+11
DEPTH, FT = 0.615E+02

AT THE BOTTOM

SKIN FRICTION COEFFICIENT- BETA = 0.250E+00
UNDRAINED SHEAR STRENGTH, LB/SQ FT = 0.000E+00
INTERNAL FRICTION ANGLE, DEG. = 0.340E+02
BLOWS PER FOOT FROM STANDARD PENETRATION TEST = 0.000E+00
SOIL UNIT WEIGHT, LB/CU FT = 0.135E+03
MAXIMUM LOAD TRANSFER FOR SOIL, LB/SQ FT = 0.100E+11
DEPTH, FT = 0.915E+02

LRFD RESISTANCE FACTOR (SIDE FRICTION) = 0.100E+01
LRFD RESISTANCE FACTOR (TIP RESISTANCE) = 0.100E+01

Abut B. sfo

LAYER NO 6-----WEAK ROCK

AT THE TOP
DIAMETER OF SOCKET, FT = 0.350E+01
SLUMP OF CONCRETE, IN = 0.000E+00
ANGLE OF INTERFACE FRICTION, DEG. = 0.000E+00
UNIAXIAL COMPRESSION STRENGTH OF ROCK, LB/SQ FT = 0.300E+06
ELASTIC MODULUS FOR THE INTACT ROCK, LB/SQ IN. = 0.497E+07
ROCK QUALITY DESIGNATION (RQD) % = 0.000E+00
DEPTH, FT = 0.915E+02

AT THE BOTTOM

DIAMETER OF SOCKET, FT = 0.350E+01
SLUMP OF CONCRETE, IN = 0.000E+00
ANGLE OF INTERFACE FRICTION, DEG. = 0.000E+00
UNIAXIAL COMPRESSION STRENGTH OF ROCK, LB/SQ FT = 0.200E+06
ELASTIC MODULUS FOR THE INTACT ROCK, LB/SQ IN. = 0.497E+07
ROCK QUALITY DESIGNATION (RQD) % = 0.000E+00
DEPTH, FT = 0.108E+03

LRFD RESISTANCE FACTOR (SIDE FRICTION) = 0.550E+00
LRFD RESISTANCE FACTOR (TIP RESISTANCE) = 0.500E+00

DRILLED SHAFT INFORMATION

DIAMETER OF STEM = 4.000 FT.
DIAMETER OF BASE = 4.000 FT.
END OF STEM TO BASE = 0.000 FT.
ANGLE OF BELL PORTION = 5.000 DEG.
IGNORED TOP PORTION = 4.000 FT.
IGNORED BOTTOM PORTION = 4.000 FT.
AREA OF ONE PERCENT STEEL = 18.098 SQ.IN.
ELASTIC MODULUS, PC = 0.312E+07 LB/SQ.IN.
VOLUME OF UNDERREAM = 0.000 CU.YDS.

PREDICTED RESULTS

QS = ULTIMATE SIDE RESISTANCE;
QB = ULTIMATE BASE RESISTANCE;
WT = WEIGHT OF DRILLED SHAFT (UPLIFT CAPACITY ONLY);
QU = TOTAL ULTIMATE RESISTANCE;
LRFD QS = TOTAL SIDE FRICTION USING LRFD RESISTANCE FACTOR
LRFD QB = TOTAL BASE BEARING USING LRFD RESISTANCE FACTOR
LRFD QU = TOTAL CAPACITY WITH LRFD RESISTANCE FACTOR.

LENGTH VOLUME OS QB QU LRFD QS LRFD QB LRFD QU
(FEET) (CU.YDS) (TONS) (TONS) (TONS) (TONS) (TONS) (TONS)

LATERAL CAPACITY ABUTMENT B

Abut B.lp7o

LPile Plus for Windows, Version 2013-07.007
 Analysis of Individual Piles and Drilled Shafts
 Subjected to Lateral Loading Using the p-y Method
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Files Used for Analysis

Path to file locations: Y:\Bridges\DELDOT\BRI-159_JAMES ST BRIDGE\FOUNDATION
 REPORT\LPile Output
 Name of input data file: Abut B.lp7d
 Name of output report file: Abut B.lp7o
 Name of plot output file: Abut B.lp7p
 Name of Runtime message file: Abut B.lp7r

Date and Time of Analysis

Date: October 16, 2014 Time: 9:50:14

Problem Title

Project Name: BRI-159 Abutment B

Job Number:

Client: delDOT

Engineer: SJM

Abut B.lp7o

Description: Abutment B Lateral Capacity

Program Options and Settings

Engineering Units of Input Data and Computations:
 - Engineering units are US Customary Units (pounds, feet, inches)

Analysis Control Options:
 - Maximum number of iterations allowed = 100
 - Deflection tolerance for convergence = 1.0000E-05 in
 - Maximum allowable deflection = 100.0000 in
 - Number of pile increments = 100

Loading Type and Number of Cycles of Loading:
 - Static loading specified

Computational Options:

- use unfactored loads in computations (conventional analysis)
 - Compute pile response under loading and nonlinear bending properties of pile
 (only if nonlinear pile properties are input)
 - use of p-y modification factors for p-y curves not selected
 - Loading by lateral soil movements acting on pile not selected
 - Input of shear resistance at the pile tip not selected
 - Computation of pile-head foundation stiffness matrix not selected
 - Push-over analysis of pile not selected
 - Buckling analysis of pile not selected

Output Options:

- No p-y curves to be computed and reported for user-specified depths
 - values of pile-head deflection, bending moment, shear force, and
 soil reaction are printed for full length of pile.
 - Printing Increment (nodal spacing of output points) = 1

Pile Structural Properties and Geometry

Total number of pile sections = 1
 Total length of pile = 50.00 ft
 Depth of ground surface below top of pile = 1.50 ft

Pile diameter values used for p-y curve computations are defined using 2 points.
 p-y curves are computed using pile diameter values interpolated with depth over
 the length of the pile.

Point	Depth x ft	Pile Diameter in
1	0.00000	49.0000000
2	50.00000	49.0000000

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Input Structural Properties:

Pile Section No. 1:

Section Type
Permanent Casing
Section Length
Section Diameter

= Drilled Shaft with
= 50.00000 ft
= 49.00000 in

Ground Slope and Pile Batter Angles

Ground Slope Angle = 0.000 degrees
= 0.000 radians
Pile Batter Angle = 0.000 degrees
= 0.000 radians

Soil and Rock Layering Information

The soil profile is modelled using 6 layers

Layer 1 is soft clay, p-y criteria by Matlock, 1970

Distance from top of pile to top of layer = 1.50000 ft
Distance from top of pile to bottom of layer = 7.00000 ft
Effective unit weight at top of layer = 57.60000 pcf
Effective unit weight at bottom of layer = 42.60000 pcf
Undrained cohesion at top of layer = 750.00000 psf
Undrained cohesion at bottom of layer = 750.00000 psf
Epsilon-50 at top of layer = 0.02000
Epsilon-50 at bottom of layer = 0.02000

Layer 2 is sand, p-y criteria by Reese et al., 1974

Distance from top of pile to top of layer = 7.00000 ft
Distance from top of pile to bottom of layer = 17.00000 ft
Effective unit weight at top of layer = 72.60000 pcf
Effective unit weight at bottom of layer = 72.60000 pcf
Friction angle at top of layer = 34.00000 deg.
Friction angle at bottom of layer = 34.00000 deg.
Subgrade k at top of layer = 60.00000 pci
Subgrade k at bottom of layer = 60.00000 pci

Layer 3 is sand, p-y criteria by Reese et al., 1974

Distance from top of pile to top of layer = 17.00000 ft
Distance from top of pile to bottom of layer = 48.00000 ft
Effective unit weight at top of layer = 57.60000 pcf
Effective unit weight at bottom of layer = 57.60000 pcf
Friction angle at top of layer = 32.00000 deg.
Friction angle at bottom of layer = 32.00000 deg.
Subgrade k at top of layer = 60.00000 pci
Subgrade k at bottom of layer = 60.00000 pci

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Layer 4 is stiff clay with water-induced erosion

Distance from top of pile to top of layer = 48.00000 ft
Distance from top of pile to bottom of layer = 63.00000 ft
Effective unit weight at top of layer = 62.60000 pcf
Effective unit weight at bottom of layer = 62.60000 pcf
Undrained cohesion at top of layer = 1000.00000 psf
Undrained cohesion at bottom of layer = 1000.00000 psf
Epsilon-50 at top of layer = 0.00700
Epsilon-50 at bottom of layer = 0.00700
Subgrade k at top of layer = 200.00000 pci
Subgrade k at bottom of layer = 200.00000 pci

Layer 5 is sand, p-y criteria by Reese et al., 1974

Distance from top of pile to top of layer = 63.00000 ft
Distance from top of pile to bottom of layer = 93.00000 ft
Effective unit weight at top of layer = 72.60000 pcf
Effective unit weight at bottom of layer = 72.60000 pcf
Friction angle at top of layer = 34.00000 deg.
Friction angle at bottom of layer = 34.00000 deg.
Subgrade k at top of layer = 125.00000 pci
Subgrade k at bottom of layer = 125.00000 pci

Layer 6 is weak rock, p-y criteria by Reese, 1997

Distance from top of pile to top of layer = 93.00000 ft
Distance from top of pile to bottom of layer = 109.70000 ft
Effective unit weight at top of layer = 87.60000 pcf
Effective unit weight at bottom of layer = 87.60000 pcf
Uniaxial compressive strength at top of layer = 1389000. psi
Uniaxial compressive strength at bottom of layer = 1389000. psi
Initial modulus of rock at top of layer = 4970000. psi
Initial modulus of rock at bottom of layer = 4970000. psi
RQD of rock at top of layer = 0.0000 %
RQD of rock at bottom of layer = 0.0000 %
k rm of rock at top of layer = 0.0000
k rm of rock at bottom of layer = 0.0000

(Depth of lowest soil layer extends 59.70 ft below pile tip)

Summary of Soil Properties

Angle of Layer Friction Num. deg.	Uniaxial Layer qu (p-y Curve Criteria) psi	Soil Type or (p-y Curve Criteria) GSI	RQD %	Strain	Layer Depth ft	Factor	Epsilon 50 pci	Effective Rock Mass Unit Wt. Rock Emass pcf	Undrained Cohesion Rock Emass psf

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1	Soft Clay	0.02000	1.500	57.600	750.000
2	Sand (Reese, et al.)	0.02000	7.000	42.600	750.000
3	Sand (Reese, et al.)	0.00700	17.000	57.600	1000.000
4	Stiff Clay with Free water	0.00700	63.000	62.600	1000.000
5	Sand (Reese, et al.)	0.00700	63.000	72.600	1000.000
6	Weak Rock	0.00	93.000	87.600	4970000.
0.00	1389000.	0.00	109.700	87.600	4970000.

Loading Type

Static loading criteria were used when computing p-y curves for all analyses.

Pile-head Loading and Pile-head Fixity Conditions

Number of Loads specified = 8

Load No.	Load Type	Condition	Condition	Axial Thrust Force, lbs
1	Yes	1	2	402100.
2	Yes	1	2	311000.

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3	Yes	Y =	M =	3729000.	in-lbs	402100.
4	Yes	1.50000	in	3729000.	in-lbs	402100.
5	Yes	2.00000	in	3729000.	in-lbs	402100.
6	Yes	0.50000	in	2808000.	in-lbs	311000.
7	Yes	1.00000	in	2808000.	in-lbs	311000.
8	Yes	1.50000	in	2808000.	in-lbs	311000.

V = perpendicular shear force applied to pile head
M = bending moment applied to pile head
Y = lateral deflection relative to pile axis
S = pile slope relative to original pile batter angle
R = rotational stiffness applied to pile head
Axial thrust is assumed to be acting axially for all pile batter angles.

Computations of Nominal Moment Capacity and Nonlinear Bending Stiffness

Axial thrust force values were determined from pile-head loading conditions

Number of Pile Sections Analyzed = 1

Pile Section No. 1:

Dimensions and Properties of Drilled Shaft (Bored Pile) with Permanent Casing:

Length of Section	=	50.00000	ft
Outer Diameter of Casing	=	49.00000	in
Concrete Cover Thickness Inside Casing	=	4.00000	in
Casing Wall Thickness	=	0.50000	in
Moment of Inertia of Steel Casing	=	22403.	in ⁴
Yield Stress of Casing	=	36000.	psi
Elastic Modulus of Casing	=	29000000.	psi
Number of Reinforcing Bars	=	12	bars
Area of Single Reinforcing Bar	=	0.79000	sq. in.
Edge-to-Edge Bar Spacing	=	9.09394	in
Maximum Concrete Aggregate Size	=	0.50000	in
Ratio of Bar Spacing to Aggregate Size	=	18.	in
Offset of Center of Rebar Cage from Center of Pile	=	0.00000	in
Yield Stress of Reinforcing Bars	=	60000.	psi
Modulus of Elasticity of Reinforcing Bars	=	29000000.	psi
Gross Area of Pile	=	1885.74099	sq. in.
Area of Concrete	=	1800.07737	sq. in.
Cross-sectional Area of Steel Casing	=	76.18362	sq. in.
Area of All Steel (Casing and Bars)	=	85.66362	sq. in.
Area Ratio of All Steel to Gross Area of Pile	=	4.34	percent

Axial Structural Capacities:

Nom. Axial Structural Capacity = 0.85 Fc Ac + Fy As	=	7901.608	Kips
Tensile Load for Cracking of Concrete	=	959.735	Kips
Nominal Axial Tensile Capacity	=	-3311.410	Kips

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Reinforcing Bar Dimensions and Positions used in Computations:

Bar Number	Bar Diam. inches	Bar Area sq. in.	X inches	Y inches
1	1.00000	0.79000	19.50000	0.00000
2	1.00000	0.79000	16.88750	9.75000
3	1.00000	0.79000	9.75000	16.88750
4	1.00000	0.79000	0.00000	19.50000
5	1.00000	0.79000	-9.75000	16.88750
6	1.00000	0.79000	-19.50000	9.75000
7	1.00000	0.79000	-16.88750	0.00000
8	1.00000	0.79000	-9.75000	-16.88750
9	1.00000	0.79000	-0.00000	-19.50000
10	1.00000	0.79000	9.75000	-16.88750
11	1.00000	0.79000	16.88750	-9.75000
12	1.00000	0.79000	16.88750	0.00000

NOTE: The positions of the above rebars were computed by LPILE

Minimum spacing between any two bars not equal to zero = 9.09394 inches between Bars 7 and 8

Concrete Properties:

Compressive Strength of Concrete = 3000.00000 psi
Modulus of Elasticity of Concrete = 3122019. psi
Modulus of Rupture of Concrete = -410.79191 psi
Compression Strain at Peak Stress = 0.00163
Tension Strain at Fracture of Concrete = -0.0001160
Maximum Coarse Aggregate Size = 0.00000 in

Number of Axial Thrust Force Values Determined from Pile-head Loadings = 2

Number	Axial Thrust Force kips
1	311.000
2	402.100

Definitions of Run Messages and Notes:

C = concrete in section has cracked in tension.
Y = stress in reinforcing steel has reached yield stress.
T = ACI 318-08 criteria for tension-controlled section met, tensile strain in reinforcement exceeds 0.005 while simultaneous compressive strain in concrete is more than 0.003. See ACI 318-08, section 10.3.4.
Z = depth of tensile zone in concrete section is less than 10 percent of section depth.

Bending stiffness (EI) = Computed Bending Moment / Curvature.
Position of neutral axis is measured from edge of compression side of pile.
Compressive stresses and strains are positive in sign.
Tensile stresses and strains are negative in sign.

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Axial Thrust Force = 311.000 kips

Bending Curvature rad/in.	Max Concrete Stress ksi	Bending Moment in-kip	Bending Steel Stress ksi	Max Casting Stress kip-in ²	Run Msg	Depth to		Max Comp		Max Tens	
						N Axis	in	Strain	in/in	Strain	in/in
0.00000625	1020.3214226	1632.14226	1.4392001	1632.14226	79.6491408	0.0000498	0.0000192	0.0000498	0.0000192	0.000000151	0.000003881
0.00001250	2040.6270179	1632.501614	1.8799267	1632.501614	52.1050455	0.0000651	0.00003881	0.0000651	0.00003881	-0.000001114	-0.0000266
0.00001875	3060.9350883	1632.89604	2.3213677	1632.89604	42.9368208	0.0000805	-0.0000114	0.0000805	-0.0000114	-0.0000266	-0.0000418
0.00002500	4079.1054018	1631.642161	2.7632821	1631.642161	38.3592360	0.0000959	-0.0000266	0.0000959	-0.0000266	-0.0000418	-0.0000570
0.00003125	5094.4916454	1630.237327	3.2054308	1630.237327	35.6152703	0.0001113	-0.0000418	0.0001113	-0.0000418	-0.0000570	-0.0000723
0.00003750	6106.4706701	1628.92179	3.6477102	1628.92179	33.7871625	0.0001267	-0.0000570	0.0001267	-0.0000570	-0.0000723	-0.0000875
0.00004375	7114.8891887	1626.60386	4.0900733	1626.60386	32.4820312	0.0001421	-0.0000723	0.0001421	-0.0000723	-0.0000875	-0.0001027
0.00005000	8119.6807854	1623.936157	4.5324959	1623.936157	31.5035924	0.0001575	-0.0001027	0.0001575	-0.0001027	-0.0001027	-0.0001181
0.00005625	9120.8127913	1621.477830	4.9749640	1621.477830	30.7428636	0.0001729	-0.0001181	0.0001729	-0.0001181	-0.0001181	-0.0001335
0.00006250	9120.8127913	1459.330047	4.9198791	1459.330047	27.3891606	0.0001712	-0.0001335	0.0001712	-0.0001335	-0.0001335	-0.0001489
0.00006875	9120.8127913	1326.663679	5.2673748	1326.663679	26.6644349	0.0001833	-0.0001489	0.0001833	-0.0001489	-0.0001489	-0.0001643
0.00007500	9120.8127913	1216.08372	5.6122200	1216.08372	26.0487700	0.0001954	-0.0001643	0.0001954	-0.0001643	-0.0001643	-0.0001797
0.00008125	9667.3567964	1189.828529	5.955031	1189.828529	25.5203447	0.0002074	-0.0001797	0.0002074	-0.0001797	-0.0001797	-0.0001951
0.00008750	6.2972361	1027.2	6.2972361	1027.2	25.0616937	0.0002193	-0.0001951	0.0002193	-0.0001951	-0.0001951	-0.0002105
0.00009375	10875	10875	10875	10875	24.6601383	0.0002312	-0.0002105	0.0002312	-0.0002105	-0.0002105	-0.0002259
0.00010000	6.6378657	11476	6.6378657	11476	24.3055242	0.0002431	-0.0002259	0.0002431	-0.0002259	-0.0002259	-0.0002413
0.00010625	-7.0903480	12075	-7.0903480	12075	23.9894799	0.0002549	-0.0002413	0.0002549	-0.0002413	-0.0002413	-0.0002567
0.00011250	-7.6308738	12673	-7.6308738	12673	23.7077461	0.0002667	-0.0002567	0.0002667	-0.0002567	-0.0002567	-0.0002721
0.00011875	-8.1716666	13270	-8.1716666	13270	23.4531991	0.0002785	-0.0002721	0.0002785	-0.0002721	-0.0002721	-0.0002875
0.00012500	-8.7133077	13865	-8.7133077	13865	23.2239888	0.0002903	-0.0002875	0.0002903	-0.0002875	-0.0002875	-0.0003029
0.00013125	-9.2549915	14460	-9.2549915	14460	23.0146565	0.0003021	-0.0003029	0.0003021	-0.0003029	-0.0003029	-0.0003183
0.00013750	-9.7974182	15053	-9.7974182	15053	22.8249906	0.0003138	-0.0003183	0.0003138	-0.0003183	-0.0003183	-0.0003337
0.00014375	-10.3395912	15646	-10.3395912	15646	22.6502315	0.0003256	-0.0003337	0.0003256	-0.0003337	-0.0003337	-0.0003491
0.00015000	-10.8824738	16241	-10.8824738	16241	22.4900158	0.0003374	-0.0003491	0.0003374	-0.0003491	-0.0003491	-0.0003645
0.00015625	-11.4259586	16836	-11.4259586	16836	22.3431824	0.0003491	-0.0003645	0.0003491	-0.0003645	-0.0003645	-0.0003799
0.00016250	-11.9678848	17431	-11.9678848	17431	22.2067237	0.0003609	-0.0003799	0.0003609	-0.0003799	-0.0003799	-0.0003953
0.00016875	-12.5108751	18026	-12.5108751	18026							

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		Abut B.1p70		Abut B.1p70			
0.0000169	180099	1067173190.	21.0801491	0.0003726	-0.0004543	2.4734381	-40.1756596
1.2007357	-13.0540051	C	22.0801491	0.0003844	-0.0004731	2.0004494	46442.
1.2357759	18597.	C	21.9631263	0.0003961	-0.0004920	2.5048659	-41.3327489
1.2357759	-13.5968759	C	21.8546689	0.0004079	-0.0005109	0.0005056	47113.
1.2661474	19186.	C	21.7530428	0.0004196	-0.0005298	2.5348518	-42.4993637
1.2661474	-14.1394865	C	21.6576430	0.0004314	-0.0005486	2.5633918	47746.
1.2838334	19773.	C	21.5686613	0.0004431	-0.0005675	2.5633918	-43.6765243
1.2838334	-14.6823142	C	21.4855159	0.0004549	-0.0005863	2.5907135	48349.
1.3303043	20360.	C	21.4076936	0.0004667	-0.0006052	2.5907135	-44.8604143
1.3303043	-15.2253274	C	21.3347397	0.0004785	-0.0006240	2.6168695	48927.
1.3619476	20946.	C	21.2653913	0.0004902	-0.0006429	2.6168695	-46.0505603
1.3619476	-15.7680764	C	21.1998678	0.0005020	-0.0006617	2.6418688	49478.
1.4243993	21532.	C	21.1381885	0.0005138	-0.0006805	2.6658063	50008.
1.4243993	-16.8527775	C	20.9734185	0.0005374	-0.0007182	2.6658063	-48.4494143
1.4552064	22701.	C	20.8781196	0.0005611	-0.0007558	2.6886247	50517.
1.4552064	-17.3947276	C	20.7920762	0.0005848	-0.0007933	2.6886247	-49.6585667
1.4856830	23285.	C	20.7138153	0.0006085	-0.0008309	2.7104145	51009.
1.4856830	-16.3105601	C	20.6432361	0.0006322	-0.0008684	2.7312497	-52.0924763
1.5186066	23868.	C	20.5794458	0.0006560	-0.0009059	2.7312497	51484.
1.5186066	-17.9369696	C	20.5216865	0.0006798	-0.0009433	2.7511599	-53.3156376
1.5457585	24451.	C	20.4693106	0.0007036	-0.0010181	2.7511599	51944.
1.5457585	-18.4791605	C	20.4217617	0.0007275	-0.0010554	2.7701722	-54.5425537
1.6000231	25032.	C	20.3785591	0.0007515	-0.0010927	2.7701722	52824.
1.6000231	-19.0210788	C	20.3392850	0.0007754	-0.0011299	2.8833362	-55.7729518
1.6000231	-16.8527775	C	20.3029816	0.0007994	-0.0011672	2.8833362	53075.
1.6337675	26195.	C	20.2698990	0.0008235	-0.0012043	2.8945565	-56.0000000
1.6337675	-20.6451877	C	20.2398320	0.0008475	-0.0012415	2.8945565	53889.
1.6910299	27354.	C	20.2125281	0.0008717	-0.0012792	2.9069538	-56.0000000
1.6910299	-21.7265436	C	20.1855151	0.0008952	-0.0013180	2.9069538	56798.
1.7471888	28512.	C	20.1532375	0.0009177	-0.0013573	2.9489336	-60.0000000
1.7471888	-22.8072597	C	20.1132375	0.0009395	-0.0013972	2.9489336	57704.
1.8020110	29667.	C	20.0734185	0.0009610	-0.0014372	2.9782536	-60.0000000
1.8020110	-23.8875842	C	20.0332361	0.0009828	-0.0014771	2.9782536	58450.
1.8576833	30819.	C	20.0006322	0.0010046	-0.0015170	2.9951357	-60.0000000
1.8576833	-24.9667602	C	20.0006560	0.0010263	-0.0015569	2.9951357	59010.
1.9083705	31969.	C	20.0006798	0.0010481	-0.0015967	2.9951357	-60.0000000
1.9083705	-26.0447778	C	20.0007036	0.0010699	-0.0016365	2.9951357	59511.
1.9598268	33117.	C	20.0007275	0.0010917	-0.0016763	2.9951357	-60.0000000
1.9598268	-27.1216267	C	20.0007515	0.0011135	-0.0017161	2.9951357	60363.
2.010287	34263.	C	20.0007754	0.0011353	-0.0017559	2.9951357	-60.0000000
2.010287	-28.1972965	C	20.0007994	0.0011571	-0.0017956	2.9951357	60736.
2.0592645	35406.	C	20.0008235	0.0011789	-0.0018353	2.9951357	-60.0000000
2.0592645	-29.2717767	C	20.0008475	0.0012003	-0.0018750	2.9951357	61064.
2.0772344	36546.	C	20.0008717	0.0012217	-0.0019147	2.9951357	-60.0000000
2.0772344	-30.3450564	C	20.0008952	0.0012431	-0.0019544	2.9951357	61305.
2.1340303	37684.	C	20.0009177	0.0012645	-0.0019941	2.9951357	-60.0000000
2.1340303	-31.4171248	C	20.0009395	0.0012859	-0.0020338	2.9951357	61546.
2.1996026	38820.	C	20.0009610	0.0013073	-0.0020735	2.9951357	-60.0000000
2.1996026	-32.4886484	C	20.0009828	0.0013287	-0.0021132	2.9951357	61787.
2.2439868	39953.	C	20.0009828	0.0013501	-0.0021529	2.9951357	-60.0000000
2.2439868	-33.5590095	C	20.0009828	0.0013715	-0.0021926	2.9951357	62028.
2.2439868	401084.	C	20.0009828	0.0013929	-0.0022323	2.9951357	-60.0000000
2.2878832	-34.6281070	C	20.0009828	0.0014143	-0.0022720	2.9951357	62269.
2.3201632	41084.	C	20.0009828	0.0014357	-0.0023117	2.9951357	-60.0000000
2.3201632	-35.6923288	C	20.0009828	0.0014571	-0.0023514	2.9951357	62510.
2.3686844	42165.	C	20.0009828	0.0014785	-0.0023911	2.9951357	-60.0000000
2.3686844	-36.7813121	C	20.0009828	0.0015000	-0.0024308	2.9951357	62751.
2.4057016	43246.	C	20.0009828	0.0015214	-0.0024705	2.9951357	-60.0000000
2.4057016	-37.8966311	C	20.0009828	0.0015428	-0.0025102	2.9951357	62992.
2.4404143	44917.	C	20.0009828	0.0015642	-0.0025499	2.9951357	-60.0000000
2.4404143	-39.0307711	C	20.0009828	0.0015856	-0.0025896	2.9951357	63233.
0.0000481	45732.	C	20.0009828	0.0016070	-0.0026293	2.9951357	-60.0000000
			19.9681413	0.0009610	-0.0013972	2.9979885	60.0000000

Abut. B.1p70		Abut. B.1p70		Abut. B.1p70		Abut. B.1p70	
Bending Max Concrete Curvature	Bending Max Steel Stress	Max Casting Stress	Bonding Steel Stress	Depth to Run N Axis	Max Comp Strain	Max Tens Strain	in/in
0.0001294	61507.	475416007.	16.7838309	0.0021714	-0.0041680		
2.9999989	60.0000000	36.0000000	CY	0.0022427	-0.0043416		
0.0001344	61689.	459080521.	CY	0.0023142	-0.0045152		
2.9997000	60.0000000	36.0000000	CY	0.0023859	-0.0046885		
0.0001394	61856.	443808545.	CY	0.0024577	-0.0048617		
2.9985066	60.0000000	36.0000000	CY	0.0025294	-0.0050349		
0.0001444	62009.	429499784.	CY	0.0026009	-0.0052085		
2.9980249	60.0000000	36.0000000	CY	0.0026727	-0.0053816		
0.0001494	62151.	416075004.	CY	0.0027445	-0.0055548		
2.9996188	60.0000000	36.0000000	CY	0.0028166	-0.0057278		
0.0001544	62279.	403427085.	CY	0.0028886	-0.0059007		
2.9972257	60.0000000	36.0000000	CY	0.0029613	-0.0060731		
0.0001594	62399.	391525321.	CY	0.0030339	-0.0062455		
2.9999123	60.0000000	36.0000000	CY	0.0031072	-0.0064171		
0.0001644	62510.	380292009.	CY	0.0031809	-0.0065884		
2.9973970	60.0000000	36.0000000	CY	0.0032547	-0.0067597		
0.0001694	62613.	369673422.	CY	0.0033283	-0.0069311		
2.9989997	60.0000000	36.0000000	CY	0.0034018	-0.0071025		
0.0001744	62713.	359442534.	CY	0.0034758	-0.0072736		
2.9964818	60.0000000	36.0000000	CY	0.0035500	-0.0074444		
0.0001794	62802.	350118290.	CY	0.0036241	-0.0076153		
2.9995780	60.0000000	36.0000000	CY	0.0036974	-0.0077869		
0.0001844	62887.	34081203.	CY	0.0037707	-0.0079587		
2.9963068	60.0000000	36.0000000	CY	0.0038443	-0.0081301		
0.0001894	62963.	332480210.	CY				
2.9983811	60.0000000	36.0000000	CY				
0.0001944	63033.	324285803.	CY				
2.9999924	60.0000000	36.0000000	CY				
0.0001994	63095.	316485703.	CY				
2.9953135	60.0000000	36.0000000	CY				
0.0002044	63154.	309012146.	CY				
2.9989045	60.0000000	36.0000000	CY				
0.0002094	63211.	301905396.	CY				
2.9959989	60.0000000	36.0000000	CY				
0.0002144	63263.	295104639.	CY				
2.9944950	60.0000000	36.0000000	CY				
0.0002194	63312.	288601629.	CY				
2.9983007	60.0000000	36.0000000	CY				
0.0002244	63360.	282384071.	CY				
2.9999224	60.0000000	36.0000000	CY				
0.0002294	63400.	276911602.	CY				
2.9960920	60.0000000	36.0000000	CY				
0.0002344	63439.	270629400.	CY				
2.9958530	60.0000000	36.0000000	CY				
0.0002394	63469.	265145637.	CY				
2.9987898	60.0000000	36.0000000	CY				
0.0002444	63492.	259813488.	CY				
2.9999767	60.0000000	36.0000000	CY				

Axial Thrust Force = 402.100 kips

Max Concrete Curvature		Max Steel Stress		Max Casting Stress		Max Comp Strain		Max Tens Strain	
0.00000625	1016.6100280	1626576045.	95.9611911	0.0000600	0.0000294				
0.2157030	11.7348560	1.7348560	60.2612117	0.0000753	0.0000141				
0.000001250	2033.2076278	1626566102.							

Load No.	Axial Thrust kips	Nominal Mom. Cap. in-kip	Max. Comp. Strain
1	311.000	6297.656	0.00300000
2	402.100	63739.524	0.00300000

Note note that the values of moment capacity in the table above are not factored by a strength reduction factor (phi-factor).

In ACI 318-08, the value of the strength reduction factor depends on whether the transverse reinforcing steel bars are tied hoops (0.65) or spirals (0.70).

The above values should be multiplied by the appropriate strength reduction factor to compute ultimate moment capacity according to ACI 318-08, Section 9.3.2.2 or the value required by the design standard being followed.

The following table presents factored moment capacities and corresponding bending stiffnesses computed for common resistance factor values used for reinforced concrete sections.

Axial Resistance Bending Stiffness Nominal Ultimate (Factored) Ultimate (Factored)

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Load Capacity No. in-kip	Factor at Ult. for Moment	Moment Capacity at Ult. Mom. Cap. kip-in ²	Axial Thrust kips	Moment
1	0.65	981485158.029	202.150	
2	0.65	992682181.838	261.365	
1	0.70	62927.656	217.700	
2	0.70	63739.524	281.470	
1	0.75	929295872.157	233.250	
2	0.75	945313053.025	301.575	

Computed Values of Pile Loading and Deflection for Lateral Loading for Load Case Number 1

Pile-head conditions are Shear and Moment (Loading Type 1)

Shear force at pile head = 55300.0 lbs
Applied moment at pile head = 3729000.0 in-lbs
Axial thrust load on pile head = 402100.0 lbs

Depth Res. X	Soil Spr. lb/inch	Deflect. Spr. lb/inch	Bending Moment in-lbs	Shear Force lbs	Slope S radians	Total Stress psi*	Bending Stiffness lb-in ²	Soil P lb/in
0.00	0.00	0.2366	3729000.0	55300.0	-0.001540	0.000	1.626E+12	
0.000	0.000	0.000	0.000	55300.0	-0.001526	0.000	1.626E+12	
0.000	0.000	0.2474	4064499.0	55300.0	-0.001510	0.000	1.626E+12	
0.000	1.000	0.000	4599962.0	55300.0	-0.001493	0.000	1.626E+12	
1.500	1.500	0.2293	4735386.0	54779.0	-0.001475	0.000	1.626E+12	
-173.8154	4547.6323	0.000	5064510.0	53725.0	-0.001456	0.000	1.625E+12	
-177.2057	4823.6874	0.000	5387209.0	52653.0	-0.001435	0.000	1.625E+12	
-180.3595	5113.5706	0.000	5703868.0	51562.0	-0.001414	0.000	1.624E+12	
-183.2750	5418.3793	0.000	6028708.0	50454.0	-0.001391	0.000	1.624E+12	
3.500	3.500	0.1194	6315000.0	49331.0	-0.001367	0.000	1.623E+12	
-185.5736	5739.3160	0.000	6611564.0	48194.0	-0.001367	0.000	1.623E+12	
-188.3029	6077.0927	0.000	6927777.0	47061.0	-0.001367	0.000	1.623E+12	
-190.5910	6434.9798	0.000	7260000.0	45928.0	-0.001367	0.000	1.623E+12	

-192.5494	5.000	0.1696	6900567.	0.000	0.000	1.623E+12	0.000	1.623E+12	0.000
-194.2668	5.500	0.1616	7182578.	0.000	0.000	1.622E+12	0.000	1.623E+12	0.000
-195.7430	6.000	0.1538	7457530.	0.000	0.000	1.622E+12	0.000	1.624E+12	0.000
-196.9779	6.500	0.1461	7725369.	0.000	0.000	1.621E+12	0.000	1.624E+12	0.000
-197.3167	7.000	0.1387	7986048.	0.000	0.000	1.621E+12	0.000	1.625E+12	0.000
-198.6197	7.500	0.1314	8225332.	0.000	0.000	1.620E+12	0.000	1.625E+12	0.000
-199.9228	8.000	0.1242	8441330.	0.000	0.000	1.620E+12	0.000	1.626E+12	0.000
-200.2259	8.500	0.1173	8633193.	0.000	0.000	1.619E+12	0.000	1.626E+12	0.000
-201.5290	9.000	0.1106	8800744.	0.000	0.000	1.619E+12	0.000	1.626E+12	0.000
-202.8321	9.500	0.1040	8943940.	0.000	0.000	1.619E+12	0.000	1.626E+12	0.000
-203.1352	10.000	0.0977	9062869.	0.000	0.000	1.618E+12	0.000	1.626E+12	0.000
-204.4383	10.500	0.0915	9157739.	0.000	0.000	1.618E+12	0.000	1.626E+12	0.000
-205.7414	11.000	0.0856	9228873.	0.000	0.000	1.618E+12	0.000	1.626E+12	0.000
-206.0445	11.500	0.0798	9276695.	0.000	0.000	1.618E+12	0.000	1.626E+12	0.000
-207.3476	12.000	0.0743	9301727.	0.000	0.000	1.618E+12	0.000	1.626E+12	0.000
-208.6507	12.500	0.0690	9304578.	0.000	0.000	1.618E+12	0.000	1.626E+12	0.000
-209.9538	13.000	0.0639	9285935.	0.000	0.000	1.618E+12	0.000	1.626E+12	0.000
-210.2569	13.500	0.0590	9246558.	0.000	0.000	1.618E+12	0.000	1.627E+12	0.000
-211.5600	14.000	0.0543	9187270.	0.000	0.000	1.618E+12	0.000	1.627E+12	0.000
-212.8631	14.500	0.0498	9108949.	0.000	0.000	1.619E+12	0.000	1.627E+12	0.000
-213.1662	15.000	0.0455	9012520.	0.000	0.000	1.619E+12	0.000	1.627E+12	0.000
-214.4693	15.500	0.0414	8898952.	0.000	0.000	1.619E+12	0.000	1.627E+12	0.000
-215.7724	16.000	0.0375	8769245.	0.000	0.000	1.619E+12	0.000	1.627E+12	0.000
-216.0755	16.500	0.0338	8624426.	0.000	0.000	1.620E+12	0.000	1.627E+12	0.000
-217.3786	17.000	0.0303	8465344.	0.000	0.000	1.620E+12	0.000	1.627E+12	0.000
-218.6817	17.500	0.0270	8293762.	0.000	0.000	1.620E+12	0.000	1.627E+12	0.000
-219.9848	18.000	0.0238	8110440.	0.000	0.000	1.621E+12	0.000	1.627E+12	0.000
-220.2879	18.500	0.0209	7915740.	0.000	0.000	1.621E+12	0.000	1.627E+12	0.000
-221.5910	19.000	0.0181	7711625.	0.000	0.000	1.621E+12	0.000	1.627E+12	0.000
-222.8941	19.500	0.0155	7486848.	0.000	0.000	1.622E+12	0.000	1.627E+12	0.000
-224.1972	20.000	0.0127	7197041.	0.000	0.000	1.622E+12	0.000	1.627E+12	0.000
-225.5003	20.500	0.0101	6900567.	0.000	0.000	1.622E+12	0.000	1.627E+12	0.000
-226.8034	21.000	0.0074	6604090.	0.000	0.000	1.623E+12	0.000	1.627E+12	0.000
-228.1065	21.500	0.0048	6308613.	0.000	0.000	1.623E+12	0.000	1.627E+12	0.000
-229.4096	22.000	0.0022	6013136.	0.000	0.000	1.623E+12	0.000	1.627E+12	0.000
-230.7127	22.500	0.0000	5717659.	0.000	0.000	1.623E+12	0.000	1.627E+12	0.000
-232.0158	23.000	0.0000	5422182.	0.000	0.000	1.623E+12	0.000	1.627E+12	0.000
-233.3189	23.500	0.0000	5126705.	0.000	0.000	1.623E+12	0.000	1.627E+12	0.000
-234.6220	24.000	0.0000	4831228.	0.000	0.000	1.623E+12	0.000	1.627E+12	0.000
-235.9251	24.500	0.0000	4535751.	0.000	0.000	1.623E+12	0.000	1.627E+12	0.000
-237.2282	25.000	0.0000	4240274.	0.000	0.000	1.623E+12	0.000	1.627E+12	0.000
-238.5313	25.500	0.0000	3944797.	0.000	0.000	1.623E+12	0.000	1.627E+12	0.000
-239.8344	26.000	0.0000	3649320.	0.000	0.000	1.623E+12	0.000	1.627E+12	0.000
-241.1375	26.500	0.0000	3353843.	0.000	0.000	1.623E+12	0.000	1.627E+12	0.000
-242.4406	27.000	0.0000	3058366.	0.000	0.000	1.623E+12	0.000	1.627E+12	0.000
-243.7437	27.500	0.0000	2762889.	0.000	0.000	1.623E+12	0.000	1.627E+12	0.000
-245.0468	28.000	0.0000	2467412.	0.000	0.000	1.623E+12	0.000	1.627E+12	0.000
-246.3499	28.500	0.0000	2171935.	0.000	0.000	1.623E+12	0.000	1.627E+12	0.000
-247.6530	29.000	0.0000	1876458.	0.000	0.000	1.623E+12	0.000	1.627E+12	0.000
-248.9561	29.500	0.0000	1580981.	0.000	0.000	1.623E+12	0.000	1.627E+12	0.000
-250.2592	30.000	0.0000	1285504.	0.000	0.000	1.623E+12	0.000	1.627E+12	0.000
-251.5623	30.500	0.0000	990027.	0.000	0.000	1.623E+12	0.000	1.627E+12	0.000
-252.8654	31.000	0.0000	692500.	0.000	0.000	1.623E+12	0.000	1.627E+12	0.000
-254.1685	31.500	0.0000	394973.	0.000	0.000	1.623E+12	0.000	1.627E+12	0.000
-255.4716	32.000	0.0000	97.206.	0.000	0.000	1.623E+12	0.000	1.627E+12	0.000
-256.7747	32.500	0.0000	0.000.	0.000	0.000	1.623E+12	0.000	1.627E+12	0.000

Abut 6.1p7e

Abut 6.1p7e

Stresses in concrete and steel may be interpolated from the output for nonlinear bending properties relative to the magnitude of bending moment developed in the pile.

Output Summary for Load Case No. 1:

Pile-head deflection = 0.2566471 inches
 Computed slope at pile head = -0.0015401 radians
 Maximum bending moment = 9304578.7 inch-lbs
 Maximum shear force = 55300. lbs
 Depth of maximum bending moment = 12.500000 feet below pile head
 Depth of maximum shear force = 0.5000000 feet below pile head
 Number of iterations = 8
 Number of zero deflection points = 2

Pile-head Deflection vs. Pile Length for Load Case 1
 Boundary Condition Type 1, Shear and Moment
 Shear Moment = 55300. lb
 Axial Load = 3729000. in-lb

Pile Length feet	Pile Head Deflection inches	Maximum Moment in-lbs	Maximum Shear lbs
50.0000	0.2566471	9304578.	55300.
47.5000	0.2612046	9429599.	55300.
45.0000	0.2615699	9427119.	55300.
42.5000	0.2617892	9411836.	55300.
40.0000	0.2624987	9374333.	55300.
37.5000	0.2649256	9309018.	55300.
35.0000	0.2784922	9368765.	55300.
32.5000	0.2916303	9225003.	-5702.
30.0000	0.3242591	9112750.	-61778.
27.5000	0.4155010	8989827.	-70341.
25.0000	0.6293221	8700625.	-79532.
22.5000	1.2350755	8521834.	-95796.
20.0000	3.0415138	8453014.	-117506.

Computed Values of Pile Loading and Deflection for Lateral Loading for Load Case Number 2

Pile-head conditions are Shear and Moment (Loading Type 1)

Shear force at pile head = 42300.0 lbs
 Applied moment at pile head = 2808000.0 in-lbs
 Axial thrust load on pile head = 3110000.0 lbs

Depth, Res. X, Es*h	Soil Spr. y	Distrib. Lat. Load	Bending Moment	Shear Force	Slope	Total Stress	Bending Stress	Soil Stiffness
0.000	1.627E+12	0.000	731051.	0.000	1.627E+12	0.000	0.000	
0.000	1.627E+12	0.000	637780.	0.000	1.627E+12	0.000	0.000	
0.000	1.627E+12	0.000	551752.	0.000	1.627E+12	0.000	0.000	
0.000	1.627E+12	0.000	472796.	0.000	1.627E+12	0.000	0.000	
0.000	1.627E+12	0.000	400721.	0.000	1.627E+12	0.000	0.000	
0.000	1.627E+12	0.000	335322.	0.000	1.627E+12	0.000	0.000	
0.000	1.627E+12	0.000	276372.	0.000	1.627E+12	0.000	0.000	
0.000	1.627E+12	0.000	223631.	0.000	1.627E+12	0.000	0.000	
0.000	1.627E+12	0.000	176845.	0.000	1.627E+12	0.000	0.000	
0.000	1.627E+12	0.000	135744.	0.000	1.627E+12	0.000	0.000	
0.000	1.627E+12	0.000	100048.	0.000	1.627E+12	0.000	0.000	
0.000	1.627E+12	0.000	69462.	0.000	1.627E+12	0.000	0.000	
0.000	1.627E+12	0.000	43683.	0.000	1.627E+12	0.000	0.000	
0.000	1.627E+12	0.000	22394.	0.000	1.627E+12	0.000	0.000	
0.000	1.627E+12	0.000	5270.4037	0.000	1.627E+12	0.000	0.000	
0.000	1.627E+12	0.000	-8022.5562	0.000	1.627E+12	0.000	0.000	
0.000	1.627E+12	0.000	-17829.	0.000	1.627E+12	0.000	0.000	
0.000	1.627E+12	0.000	-24502.	0.000	1.627E+12	0.000	0.000	
0.000	1.627E+12	0.000	-28403.	0.000	1.627E+12	0.000	0.000	
0.000	1.627E+12	0.000	-29901.	0.000	1.627E+12	0.000	0.000	
0.000	1.627E+12	0.000	-29374.	0.000	1.627E+12	0.000	0.000	
0.000	1.627E+12	0.000	-27209.	0.000	1.627E+12	0.000	0.000	
0.000	1.627E+12	0.000	-19349.	0.000	1.627E+12	0.000	0.000	
0.000	1.627E+12	0.000	-13342.	0.000	1.627E+12	0.000	0.000	
0.000	1.627E+12	0.000	6370.8989	0.000	1.627E+12	0.000	0.000	
0.000	1.627E+12	0.000	1695.9632	0.000	1.627E+12	0.000	0.000	
0.000	1.627E+12	0.000	301067.	0.000	1.627E+12	0.000	0.000	
0.000	1.627E+12	0.000	0.000	0.000	1.627E+12	0.000	0.000	

* This analysis computed pile response using nonlinear moment-curvature relationships. Only values of total stress due to combined axial and bending stresses are computed for elastic sections only and do not equal the actual stresses in concrete and steel.

Abut. B.1p7o

Abut. B.1p7o	1.627E+12	0.000	731051.	-0.000	36.500	-0.007964	205.5305	154837	-16144.	4.361E-05	0.000	1.627E+12	0.000	1.627E+12
-14923.			637780.		37.000	-0.007695	201.3398	156997	-13729.	4.833E-05	0.000	1.627E+12	0.000	1.627E+12
-12566.			472796.		38.000	-0.007115	196.5804	159157	-11435.	5.183E-05	0.000	1.627E+12	0.000	1.627E+12
-11435.			400721.		38.500	-0.006808	191.2883	161317	-10341.	5.318E-05	0.000	1.627E+12	0.000	1.627E+12
-10341.			335322.		39.000	-0.006493	185.4979	163477	-9285.7215	5.431E-05	0.000	1.627E+12	0.000	1.627E+12
-9285.7215			276372.		39.500	-0.006170	179.2470	165637	-8271.7015	5.523E-05	0.000	1.627E+12	0.000	1.627E+12
-8271.7015			223631.		40.000	-0.005841	165.4552	169957	-7301.3955	5.597E-05	0.000	1.627E+12	0.000	1.627E+12
-7301.3955			176845.		40.500	-0.005507	157.9802	172117	-6377.0020	5.655E-05	0.000	1.627E+12	0.000	1.627E+12
-6377.0020			135744.		41.000	-0.005169	150.1510	174277	-5500.5780	5.698E-05	0.000	1.627E+12	0.000	1.627E+12
-5500.5780			100048.		41.500	-0.004829	141.9903	176437	-4674.0520	5.730E-05	0.000	1.627E+12	0.000	1.627E+12
-4674.0520			69462.		42.000	-0.004486	133.5183	178597	-3899.2377	5.751E-05	0.000	1.627E+12	0.000	1.627E+12
-3899.2377			43683.		42.500	-0.004141	124.7531	180757	-3177.8477	5.763E-05	0.000	1.627E+12	0.000	1.627E+12
-3177.8477			22394.		43.000	-0.003795	115.7103	182917	-2511.5068	5.768E-05	0.000	1.627E+12	0.000	1.627E+12
-2511.5068			5270.4037		43.500	-0.003449	106.4034	185077	-1901.7655	5.767E-05	0.000	1.627E+12	0.000	1.627E+12
-1901.7655			-8022.5562		44.000	-0.003103	96.8437	187237	-1350.1130	5.763E-05	0.000	1.627E+12	0.000	1.627E+12
-1350.1130			-17829.		44.500	-0.002757	87.0405	189397	-857.9895	5.755E-05	0.000	1.627E+12	0.000	1.627E+12
-857.9895			-24502.		45.000	-0.002412	77.0007	191557	-426.7984	5.745E-05	0.000	1.627E+12	0.000	1.627E+12
-426.7984			-28403.		45.500	-0.002067	66.7297	193717	-57.9173	5.734E-05	0.000	1.627E+12	0.000	1.627E+12
-57.9173			-29901.		46.000	-0.001722	56.2307	195877	247.2918	5.723E-05	0.000	1.627E+12	0.000	1.627E+12
247.2918			-29374.		46.500	-0.001379	45.5057	198037	487.4732	5.713E-05	0.000	1.627E+12	0.000	1.627E+12
487.4732			-27209.		47.000	-0.001036	34.5548	200197	661.2694	5.704E-05	0.000	1.627E+12	0.000	1.627E+12
661.2694			-23800.		47.500	-0.000693	23.3773	202357	911.1242	5.696E-05	0.000	1.627E+12	0.000	1.627E+12
911.1242			-19349.		48.000	-0.000351	59.9077	204517	1121.0859	5.690E-05	0.000	1.627E+12	0.000	1.627E+12
1121.0859			-13342.		48.500	-9.685E-06	10.1735	206677	976.8360	5.686E-05	0.000	1.627E+12	0.000	1.627E+12
976.8360			6370.8989		49.000	0.000332	-38.1628	208837	553.7653	5.684E-05	0.000	1.627E+12	0.000	1.627E+12
553.7653			-1695.9632		49.500	0.000673	-82.8608	210997	0.000	5.684E-05	0.000	1.627E+12	0.000	1.627E+12
0.000			301067.		50.000	0.001014	-101.7277	301067.			0.000	1.627E+12	0.000	1.627E+12

* This analysis computed pile response using nonlinear moment-curvature relationships. Only values of total stress due to combined axial and bending stresses are computed for elastic sections only and do not equal the actual stresses in concrete and steel.

MOMENT FIXITY
 EL. 40-49 = -45.0

feet	inches	in-lbs	Abut B.1p70 lbs	radians	psi*	lb-in ²	lb/in
0.00	0.00	2808000.	42300.	-0.001140	0.000	1.632E+12	0.000
0.000	0.000	3063917.	42300.	-0.001129	0.000	1.632E+12	0.000
0.000	0.000	3319813.	42300.	-0.001117	0.000	1.632E+12	0.000
0.000	0.000	3575686.	41829.	-0.001104	0.000	1.632E+12	0.000
-156.9066	5580.4767	0.000	40879.	-0.001091	0.000	1.632E+12	0.000
-159.9556	5920.0707	0.000	39910.	-0.001076	0.000	1.632E+12	0.000
-162.7905	6276.7584	0.000	38926.	-0.001061	0.000	1.631E+12	0.000
-165.4103	6651.8963	0.000	37926.	-0.001045	0.000	1.631E+12	0.000
-167.8142	7046.9700	0.000	36913.	-0.001027	0.000	1.631E+12	0.000
-170.0018	7463.6101	0.000	35887.	-0.001010	0.000	1.630E+12	0.000
-171.9724	7903.6086	0.000	34850.	-0.000991	0.000	1.630E+12	0.000
-173.7255	8368.9389	0.000	33803.	-0.000971	0.000	1.630E+12	0.000
-175.2608	8861.7764	0.000	32747.	-0.000951	0.000	1.629E+12	0.000
-176.5781	9384.5231	0.000	31684.	-0.000930	0.000	1.629E+12	0.000
-177.6772	9939.8359	0.000	29729.	-0.000908	0.000	1.629E+12	0.000
-178.6772	10517.7192	0.000	26856.	-0.000886	0.000	1.628E+12	0.000
-179.5964	11118.6064	0.000	23935.	-0.000863	0.000	1.628E+12	0.000
-180.4366	11743.6064	0.000	20984.	-0.000839	0.000	1.628E+12	0.000
-181.1991	12393.6064	0.000	18021.	-0.000815	0.000	1.627E+12	0.000
-181.8844	13068.6064	0.000	15061.	-0.000791	0.000	1.627E+12	0.000
-182.4844	13768.6064	0.000	12120.	-0.000766	0.000	1.627E+12	0.000
-182.9991	14493.6064	0.000	9213.0325	-0.000741	0.000	1.627E+12	0.000
-183.4333	15243.6064	0.000	6352.2836	-0.000716	0.000	1.627E+12	0.000
-183.7877	16018.6064	0.000	3550.2786	-0.000690	0.000	1.627E+12	0.000
-184.0622	16818.6064	0.000	818.1776	-0.000665	0.000	1.627E+12	0.000
-184.2577	17643.6064	0.000	-1833.8723	-0.000639	0.000	1.627E+12	0.000
-184.3733	18493.6064	0.000	-4396.7222	-0.000614	0.000	1.627E+12	0.000
-184.4091	19368.6064	0.000	-6862.2029	-0.000588	0.000	1.627E+12	0.000
-184.3644	20268.6064	0.000	-9223.1034	-0.000563	0.000	1.627E+12	0.000
-184.2399	21193.6064	0.000	-11473.	-0.000538	0.000	1.627E+12	0.000
-184.0354	22143.6064	0.000	6756899.				

Abut B.1p70

-365.5267	60356.	0.000	-13607.	-0.000513	0.000	1.627E+12	0.000
-345.7450	62516.	0.000	-15620.	-0.000489	0.000	1.627E+12	0.000
-325.2861	64676.	0.000	-17509.	-0.000465	0.000	1.627E+12	0.000
-304.2881	66836.	0.000	-19270.	-0.000441	0.000	1.628E+12	0.000
-282.8832	68996.	0.000	-20896.	-0.000418	0.000	1.628E+12	0.000
-259.1468	70597.	0.000	-22386.	-0.000395	0.000	1.628E+12	0.000
-237.5274	72757.	0.000	-23747.	-0.000372	0.000	1.629E+12	0.000
-215.8479	74917.	0.000	-24977.	-0.000351	0.000	1.629E+12	0.000
-194.2155	77077.	0.000	-26078.	-0.000329	0.000	1.629E+12	0.000
-172.7308	79237.	0.000	-27050.	-0.000309	0.000	1.629E+12	0.000
-151.4872	81397.	0.000	-27896.	-0.000289	0.000	1.630E+12	0.000
-130.5718	83557.	0.000	-28618.	-0.000269	0.000	1.630E+12	0.000
-110.0645	85717.	0.000	-29219.	-0.000250	0.000	1.630E+12	0.000
-90.0386	87877.	0.000	-29700.	-0.000232	0.000	1.631E+12	0.000
-70.5605	90037.	0.000	-30067.	-0.000214	0.000	1.631E+12	0.000
-51.6903	92197.	0.000	-30323.	-0.000198	0.000	1.631E+12	0.000
-33.4814	94357.	0.000	-30471.	-0.000181	0.000	1.631E+12	0.000
-15.9810	96517.	0.000	-30517.	-0.000166	0.000	1.632E+12	0.000
0.7702	98677.	0.000	-30464.	-0.000151	0.000	1.632E+12	0.000
16.7372	100837.	0.000	-30318.	-0.000137	0.000	1.632E+12	0.000
31.8910	102997.	0.000	-30084.	-0.000123	0.000	1.632E+12	0.000
46.2079	105157.	0.000	-29766.	-0.000110	0.000	1.632E+12	0.000
59.6697	107317.	0.000	-29371.	-9.812E-05	0.000	1.632E+12	0.000
72.2633	109477.	0.000	-28902.	-8.657E-05	0.000	1.632E+12	0.000
83.9803	111637.	0.000	-28365.	-7.565E-05	0.000	1.632E+12	0.000
94.8171	113797.	0.000	-27767.	-6.535E-05	0.000	1.632E+12	0.000
104.7739	115957.	0.000	-27111.	-5.567E-05	0.000	1.632E+12	0.000
113.8800	118117.	0.000	-26403.	-4.659E-05	0.000	1.632E+12	0.000
122.0820	120277.	0.000	-25649.	-3.808E-05	0.000	1.632E+12	0.000
129.2750	122437.	0.000	-24852.	-3.015E-05	0.000	1.632E+12	0.000
135.9438	124597.	0.000	-24020.	-2.276E-05	0.000	1.633E+12	0.000
141.6363	126757.	0.000					

Abut. B. 1p7o		Abut. B. 1p7o	
30.500	-0.006819	1795690.	1.633E+12
146.5247	128917	0.000	0.000
31.000	-0.006895	1659420.	1.633E+12
150.6309	131077	0.000	0.000
31.500	-0.006934	1528561.	1.633E+12
153.9789	133237	0.000	0.000
32.000	-0.006939	1403235.	1.633E+12
156.5943	135397	0.000	0.000
32.500	-0.006914	1283537.	1.633E+12
158.5041	137557	0.000	0.000
33.000	-0.006860	1169536.	1.633E+12
159.7364	139177	0.000	0.000
33.500	-0.006780	1061278.	1.633E+12
160.3199	141877	0.000	0.000
34.000	-0.006677	958784.	1.633E+12
160.2842	144037	0.000	0.000
34.500	-0.006552	862053.	1.633E+12
159.6590	146197	0.000	0.000
35.000	-0.006409	771064.	1.633E+12
158.4743	148357	0.000	0.000
35.500	-0.006249	685776.	1.633E+12
156.7598	150517	0.000	0.000
36.000	-0.006073	606125.	1.633E+12
154.5451	152677	0.000	0.000
36.500	-0.005885	532034.	1.633E+12
151.8592	154837	0.000	0.000
37.000	-0.005684	463407.	1.633E+12
148.7303	156997	0.000	0.000
37.500	-0.005473	400131.	1.633E+12
145.1860	159157	0.000	0.000
38.000	-0.005254	342078.	1.633E+12
141.2527	161317	0.000	0.000
38.500	-0.005027	289108.	1.633E+12
136.9557	163477	0.000	0.000
39.000	-0.004793	241067.	1.633E+12
132.3193	165637	0.000	0.000
39.500	-0.004554	197788.	1.633E+12
127.3660	167797	0.000	0.000
40.000	-0.004311	159092.	1.633E+12
122.1173	169957	0.000	0.000
40.500	-0.004064	124792.	1.633E+12
116.5928	172117	0.000	0.000
41.000	-0.003815	94688.	1.633E+12
110.8108	174277	0.000	0.000
41.500	-0.003563	68572.	1.633E+12
104.7877	176437	0.000	0.000
42.000	-0.003310	46229.	1.633E+12
98.5386	178597	0.000	0.000
42.500	-0.003056	27432.	1.633E+12
92.0766	180757	0.000	0.000
43.000	-0.002802	11950.	1.633E+12
85.4132	182917	0.000	0.000
43.500	-0.002547	-456.9412	1.633E+12
78.5583	185077	0.000	0.000
44.000	-0.002292	-10036.	1.633E+12
71.5202	187237	0.000	0.000
44.500	-0.002037	-17040.	1.633E+12
64.3055	189397	0.000	0.000
45.000	-0.001783	-21229.	1.633E+12
56.9195	191557	0.000	0.000
45.500	-0.001529	-22369.	1.633E+12
49.3658	193717	0.000	0.000
46.000	-0.001276	-25232.	1.633E+12

41.6469	195877.	0.000	0.000
46.500	-0.001023	-24595.	1.633E+12
33.7640	198037.	0.000	0.000
47.000	-0.000771	-22742.	1.633E+12
25.7172	200197.	0.000	0.000
47.500	-0.000519	-19964.	1.633E+12
17.5057	202357.	0.000	0.000
48.000	-0.000268	-16555.	1.633E+12
52.3200	1172255.	0.000	0.000
48.500	-1.690E-05	-11262.	1.633E+12
13.2463	4704187.	0.000	0.000
49.000	0.000234	-5492.7228	1.633E+12
-48.8265	1253282.	0.000	0.000
49.500	0.000484	-1480.9502	1.633E+12
-70.3009	870994.	0.000	0.000
50.000	0.000735	0.000	0.000
-86.6030	353590.	0.000	0.000

* This analysis computed pile response using nonlinear moment-curvature relationships.
 Values of total stress due to combined axial and bending stresses are computed only for elastic sections only and do not equal the actual stresses in concrete and steel.
 Stresses in concrete and steel may be interpolated from the output for nonlinear bending properties relative to the magnitude of bending moment developed in the pile.

Output Summary for Load Case No. 2:
 Pile-head deflection = 0.1889141 inches
 Computed slope at pile head = -0.0011396 radians
 Maximum bending moment = 6917902. inch-lbs
 Maximum shear force = 42300. lbs
 Depth of maximum bending moment = 12.000000 feet below pile head
 Number of iterations = 8
 Number of zero deflection points = 2

----- Pile-head Deflection vs. Pile Length for Load Case 2 -----
 Boundary Condition Type 1, Shear and Moment
 Shear Moment = 42300. lb
 Axial Load = 2808000. in-lb
 = 311000. lb

Pile Length feet	Pile Head Deflection inches	Maximum Moment in-lb	Maximum Shear lbs
50.0000	0.1889141	6917902.	42300.
47.5000	0.1926131	7021285.	42300.
45.0000	0.1927952	7017190.	42300.
42.5000	0.1928455	7002310.	42300.
40.0000	0.1932162	6970058.	42300.
37.5000	0.1947160	6918623.	42300.

Abut B. 1p70		
95990.	-0.004214	0.000 1.102E+12
88429.	-0.004114	0.000 1.097E+12
80556.	-0.004011	0.000 1.092E+12
72438.	-0.003904	0.000 1.088E+12
64133.	-0.003795	0.000 1.084E+12
55683.	-0.003683	0.000 1.081E+12
47149.	-0.003569	0.000 1.079E+12
38611.	-0.003453	0.000 1.077E+12
30114.	-0.003335	0.000 1.075E+12
21646.	-0.003217	0.000 1.074E+12
13230.	-0.003097	0.000 1.073E+12
4937.8794	-0.002977	0.000 1.073E+12
-3160.1181	-0.002857	0.000 1.072E+12
-10993.	-0.002737	0.000 1.073E+12
-18491.	-0.002617	0.000 1.073E+12
-25589.	-0.002498	0.000 1.074E+12
-32013.	-0.002379	0.000 1.076E+12
-37701.	-0.002262	0.000 1.077E+12
-43048.	-0.002147	0.000 1.079E+12
-48257.	-0.002033	0.000 1.081E+12
-53305.	-0.001920	0.000 1.083E+12
-58172.	-0.001810	0.000 1.086E+12
-62834.	-0.001702	0.000 1.089E+12
-67272.	-0.001597	0.000 1.093E+12
-71467.	-0.001493	0.000 1.097E+12
-75438.	-0.001393	0.000 1.101E+12
-79216.	-0.001296	0.000 1.106E+12
-82786.	-0.001201	0.000 1.111E+12
-86126.	-0.001110	0.000 1.117E+12
-89121.	-0.001022	0.000 1.123E+12
-91627.	-0.000937	0.000 1.130E+12

Res. Soil Spr. Y	Depth X	Deflect. inches	Bending Moment in-lbs	Shear Force lbs	Slope radians	Total stress psi*	Bending stiffness lb-in ²	Soil stiffness P lb/in
35.0000	0.2042915	6962051.	42300.	6962051.	42300.	1.000000	1.626E+12	0.000
32.5000	0.2123715	6836385.	42300.	6836385.	42300.	1.000000	1.626E+12	0.000
30.0000	0.2313764	6725119.	44859.	6725119.	44859.	3729000.0	1.626E+12	0.000
27.5000	0.2713720	6630028.	49945.	6630028.	49945.	402100.0	1.625E+12	0.000
25.0000	0.3589947	6448177.	55626.	6448177.	55626.	1.000000	1.625E+12	0.000
22.5000	0.6255475	6312614.	60052.	6312614.	60052.	1.000000	1.619E+12	0.000
20.0000	1.3630075	6133162.	80052.	6133162.	80052.	1.000000	1.619E+12	0.000
17.5000	3.9970926	6159757.	-105117.	6159757.	-105117.	1.000000	1.617E+12	0.000

Computed Values of Pile Loading and Deflection for Lateral Loading for Load Case Number 3		
-1166.8732	9.000	18030031.
9.000	4.770	18030031.
-1231.2795	15488.	0.000
9.500	4.520	18593857.
-1288.9639	17109.	0.000
10.000	4.426	19111035.
-1335.5344	18738.	0.000
10.500	4.4039	19579880.
-1370.2811	20356.	0.000
11.000	4.3808	19999135.
-1398.1814	22031.	0.000
11.500	4.3584	20367788.
-1418.6064	23752.	0.000
12.000	4.3366	20685098.
-1426.0036	25419.	0.000
12.500	4.3155	20950795.
-1419.8081	26998.	0.000
13.000	4.2952	21165097.
-1412.7091	28717.	0.000
13.500	4.2755	21328256.
-1409.8937	30705.	0.000
14.000	4.2566	21440372.
-1395.3318	32631.	0.000
14.500	4.2383	21501967.
-1368.8569	34460.	0.000
15.000	4.2208	21513992.
-1330.4756	36148.	0.000
15.500	4.2041	21477830.
-1280.3933	37648.	0.000
16.000	4.1880	21395284.
-1219.0408	38906.	0.000
16.500	4.1727	21268564.
-1147.1017	39863.	0.000
17.000	4.1580	21100262.
-994.1684	37747.	0.000
17.500	4.1441	20895886.
-901.6555	37542.	0.000
18.000	4.1309	20658769.
-880.6119	40371.	0.000
18.500	4.1183	20389673.
-855.7517	43386.	0.000
19.000	4.1065	20089497.
-827.1580	46606.	0.000
19.500	4.0953	19759275.
-794.9379	50049.	0.000
20.000	4.0848	19400172.
-759.2216	53740.	0.000
20.500	4.0749	19013479.
-720.1599	57710.	0.000
-677.9221	61996.	0.000
21.000	4.0656	18600608.
-646.0632	66864.	0.000
21.500	4.0570	18163087.
-613.1826	72353.	0.000
22.000	4.0489	17702069.
-576.1250	78014.	0.000
22.500	4.0414	17218744.
-536.4890	83576.	0.000
23.000	4.0345	16714432.
-461.3409	89676.	0.000
23.500	4.0281	16180551.
24.000	4.0222	15649511.
-373.4009	96837.	0.000

Pile-head conditions are displacement and Moment (Loading Type 4)		
Displacement of pile head	=	1.000000 inches
Moment at pile head	=	3729000.0 in-lbs
AXIAL Load at pile head	=	402100.0 lbs
144640.	-0.005193	0.000 1.626E+12
144640.	-0.005178	0.000 1.626E+12
144640.	-0.005159	0.000 1.625E+12
143815.	-0.005137	0.000 1.624E+12
142148.	-0.005112	0.000 1.622E+12
140448.	-0.005084	0.000 1.621E+12
138715.	-0.005052	0.000 1.619E+12
136953.	-0.005017	0.000 1.617E+12
135163.	-0.004973	0.000 1.232E+12
133347.	-0.004919	0.000 1.210E+12
131509.	-0.004860	0.000 1.190E+12
129649.	-0.004796	0.000 1.173E+12
127770.	-0.004726	0.000 1.159E+12
125875.	-0.004652	0.000 1.146E+12
122145.	-0.004574	0.000 1.135E+12
116317.	-0.004490	0.000 1.125E+12
109976.	-0.004402	0.000 1.116E+12
103185.	-0.004310	0.000 1.109E+12

Computed Values of Pile Loading and Deflection for Lateral Loading for Load Case Number 3		
35.0000	0.2042915	6962051.
32.5000	0.2123715	6836385.
30.0000	0.2313764	6725119.
27.5000	0.2713720	6630028.
25.0000	0.3589947	6448177.
22.5000	0.6255475	6312614.
20.0000	1.3630075	6133162.
17.5000	3.9970926	6159757.

Computed Values of Pile Loading and Deflection for Lateral Loading for Load Case Number 3		
35.0000	0.2042915	6962051.
32.5000	0.2123715	6836385.
30.0000	0.2313764	6725119.
27.5000	0.2713720	6630028.
25.0000	0.3589947	6448177.
22.5000	0.6255475	6312614.
20.0000	1.3630075	6133162.
17.5000	3.9970926	6159757.

Abut. B. 1p7o		Abut. B. 1p7o		Abut. B. 1p7o		Abut. B. 1p7o	
24.500	0.0168	15095588.	0.000	1.138E+12	0.000	1.138E+12	0.000
-289.1896	102997.	0.000	0.000	1.147E+12	0.000	1.147E+12	0.000
25.000	0.0120	14530662.	0.000	1.156E+12	0.000	1.156E+12	0.000
-209.4778	105157.	0.000	0.000	1.167E+12	0.000	1.167E+12	0.000
25.500	0.007514	13958011.	0.000	1.178E+12	0.000	1.178E+12	0.000
-134.3998	107317.	0.000	0.000	1.191E+12	0.000	1.191E+12	0.000
26.000	0.003511	13380348.	0.000	1.204E+12	0.000	1.204E+12	0.000
-64.0548	109477.	0.000	0.000	1.220E+12	0.000	1.220E+12	0.000
26.500	-8.017E-05	12800212.	0.000	1.236E+12	0.000	1.236E+12	0.000
1.4916	111637.	0.000	0.000	1.250E+12	0.000	1.250E+12	0.000
27.000	-0.003280	12219973.	0.000	1.261E+12	0.000	1.261E+12	0.000
62.2056	113797.	0.000	0.000	1.262E+12	0.000	1.262E+12	0.000
27.500	-0.006110	11641825.	0.000	1.266E+12	0.000	1.266E+12	0.000
118.0833	115957.	0.000	0.000	1.266E+12	0.000	1.266E+12	0.000
28.000	-0.008592	11067788.	0.000	1.266E+12	0.000	1.266E+12	0.000
169.1486	118117.	0.000	0.000	1.266E+12	0.000	1.266E+12	0.000
28.500	-0.0107	10499709.	0.000	1.266E+12	0.000	1.266E+12	0.000
215.4519	120277.	0.000	0.000	1.266E+12	0.000	1.266E+12	0.000
29.000	-0.0126	9939263.	0.000	1.266E+12	0.000	1.266E+12	0.000
257.0668	122437.	0.000	0.000	1.266E+12	0.000	1.266E+12	0.000
29.500	-0.0142	9387983.	0.000	1.266E+12	0.000	1.266E+12	0.000
295.4173	124597.	0.000	0.000	1.266E+12	0.000	1.266E+12	0.000
30.000	-0.0156	8847253.	0.000	1.266E+12	0.000	1.266E+12	0.000
330.5271	126757.	0.000	0.000	1.266E+12	0.000	1.266E+12	0.000
30.500	-0.0169	818344.	0.000	1.266E+12	0.000	1.266E+12	0.000
362.4322	128917.	0.000	0.000	1.266E+12	0.000	1.266E+12	0.000
31.000	-0.0179	7802408.	0.000	1.266E+12	0.000	1.266E+12	0.000
391.1799	131077.	0.000	0.000	1.266E+12	0.000	1.266E+12	0.000
416.6276	133237.	0.000	0.000	1.266E+12	0.000	1.266E+12	0.000
439.4420	135397.	0.000	0.000	1.266E+12	0.000	1.266E+12	0.000
459.0977	137557.	0.000	0.000	1.266E+12	0.000	1.266E+12	0.000
475.8763	139717.	0.000	0.000	1.266E+12	0.000	1.266E+12	0.000
489.8658	141877.	0.000	0.000	1.266E+12	0.000	1.266E+12	0.000
501.1591	144037.	0.000	0.000	1.266E+12	0.000	1.266E+12	0.000
509.8533	146197.	0.000	0.000	1.266E+12	0.000	1.266E+12	0.000
516.0488	148357.	0.000	0.000	1.266E+12	0.000	1.266E+12	0.000
519.8485	150517.	0.000	0.000	1.266E+12	0.000	1.266E+12	0.000
521.3570	152677.	0.000	0.000	1.266E+12	0.000	1.266E+12	0.000
520.6795	154837.	0.000	0.000	1.266E+12	0.000	1.266E+12	0.000
517.9216	156997.	0.000	0.000	1.266E+12	0.000	1.266E+12	0.000
513.1861	159157.	0.000	0.000	1.266E+12	0.000	1.266E+12	0.000
506.3828	161317.	0.000	0.000	1.266E+12	0.000	1.266E+12	0.000
498.2074	163477.	0.000	0.000	1.266E+12	0.000	1.266E+12	0.000
488.1642	165637.	0.000	0.000	1.266E+12	0.000	1.266E+12	0.000
476.3407	167797.	0.000	0.000	1.266E+12	0.000	1.266E+12	0.000
40.000	-0.0164	1423409.	0.000	1.266E+12	0.000	1.266E+12	0.000

* This analysis computed pile response using nonlinear moment-curvature relationships. Values of total stress due to combined axial and bending stresses are computed only for elastic sections only and do not equal the actual stresses in concrete and steel. Stresses in concrete and steel may be interpolated from the output for nonlinear bending properties relative to the magnitude of bending moment developed in the pile.

Output Summary for Load Case No. 3:

Pile-head deflection = 1.000000 inches
Computed slope at pile head = -0.0051930 radians
Maximum bending moment = 21513992. inch-lbs
Maximum shear force = 144640. lbs
Depth of maximum bending moment = 15.000000 feet below pile head
Depth of maximum shear force = 0.000000 feet below pile head
Number of iterations = 14
Number of zero deflection points = 2

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Pile-head Deflection vs. Pile Length for Load Case 3

Boundary Condition Type 4, Deflection and Moment

Deflection = 1.00000 in
Moment = 3729000. in-lb
Axial Load = 402100. lb

Pile Length feet	Pile Head Deflection inches	Maximum Moment in-lbs	Maximum Shear lbs
50.0000	1.0000000	21513992.	144640.
47.5000	1.0000000	21468475.	142674.
45.0000	1.0000000	21432543.	142419.
42.5000	1.0000000	21309828.	141902.
40.0000	1.0000000	21071370.	140968.
37.5000	1.0000000	20541222.	138610.
35.0000	1.0000000	19393134.	130494.
32.5000	1.0000000	17625872.	-122135.
30.0000	1.0000000	15323757.	-117307.
27.5000	1.0000000	12818859.	-98593.
25.0000	1.0000000	10355076.	-7909765.
22.5000	1.0000000	5917488.	-52139.
20.0000	1.0000000	4480176.	-5329.
17.5000	1.0000000	3750193.	-45554.
15.0000	1.0000000	3729000.	-47443.
12.5000	1.0000000	3729000.	57886.
10.0000	1.0000000	3729000.	27220.
7.5000	1.0000000	3729000.	3.764805E+12

Computed Values of Pile Loading and Deflection for Lateral Loading for Load Case Number 4

Pile-head conditions are displacement and moment (Loading Type 4)
Displacement of pile head = 1.500000 inches
Moment at pile head = 3729000.0 in-lbs
Axial load at pile head = 402100.0 lbs

Depth feet	Soil Spr.	Deflect. inches	Bending Moment in-lbs	Shear Force lbs	Slope radians	Total Stress psi*	Bending Stiffness lb-in ²	Soil P
0.000	1.5000	3729000.	189145.	-0.007404	0.000	1.626E+12		
0.000	0.500	1.4556	4881717.	189145.	-0.007388	0.000	1.626E+12	
0.000	1.000	1.4113	6034390.	189145.	-0.007368	0.000	1.624E+12	

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0.000	1.500	0.000	0.000	0.000	0.000	0.000	0.000	0.000	1.622E+12
-315.1680	1383.1194	1.3672	7187009.	188200.	-0.007343	0.000	1.620E+12		
2.000	1.3232	8328219.	0.000	186288.	-0.007315	0.000	1.618E+12		
-322.0572	1460.3285	0.000	0.000	184336.	-0.007282	0.000	1.234E+12		
2.500	1.2794	9457760.	0.000	182346.	-0.007238	0.000	1.203E+12		
-328.5613	1540.8175	0.000	0.000	180321.	-0.007184	0.000	1.179E+12		
3.000	1.2358	10575388.	0.000	178263.	-0.007122	0.000	1.158E+12		
-334.6761	1624.8447	0.000	0.000	176173.	-0.007054	0.000	1.141E+12		
3.500	1.1926	11680843.	0.000	174056.	-0.006978	0.000	1.126E+12		
-340.4038	1712.6245	0.000	0.000	171912.	-0.006897	0.000	1.113E+12		
4.000	1.1496	12773904.	0.000	169744.	-0.006808	0.000	1.102E+12		
-345.7426	1804.4356	0.000	0.000	167555.	-0.006713	0.000	1.092E+12		
4.500	1.1071	13854361.	0.000	163268.	-0.006612	0.000	1.084E+12		
-350.6905	1900.5799	0.000	0.000	156577.	-0.006504	0.000	1.076E+12		
5.000	1.0650	14922020.	0.000	149279.	-0.006390	0.000	1.070E+12		
-355.2459	2001.3859	0.000	0.000	141437.	-0.006270	0.000	1.064E+12		
5.500	1.0234	15976700.	0.000	133104.	-0.006145	0.000	1.059E+12		
-359.4074	2107.2106	0.000	0.000	124319.	-0.005879	0.000	1.051E+12		
6.000	0.9822	17018237.	0.000	105652.	-0.005739	0.000	1.048E+12		
-363.1740	2218.4430	0.000	0.000	95899.	-0.005595	0.000	1.045E+12		
6.500	0.9417	18046478.	0.000	85916.	-0.005447	0.000	1.043E+12		
-366.5446	2335.5070	0.000	0.000	75762.	-0.005296	0.000	1.040E+12		
-1062.2234	7068.2843	0.000	0.000	65522.	-0.005142	0.000	1.039E+12		
7.000	0.8823	20037603.	0.000	55240.	-0.004985	0.000	1.037E+12		
-1168.2643	8128.7069	0.000	0.000	44894.	-0.004825	0.000	1.036E+12		
8.000	0.8236	20971594.	0.000	34503.	-0.004664	0.000	1.035E+12		
-1264.4223	9211.0517	0.000	0.000	24146.	-0.004502	0.000	1.035E+12		
8.500	0.7856	21859783.	0.000	13905.	-0.004339	0.000	1.035E+12		
-1349.4847	10306.	0.000	0.000	3864.9911	-0.004175	0.000	1.034E+12		
9.000	0.7484	22699096.	0.000	-5891.1170	-0.004010	0.000	1.034E+12		
-1428.3842	11452.	0.000	0.000	-15280.	-0.003846	0.000	1.035E+12		
9.500	0.7119	23486677.	0.000	31165.					
-1499.6934	12640.	0.000	0.000						
10.000	0.6762	24219949.	0.000						
-1558.8437	13831.	0.000	0.000						
10.500	0.6414	24896771.	0.000						
-1604.9869	15015.	0.000	0.000						
-1646.0800	16262.	0.000	0.000						
11.000	0.6073	25513470.	0.000						
-1681.6110	17571.	0.000	0.000						
12.000	0.5420	26572746.	0.000						
-1703.1892	18855.	0.000	0.000						
12.500	0.5107	27009250.	0.000						
-1710.0147	20092.	0.000	0.000						
13.000	0.4803	27383619.	0.000						
-1717.3356	21454.	0.000	0.000						
13.500	0.4508	27696181.	0.000						
-1731.3483	23041.	0.000	0.000						
14.000	0.4224	27943629.	0.000						
-1732.3765	24609.	0.000	0.000						
14.500	0.3949	28132721.	0.000						
-1711.9070	26360.	0.000	0.000						
15.000	0.3683	28357305.	0.000						
-1693.5836	28257.	0.000	0.000						
15.500	0.3426	28520520.	0.000						
-1633.2197	29856.	0.000	0.000						
16.000	0.3183	28323829.	0.000						
-1598.8203	30342.	0.000	0.000						
16.500	0.2947	28269179.	0.000						
-1530.6553	31165.	0.000	0.000						

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17.000	0.2721	28159029.	0.000	1.035E+12	0.000	574.2973	137557.	0.000	0.000	0.000	1.619E+12	0.000	
-1346.7500	29697.	0.000	0.000	1.036E+12	0.000	33.000	-0.0260	9016353.	-107491.	-0.000135	0.000	1.620E+12	0.000
17.500	0.2505	28000005.	0.000	1.037E+12	0.000	604.4652	139717.	0.000	-103786.	-0.000102	0.000	1.621E+12	0.000
-1231.8405	29506.	0.000	0.000	1.038E+12	0.000	630.5455	141877.	0.000	-99936.	-7.253E-05	0.000	1.622E+12	0.000
18.000	0.2299	27796243.	0.000	1.039E+12	0.000	652.6637	144037.	0.000	-95966.	-4.487E-05	0.000	1.623E+12	0.000
-1214.0911	31691.	0.000	0.000	1.041E+12	0.000	685.5519	148357.	0.000	-91896.	-1.935E-05	0.000	1.624E+12	0.000
18.500	0.2102	27548386.	0.000	1.043E+12	0.000	696.6047	150517.	0.000	-83547.	2.562E-05	0.000	1.625E+12	0.000
-1191.4438	34010.	0.000	0.000	1.045E+12	0.000	704.2588	152677.	0.000	-79308.	4.527E-05	0.000	1.626E+12	0.000
19.000	0.1915	27257252.	0.000	1.047E+12	0.000	708.6638	154837.	0.000	-75052.	6.316E-05	0.000	1.627E+12	0.000
-1163.3363	36472.	0.000	0.000	1.050E+12	0.000	709.9710	156997.	0.000	-70797.	7.938E-05	0.000	1.628E+12	0.000
19.500	0.1737	26923838.	0.000	1.052E+12	0.000	708.3316	159157.	0.000	-66561.	9.403E-05	0.000	1.629E+12	0.000
-1131.6379	39086.	0.000	0.000	1.056E+12	0.000	703.8962	161317.	0.000	-62359.	0.000107	0.000	1.630E+12	0.000
20.000	0.1569	26549309.	0.000	1.059E+12	0.000	696.8139	163477.	0.000	-58206.	0.000119	0.000	1.631E+12	0.000
-1094.6487	41867.	0.000	0.000	1.063E+12	0.000	687.2312	165637.	0.000	-54119.	0.000130	0.000	1.632E+12	0.000
20.500	0.1410	26135005.	0.000	1.067E+12	0.000	675.2913	167797.	0.000	-50110.	0.000139	0.000	1.633E+12	0.000
-1053.0999	44827.	0.000	0.000	1.072E+12	0.000	661.1337	169957.	0.000	-46192.	0.000147	0.000	1.634E+12	0.000
-1007.1521	47984.	0.000	0.000	1.077E+12	0.000	644.8929	172117.	0.000	-42377.	0.000154	0.000	1.635E+12	0.000
-973.6019	52250.	0.000	0.000	1.083E+12	0.000	626.6982	174277.	0.000	-38677.	0.000160	0.000	1.636E+12	0.000
22.000	0.0985	24668650.	0.000	1.089E+12	0.000	606.6731	176437.	0.000	-35102.	0.000166	0.000	1.637E+12	0.000
-938.9216	57177.	0.000	0.000	1.096E+12	0.000	584.9345	178597.	0.000	-31662.	0.000170	0.000	1.638E+12	0.000
22.500	0.0861	24109922.	0.000	1.104E+12	0.000	561.5927	180757.	0.000	-28367.	0.000174	0.000	1.639E+12	0.000
-900.1033	62726.	0.000	0.000	1.113E+12	0.000	536.7508	182917.	0.000	-25225.	0.000178	0.000	1.640E+12	0.000
-857.0168	69028.	0.000	0.000	1.122E+12	0.000	510.5045	185077.	0.000	-22245.	0.000180	0.000	1.641E+12	0.000
23.000	0.0745	23518460.	0.000	1.132E+12	0.000	482.9419	187237.	0.000	-19434.	0.000182	0.000	1.642E+12	0.000
-809.4853	76264.	0.000	0.000	1.143E+12	0.000	454.1433	189397.	0.000	-16799.	0.000184	0.000	1.643E+12	0.000
-757.2609	84683.	0.000	0.000	1.156E+12	0.000	424.1815	191557.	0.000	-14347.	0.000186	0.000	1.644E+12	0.000
-699.9851	94652.	0.000	0.000	1.170E+12	0.000	393.1213	193717.	0.000	-12085.	0.000187	0.000	1.645E+12	0.000
-627.6918	105157.	0.000	0.000	1.185E+12	0.000	361.0203	195877.	0.000	-10018.	0.000188	0.000	1.646E+12	0.000
25.000	0.0280	20130918.	0.000	1.202E+12	0.000	327.9283	198037.	0.000	-8152.2716	0.000188	0.000	1.647E+12	0.000
-499.9913	107317.	0.000	0.000	1.220E+12	0.000	293.8885	200197.	0.000	-6493.7946	0.000189	0.000	1.648E+12	0.000
-378.8395	109477.	0.000	0.000	1.242E+12	0.000	258.9372	202357.	0.000	-4941.6447	0.000189	0.000	1.649E+12	0.000
-264.4278	111637.	0.000	0.000	1.262E+12	0.000	258.4461	236915.	0.000			0.000	1.650E+12	0.000
-156.8968	113797.	0.000	0.000										
27.000	0.008272	17854493.	0.000										
27.500	0.002915	17078661.	0.000										
-56.3394	115957.	0.000	0.000										
37.1971	118117.	0.000	0.000										
28.500	-0.006171	15523624.	0.000										
123.7082	120277.	0.000	0.000										
29.000	-0.009959	14750925.	0.000										
203.2996	122437.	0.000	0.000										
29.500	-0.01133	13985355.	0.000										
275.8347	124597.	0.000	0.000										
30.000	-0.01162	13229341.	0.000										
341.6310	126757.	0.000	0.000										
400.7581	128517.	0.000	0.000										
31.000	0.10187	12485861.	0.000										
433.5556	0.1208	11756456.	0.000										
499.7027	13107.7225	11035331.	0.000										
539.9219	133237239	10347865.	0.000										
32.500	-0.0250	9671815.	0.000										

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48.500 -0.005412 29500. -3461.3615 0.000189 0.000 1.627E+12
 234.9816 260524. 0.000 12506. -2129.7710 0.000189 0.000 1.627E+12
 208.8819 292993. 0.000 3030.6376 -966.0991 0.000189 0.000 1.627E+12
 179.0087 341721. 0.000 0.000 0.000 0.000189 0.000 1.627E+12
 143.0243 213626. 0.000

Abut B.1p7o
 12.5000 1.5000000 3729000. -51369.
 10.0000 1.5000000 3729000. -51363.
 7.5000 1.5000000 3729000. 58725.
 5.0000 1.5000000 3729000. 27774.
 5.0000 0.0000000 6.230176E+12 5.647209E+12

* This analysis computed pile response using nonlinear moment-curvature relationships. Values of total stress due to combined axial and bending stresses are computed only for elastic sections only and do not equal the actual stresses in concrete and steel. Stresses in concrete and steel may be interpolated from the output for nonlinear bending properties relative to the magnitude of bending moment developed in the pile.

Output Summary for Load Case No. 4:

Pile-head deflection = 1.500000 inches
 Computed slope at pile head = -0.0074038 radians
 Maximum bending moment = 28323825. inch-lbs
 Maximum shear force = 189145. lbs
 Depth of maximum bending moment = 16.0000000 feet below pile head
 Depth of maximum shear force = 1.0000000 feet below pile head
 Number of iterations = 15
 Number of zero deflection points = 1

Pile-head Deflection vs. Pile Length for Load Case 4

Boundary Condition Type 4, Deflection and Moment

Deflection = 1.50000 in
 Moment = 3729000. in-lb
 Axial Load = 402100. lb

Pile Length feet	Pile Head Deflection inches	Maximum Moment in-lbs	Maximum Shear lbs
50.0000	1.500000	28323825.	189145.
47.5000	1.500000	26323825.	189145.
45.0000	1.500000	24323825.	189145.
42.5000	1.500000	22323825.	189145.
40.0000	1.500000	20323825.	189145.
37.5000	1.500000	18323825.	189145.
35.0000	1.500000	16323825.	189145.
32.5000	1.500000	14323825.	189145.
30.0000	1.500000	12323825.	189145.
27.5000	1.500000	10323825.	189145.
25.0000	1.500000	8323825.	189145.
22.5000	1.500000	6323825.	189145.
20.0000	1.500000	4323825.	189145.
17.5000	1.500000	2323825.	189145.
15.0000	1.500000	3873827.	-61706.

Computed Values of Pile Loading and Deflection for Lateral Loading for Load Case Number 5
 Pile-head conditions are Displacement and Moment (Loading Type 4)
 Displacement of pile head = 2.000000 inches
 Moment at pile head = 3729000.0 in-lbs
 Axial load at pile head = 402100.0 lbs

Res. X	Depth, feet	Soil spr. lb/inch	Deflect. inches	Lat. Load lb/inch	Bending Moment in-lbs	Shear Force lbs	Slope radians	Total Stress psi*	Bending Stiffness lb-in^2	Soil P lb/in
0.000	0.00	0.00	2.0000	0.00	3729000.	229310.	-0.009545	0.000	1.626E+12	0.000
0.000	0.00	0.00	0.0000	0.00	0.000	229310.	-0.009528	0.000	1.626E+12	0.000
0.000	0.00	0.00	1.9428	0.00	5127872.	229310.	-0.009507	0.000	1.624E+12	0.000
0.000	1.000	1.8857	1.8857	0.00	6526698.	229310.	-0.009480	0.000	1.621E+12	0.000
0.000	1.500	1.8287	1.8287	7925466.	7925466.	228268.	-0.009448	0.000	1.618E+12	0.000
-347.2516	2.000	1.139	1.7719	9311663.	9311663.	226162.	-0.009405	0.000	1.614E+12	0.000
-354.9779	2.500	1.202	0.255	0.000	10684996.	224010.	-0.009349	0.000	1.610E+12	0.000
-362.2919	3.000	1.267	1.267	0.000	12045162.	221815.	-0.009284	0.000	1.606E+12	0.000
-369.1946	3.500	1.335	2.104	0.000	13391890.	219581.	-0.009211	0.000	1.602E+12	0.000
-375.6839	4.000	1.406	0.638	0.000	14724828.	217308.	-0.009129	0.000	1.598E+12	0.000
-381.7576	4.500	1.480	0.308	0.000	16044036.	215001.	-0.009040	0.000	1.594E+12	0.000
-387.4138	5.000	1.557	3376	0.000	17348991.	212661.	-0.008942	0.000	1.590E+12	0.000
-392.6508	5.500	1.638	2289	0.000	18639584.	210290.	-0.008836	0.000	1.586E+12	0.000
-397.4673	6.000	1.722	9704	0.000	19915623.	207892.	-0.008722	0.000	1.582E+12	0.000
-401.8619	6.500	1.811	8505	0.000	21176828.	205469.	-0.008599	0.000	1.578E+12	0.000
-405.9338	7.000	1.905	1852	0.000	22423338.	203063.	-0.008469	0.000	1.574E+12	0.000
-1189.5050	7.500	5820	8173	0.000	23626622.	193194.	-0.008332	0.000	1.570E+12	0.000
-1306.9590	8.000	6671	1925	0.000	24782530.	185033.	-0.008187	0.000	1.566E+12	0.000
-1413.2728	8.500	7541	6343	0.000	25887225.	176272.	-0.008035	0.000	1.562E+12	0.000
-1507.2524	9.000	8413	1902	0.000	26937299.	166967.	-0.007877	0.000	1.558E+12	0.000
-1594.4786	9.500	9322	2030	0.000				0.000	1.554E+12	0.000

STR 1
 2" DEFLECTION

9.500	0.9785	27929596.	157162.	-0.007876	0.000	1.036E+12	-921.2028	84150.	0.000	Abut B.1p7o	1.045E+12
-1673.6390	10262.	0.000	146921.	-0.007712	0.000	1.032E+12	25.500	0.0542	26140112.	-144179.	0.000
10.000	0.9317	28861253.	136318.	-0.007541	0.000	1.029E+12	-849.0900	94028.	0.000	-149037.	0.000
-1740.3128	11207.	0.000	125402.	-0.007365	0.000	1.025E+12	26.000	0.0436	25264019.	-153237.	0.000
10.500	0.8860	29729853.	114188.	-0.007184	0.000	1.020E+12	-770.2352	106043.	0.000	-156545.	0.000
-1793.7882	12148.	0.000	102726.	-0.006998	0.000	1.018E+12	26.500	0.0338	24359848.	-158941.	0.000
11.000	0.8412	30533459.	91107.	-0.006809	0.000	1.016E+12	-629.7607	111637.	0.000	-160478.	0.000
-1844.8531	13158.	0.000	79369.	-0.006615	0.000	1.015E+12	27.000	0.0249	23432672.	-161211.	0.000
11.500	0.7976	31270219.	67481.	-0.006418	0.000	1.014E+12	-473.1095	113797.	0.000	-161196.	0.000
-1893.2320	14242.	0.000	55456.	-0.006219	0.000	1.013E+12	27.500	0.0168	22488144.	-160487.	0.000
12.000	0.7550	31938380.	43379.	-0.006017	0.000	1.012E+12	-325.4335	115957.	0.000	-159141.	0.000
-1927.3214	15316.	0.000	31338.	-0.005814	0.000	1.011E+12	28.000	0.00943	21531594.	-157210.	0.000
12.500	0.7136	32536705.	19425.	-0.005609	0.000	1.011E+12	-186.8754	118117.	0.000	-154749.	0.000
-1945.9743	16362.	0.000	7734.3034	-0.005403	0.000	1.011E+12	28.500	0.002869	20568026.	-151810.	0.000
13.000	0.6733	33064511.	3638.6083	-0.005197	0.000	1.011E+12	-57.5183	120277.	0.000	-148444.	0.000
-1966.5622	17524.	0.000	14205.	-0.004991	0.000	1.011E+12	62.6122	122437.	0.000	-144701.	0.000
13.500	0.6342	33521051.	-14205.	-0.004991	0.000	1.011E+12	29.500	-0.003068	19602112.	-140628.	0.000
-1996.1404	18884.	0.000	-23747.	-0.004786	0.000	1.012E+12	29.500	-0.008357	18638191.	-136271.	0.000
-2012.0727	20245.	0.000	-32848.	-0.004581	0.000	1.012E+12	173.5438	124597.	0.000	-131674.	0.000
14.000	0.5963	33905252.	-41851.	-0.004377	0.000	1.013E+12	30.000	-0.0130	17680272.	-126880.	0.000
-2013.5957	21590.	0.000	-50719.	-0.004175	0.000	1.013E+12	30.000	-0.0171	16732034.	-121922.	0.000
-2000.0612	22897.	0.000	-59420.	-0.003976	0.000	1.015E+12	275.3541	126757.	0.000	-116830.	0.000
-1970.9647	24143.	0.000	-67918.	-0.003778	0.000	1.016E+12	308.1671	128917.	0.000	-106354.	0.000
15.000	0.5596	34216533.	-76180.	-0.003583	0.000	1.017E+12	30.500	0.0207	15796833.	-95657.	0.000
-1925.9789	25298.	0.000	-84172.	-0.003391	0.000	1.019E+12	30.500	-0.0238	14877707.	-84928.	0.000
-1864.9916	26330.	0.000	-91919.	-0.003202	0.000	1.023E+12	31.000	0.0263	13977382.	-79605.	0.000
16.000	0.5241	34454836.	-99456.	-0.003016	0.000	1.025E+12	32.000	0.0285	13098284.	-74336.	0.000
-1970.9647	27897.	0.000	-106766.	-0.002835	0.000	1.028E+12	32.000	-0.0285	13098284.	-69138.	0.000
16.500	0.4898	34620644.	-113819.	-0.002658	0.000	1.030E+12	32.000	0.0302	12242543.	-64030.	0.000
-1925.9789	28284.	0.000	-120586.	-0.002485	0.000	1.033E+12	32.000	0.0316	11412011.	-59470.	0.000
-1864.9916	29288.	0.000	-127038.	-0.002316	0.000	1.036E+12	32.000	-0.0327	10608268.	-547262.	0.000
17.000	0.4568	34715002.	-133142.	-0.002153	0.000	1.037E+12	32.000	0.0338	982634.	0.000	
-1970.9647	30245.	0.000	-138868.	-0.001995	0.000	1.041E+12	32.000	0.0344	982634.	0.000	
-1864.9916	31305.	0.000	75828.	0.001995	0.000	1.041E+12	32.000	-0.0334	982634.	0.000	
17.500	0.4250	34793227.	0.0657	26985276.	0.000	1.041E+12	32.000	0.0339	9086213.	0.000	
-1657.1037	32508.	0.000	0.0657	26985276.	0.000	1.041E+12	32.000	-0.0342	8369901.	0.000	
-1523.6513	33770.	0.000	0.0657	26985276.	0.000	1.041E+12	32.000	0.0344	7684423.	0.000	
-1510.0575	34931511.	0.000	0.0657	26985276.	0.000	1.041E+12	32.000	-0.0343	7030345.	0.000	
18.000	0.3370	34434541.	0.0657	26985276.	0.000	1.041E+12	32.000	0.0341	6408075.	0.000	
-1490.6927	35040.	0.000	0.0657	26985276.	0.000	1.041E+12	32.000	0.0338	5817872.	0.000	
18.500	0.3101	34221076.	0.0657	26985276.	0.000	1.041E+12	32.000	0.0333	5259856.	0.000	
-1465.3480	36885.	0.000	0.0657	26985276.	0.000	1.041E+12	32.000	0.0327	4734012.	0.000	
19.000	0.2845	33953456.	0.0657	26985276.	0.000	1.041E+12	32.000	0.0320	4240038.	0.000	
-1434.6500	39911.	0.000	0.0657	26985276.	0.000	1.041E+12	32.000	0.0316	3778053.	0.000	
-1398.0619	40911.	0.000	0.0657	26985276.	0.000	1.041E+12	32.000	0.0316	3778053.	0.000	
19.500	0.2600	33623592.	0.0657	26985276.	0.000	1.041E+12	32.000	0.0316	3778053.	0.000	
-1335.8839	42368.	0.000	0.0657	26985276.	0.000	1.041E+12	32.000	0.0316	3778053.	0.000	
-1274.0259	43429.	0.000	0.0657	26985276.	0.000	1.041E+12	32.000	0.0316	3778053.	0.000	
-1235.9296	44737.	0.000	0.0657	26985276.	0.000	1.041E+12	32.000	0.0316	3778053.	0.000	
-1195.0602	46138.	0.000	0.0657	26985276.	0.000	1.041E+12	32.000	0.0316	3778053.	0.000	
-1155.9195	47639.	0.000	0.0657	26985276.	0.000	1.041E+12	32.000	0.0316	3778053.	0.000	
-1103.8486	49249.	0.000	0.0657	26985276.	0.000	1.041E+12	32.000	0.0316	3778053.	0.000	
-1047.2011	50971.	0.000	0.0657	26985276.	0.000	1.041E+12	32.000	0.0316	3778053.	0.000	
-987.2157	52828.	0.000	0.0657	26985276.	0.000	1.041E+12	32.000	0.0316	3778053.	0.000	
25.000	0.0657	26985276.	0.0657	26985276.	0.000	1.041E+12	32.000	0.0316	3778053.	0.000	

Abut. B. 1p7o

 Pile-head Deflection vs. Pile Length for Load Case 5

Boundary Condition Type 4, Deflection and Moment

Deflection = 2.00000 in
 Moment = 3729000.0 in-lb
 Axial Load = 402100.0 lb

Pile Length feet	Pile Head Deflection inches	Maximum Moment in-lbs	Maximum Shear lbs
50.0000	2.0000000	34739527	229310
47.5000	2.0000000	34664979	226721
45.0000	2.0000000	34543591	226058
42.5000	2.0000000	34209080	224624
40.0000	2.0000000	33534538	221792
37.5000	2.0000000	31805828	213802
35.0000	2.0000000	28913694	196846
32.5000	2.0000000	25375345	188850
30.0000	2.0000000	21331603	173735
27.5000	2.0000000	17293771	152885
25.0000	2.0000000	13549660	136109
22.5000	2.0000000	10129474	116379
20.0000	2.0000000	7341856	98146
17.5000	2.0000000	5323151	83193
15.0000	2.0000000	3998224	68385
12.5000	2.0000000	2729000	56138
10.0000	2.0000000	1729000	45060
7.5000	2.0000000	9729000	28304
5.0000	2.0000000	3729000	18304
5.0000	0.000000	8.486800E+12	7.529613E+12

 Computed Values of Pile Loading and Deflection
 for Lateral Loading for Load Case Number 6

Pile-head conditions are Displacement and Moment (Loading Type 4)
 Displacement of pile head = 0.500000 inches
 Moment at pile head = 2806000.0 in-lbs
 Axial load at pile head = 311000.0 lbs

Depth Res. Soil	X Spr.	Y Dist.	Bending Moment	Shear Force	Slope S	Total Stress	Bending Stiffness
feet	lb/inch	inches	in-lbs	lbs	radians	psi*	lb-in^2
0.00	0.00	0.5000	2808000.	94031.	-0.002820	0.000	1.632E+12
0.000	0.500	0.000	0.000	94031.	-0.002808	0.000	1.632E+12
0.000	1.000	0.000	0.4663	94031.	-0.002795	0.000	1.632E+12
0.000	1.500	0.4496	4516236.	93378.	-0.002779	0.000	1.631E+12
-217.5368	2903.2200	0.000	0.000				

Abut. B. 1p7o

 Pile-head Deflection vs. Pile Length for Load Case 5

Boundary Condition Type 4, Deflection and Moment

Deflection = 2.00000 in
 Moment = 3729000.0 in-lb
 Axial Load = 402100.0 lb

Pile Length feet	Pile Head Deflection inches	Maximum Moment in-lbs	Maximum Shear lbs
50.0000	2.0000000	34739527	229310
47.5000	2.0000000	34664979	226721
45.0000	2.0000000	34543591	226058
42.5000	2.0000000	34209080	224624
40.0000	2.0000000	33534538	221792
37.5000	2.0000000	31805828	213802
35.0000	2.0000000	28913694	196846
32.5000	2.0000000	25375345	188850
30.0000	2.0000000	21331603	173735
27.5000	2.0000000	17293771	152885
25.0000	2.0000000	13549660	136109
22.5000	2.0000000	10129474	116379
20.0000	2.0000000	7341856	98146
17.5000	2.0000000	5323151	83193
15.0000	2.0000000	3998224	68385
12.5000	2.0000000	2729000	56138
10.0000	2.0000000	1729000	45060
7.5000	2.0000000	9729000	28304
5.0000	2.0000000	3729000	18304
5.0000	0.000000	8.486800E+12	7.529613E+12

 Computed Values of Pile Loading and Deflection
 for Lateral Loading for Load Case Number 6

Pile-head conditions are Displacement and Moment (Loading Type 4)
 Displacement of pile head = 0.500000 inches
 Moment at pile head = 2806000.0 in-lbs
 Axial load at pile head = 311000.0 lbs

Depth Res. Soil	X Spr.	Y Dist.	Bending Moment	Shear Force	Slope S	Total Stress	Bending Stiffness
feet	lb/inch	inches	in-lbs	lbs	radians	psi*	lb-in^2
0.00	0.00	0.5000	2808000.	94031.	-0.002820	0.000	1.632E+12
0.000	0.500	0.000	0.000	94031.	-0.002808	0.000	1.632E+12
0.000	1.000	0.000	0.4663	94031.	-0.002795	0.000	1.632E+12
0.000	1.500	0.4496	4516236.	93378.	-0.002779	0.000	1.631E+12
-217.5368	2903.2200	0.000	0.000				

* This analysis computed pile response using nonlinear moment-curvature relationships. Values of total stress due to combined axial and bending stresses are computed only for elastic sections only and do not equal the actual stresses in concrete and steel. Stresses in concrete and steel may be interpolated from the output for nonlinear bending properties relative to the magnitude of bending moment developed in the pile.

Output Summary for Load Case No. 5:

Pile-head deflection	=	2.0000000 inches
Computed slope at pile head	=	-0.0095447 radians
Maximum bending moment	=	34739527 in-lbs
Maximum shear force	=	229310 lbs
Depth of maximum bending moment	=	16.5000000 feet below pile head
Depth of maximum shear force	=	0.0000000 feet below pile head
Number of iterations	=	11
Number of zero deflection points	=	1

2.000	0.4330	5077760.	0.000	1.630E+12	58081.	0.000	1.134E+12
-221.9230	3075.4875	0.000	0.000	0.000	1222.5683.	0.000	0.000
2.500	0.4164	5631260.	0.000	1.629E+12	0.0469	-40.176.	-0.000969
-226.0107	3256.3336	0.000	0.000	0.000	62743.	0.000	0.000
3.000	0.4001	6176585.	0.000	1.628E+12	0.0413	-43048.	-0.000905
-229.7961	3446.5073	0.000	0.000	0.000	67790.	0.000	0.000
3.500	0.3838	6713595.	0.000	1.627E+12	0.0361	-45769.	-0.000843
-233.2755	3646.8431	0.000	0.000	0.000	73277.	0.000	0.000
4.000	0.3677	7242160.	0.000	1.626E+12	0.0312	-48327.	-0.000782
-236.4447	3858.2734	0.000	0.000	0.000	11431455.	0.000	0.000
4.500	0.3518	7762164.	0.000	1.625E+12	0.0267	-50677.	-0.000723
-239.2995	4081.8441	0.000	0.000	0.000	11135482.	0.000	0.000
-241.8353	4318.7326	0.000	0.000	1.624E+12	10826028.	0.000	0.000
5.000	0.3360	8273500.	0.000	1.623E+12	20.500	-52756.	-0.000666
5.500	0.3204	8776072.	0.000	1.622E+12	0.0225	-54542.	-0.000611
-244.0473	4570.2694	0.000	0.000	1.622E+12	85717.	0.000	0.000
-245.9302	4837.9636	0.000	0.000	1.208E+12	10504893.	0.000	0.000
6.000	0.3050	9269798.	0.000	1.208E+12	10173810.	0.000	0.000
-245.9302	4837.9636	0.000	0.000	1.187E+12	9834433.	0.000	0.000
6.500	0.2899	9754585.	0.000	1.187E+12	0.0120	-57280.	-0.000508
-247.4983	5122.7090	0.000	0.000	1.175E+12	92197.	0.000	0.000
7.000	0.2751	10230369.	0.000	1.175E+12	0.009080	-58261.	-0.000459
-733.1497	15992.	0.000	0.000	1.164E+12	9483339.	0.000	0.000
7.500	0.2606	10679663.	0.000	1.164E+12	94357.	-59001.	-0.000418
-800.4495	18433.	0.000	0.000	1.155E+12	0.006469	0.000	0.000
-859.0094	20919.	0.000	0.000	1.147E+12	96517.	-59514.	-0.000384
-859.0094	20919.	0.000	0.000	1.147E+12	0.004068	0.000	0.000
-908.0139	23428.	0.000	0.000	1.141E+12	8242275.	-59809.	-0.000352
-952.6731	26092.	0.000	0.000	1.141E+12	0.001863	-59895.	-0.000321
-991.8615	28892.	0.000	0.000	1.135E+12	8065485.	-59782.	-0.000292
-1021.5859	31715.	0.000	0.000	1.130E+12	0.001994	0.000	0.000
-1041.3459	34529.	0.000	0.000	1.126E+12	34.9542	-59481.	-0.000265
-1052.5773	37360.	0.000	0.000	1.126E+12	105157	-59001.	-0.000238
-1054.6764	40165.	0.000	0.000	1.120E+12	107317	-58354.	-0.000213
-1045.6310	42831.	0.000	0.000	1.118E+12	109477	0.000	0.000
-1045.6310	42831.	0.000	0.000	1.118E+12	94.3169	0.000	0.000
-1025.8595	45288.	0.000	0.000	1.117E+12	26.500	6642064.	0.000
-1002.8595	47902.	0.000	0.000	1.116E+12	26.500	6294497.	0.000
-982.3330	50886.	0.000	0.000	1.116E+12	121.3183	6294497.	0.000
-952.6018	53681.	0.000	0.000	1.116E+12	111637.	5952160.	0.000
-913.19766	56215.	0.000	0.000	1.116E+12	146.5054	0.000	0.000
-866.13943	58406.	0.000	0.000	1.119E+12	169.8695	0.000	0.000
-811.15200	60165.	0.000	0.000	1.121E+12	189.000	0.000	0.000
-750.16500	61400.	0.000	0.000	1.124E+12	191.4104	0.000	0.000
-683.5348	63009.	0.000	0.000	1.124E+12	28.500	5286487.	0.000
-575.1920	58165.	0.000	0.000	1.130E+12	211.1357	0.000	0.000
17.500	0.0529	12456042.	0.000	1.130E+12	229.0610	4964642.	0.000

Abut B.1p70

Abut B.1p70

Abut. B.1p7o

-38.5603	1591779.	0.000	0.000	1.633E+12
49.500	0.000661	-1812.4875	575.2567	8.589E-05
-82.1549	746065.	0.000	0.000	1.633E+12
50.000	0.001176	0.000	0.000	1.633E+12
-109.5973	279579.	0.000	0.000	1.633E+12

* This analysis computed pile response using nonlinear moment-curvature relationships.
 Values of total stress due to combined axial and bending stresses are computed only for elastic sections only and do not equal the actual stresses in concrete and steel.
 Stresses in concrete and steel may be interpolated from the output for nonlinear bending properties relative to the magnitude of bending moment developed in the pile.

Output Summary for Load Case No. 6:

Pile-head deflection	=	0.5000000 inches
Computed slope at pile head	=	-0.0028196 radians
Maximum bending moment	=	13408332. inch-lbs
Maximum shear force	=	94031. lbs
Depth of maximum bending moment	=	13.5000000 feet below pile head
Depth of maximum shear force	=	0.0000000 feet below pile head
Number of iterations	=	13
Number of zero deflection points	=	2

Pile-head Deflection vs. Pile Length for Load Case 6

Boundary Condition Type 4, Deflection and Moment

Deflection =	0.50000 in
Moment =	2808000. in-lb
Axial Load =	311000. lb

Pile Length feet	Pile Head Deflection inches	Maximum Moment in-lbs	Maximum Shear lbs
50.0000	0.5000000	13408332.	94031.
47.5000	0.5000000	13372658.	92503.
45.0000	0.5000000	13363894.	92419.
42.5000	0.5000000	13319300.	92251.
40.0000	0.5000000	13225399.	91959.
37.5000	0.5000000	13027375.	91191.
35.0000	0.5000000	12579276.	87249.
32.5000	0.5000000	11917890.	83891.
30.0000	0.5000000	10728329.	77319.
27.5000	0.5000000	9276777.	-75068.
25.0000	0.5000000	5359065.	-68370.
22.5000	0.5000000	1776342.	-58447.
20.0000	0.5000000	1344193.	-49849.
17.5000	0.5000000	2826345.	-52932.
15.0000	0.5000000	2808000.	-31382.
12.5000	0.5000000	2808000.	-33318.
10.0000	0.5000000	2808000.	-33318.

Abut. B.1p7o	Abut. B.1p7o	Abut. B.1p7o	Abut. B.1p7o	Abut. B.1p7o
-37727.	1.488E-05	0.000	1.632E+12	0.000
-35832.	2.364E-05	0.000	1.632E+12	0.000
-33929.	3.161E-05	0.000	1.632E+12	0.000
-32026.	3.884E-05	0.000	1.633E+12	0.000
-30129.	4.535E-05	0.000	1.633E+12	0.000
-28246.	5.121E-05	0.000	1.633E+12	0.000
-26384.	5.644E-05	0.000	1.633E+12	0.000
-24548.	6.109E-05	0.000	1.633E+12	0.000
-22745.	6.519E-05	0.000	1.633E+12	0.000
-20980.	6.880E-05	0.000	1.633E+12	0.000
-19258.	7.194E-05	0.000	1.633E+12	0.000
-17585.	7.465E-05	0.000	1.633E+12	0.000
-15964.	7.698E-05	0.000	1.633E+12	0.000
-14400.	7.895E-05	0.000	1.633E+12	0.000
-12897.	8.061E-05	0.000	1.633E+12	0.000
-11458.	8.198E-05	0.000	1.633E+12	0.000
-10089.	8.310E-05	0.000	1.633E+12	0.000
-8790.3983	8.400E-05	0.000	1.633E+12	0.000
-7566.9405	8.470E-05	0.000	1.633E+12	0.000
-6421.1811	8.523E-05	0.000	1.633E+12	0.000
-5355.9042	8.562E-05	0.000	1.633E+12	0.000
-4373.7557	8.590E-05	0.000	1.633E+12	0.000
-3477.2630	8.607E-05	0.000	1.633E+12	0.000
-2668.8531	8.617E-05	0.000	1.633E+12	0.000
-1950.8706	8.621E-05	0.000	1.633E+12	0.000
-1325.5945	8.620E-05	0.000	1.633E+12	0.000
-795.2540	8.617E-05	0.000	1.633E+12	0.000
-362.0422	8.612E-05	0.000	1.633E+12	0.000
-28.1293	8.606E-05	0.000	1.633E+12	0.000
399.0325	8.599E-05	0.000	1.633E+12	0.000
868.7080	8.594E-05	0.000	1.633E+12	0.000
937.4024	8.591E-05	0.000	1.633E+12	0.000

2494700.	-0.0133	299.5739	0.000	1.633E+12
141877.	141877.	159157.	0.000	1.633E+12
314.8567	141877.	161317.	0.000	1.633E+12
34.0000	-0.0132	163477.	0.000	1.633E+12
316.8473	144037.	165637.	0.000	1.633E+12
34.5000	-0.0130	167797.	0.000	1.633E+12
317.5319	146197.	169957.	0.000	1.633E+12
35.0000	-0.0128	172117.	0.000	1.633E+12
316.9706	148357.	176437.	0.000	1.633E+12
35.5000	-0.0126	178597.	0.000	1.633E+12
315.2237	150517.	182917.	0.000	1.633E+12
312.3514	152677.	187337.	0.000	1.633E+12
308.4133	154837.	191757.	0.000	1.633E+12
303.4683	156997.	196177.	0.000	1.633E+12
297.5739	159157.	200597.	0.000	1.633E+12
290.7858	161317.	205017.	0.000	1.633E+12
283.1580	163477.	209437.	0.000	1.633E+12
274.7423	165637.	213857.	0.000	1.633E+12
265.5879	167797.	218277.	0.000	1.633E+12
255.7415	169957.	222697.	0.000	1.633E+12
245.2469	172117.	227117.	0.000	1.633E+12
234.1447	174277.	231537.	0.000	1.633E+12
222.4728	176437.	235957.	0.000	1.633E+12
210.2654	178597.	240377.	0.000	1.633E+12
197.5528	180757.	244797.	0.000	1.633E+12
184.3660	182917.	249217.	0.000	1.633E+12
170.7264	185077.	253637.	0.000	1.633E+12
156.6565	187237.	258057.	0.000	1.633E+12
142.1744	189397.	262477.	0.000	1.633E+12
127.2935	191557.	266897.	0.000	1.633E+12
112.0320	193717.	271317.	0.000	1.633E+12
96.3934	195877.	275737.	0.000	1.633E+12
80.3866	198037.	280157.	0.000	1.633E+12
64.0171	200197.	284577.	0.000	1.633E+12
47.3877	202357.	288997.	0.000	1.633E+12
30.4480	204517.	293417.	0.000	1.633E+12
13.4584	206677.	297837.	0.000	1.633E+12
6.4584	208837.	302257.	0.000	1.633E+12
49.0000	0.000145	306677.	0.000	1.633E+12

Abut B. 1p7o

Abut B. 1p7o

Computed Values of Pile Loading and Deflection
for Lateral Loading for Load Case Number 7

Pile-head conditions are Displacement and Moment (Loading Type 4)
 Displacement of pile head = 1.000000 inches
 Moment at pile head = 2808000.0 in-lbs
 Axial load at pile head = 3110000.0 lbs

Res. X	Depth	Deflect.	Bending	Shear	Slope	Total	Bending	Soil
feet	feet	inches	in-lbs	lbs	radians	psi*	lb-in^2	lb/in
0.000	0.00	1.0000	2808000.0	146979	-0.005151	0.000	1.632E+12	0.000
0.000	0.00	0.000	0.000	146979	-0.005139	0.000	1.632E+12	0.000
0.000	0.00	0.9691	3699477.	146979.	-0.005123	0.000	1.631E+12	0.000
1.000	0.00	0.9383	4590929.	146979.	-0.005105	0.000	1.629E+12	0.000
1.500	0.00	0.9076	5482350.	146155.	-0.005083	0.000	1.628E+12	0.000
2.000	0.00	0.8771	6363835.	144487.	-0.005058	0.000	1.626E+12	0.000
2.500	0.00	0.8466	7235167.	142786.	-0.005030	0.000	1.624E+12	0.000
3.000	0.00	0.8164	8096142.	141053.	-0.004998	0.000	1.622E+12	0.000
3.500	0.00	0.7863	8946369.	139289.	-0.004957	0.000	1.187E+12	0.000
4.000	0.00	0.7564	9786267.	137498.	-0.004905	0.000	1.166E+12	0.000
4.500	0.00	0.7268	10615047.	135682.	-0.004848	0.000	1.148E+12	0.000
5.000	0.00	0.6975	11432753.	133842.	-0.004785	0.000	1.134E+12	0.000
5.500	0.00	0.6686	12239242.	131981.	-0.004718	0.000	1.121E+12	0.000
6.000	0.00	0.6401	13034381.	130101.	-0.004646	0.000	1.110E+12	0.000
6.500	0.00	0.6120	13818056.	128203.	-0.004569	0.000	1.100E+12	0.000
7.000	0.00	0.5854	14590160.	124470.	-0.004487	0.000	1.092E+12	0.000
7.500	0.00	0.5597	153528743.	118636.	-0.004400	0.000	1.085E+12	0.000
8.000	0.00	0.5350	16030359.	112289.	-0.004310	0.000	1.078E+12	0.000
8.500	0.00	0.5112	16692652.	105489.	-0.004215	0.000	1.073E+12	0.000
9.000	0.00	0.4888	17312986.	98286.	-0.004116	0.000	1.068E+12	0.000
9.500	0.00	0.4678	17897787.	90716.	-0.004014	0.000	1.064E+12	0.000
10.000	0.00	0.4484	18416470.	82832.	-0.003909	0.000	1.061E+12	0.000
10.500	0.00	0.4305	18896757.	74702.	-0.003800	0.000	1.058E+12	0.000
11.000	0.00	0.4141	19339100.	66322.	-0.003690	0.000	1.055E+12	0.000
11.500	0.00	0.3991	19742700.	57772.	-0.003579	0.000	1.053E+12	0.000
12.000	0.00	0.3854	20107700.	49152.	-0.003467	0.000	1.051E+12	0.000
12.500	0.00	0.3729	20434400.	40472.	-0.003354	0.000	1.050E+12	0.000
13.000	0.00	0.3615	20723100.	31752.	-0.003240	0.000	1.049E+12	0.000
13.500	0.00	0.3509	21004100.	23002.	-0.003125	0.000	1.048E+12	0.000
14.000	0.00	0.3411	21286900.	14252.	-0.003009	0.000	1.048E+12	0.000
14.500	0.00	0.3320	21571800.	5502.	-0.002892	0.000	1.047E+12	0.000
15.000	0.00	0.3236	21858200.	-3398.	-0.002774	0.000	1.048E+12	0.000
15.500	0.00	0.3159	22145500.	-12358.	-0.002655	0.000	1.048E+12	0.000
16.000	0.00	0.3088	22434100.	-21282.	-0.002535	0.000	1.048E+12	0.000
16.500	0.00	0.3023	22723500.	-30172.	-0.002414	0.000	1.049E+12	0.000
17.000	0.00	0.2964	23014100.	-39028.	-0.002292	0.000	1.050E+12	0.000
17.500	0.00	0.2911	23305300.	-47850.	-0.002169	0.000	1.051E+12	0.000
18.000	0.00	0.2863	23597500.	-56640.	-0.002045	0.000	1.052E+12	0.000
18.500	0.00	0.2820	23891100.	-65388.	-0.001920	0.000	1.054E+12	0.000
19.000	0.00	0.2782	24185500.	-74096.	-0.001794	0.000	1.056E+12	0.000
19.500	0.00	0.2748	24481100.	-82764.	-0.001667	0.000	1.058E+12	0.000
20.000	0.00	0.2719	24777300.	-91394.	-0.001540	0.000	1.060E+12	0.000
20.500	0.00	0.2694	25074500.	-100000.	-0.001412	0.000	1.063E+12	0.000
21.000	0.00	0.2672	25372100.	-108680.	-0.001284	0.000	1.066E+12	0.000
21.500	0.00	0.2654	25670500.	-117420.	-0.001155	0.000	1.069E+12	0.000
22.000	0.00	0.2640	25970000.	-126220.	-0.001026	0.000	1.073E+12	0.000
22.500	0.00	0.2630	26270000.	-135080.	-0.000896	0.000	1.077E+12	0.000
23.000	0.00	0.2624	26571000.	-144000.	-0.000765	0.000	1.082E+12	0.000
23.500	0.00	0.2622	26873000.	-152980.	-0.000634	0.000	1.087E+12	0.000
24.000	0.00	0.2624	27176000.	-162020.	-0.000502	0.000	1.093E+12	0.000
24.500	0.00	0.2630	27480000.	-171120.	-0.000370	0.000	1.099E+12	0.000
25.000	0.00	0.2640	27785000.	-180280.	-0.000237	0.000	1.099E+12	0.000
25.500	0.00	0.2654	28091000.	-189500.	-0.000104	0.000	1.105E+12	0.000
26.000	0.00	0.2672	28398000.	-198780.	0.000030	0.000	1.113E+12	0.000
26.500	0.00	0.2694	28707000.	-208120.	0.000104	0.000	1.121E+12	0.000
27.000	0.00	0.2719	29018000.	-217520.	0.000178	0.000	1.130E+12	0.000

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SEV H
 @ 1' Deflection

4.2996		111637		Abut B. 1p70		1.140E+12		Abut B. 1p70		1.633E+12	
27.000	-0.003452	0.000	-94873.	-0.000505	0.000	1.140E+12	623156.	0.000	1.633E+12	0.000	1.633E+12
65.4638	113797.	11893009.	0.000	-0.000445	0.000	1.151E+12	368.1948	180757.	-18640.	0.000132	0.000132
27.500	-0.006296	11325832.	0.000	-0.000387	0.000	1.162E+12	43.000	-0.0114	-16491.	0.000135	0.000135
121.6868	115957.	0.000	-93428.	-0.000333	0.000	1.176E+12	348.1543	182917.	-14465.	0.000136	0.000136
28.000	-0.008787	10762925.	0.000	-0.000283	0.000	1.190E+12	43.500	-0.0106	-12568.	0.000138	0.000138
172.9819	118117.	0.000	-92251.	-0.000242	0.000	1.621E+12	327.1844	185077.	-10804.	0.000139	0.000139
28.500	-0.0109	10206142.	0.000	-0.000209	0.000	1.623E+12	44.000	-0.009784	-7695.6321	0.000140	0.000140
219.3885	120277.	0.000	-90810.	-0.000178	0.000	1.624E+12	44.500	-0.008954	-6360.6763	0.000141	0.000141
29.000	-0.0128	9657160.	0.000	-0.000149	0.000	1.625E+12	282.6577	189397.	-5177.4815	0.000142	0.000142
260.9707	122437.	0.000	-89133.	-0.000122	0.000	1.626E+12	45.000	-0.008118	-4150.1540	0.000142	0.000142
297.8157	124597.	0.000	-87245.	-0.000105	0.000	1.627E+12	259.1885	191557.	-3282.6759	0.000142	0.000142
331.5021	126757.	0.000	-85165.	-0.000085	0.000	1.628E+12	45.500	-0.007278	-2361.1376	0.000142	0.000142
362.0667	128917.	0.000	-82910.	-0.000065	0.000	1.629E+12	234.9654	193717.	-1384.7736	0.000142	0.000142
389.5575	131077.	0.000	-80499.	-0.000045	0.000	1.630E+12	46.000	-0.006433	-586.5990	0.000142	0.000142
414.0321	133237.	0.000	-77950.	-0.000025	0.000	1.631E+12	46.500	-0.005586	-26.1026	0.000142	0.000142
435.5571	135397.	0.000	-75281.	-0.000015	0.000	1.632E+12	184.3785	198037.	0.000	0.000142	0.000142
454.2063	137557.	0.000	-72508.	-0.000010	0.000	1.632E+12	158.0640	200197.	0.000	0.000142	0.000142
470.0609	139717.	0.000	-69648.	-0.000005	0.000	1.632E+12	47.500	-0.004737	0.000	0.000142	0.000142
483.2075	141877.	0.000	-66718.	-0.000002	0.000	1.632E+12	131.0953	202357.	0.000	0.000142	0.000142
493.7377	144037.	0.000	-63731.	0.000000	0.000	1.632E+12	48.000	-0.003887	0.000	0.000142	0.000142
501.7469	146197.	0.000	-60704.	0.000000	0.000	1.632E+12	176.0841	347985.	0.000	0.000142	0.000142
507.3596	148357.	0.000	-57650.	0.000000	0.000	1.632E+12	48.500	-0.002185	0.000	0.000142	0.000142
510.3530	150517.	0.000	-54583.	0.000000	0.000	1.632E+12	149.3706	410232.	0.000	0.000142	0.000142
511.8448	152677.	0.000	-51517.	0.000000	0.000	1.632E+12	49.000	-0.001333	0.000	0.000142	0.000142
510.5630	154837.	0.000	-48463.	0.000000	0.000	1.632E+12	116.6876	525170.	0.000	0.000142	0.000142
507.3926	156997.	0.000	-45433.	0.000000	0.000	1.632E+12	70.1445	873914.	0.000	0.000142	0.000142
502.4932	159157.	0.000	-42438.	0.000000	0.000	1.632E+12	-61.4436	498265.	0.000	0.000142	0.000142
495.6866	161317.	0.000	-39489.	0.000000	0.000	1.632E+12					
487.1674	163477.	0.000	-36597.	0.000000	0.000	1.632E+12					
477.0324	165637.	0.000	-33770.	0.000000	0.000	1.632E+12					
465.3749	167797.	0.000	-31017.	0.000000	0.000	1.632E+12					
452.2846	169957.	0.000	-28346.	0.000000	0.000	1.632E+12					
437.8475	172117.	0.000	-25766.	0.000000	0.000	1.632E+12					
422.1453	174277.	0.000	-23284.	0.000000	0.000	1.632E+12					
405.2551	176437.	0.000	-20907.	0.000000	0.000	1.632E+12					
387.2491	178597.	0.000									

* This analysis computed pile response using nonlinear moment-curvature relationships.
 Values of total stress due to combined axial and bending stresses are computed only for elastic sections only and do not equal the actual stresses in concrete and steel.
 Stresses in concrete and steel may be interpolated from the output for nonlinear bending properties relative to the magnitude of bending moment developed in the pile.

Output Summary for Load Case No. 7:

Pile-head deflection = 1.000000 inches
 Computed slope at pile head = -0.0051306 radians
 Maximum bending moment = 2092816. inch-lbs
 Maximum shear force = 146979. lbs
 Depth of maximum bending moment = 15.000000 feet below pile head
 Depth of maximum shear force = 1.0000000 feet below pile head
 Number of iterations = 21
 Number of zero deflection points = 2

----- Pile-head Deflection vs. Pile Length for Load Case 7 -----

Boundary Condition Type 4, Deflection and Moment

Deflection =		1.00000 in		Abut B. 1p7o		Abut B. 1p7o			
Moment =		2808000. in-lb							
Axial Load =		311000. lb							
Pile Length feet	Pile Head Deflection inches	Maximum Moment in-lbs	Maximum Shear lbs						
50.0000	1.0000000	2092816.	146979.	-345.8941	1802.8548	0.000	178505.	-0.007035	0.000
47.5000	1.0000000	2088563.	145016.	-350.8622	1898.7190	13023114.	176386.	-0.006962	0.000
45.0000	1.0000000	2083816.	144705.	-355.4382	1999.2200	14100890.	174241.	-0.006882	0.000
42.5000	1.0000000	20736165.	144291.	-359.6206	2104.7126	15165727.	172072.	-0.006796	0.000
40.0000	1.0000000	20504282.	143398.	-363.4081	2215.5835	16217463.	169881.	-0.006703	0.000
37.5000	1.0000000	19884476.	141108.	-366.8000	2332.2539	17255948.	165591.	-0.006603	0.000
35.0000	1.0000000	18886765.	133342.	-1063.0189	7057.6998	18281048.	158895.	-0.006497	0.000
32.5000	1.0000000	17155181.	124168.	-1169.1853	8115.5737	19267688.	151591.	-0.006385	0.000
30.0000	1.0000000	14875623.	114679.	-1265.4676	9195.0624	20212033.	143742.	-0.006266	0.000
27.5000	1.0000000	12396281.	-106070.	-1350.6811	10287.	21110606.	135401.	-0.006143	0.000
25.0000	1.0000000	9940976.	-95605.	-1429.7428	11430.	21960329.	126608.	-0.006014	0.000
22.5000	1.0000000	7531431.	-82441.	-1501.2170	12614.	22758344.	117423.	-0.005880	0.000
20.0000	1.0000000	5528661.	-69852.	-1560.5327	13802.	23502071.	107921.	-0.005741	0.000
17.5000	1.0000000	4034792.	-48715.	-1606.8395	14982.	24189363.	98156.	-0.005598	0.000
15.0000	1.0000000	3063264.	-39478.	-1648.1189	16224.	24818547.	88160.	-0.005451	0.000
12.5000	1.0000000	2808000.	-37038.	-1683.8617	17350.	25388128.	77992.	-0.005301	0.000
				-1705.6530	18809.	26343811.	67737.	-0.005148	0.000
				-1712.6896	20042.	26728864.	57438.	-0.004992	0.000
				-1720.2428	21400.	27051694.	47073.	-0.004834	0.000
				-1734.5200	22983.	27311785.	36662.	-0.004674	0.000
				-1733.8072	24546.	27509086.	26284.	-0.004512	0.000
				-1723.5924	26066.	27644035.	16021.	-0.004349	0.000
				-1697.5073	27313.	27717569.	5956.3995	-0.004186	0.000
				-1657.3571	28861.	27731133.	-3825.1244	-0.004022	0.000
				-1603.1509	30986.	27686679.	-13240.	-0.003859	0.000
				-1535.1397	31297.	27386500.	-21898.	-0.003696	0.000
				-1530.9600	32526.	27366506.	-29659.	-0.003533	0.000
				-1350.7500	35119.	27437690.	-29659.	-0.003372	0.000
				-1235.8470	36432.	27243936.	-37021.	-0.003212	0.000
				-1218.1938	37611.	27006026.	-44262.	-0.003054	0.000
				-1195.6182	38922.	26724777.	-51334.	-0.002898	0.000
				-1168.1583	39377.	26401182.	-58266.	-0.002737	0.000
				-340.5354	1711.3010	26401182.			
				4.000	1.1512	11932577.			

Computed values of Pile Loading and Deflection for Lateral Loading for Load Case Number 8

Depth Res. X	Soil Spr. y	Deflect. in-lb	Bending Moment in-lb	Shear Force lbs	Slope radians	Total Stress psi*	Bending Stiffness lb-in ²	Soil P lb/in
0.000	0.000	1.5000	2808000.	191481.	-0.007359	0.000	1.632E+12	
0.000	0.500	1.4559	3970606.	191481.	-0.007347	0.000	1.632E+12	
0.000	1.000	1.4118	5133186.	191481.	-0.007330	0.000	1.630E+12	
1.500	1.3679	6295730.	190535.	190535.	-0.007309	0.000	1.628E+12	
-315.2227	1382.6395	0.000	188623.	188623.	-0.007284	0.000	1.625E+12	
-322.1309	1459.6604	0.000	186671.	186671.	-0.007254	0.000	1.623E+12	
-328.6542	1539.9470	0.000	184680.	184680.	-0.007214	0.000	1.189E+12	
-334.7881	1623.7573	0.000	182654.	182654.	-0.007161	0.000	1.161E+12	
-340.5354	1711.3010	0.000	180595.	180595.	-0.007102	0.000	1.139E+12	

Pile-head conditions are Displacement and Moment (Loading Type 4)
 Displacement of pile head = 1.500000 inches
 Moment at pile head = 2808000.0 in-lb
 Axial load at pile head = 311000.0 lbs

20.000	0.1579	26036405.	0.000	1.023E+12	0.000	693.9172	150517.	0.000	0.000	0.000	1.630E+12
-1098.8797	41756.	0.000	0.000	1.024E+12	0.000	36.000	-0.0275	5379893.	-81576.	3.287E-05	0.000
20.500	0.1419	25631784.	0.000	1.026E+12	0.000	700.3695	152677.	0.000	0.000	0.000	1.630E+12
-1057.2866	44708.	0.000	0.000	1.028E+12	0.000	36.500	-0.0273	4902963.	-77364.	5.179E-05	0.000
21.000	0.1268	25188820.	0.000	1.031E+12	0.000	703.6356	154837.	0.000	0.000	0.000	1.631E+12
-1011.2587	47857.	0.000	0.000	1.033E+12	0.000	37.000	-0.0269	4451331.	-73141.	6.900E-05	0.000
21.500	0.1126	24709176.	0.000	1.036E+12	0.000	703.9243	156997.	0.000	0.000	0.000	1.632E+12
-977.6225	52112.	0.000	0.000	1.039E+12	0.000	37.500	-0.0264	4025009.	-68926.	8.459E-05	0.000
22.000	0.0992	24194068.	0.000	1.042E+12	0.000	701.3242	159157.	0.000	0.000	0.000	1.632E+12
-942.8253	57024.	0.000	0.000	1.046E+12	0.000	38.000	-0.0259	3623908.	-64734.	9.865E-05	0.000
22.500	0.0867	23644756.	0.000	1.050E+12	0.000	696.0030	161317.	0.000	0.000	0.000	1.632E+12
-903.8499	62558.	0.000	0.000	1.055E+12	0.000	38.500	-0.0253	3247838.	-60581.	0.000111	0.000
23.000	0.0750	23062650.	0.000	1.060E+12	0.000	688.1062	163477.	0.000	0.000	0.000	1.632E+12
-860.5620	68845.	0.000	0.000	1.065E+12	0.000	39.000	-0.0246	2896518.	-56484.	0.000123	0.000
23.500	0.0641	22449313.	0.000	1.071E+12	0.000	677.7770	165637.	0.000	0.000	0.000	1.632E+12
-812.7797	76064.	0.000	0.000	1.078E+12	0.000	665.1548	167797.	0.000	0.000	0.000	1.632E+12
24.000	0.0540	21806475.	0.000	1.085E+12	0.000	650.3749	169957.	0.000	0.000	0.000	1.632E+12
-760.2489	84468.	0.000	0.000	1.093E+12	0.000	633.5679	172117.	0.000	0.000	0.000	1.633E+12
24.500	0.0446	21136034.	0.000	1.102E+12	0.000	614.8589	174277.	0.000	0.000	0.000	1.633E+12
-702.6031	94424.	0.000	0.000	1.112E+12	0.000	594.3671	176437.	0.000	0.000	0.000	1.633E+12
25.000	0.0360	20440072.	0.000	1.123E+12	0.000	572.2054	178597.	0.000	0.000	0.000	1.633E+12
-631.2210	105157.	0.000	0.000	1.135E+12	0.000	548.4798	180757.	0.000	0.000	0.000	1.633E+12
25.500	0.0281	19721169.	0.000	1.148E+12	0.000	523.2895	182917.	0.000	0.000	0.000	1.633E+12
-502.3657	107317.	0.000	0.000	1.163E+12	0.000	496.7260	185077.	0.000	0.000	0.000	1.633E+12
26.000	0.0208	18983972.	0.000	1.179E+12	0.000	468.8738	187237.	0.000	0.000	0.000	1.633E+12
-380.0812	109477.	0.000	0.000	1.204E+12	0.000	439.8094	189397.	0.000	0.000	0.000	1.633E+12
26.500	0.0142	18232891.	0.000	1.242E+12	0.000	409.6020	191557.	0.000	0.000	0.000	1.633E+12
-264.5694	111637.	0.000	0.000	1.282E+12	0.000	378.3133	193717.	0.000	0.000	0.000	1.633E+12
27.000	0.008224	17472094.	0.000	1.339E+12	0.000	345.9976	195877.	0.000	0.000	0.000	1.633E+12
-155.9820	113797.	0.000	0.000	1.406E+12	0.000	312.7023	198037.	0.000	0.000	0.000	1.633E+12
27.500	0.002816	16705499.	0.000	1.496E+12	0.000	278.4677	200197.	0.000	0.000	0.000	1.633E+12
-54.4231	115957.	0.000	0.000	1.606E+12	0.000	243.3280	202357.	0.000	0.000	0.000	1.633E+12
28.000	-0.002034	15936771.	0.000	1.757E+12	0.000	249.1260	245768.	0.000	0.000	0.000	1.633E+12
40.0487	118117.	0.000	0.000	1.939E+12	0.000	224.6811	272449.	0.000	0.000	0.000	1.633E+12
28.500	-0.006356	15169321.	0.000	2.123E+12	0.000	197.2142	310289.	0.000	0.000	0.000	1.633E+12
127.4170	120277.	0.000	0.000	2.379E+12	0.000	165.2356	370109.	0.000	0.000	0.000	1.633E+12
207.7061	122437.	0.000	0.000	2.679E+12	0.000	125.3459	243570.	0.000	0.000	0.000	1.633E+12
280.9772	124597.	0.000	0.000	3.039E+12	0.000						
30.000	-0.0135	13650614.	0.000	3.479E+12	0.000						
347.3261	126757.	0.000	0.000	4.019E+12	0.000						
30.500	-0.0164	12904904.	0.000	4.679E+12	0.000						
406.8805	128917.	0.000	0.000	5.479E+12	0.000						
459.7967	131077.	0.000	0.000	6.579E+12	0.000						
31.000	-0.0210	11452763.	0.000	7.979E+12	0.000						
506.2573	133237.	0.000	0.000	9.779E+12	0.000						
31.500	-0.0228	10750396.	0.000	1.197E+13	0.000						
546.4675	135337.	0.000	0.000	1.477E+13	0.000						
32.000	-0.0242	10066152.	0.000	1.797E+13	0.000						
580.6526	137557.	0.000	0.000	2.197E+13	0.000						
32.500	-0.0253	9401485.	0.000	2.797E+13	0.000						
33.000	-0.0262	8757634.	0.000	3.497E+13	0.000						
609.0905	139717.	0.000	0.000	4.497E+13	0.000						
33.500	-0.0268	8135649.	0.000	5.797E+13	0.000						
633.5304	141877.	0.000	0.000	7.497E+13	0.000						
34.000	-0.0272	7536416.	0.000	9.797E+13	0.000						
654.0980	144037.	0.000	0.000	1.279E+14	0.000						
34.500	-0.0275	6960678.	0.000	1.679E+14	0.000						
670.9255	146197.	0.000	0.000	2.179E+14	0.000						
35.000	-0.0277	6409046.	0.000	2.879E+14	0.000						
684.1512	148357.	0.000	0.000	3.879E+14	0.000						
35.500	-0.0277	5881999.	0.000	5.179E+14	0.000						

* This analysis computed pile response using nonlinear moment-curvature relationships.
Values of total stress due to combined axial and bending stresses are computed

only for elastic sections only and do not equal the actual stresses in concrete and steel.
 Stresses in concrete and steel may be interpolated from the output for nonlinear bending properties relative to the magnitude of bending moment developed in the pile.

Output Summary for Load Case No. 8:

Pile-head deflection = 1.5000000 inches
 Computed slope at pile head = -0.0073591 radians
 Maximum bending moment = 27731133. inch-lbs
 Maximum shear force = 191481. lbs
 Depth of maximum bending moment = 16.0000000 feet below pile head
 Depth of maximum shear force = 0.5000000 feet below pile head
 Number of iterations = 14
 Number of zero deflection points = 1

Pile-head Deflection vs. Pile Length for Load Case 8

Boundary Condition Type 4, Deflection and Moment

Deflection = 1.50000 in
 Moment = 2808000. in-lb
 Axial Load = 311000. lb

Pile Length feet	Pile Head Deflection inches	Maximum Moment in-lbs	Maximum Shear lbs
50.0000	1.5000000	27731133.	191481.
47.5000	1.5000000	27675434.	189202.
45.0000	1.5000000	27612376.	188801.
42.5000	1.5000000	27402575.	187911.
40.0000	1.5000000	26979813.	186180.
37.5000	1.5000000	26002014.	181764.
35.0000	1.5000000	23971019.	168900.
32.5000	1.5000000	21318151.	-155018.
30.0000	1.5000000	18123005.	-144757.
27.5000	1.5000000	14828393.	-130939.
25.0000	1.5000000	11692252.	-115731.
22.5000	1.5000000	8765229.	-99294.
20.0000	1.5000000	6333756.	-83394.
17.5000	1.5000000	452671.	-70190.
15.0000	1.5000000	3271292.	-56859.
12.5000	1.5000000	2808000.	-45096.
10.0000	1.5000000	2808000.	-40252.
7.5000	1.5000000	2808000.	60714.
5.0000	1.5000000	2808000.	28175.
0.000000	0.0000000	6.224330E+12	5.668093E+12

Summary of Pile Response(s)

Definitions of Pile-head Loading Conditions:

Load Type 1: Load 1 = Shear, lbs, and Load 2 = Moment, in-lbs
 Load Type 2: Load 1 = Shear, lbs, and Load 2 = Slope, radians
 Load Type 3: Load 1 = Shear, lbs, and Load 2 = Rotational stiffness, in-lbs/radian
 Load Type 4: Load 1 = Top Deflection, inches, and Load 2 = Moment, in-lbs
 Load Type 5: Load 1 = Top Deflection, inches, and Load 2 = Slope, radians

Load Case No.	Load Type	Maximum Shear in Pile, lbs	Maximum Moment in Pile, in-lb/rad.	Pile-head Condition 1, Rotation or in-lb/rad., radians	Pile-head Condition 2, in-lb, rad., or in-lb/rad., radians	Axial Loading, lbs	Pile-head Deflection, inches	Maximum Moment in Pile, in-lbs
1	1	V = 55300.	M = 3729000.			402100.	0.25664708	
2	1	V = 55300.	M = 3729000.			311000.	0.18891412	
3	4	Y = 42300.	M = 2808000.			402100.	1.00000000	
4	4	Y = 144640.	M = 3729000.			402100.	1.50000000	
5	4	Y = 189145.	M = 3729000.			402100.	2.00000000	
6	4	Y = 229310.	M = 3729000.			311000.	0.50000000	
7	4	Y = 94031.	M = 2808000.			311000.	1.00000000	
8	4	Y = 146979.	M = 2808000.			311000.	1.50000000	
9	4	Y = 191481.	M = 2808000.			311000.	1.50000000	

The analysis ended normally.

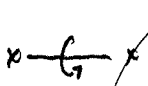
SER 1
 $\Delta = 0.19 < 1.0$
 OK

LATERAL CAPACITY @ 2" Deflection (SER 1) = 229.3 K
 LATERAL CAPACITY @ 1" Deflection (SER 2) = 146.98 K

PROJECT BR 1-159 JOB NO. _____ SHEET NO. 1 OF 1
 LOCATION JAMES ST OVER CHRISTINA RIVER
 SUBJECT ABUT B
 DESIGNED BY ZMR DATE 10/14/14 CHECKED BY _____ DATE _____
 REVISED BY _____ DATE _____ BACK CHECKED BY _____ DATE _____

ABUTMENT B

AXIAL = 402.1 K
 LATERAL = 55.3 K
 MOMENT = 3729 K-IN



Actual Deflection = 0.26"

STRENGTH I

@ 1" Deflection, Lateral = 144.64 k
 @ 1.5" " " = 189.15 k
 @ 2.0" " " = 229.3 k
 229.3 > 55.3 k ✓

SERVICE II

AXIAL = 311 K
 LATERAL = 42.3 K
 MOMENT = 2908 K-IN



Actual Deflection = 0.19"

@ 0.5" Deflection, Lateral = 94.03 k
 @ 1.0" " " = 146.98 k
 @ 1.5" " " = 191.48 k

[4-PISSINS @ 13L6"]

146.98 k > 42.3 k ✓

GEOTECHNICAL STRENGTH AXIAL CAPACITY
 415^k COMPRESSION > 402.1^k ✓

REF./REM.

FINAL FOUNDATION REPORT (REV. November 2014)
BR 1-159 - Newport Bridge
James Street Over Christina River
New Castle County, Delaware

APPENDIX C-2

Piers Design Calculations

PIER 1

LAYER

Boring No. JS-3

By: SJM

Chk: AT
OG Elev. =

11.00

Sample No.	Depth of SS run (ft)	N-Values Field	q' _v (ksf)	C _H	N _{CORR}
2	2	18	0.220	1.740	31
3	4	8	0.440	1.508	9
4	6	7	0.288	1.853	12
5	8	60	0.381	1.856	78
6	10	4	0.476	1.482	6
7	12	2	0.671	1.421	3
8	14	44	0.688	1.389	60
9	16	18	0.782	1.325	24
10	18	3	0.887	1.285	4
11	20	4	0.952	1.250	5
13	24	5	1.142	1.189	6
14	26	13	1.238	1.162	15
15	28	49	1.333	1.138	55
16	30	8	1.428	1.114	9
17	32	30	1.523	1.093	33
18	34	33	1.618	1.073	35
19	36	72	1.714	1.053	78
20	38	32	1.809	1.035	39
21	40	30	1.904	1.018	31
22	43	14	2.047	0.994	14
23	48	11	2.288	0.957	11
24	53	25	2.523	0.924	23
25	58	29	2.761	0.894	28
26	63	23	2.999	0.866	20
27	68	10	3.237	0.841	8
28	73	16	3.475	0.817	13
29	78	18	3.713	0.795	14
30	83	37	3.951	0.774	29
31	88	61	4.189	0.755	46
32	93	67	4.427	0.738	42
33	98	46	4.665	0.719	32
34	103	84	4.903	0.702	45
35	108	50	5.141	0.688	34
36	113	60	5.379	0.671	34
37	118	60	5.617	0.658	33

GWTE = 5.0
γ = 110 lb/ft³
γ' = 47.6 lb/ft³

- ① 3-60
- ② 8-76
- ③ 13-46
- ④ 32-45

$C_H = 0.77 \times \log(40/q'_v)$
 $N_{CORR} = N_{FIELD} \times C_H$

N_{avg} (below SPT)
(Ref. AASHTO Eqn 10.4.8.2.4-1)

Boring No. JS-4

By: SJM

Chk: AT
OG Elev. =

4-0

Sample No.	Depth of SS run (ft)	N-Values Field	q' _v (ksf)	C _H	N _{CORR}
2A	2	4	0.220	1.740	7
2B	3	3	0.330	1.604	6
3	4	4	0.190	1.788	7
4	6	3	0.288	1.853	6
U-1	8	0	0.381	1.856	0
6	10	2	0.476	1.482	3
8	12	2	0.671	1.421	3
7	14	2	0.688	1.389	3
8	16	4	0.782	1.325	5
9	18	2	0.887	1.285	3
10	23	8	1.085	1.203	10
11	28	38	1.333	1.138	41
12	33	19	1.571	1.083	21
13	38	18	1.809	1.035	19
14	43	32	2.047	0.994	32
15	48	40	2.288	0.957	38
16	53	34	2.523	0.924	31
17	58	22	2.761	0.894	20
18	63	18	2.999	0.866	14
19	68	14	3.237	0.841	12
20	73	25	3.475	0.817	20
21	78	40	3.713	0.795	32
22	83	40	3.951	0.774	31
23	88	48	4.189	0.755	36
24	93	45	4.427	0.738	33
25	98	38	4.665	0.719	27
26	104.7	68	4.884	0.698	61
27	108	80	5.141	0.688	34
28	113.2	60	5.388	0.670	34
29	118	50	5.617	0.658	33

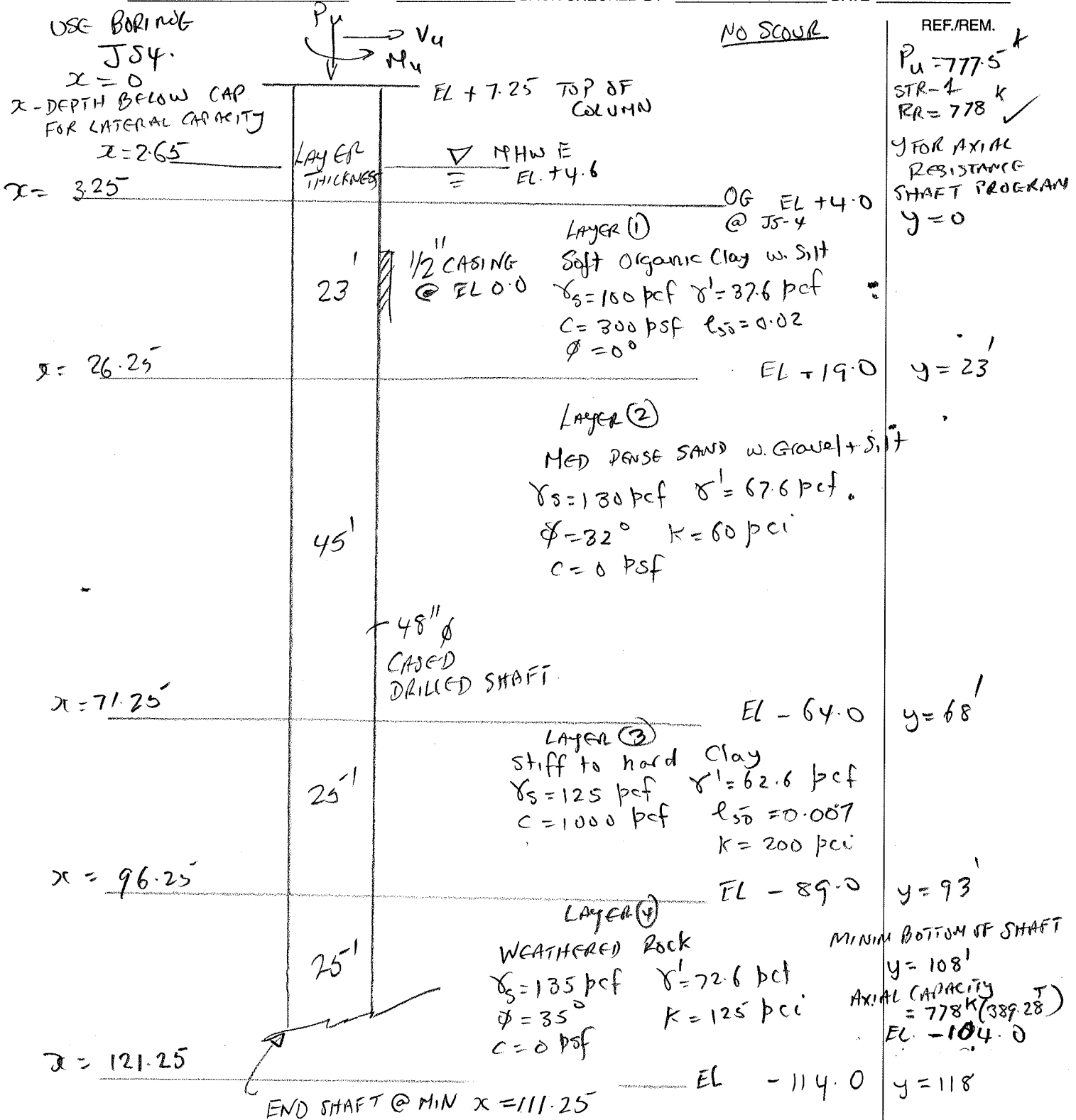
5.0 assumed
γ = 110 lb/ft³
γ' = 47.6 lb/ft³

- ① 0-10
- ② 12-41
- ③ 20-35
- ④ 27-61

$C_H = 0.77 \times \log(40/q'_v)$
 $N_{CORR} = N_{FIELD} \times C_H$

N_{avg} (below SPT)
(Ref. AASHTO Eqn 10.4.8.2.4-1)

PROJECT BR 1-159 JOB NO. _____ SHEET NO. 1 OF 1
 LOCATION PIER 1
 SUBJECT AXIAL & LATERAL CAPACITIES (4-COL/INDIVIDUAL DRILLED SHAFTS)
 DESIGNED BY SJM DATE 7/14 CHECKED BY AT DATE 8/14
 REVISED BY _____ DATE _____ BACK CHECKED BY _____ DATE _____



AXIAL CAPACITY

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=====
Pier 11.sffd.sfo
SHAFT for windows, Version 2012.7.11
Serial Number : 228741384
VERTICALLY LOADED DRILLED SHAFT ANALYSIS
(c) Copyright ENSOFT, Inc., 1987-2012
All Rights Reserved
=====

Path to file locations : Y:\Bridges\DELDOT\BRI-159_JAMES ST
BRIDGE\FOUNDATION REPORT\SHAFT output\
Name of input data file : Pier 11.sffd.sfo
Name of output file : Pier 11.sffd.sfo
Name of plot output file : Pier 11.sffd.sfp
Name of runtime file : Pier 11.sffd.sfr
-----
Time and Date of Analysis
-----
Date: October 27, 2014 Time: 15:11:36
BRI-159 Pier 1
PROPOSED DEPTH = 110.0 FT
-----
NUMBER OF LAYERS = 4
-----
WATER TABLE DEPTH = 0.0 FT.
-----

SOIL INFORMATION
-----
LAYER NO 1-----CLAY
AT THE TOP
STRENGTH REDUCTION FACTOR-ALPHA = 0.550E+00
END BEARING COEFFICIENT-NC = 0.800E+01
UNDRAINED SHEAR STRENGTH, LB/SQ FT = 0.300E+03
INTERNAL FRICTION ANGLE, DEG. = 0.000E+00
BLOWS PER FOOT FROM STANDARD PENETRATION TEST = 0.000E+00
SOIL UNIT WEIGHT, LB/CU FT = 0.100E+03
MAXIMUM LOAD TRANSFER FOR SOIL, LB/SQ FT = 0.100E+11
DEPTH, FT = 0.000E+00

AT THE BOTTOM
STRENGTH REDUCTION FACTOR-ALPHA = 0.550E+00
END BEARING COEFFICIENT-NC = 0.800E+01
UNDRAINED SHEAR STRENGTH, LB/SQ FT = 0.300E+03
INTERNAL FRICTION ANGLE, DEG. = 0.000E+00
BLOWS PER FOOT FROM STANDARD PENETRATION TEST = 0.000E+00
SOIL UNIT WEIGHT, LB/CU FT = 0.100E+03
MAXIMUM LOAD TRANSFER FOR SOIL, LB/SQ FT = 0.100E+11
DEPTH, FT = 0.000E+00

LAYER NO 2-----SAND
AT THE TOP
SKIN FRICTION COEFFICIENT- BETA = 0.853E+00
UNDRAINED SHEAR STRENGTH, LB/SQ FT = 0.000E+00
INTERNAL FRICTION ANGLE, DEG. = 0.320E+02
BLOWS PER FOOT FROM STANDARD PENETRATION TEST = 0.000E+00
SOIL UNIT WEIGHT, LB/CU FT = 0.130E+03
MAXIMUM LOAD TRANSFER FOR SOIL, LB/SQ FT = 0.100E+11
DEPTH, FT = 0.230E+02

AT THE BOTTOM
SKIN FRICTION COEFFICIENT- BETA = 0.387E+00
UNDRAINED SHEAR STRENGTH, LB/SQ FT = 0.000E+00
INTERNAL FRICTION ANGLE, DEG. = 0.320E+02
BLOWS PER FOOT FROM STANDARD PENETRATION TEST = 0.000E+00
SOIL UNIT WEIGHT, LB/CU FT = 0.130E+03
MAXIMUM LOAD TRANSFER FOR SOIL, LB/SQ FT = 0.680E+02

LAYER NO 3-----CLAY
AT THE TOP
STRENGTH REDUCTION FACTOR-ALPHA = 0.550E+00
END BEARING COEFFICIENT-NC = 0.800E+01
UNDRAINED SHEAR STRENGTH, LB/SQ FT = 0.100E+04
INTERNAL FRICTION ANGLE, DEG. = 0.000E+00
BLOWS PER FOOT FROM STANDARD PENETRATION TEST = 0.000E+00
SOIL UNIT WEIGHT, LB/CU FT = 0.125E+03
MAXIMUM LOAD TRANSFER FOR SOIL, LB/SQ FT = 0.100E+11
DEPTH, FT = 0.680E+02

AT THE BOTTOM
STRENGTH REDUCTION FACTOR-ALPHA = 0.550E+00
END BEARING COEFFICIENT-NC = 0.800E+01
UNDRAINED SHEAR STRENGTH, LB/SQ FT = 0.100E+04
INTERNAL FRICTION ANGLE, DEG. = 0.000E+00
BLOWS PER FOOT FROM STANDARD PENETRATION TEST = 0.000E+00
=====

```

Pier 11.sffd.sfo

Pier 11.sffdd.sfo
 SOIL UNIT WEIGHT, LB/CU FT = 0.125E+03
 MAXIMUM LOAD TRANSFER FOR SOIL, LB/SQ FT = 0.100E+11
 DEPTH, FT = 0.930E+02

LRFD RESISTANCE FACTOR (SIDE FRICTION) = 0.450E+00
 LRFD RESISTANCE FACTOR (TOP RESISTANCE) = 0.400E+00

LAYER NO 4-----SAND

AT THE TOP

SKIN FRICTION COEFFICIENT- BETA = 0.250E+00
 UNDRAINED SHEAR STRENGTH, LB/SQ FT = 0.000E+00
 INTERNAL FRICTION ANGLE, DEG. = 0.350E+02
 BLOWS PER FOOT FROM STANDARD PENETRATION TEST = 0.000E+00
 SOIL UNIT WEIGHT, LB/CU FT = 0.135E+03
 MAXIMUM LOAD TRANSFER FOR SOIL, LB/SQ FT = 0.100E+11
 DEPTH, FT = 0.930E+02

AT THE BOTTOM

SKIN FRICTION COEFFICIENT- BETA = 0.250E+00
 UNDRAINED SHEAR STRENGTH, LB/SQ FT = 0.000E+00
 INTERNAL FRICTION ANGLE, DEG. = 0.350E+02
 BLOWS PER FOOT FROM STANDARD PENETRATION TEST = 0.000E+00
 SOIL UNIT WEIGHT, LB/CU FT = 0.135E+03
 MAXIMUM LOAD TRANSFER FOR SOIL, LB/SQ FT = 0.100E+11
 DEPTH, FT = 0.118E+03

LRFD RESISTANCE FACTOR (SIDE FRICTION) = 0.550E+00
 LRFD RESISTANCE FACTOR (TOP RESISTANCE) = 0.500E+00

DRILLED SHAFT INFORMATION

DIAMETER OF STEM = 4.000 FT.
 DIAMETER OF BASE = 4.000 FT.
 END OF STEM TO BASE = 0.000 FT.
 ANGLE OF BELL = 0.000 DEG.
 IGNORED TOP PORTION = 5.000 FT.
 IGNORED BOTTOM PORTION = 4.000 FT.
 AREA OF ONE PERCENT STEEL = 18.098 SQ.IN.
 ELASTIC MODULUS, EC = 0.312E+07 LB/SQ IN
 VOLUME OF UNDERREAM = 0.000 CU.YDS.

PREDICTED RESULTS

QS = ULTIMATE SIDE RESISTANCE;
 QB = ULTIMATE BASE RESISTANCE;
 WT = WEIGHT OF DRILLED SHAFT (UPLIFT CAPACITY ONLY);
 QU = TOTAL ULTIMATE RESISTANCE;
 LRFD QS = TOTAL SIDE FRICTION USING LRFD RESISTANCE FACTOR

Pier 11.sffdd.sfo
 TO THE ULTIMATE SIDE RESISTANCE:
 LRFD QB = TOTAL BASE BEARING USING LRFD RESISTANCE FACTOR
 TO THE ULTIMATE BASE RESISTANCE
 LRFD QU = TOTAL CAPACITY WITH LRFD RESISTANCE FACTOR.

LENGTH (FEET)	VOLUME (CU.YDS)	QS (TONS)	QB (TONS)	QU (TONS)	LRFD QS (TONS)	LRFD QB (TONS)	LRFD QU (TONS)
10.0	4.65	1.04	15.08	16.12	0.47	6.03	6.50
11.0	5.12	2.07	15.08	17.16	0.93	6.03	6.97
12.0	5.59	3.11	15.08	18.19	1.40	6.03	7.43
13.0	6.05	4.15	15.08	19.23	1.87	6.03	7.90
14.0	6.52	5.18	15.08	20.27	2.33	6.03	8.37
15.0	6.98	6.22	15.08	21.30	2.80	6.03	8.83
16.0	7.45	7.26	22.88	30.13	3.27	9.15	12.42
17.0	7.91	8.29	31.53	39.83	3.73	12.61	16.35
18.0	8.38	9.33	41.06	49.53	4.20	16.42	20.62
19.0	8.84	10.37	51.45	61.82	4.67	20.58	25.25
20.0	9.31	11.41	59.24	70.65	5.13	23.70	28.83
21.0	9.78	12.44	64.44	76.88	5.60	25.78	31.38
22.0	10.24	13.48	67.04	80.52	6.07	26.82	32.88
23.0	10.71	14.52	67.04	81.55	6.53	33.52	40.05
24.0	11.17	15.55	67.04	82.59	7.00	33.52	40.98
25.0	11.64	16.59	67.04	83.63	7.47	33.52	41.45
26.0	12.10	17.63	67.04	84.66	7.93	33.52	41.92
27.0	12.57	18.66	67.04	85.70	8.40	33.52	42.39
28.0	13.03	23.40	67.04	90.44	11.00	33.52	44.52
29.0	13.50	28.41	67.04	95.45	13.76	33.52	47.28
30.0	13.96	33.68	67.04	100.72	16.66	33.52	50.18
31.0	14.43	39.21	67.04	106.25	19.70	33.52	53.22
32.0	14.90	44.98	67.04	112.02	22.87	33.52	56.39
33.0	15.36	50.99	67.04	118.02	26.18	33.52	59.69
34.0	15.83	57.22	67.04	124.26	29.60	33.52	63.12
35.0	16.29	63.67	67.04	130.71	33.15	33.52	66.67
36.0	16.76	70.33	67.04	137.37	36.82	33.52	70.33
37.0	17.22	77.19	67.04	144.23	40.59	33.52	74.11
38.0	17.69	84.24	67.04	151.28	44.47	33.52	77.99
39.0	18.15	91.48	67.04	158.52	48.45	33.52	81.97
40.0	18.62	98.90	67.04	165.93	52.53	33.52	86.05
41.0	19.08	106.48	67.04	173.52	56.70	33.52	90.22
42.0	19.55	114.22	67.04	181.26	60.95	33.52	94.47
43.0	20.02	122.12	67.04	189.15	65.30	33.52	98.82
44.0	20.48	130.16	67.04	197.19	69.72	33.52	103.24
45.0	20.95	138.34	67.04	205.37	74.22	33.52	107.74
46.0	21.41	146.64	67.04	213.68	78.79	33.52	112.31
47.0	21.88	155.08	67.04	222.12	83.43	33.52	116.95
48.0	22.34	163.63	67.04	230.66	88.13	33.52	121.65
49.0	22.81	172.29	67.04	239.32	92.89	33.52	126.41
50.0	23.27	181.05	67.04	248.09	97.71	33.52	131.23
51.0	23.74	189.90	67.04	256.94	102.58	33.52	136.10
52.0	24.21	198.85	67.04	265.89	107.50	33.52	141.02
53.0	24.67	207.88	67.04	274.92	112.47	33.52	145.99
54.0	25.14	216.98	67.04	284.02	117.47	33.52	150.99
55.0	25.60	226.15	67.04	293.19	122.52	33.52	156.04
56.0	26.07	235.39	67.04	302.43	127.60	33.52	161.12
57.0	26.53	244.68	67.04	311.72	132.71	33.52	166.23
58.0	27.00	254.02	67.04	321.06	137.85	33.52	171.37
59.0	27.46	263.41	67.04	330.45	143.01	33.52	176.53
60.0	27.93	272.83	67.04	339.87	148.19	33.52	181.71
61.0	28.39	282.29	67.04	349.31	153.39	33.52	186.95
62.0	28.86	291.77	67.04	358.78	158.61	33.52	192.23
63.0	29.33	301.27	67.04	368.25	163.83	33.52	197.53
64.0	29.79	310.78	67.04	377.73	169.06	33.52	202.85
65.0	30.26	320.30	67.04	387.21	174.30	33.52	208.19

Pier 11.sfffd.sfo		Pier 11.sfffd.sfo		Pier 11.sfffd.sfo		Pier 11.sfffd.sfo	
TOP LOAD	TIP MOVEMENT	TOP LOAD	TIP MOVEMENT	TOP LOAD	TIP MOVEMENT	TOP LOAD	TIP MOVEMENT
ton	IN.	ton	IN.	ton	IN.	ton	IN.
66.0	0.307E-01	329.82	0.1746E-02	51.11	0.1746E-02	184.77	0.1746E-02
67.0	0.1000E-04	339.34	0.1746E-02	50.27	0.1746E-02	389.61	0.1746E-02
68.0	0.5000E-03	348.85	0.1746E-02	50.27	0.1746E-02	399.12	0.1746E-02
69.0	0.1000E-03	358.34	0.1746E-02	50.27	0.1746E-02	408.61	0.1746E-02
70.0	0.5000E-02	367.81	0.1746E-02	50.27	0.1746E-02	418.08	0.1746E-02
71.0	0.7500E-02	377.26	0.1746E-02	50.27	0.1746E-02	427.53	0.1746E-02
72.0	0.1000E-01	386.67	0.1746E-02	50.27	0.1746E-02	436.94	0.1746E-02
73.0	0.2500E+00	390.13	0.1746E-02	50.27	0.1746E-02	446.40	0.1746E-02
74.0	0.5000E+00	393.58	0.1746E-02	50.27	0.1746E-02	455.85	0.1746E-02
75.0	0.7500E+00	397.04	0.1746E-02	50.27	0.1746E-02	465.31	0.1746E-02
76.0	0.1000E+00	400.49	0.1746E-02	50.27	0.1746E-02	474.77	0.1746E-02
77.0	0.2500E+00	403.95	0.1746E-02	50.27	0.1746E-02	484.22	0.1746E-02
78.0	0.5000E+00	407.41	0.1746E-02	50.27	0.1746E-02	493.68	0.1746E-02
79.0	0.7500E+00	410.86	0.1746E-02	50.27	0.1746E-02	503.13	0.1746E-02
80.0	0.1000E+00	414.32	0.1746E-02	50.27	0.1746E-02	512.59	0.1746E-02
81.0	0.2500E+00	417.78	0.1746E-02	50.27	0.1746E-02	522.04	0.1746E-02
82.0	0.5000E+00	421.23	0.1746E-02	50.27	0.1746E-02	531.49	0.1746E-02
83.0	0.7500E+00	424.69	0.1746E-02	50.27	0.1746E-02	540.94	0.1746E-02
84.0	0.1000E+00	428.14	0.1746E-02	50.27	0.1746E-02	550.39	0.1746E-02
85.0	0.2500E+00	431.60	0.1746E-02	50.27	0.1746E-02	559.84	0.1746E-02
86.0	0.5000E+00	435.06	0.1746E-02	50.27	0.1746E-02	569.29	0.1746E-02
87.0	0.7500E+00	438.51	0.1746E-02	50.27	0.1746E-02	578.74	0.1746E-02
88.0	0.1000E+00	441.97	0.1746E-02	50.27	0.1746E-02	588.19	0.1746E-02
89.0	0.2500E+00	445.43	0.1746E-02	50.27	0.1746E-02	597.64	0.1746E-02
90.0	0.5000E+00	448.88	0.1746E-02	50.27	0.1746E-02	607.09	0.1746E-02
91.0	0.7500E+00	452.34	0.1746E-02	50.27	0.1746E-02	616.54	0.1746E-02
92.0	0.1000E+00	455.79	0.1746E-02	50.27	0.1746E-02	625.99	0.1746E-02
93.0	0.2500E+00	459.25	0.1746E-02	50.27	0.1746E-02	635.44	0.1746E-02
94.0	0.5000E+00	462.71	0.1746E-02	50.27	0.1746E-02	644.89	0.1746E-02
95.0	0.7500E+00	466.16	0.1746E-02	50.27	0.1746E-02	654.34	0.1746E-02
96.0	0.1000E+00	469.62	0.1746E-02	50.27	0.1746E-02	663.79	0.1746E-02
97.0	0.2500E+00	473.07	0.1746E-02	50.27	0.1746E-02	673.24	0.1746E-02
98.0	0.5000E+00	476.53	0.1746E-02	50.27	0.1746E-02	682.69	0.1746E-02
99.0	0.7500E+00	480.00	0.1746E-02	50.27	0.1746E-02	692.14	0.1746E-02
100.0	0.1000E+00	483.46	0.1746E-02	50.27	0.1746E-02	701.59	0.1746E-02
101.0	0.2500E+00	486.93	0.1746E-02	50.27	0.1746E-02	711.04	0.1746E-02
102.0	0.5000E+00	490.39	0.1746E-02	50.27	0.1746E-02	720.49	0.1746E-02
103.0	0.7500E+00	493.86	0.1746E-02	50.27	0.1746E-02	729.94	0.1746E-02
104.0	0.1000E+00	497.32	0.1746E-02	50.27	0.1746E-02	739.39	0.1746E-02
105.0	0.2500E+00	500.79	0.1746E-02	50.27	0.1746E-02	748.84	0.1746E-02
106.0	0.5000E+00	504.25	0.1746E-02	50.27	0.1746E-02	758.29	0.1746E-02
107.0	0.7500E+00	507.71	0.1746E-02	50.27	0.1746E-02	767.74	0.1746E-02
108.0	0.1000E+00	511.18	0.1746E-02	50.27	0.1746E-02	777.19	0.1746E-02
109.0	0.2500E+00	514.64	0.1746E-02	50.27	0.1746E-02	786.64	0.1746E-02
110.0	0.5000E+00	518.11	0.1746E-02	50.27	0.1746E-02	796.09	0.1746E-02

$R_a = 778$

$y = 108$

RESULT FROM TREND (AVERAGED) LINE		RESULT FROM UPPER-BOUND LINE		RESULT FROM LOWER-BOUND LINE	
TOP LOAD	TIP MOVEMENT	TOP LOAD	TIP MOVEMENT	TOP LOAD	TIP MOVEMENT
ton	IN.	ton	IN.	ton	IN.
0.5497E-01	0.2385E-04	0.8271E-01	0.1746E-02	0.3156E-01	0.1817E-04
0.2748E+00	0.1193E-03	0.8271E-01	0.1746E-02	0.1526E-01	0.9065E-04
0.5497E+00	0.2385E-03	0.8271E-01	0.1746E-02	0.1526E-01	0.9065E-04
0.2748E+00	0.1193E-03	0.8271E-01	0.1746E-02	0.1526E-01	0.9065E-04
0.5504E+02	0.1789E-01	0.8271E-01	0.1746E-02	0.1526E-01	0.9065E-04
0.1375E+03	0.2386E-01	0.8271E-01	0.1746E-02	0.1526E-01	0.9065E-04
0.2500E+03	0.5971E-01	0.8271E-01	0.1746E-02	0.1526E-01	0.9065E-04
0.3262E+03	0.1148E+00	0.8271E-01	0.1746E-02	0.1526E-01	0.9065E-04
0.3814E+03	0.1601E+00	0.8271E-01	0.1746E-02	0.1526E-01	0.9065E-04
0.5184E+03	0.2011E+00	0.8271E-01	0.1746E-02	0.1526E-01	0.9065E-04
0.5719E+03	0.2500E+00	0.8271E-01	0.1746E-02	0.1526E-01	0.9065E-04
	0.6626E+00	0.8271E-01	0.1746E-02	0.1526E-01	0.9065E-04

PIER 1 LATERAL CAPACITY

Pier 1.laff.lp7o

Pier 1.laff.lp7o

Description: Pier 1 Lateral Capacity

LPile Plus for Windows, version 2013-07.007

Analysis of Individual Piles and Drilled Shafts
Subjected to Lateral Loading Using the p-y Method

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Files Used for Analysis

Path to file locations: Y:\Bridges\DELDOT\BRI-159_JAMES ST BRIDGE\FOUNDATION
REPORT\LPILE Output) Pier 1.laff.lp7d
Name of input data file: Pier 1.laff.lp7o
Name of output report file: Pier 1.laff.lp7p
Name of plot output file: Pier 1.laff.lp7p
Name of runtime message file: Pier 1.laff.lp7r

Date and Time of Analysis

Date: October 27, 2014 Time: 15:28:45

Problem Title

Project Name: BRI-159 Pier 1

Job Number:

Client: DELDOT

Engineer: SJM

Program Options and Settings

Engineering Units of Input Data and Computations:
- Engineering units are US Customary Units (pounds, feet, inches)

Analysis Control Options:
- Maximum number of iterations allowed = 500
- Deflection tolerance for convergence = 1.0000E-05 in
- Maximum allowable deflection = 300.0000 in
- Number of pile increments = 100

Loading Type and Number of Cycles of Loading:
- Static loading specified

Computational Options:

- Use unfactored loads in computations (conventional analysis)
- Compute pile response under loading and nonlinear bending properties of pile (only if nonlinear pile properties are input)
- Use of p-y modification factors for p-y curves not selected
- Loading by lateral soil movements acting on pile not selected
- Input of shear resistance at the pile tip not selected
- Computation of pile-head foundation stiffness matrix not selected
- Push-over analysis of pile not selected
- Buckling analysis of pile not selected

Output Options:

- No p-y curves to be computed and reported for user-specified depths
- Values of pile-head deflection, bending moment, shear force, and soil reaction are printed for full length of pile.
- Printing Increment (nodal spacing of output points) = 1

Pile Structural Properties and Geometry

Total number of pile sections = 2
Total length of pile = 111.25 ft
Depth of ground surface below top of pile = 3.25 ft

Pile diameter values used for p-y curve computations are defined using 4 points.
p-y curves are computed using pile diameter values interpolated with depth over the length of the pile.

Point	Depth X ft	Pile Diameter in
1	0.00000	48.0000000
2	7.25000	48.0000000
3	7.25000	49.0000000

4 111.250000 Pier 11aff.1p7o
 49.00000000

Input Structural Properties:

 Pile Section No. 1:
 Section Type = Drilled Shaft (Bored Pile)
 Section Length = 7.25000 ft
 Section Diameter = 48.00000 in

Pile Section No. 2:
 Section Type = Drilled Shaft with
 Permanent Casing
 Section Length = 104.00000 ft
 Section Diameter = 49.00000 in

 Ground Slope and Pile Batter Angles

 Ground Slope Angle = 0.000 degrees
 = 0.000 radians
 Pile Batter Angle = 0.000 degrees
 = 0.000 radians

 Soil and Rock Layering Information

The soil profile is modelled using 4 layers
 Layer 1 is soft clay, p-y criteria by Matlock, 1970
 Distance from top of pile to top of layer = 3.25000 ft
 Distance from top of pile to bottom of layer = 26.25000 ft
 Effective unit weight at top of layer = 37.60000 pcf
 Effective unit weight at bottom of layer = 37.60000 pcf
 Undrained cohesion at top of layer = 300.00000 psf
 Undrained cohesion at bottom of layer = 300.00000 psf
 Epsilon-50 at top of layer = 0.02000
 Epsilon-50 at bottom of layer = 0.02000

Layer 2 is sand, p-y criteria by Reese et al., 1974
 Distance from top of pile to top of layer = 26.25000 ft
 Distance from top of pile to bottom of layer = 71.25000 ft
 Effective unit weight at top of layer = 67.60000 pcf
 Effective unit weight at bottom of layer = 67.60000 pcf
 Friction angle at top of layer = 32.00000 deg.
 Friction angle at bottom of layer = 32.00000 deg.
 Subgrade k at top of layer = 60.00000 pci
 Subgrade k at bottom of layer = 60.00000 pci

Layer 3 is stiff clay with water-induced erosion
 Distance from top of pile to top of layer = 71.25000 ft
 Distance from top of pile to bottom of layer = 96.25000 ft
 Effective unit weight at top of layer = 62.60000 pcf
 Effective unit weight at bottom of layer = 62.60000 pcf
 Friction angle at top of layer = 35.00000 deg.
 Friction angle at bottom of layer = 35.00000 deg.
 Subgrade k at top of layer = 125.00000 pci
 Subgrade k at bottom of layer = 125.00000 pci

Pier 11aff.1p7o
 71.25000 ft
 96.25000 ft
 62.60000 pcf
 62.60000 pcf
 1000.00000 psf
 1000.00000 psf
 0.00700
 0.00700
 200.00000 pci
 200.00000 pci

Layer 4 is sand, p-y criteria by Reese et al., 1974
 Distance from top of pile to top of layer = 96.25000 ft
 Distance from top of pile to bottom of layer = 121.25000 ft
 Effective unit weight at top of layer = 72.60000 pcf
 Effective unit weight at bottom of layer = 72.60000 pcf
 Friction angle at top of layer = 35.00000 deg.
 Friction angle at bottom of layer = 35.00000 deg.
 Subgrade k at top of layer = 125.00000 pci
 Subgrade k at bottom of layer = 125.00000 pci

(Depth of lowest soil layer extends 10.00 ft below pile tip)

 Summary of Soil Properties

Layer Num.	Soil Type	Layer Depth	Effective Unit wt.	Undrained Cohesion
deg.	(p-y Curve Criteria)	ft	pcf	psf
1	Soft Clay	3.250	37.600	300.000
	Factor Epsilon 50			
	0.02000			
2	Sand (Reese, et al.)	26.250	37.600	300.000
	60.000			
3	Stiff Clay with Free Water	71.250	67.600	--
	200.000			
4	Sand (Reese, et al.)	96.250	62.600	1000.000
	125.000			
35.000	--	121.250	72.600	--

Pier 11aff.1p7o
 Static loading criteria were used when computing p-y curves for all analyses.
 Pile-head Loading and Pile-head Fixity Conditions
 Number of loads specified = 10

Load Compute	Condition	Condition	Axial Thrust Force, lbs
No. Type	1	2	
Top y vs. Pile Length			
1 4	Y = 0.50000 in	M = 5499600. in-lbs	0.0000000
2 4	Y = 1.00000 in	M = 5499600. in-lbs	0.0000000
3 4	Y = 1.50000 in	M = 5499600. in-lbs	0.0000000
4 4	Y = 2.00000 in	M = 5499600. in-lbs	0.0000000
5 4	Y = 0.50000 in	M = 783600. in-lbs	0.0000000
6 4	Y = 1.00000 in	M = 783600. in-lbs	0.0000000
7 4	Y = 1.50000 in	M = 783600. in-lbs	0.0000000
8 4	Y = 2.00000 in	M = 783600. in-lbs	0.0000000
9 1	V = 13600. lbs	M = 5499600. in-lbs	0.0000000
10 1	V = 9900.00000 lbs	M = 783600. in-lbs	0.0000000

V = perpendicular shear force applied to pile head
 M = bending moment applied to pile head
 y = lateral deflection relative to pile axis
 S = pile slope relative to original pile batter angle
 R = rotational stiffness applied to pile head
 Axial thrust is assumed to be acting axially for all pile batter angles.

Computations of Nominal Moment Capacity and NonLinear Bending Stiffness

Axial thrust force values were determined from pile-head loading conditions
 Number of Pile Sections Analyzed = 2

Pile Section No. 1:

Dimensions and Properties of Drilled shaft (Bored Pile):
 Length of Section = 7.25000 ft
 Shaft Diameter = 48.00000 in
 Concrete Cover Thickness = 4.00000 in
 Number of Reinforcing Bars = 50 bars

Pier 11aff.1p7o
 Yield stress of Reinforcing Bars = 60000. psi
 Modulus of Elasticity of Reinforcing Bars = 29000000. psi
 Gross Area of Shaft = 1809.55737 sq. in.
 Total Area of Reinforcing steel = 39.50000 sq. in.
 Area Ratio of Steel Reinforcement = 2.18 percent
 Edge-to-Edge Bar Spacing = 2.89438 in
 Maximum Concrete Aggregate Size = 0.37500 in
 Ratio of Bar Spacing to Aggregate Size = 7.72
 Offset of Center of Rebar Cage from Center of Pile = 0.00000 in

Axial structural Capacities:

Nom. Axial structural Capacity = 0.85 Fc Ac + Fy As = 9140.470 kips
 Tensile Load for Cracking of Concrete = -911.303 kips
 Nominal Axial Tensile Capacity = -2370.000 kips

Reinforcing Bar Dimensions and Positions Used in Computations:

Bar Number	Bar Diam. inches	Bar Area sq. in.	X inches	Y inches
1	1.00000	0.79000	19.49359	-0.49995
2	1.00000	0.79000	19.49359	0.49995
3	1.00000	0.79000	19.00549	4.36362
4	1.00000	0.79000	18.75683	5.33210
5	1.00000	0.79000	17.32321	8.95300
6	1.00000	0.79000	16.84151	9.82921
7	1.00000	0.79000	14.52454	12.97984
8	1.00000	0.79000	13.86798	13.70873
9	1.00000	0.79000	10.86731	16.19110
10	1.00000	0.79000	10.02307	16.72687
11	1.00000	6.49933	6.49933	18.38501
12	1.00000	5.54837	5.54837	18.69400
13	1.00000	1.72297	1.72297	19.42373
14	1.00000	0.72505	0.72505	19.48652
15	1.00000	0.79000	-3.16184	19.24199
16	1.00000	0.79000	-4.14382	19.05462
17	1.00000	0.79000	-7.84760	17.85119
18	1.00000	0.79000	-8.75233	17.45346
19	1.00000	0.79000	-12.04047	15.33875
20	1.00000	0.79000	-12.81090	14.70139
21	1.00000	0.79000	-15.47679	11.86271
22	1.00000	0.79000	-16.06451	11.03536
23	1.00000	0.79000	-17.94064	7.64051
24	1.00000	0.79000	-18.30872	6.71163
25	1.00000	0.79000	-19.27722	2.93370
26	1.00000	0.79000	-19.40234	1.84719
27	1.00000	0.79000	-19.50254	-1.85019
28	1.00000	0.79000	-19.27622	-2.93370
29	1.00000	0.79000	-16.30822	-9.61063
30	1.00000	0.79000	-17.94064	-11.64326
31	1.00000	0.79000	-16.05451	-11.83336
32	1.00000	0.79000	-11.87609	-11.90139
33	1.00000	0.79000	-12.81090	-15.33875
34	1.00000	0.79000	-12.04047	-15.45346
35	1.00000	0.79000	-9.82921	-17.38546
36	1.00000	0.79000	-7.84760	-17.85119
37	1.00000	0.79000	-4.14382	-19.05462
38	1.00000	0.79000	-3.16184	-19.24199
39	1.00000	0.79000	0.72505	-19.48652
40	1.00000	0.79000	1.72297	-19.42373

Pier 11aff. 1p70

41	1.00000	5.54837	-18.69400	0.000000625	845.9514339	24.0001518	0.0000150	-0.0000150
42	1.00000	4.49933	-18.38501	0.000001250	1688.2814444	24.0001524	0.0000300	-0.0000300
43	1.00000	10.02307	-16.72687	0.000001875	0.8613035	24.0001529	0.0000450	-0.0000450
44	1.00000	10.86731	-16.19110	0.000002500	1.2919583	24.0001534	0.0000600	-0.0000600
45	1.00000	13.86798	-13.70873	0.000003125	1.7261111	24.0001540	0.0000750	-0.0000750
46	1.00000	14.55245	-12.97984	0.000003750	2.1532639	24.0001545	0.0000900	-0.0000900
47	1.00000	16.84151	-9.82921	0.000004375	2.5839168	24.0001551	0.0001050	-0.0001050
48	1.00000	17.32321	-8.95300	0.000005000	3.0145696	24.0001551	0.0001200	-0.0001200
49	1.00000	18.75683	-5.33210	0.000005625	4.193.5429353	24.0001540	0.0001350	-0.0001350
50	1.00000	19.00549	-4.36362	0.000006250	5.021.3872521	24.0001545	0.0001500	-0.0001500

NOTE: The positions of the above rebars were computed by LPIE
 Minimum spacing between any two bars not equal to zero = -0.0001096 inches between Bars 1 and 2
 Spacing to aggregate size ratio = -0.0002922

Concrete Properties:

Compressive Strength of Concrete = 4500.00000 psi
 Modulus of Elasticity of Concrete = 3823876. psi
 Modulus of Rupture of Concrete = -503.11528 psi
 Compression Strain at Peak Stress = 0.00200
 Tensile Strain at Fracture of Concrete = -0.0001152
 Maximum Coarse Aggregate Size = 0.37500 in

Number of Axial Thrust Force Values Determined from Pile-head Loadings = 1

Number	Axial Thrust Force
1	0.000

Definitions of Run Messages and Notes:

C = concrete in section has cracked in tension.
 Y = stress in reinforcing steel has reached yield stress.
 T = ACI 318-08 criteria for tension-controlled section met, tensile strain in reinforcement exceeds 0.005 while simultaneously compressive strain in concrete more than 0.005. See ACI 318-08, Section 10.3.4.
 Z = depth of tensile zone in concrete section is less than 10 percent of section depth.

Bending Stiffness (EI) = Computed Bending Moment / Curvature.
 Position of neutral axis is measured from edge of compression side of pile.
 Compressive stresses and strains are positive in sign.
 Tensile stresses and strains are negative in sign.

Axial Thrust Force = 0.000 kips			
Bending Curvature rad/in.	Bending Moment Stiffness In-Kip	Depth to N Axis in	Max Tens Strain in/in
1.0655338	-18.2030577	C	1.0000169
1.0369310	-16.9943451	C	1.0000175
1.0718081	-17.5988943	C	1.0000181
0.9657234	17.3529272	C	0.9657234
0.6602819	603.9740373	C	0.6602819
0.6000150	678.9710083	C	0.6000150
0.8959132	41.5753048	C	0.8959132
0.0000115	654.7048985	C	0.0000115
0.9213934	115.1803901	C	0.9213934
0.0000163	6802.3956702	C	0.0000163
1.0000169	7061.5545606	C	1.0000169
1.0001026	-16.3900109	C	1.0001026
1.0369310	7330.5250670	C	1.0369310
1.0718081	7579.3065976	C	1.0718081
0.9657234	7837.8985565	C	0.9657234
0.6602819	7837.8985565	C	0.6602819
0.6000150	-18.2030577	C	0.6000150

Pier 11aff. 1p70

0.000000625	845.9514339	24.0001518	0.0000150	-0.0000150
0.000001250	1688.2814444	24.0001524	0.0000300	-0.0000300
0.000001875	0.8613035	24.0001529	0.0000450	-0.0000450
0.000002500	1.2919583	24.0001534	0.0000600	-0.0000600
0.000003125	1.7261111	24.0001540	0.0000750	-0.0000750
0.000003750	2.1532639	24.0001545	0.0000900	-0.0000900
0.000004375	2.5839168	24.0001551	0.0001050	-0.0001050
0.000005000	3.0145696	24.0001551	0.0001200	-0.0001200
0.000005625	4.193.5429353	24.0001540	0.0001350	-0.0001350
0.000006250	5.021.3872521	24.0001545	0.0001500	-0.0001500
0.000006875	5.845.6101456	24.0001551	0.0001650	-0.0001650
0.000007500	6.670.0004375	24.0001551	0.0001800	-0.0001800
0.000008125	7.4937.87876	24.0001551	0.0001950	-0.0001950
0.000008750	8.368.0000922	24.0001540	0.0002100	-0.0002100
0.000009375	9.242.0000092	24.0001545	0.0002250	-0.0002250
0.000010000	10.116.0000100	24.0001551	0.0002400	-0.0002400
0.000010625	11.000.0000106	24.0001551	0.0002550	-0.0002550
0.000011250	11.884.0000112	24.0001551	0.0002700	-0.0002700
0.000011875	12.768.0000118	24.0001551	0.0002850	-0.0002850
0.000012500	13.652.0000125	24.0001551	0.0003000	-0.0003000
0.000013125	14.536.0000131	24.0001551	0.0003150	-0.0003150
0.000013750	15.420.0000137	24.0001551	0.0003300	-0.0003300
0.000014375	16.304.0000143	24.0001551	0.0003450	-0.0003450
0.000015000	17.188.0000150	24.0001551	0.0003600	-0.0003600
0.000015625	18.072.0000156	24.0001551	0.0003750	-0.0003750
0.000016250	18.956.0000162	24.0001551	0.0003900	-0.0003900
0.000016875	19.840.0000168	24.0001551	0.0004050	-0.0004050
0.000017500	20.724.0000175	24.0001551	0.0004200	-0.0004200
0.000018125	21.608.0000181	24.0001551	0.0004350	-0.0004350
0.000018750	22.492.0000187	24.0001551	0.0004500	-0.0004500
0.000019375	23.376.0000193	24.0001551	0.0004650	-0.0004650
0.000020000	24.260.0000200	24.0001551	0.0004800	-0.0004800
0.000020625	25.144.0000206	24.0001551	0.0004950	-0.0004950
0.000021250	26.028.0000212	24.0001551	0.0005100	-0.0005100
0.000021875	26.912.0000218	24.0001551	0.0005250	-0.0005250
0.000022500	27.796.0000225	24.0001551	0.0005400	-0.0005400
0.000023125	28.680.0000231	24.0001551	0.0005550	-0.0005550
0.000023750	29.564.0000237	24.0001551	0.0005700	-0.0005700
0.000024375	30.448.0000243	24.0001551	0.0005850	-0.0005850
0.000025000	31.332.0000250	24.0001551	0.0006000	-0.0006000
0.000025625	32.216.0000256	24.0001551	0.0006150	-0.0006150
0.000026250	33.100.0000262	24.0001551	0.0006300	-0.0006300
0.000026875	33.984.0000268	24.0001551	0.0006450	-0.0006450
0.000027500	34.868.0000275	24.0001551	0.0006600	-0.0006600
0.000028125	35.752.0000281	24.0001551	0.0006750	-0.0006750
0.000028750	36.636.0000287	24.0001551	0.0006900	-0.0006900
0.000029375	37.520.0000293	24.0001551	0.0007050	-0.0007050
0.000030000	38.404.0000300	24.0001551	0.0007200	-0.0007200
0.000030625	39.288.0000306	24.0001551	0.0007350	-0.0007350
0.000031250	40.172.0000312	24.0001551	0.0007500	-0.0007500
0.000031875	41.056.0000318	24.0001551	0.0007650	-0.0007650
0.000032500	41.940.0000325	24.0001551	0.0007800	-0.0007800
0.000033125	42.824.0000331	24.0001551	0.0007950	-0.0007950
0.000033750	43.708.0000337	24.0001551	0.0008100	-0.0008100
0.000034375	44.592.0000343	24.0001551	0.0008250	-0.0008250
0.000035000	45.476.0000350	24.0001551	0.0008400	-0.0008400
0.000035625	46.360.0000356	24.0001551	0.0008550	-0.0008550
0.000036250	47.244.0000362	24.0001551	0.0008700	-0.0008700
0.000036875	48.128.0000368	24.0001551	0.0008850	-0.0008850
0.000037500	49.012.0000375	24.0001551	0.0009000	-0.0009000
0.000038125	49.896.0000381	24.0001551	0.0009150	-0.0009150
0.000038750	50.780.0000387	24.0001551	0.0009300	-0.0009300
0.000039375	51.664.0000393	24.0001551	0.0009450	-0.0009450
0.000040000	52.548.0000400	24.0001551	0.0009600	-0.0009600
0.000040625	53.432.0000406	24.0001551	0.0009750	-0.0009750
0.000041250	54.316.0000412	24.0001551	0.0009900	-0.0009900
0.000041875	55.200.0000418	24.0001551	0.0010050	-0.0010050
0.000042500	56.084.0000425	24.0001551	0.0010200	-0.0010200
0.000043125	56.968.0000431	24.0001551	0.0010350	-0.0010350
0.000043750	57.852.0000437	24.0001551	0.0010500	-0.0010500
0.000044375	58.736.0000443	24.0001551	0.0010650	-0.0010650
0.000045000	59.620.0000450	24.0001551	0.0010800	-0.0010800
0.000045625	60.504.0000456	24.0001551	0.0010950	-0.0010950
0.000046250	61.388.0000462	24.0001551	0.0011100	-0.0011100
0.000046875	62.272.0000468	24.0001551	0.0011250	-0.0011250
0.000047500	63.156.0000475	24.0001551	0.0011400	-0.0011400
0.000048125	64.040.0000481	24.0001551	0.0011550	-0.0011550
0.000048750	64.924.0000487	24.0001551	0.0011700	-0.0011700
0.000049375	65.808.0000493	24.0001551	0.0011850	-0.0011850
0.000050000	66.692.0000500	24.0001551	0.0012000	-0.0012000
0.000050625	67.576.0000506	24.0001551	0.0012150	-0.0012150
0.000051250	68.460.0000512	24.0001551	0.0012300	-0.0012300
0.000051875	69.344.0000518	24.0001551	0.0012450	-0.0012450
0.000052500	70.228.0000525	24.0001551	0.0012600	-0.0012600
0.000053125	71.112.0000531	24.0001551	0.0012750	-0.0012750
0.000053750	72.000.0000537	24.0001551	0.0012900	-0.0012900
0.000054375	72.884.0000543	24.0001551	0.0013050	-0.0013050
0.000055000	73.768.0000550	24.0001551	0.0013200	-0.0013200
0.000055625	74.652.0000556	24.0001551	0.0013350	-0.0013350
0.000056250	75.536.0000562	24.0001551	0.0013500	-0.0013500
0.000056875	76.420.0000568	24.0001551	0.0013650	-0.0013650
0.000057500	77.304.0000575	24.0001551	0.0013800	-0.0013800
0.000058125	78.188.0000581	24.0001551	0.0013950	-0.0013950
0.000058750	79.072.0000587	24.0001551	0.0014100	-0.0014100
0.000059375	79.956.0000593	24.0001551	0.0014250	-0.0014250
0.000060000	80.840.0000600	24.0001551	0.0014400	-0.0014400
0.000060625	81.724.0000606	24.0001551	0.0014550	-0.0014550
0.000061250	82.608.0000612	24.0001551	0.0014700	-0.0014700
0.000061875	83.492.0000618	24.0001551	0.0014850	-0.0014850
0.000062500	84.376.0000625	24.0001551	0.0015000	-0.0015000

				Pier 11aff. 1p7o					Pier 11aff. 1p7o
0.0000194	8096.3003444								
1.141076	-18.8070346	417873566.	14.2880807	0.0002768	-0.0006532	2.7739299	-51.1240649	409065400.	14.5875072
0.0000200	8354.5113583	417725568.	14.2930611	0.0002859	-0.0006741	2.2243.	22243.	408729291.	14.5990567
1.1755294	-19.4108245	417577260.	14.2980536	0.0002949	-0.0006951	2.8252088	-52.3088745	408391538.	14.6106719
0.0000206	8612.5309914	417428642.	14.3030584	0.0003039	-0.0007161	2.8758017	-53.4927466	408052124.	14.6223538
1.2097988	-20.0144267	417279711.	14.3080753	0.0003130	-0.0007370	2.9257055	-54.6756728	407711031.	14.6341029
0.0000213	8870.3586334	417130466.	14.3131046	0.0003220	-0.0007580	2.9749169	-55.8576448	407368552.	14.6457265
1.2439155	-21.2210647	416980906.	14.3181462	0.0003311	-0.0007789	3.0234323	-57.0386538	407024713.	14.6572221
1.2778793	9385.4354826	416831029.	14.3232002	0.0003402	-0.0007998	3.0712187	-58.2190319	406679201.	14.6687831
1.3116898	-21.8240993	416680834.	14.3282668	0.0003493	-0.0008207	3.1182718	-59.3987969	406331998.	14.6804101
1.3433467	9642.6834500	416379475.	14.3384375	0.0003674	-0.0008626	3.1646176	-60.0000000	405983085.	14.6921039
1.3788497	-22.4276943	416076834.	14.3486590	0.0003856	-0.0009044	3.2102527	-60.0000000	405632443.	14.7038654
1.3788497	9899.7369459	415772890.	14.3589318	0.0004038	-0.0009462	3.2551736	-60.0000000	405280053.	14.7156953
0.0000244	-23.0295958	415467630.	14.3692563	0.0004221	-0.0009879	3.2993766	-60.0000000	404925896.	14.7275946
1.4121986	-23.6320564	415161043.	14.3796331	0.0004404	-0.0010296	3.3428584	-60.0000000	404569952.	14.7395639
0.0000256	10670.	414853116.	14.4005458	0.0004587	-0.0010713	3.3856151	-60.0000000	404091673.	14.7500835
1.4784325	-24.8363989	414543834.	14.4110828	0.0004954	-0.0011130	3.4276432	-60.0000000	403072266.	14.7537205
0.0000269	11182.	414233186.	14.4216743	0.0005138	-0.0011962	3.4687035	-60.0000000	401455043.	14.7495436
1.5440460	-26.0399641	413921159.	14.4323209	0.0005322	-0.0012378	3.5079550	-60.0000000	392246336.	14.6948027
0.0000281	11694.	413607737.	14.44323209	0.0005506	-0.0012794	3.5452601	-60.0000000	381149774.	14.6090319
1.6090366	-27.2427466	413292908.	14.4430232	0.0005506	-0.0012794	3.6813494	-60.0000000	369362560.	14.5055975
0.0000294	12204.	412976658.	14.4537818	0.0005691	-0.0013209	3.8013803	-60.0000000	357505362.	14.3951856
1.6734018	-28.4447402	412658972.	14.4645973	0.0005876	-0.0013624	3.9079319	-60.0000000	345931693.	14.2834974
0.0000306	12714.	412339835.	14.4754703	0.0006062	-0.0014038	4.0031450	-60.0000000	334703122.	14.1715893
1.7311390	-29.6459388	412019235.	14.4864015	0.0006247	-0.0014453	4.0883438	-60.0000000	323940666.	13.9461294
0.0000319	13223.	411697154.	14.4973914	0.0006433	-0.0014867	4.1641357	-60.0000000	313627073.	13.8392296
1.8002456	-30.8463362	411373379.	14.5084408	0.0006619	-0.0015281	4.2307884	-60.0000000	303860741.	13.7351344
0.0000331	13732.	411048519.	14.5195502	0.0006806	-0.0015694	4.2891684	-60.0000000	294530941.	13.6338565
1.9245567	-32.2447024	410721909.	14.5307205	0.0006993	-0.0016107	4.3399744	-60.0000000	285688006.	13.5348499
1.9857559	14746.	410393756.	14.5419521	0.0007180	-0.0016520	4.3832660	-60.0000000	277303670.	13.4348499
2.0463138	15252.	410064046.	14.5532459	0.0007368	-0.0016932	4.4193369	-60.0000000	269310170.	13.4391679
2.1062279	16261.	409732761.	14.5646025	0.0007555	-0.0017345	4.4484203	-60.0000000	261702218.	13.3473027
2.1654952	-38.0315387	409399885.	14.5760227	0.0007744	-0.0017756	4.4708379	-60.0000000		
2.2241131	17267.					4.4868079	-60.0000000		
2.2820786	-39.2261471								
2.3938890	17768.								
2.3960413	-41.6127951								
2.4520326	18269.								
2.5073600	-42.8048205								
0.0000481	18769.								
2.3620203	-43.9959704								
2.6160105	19268.								
2.6695276	-44.1862362								
0.0000506	19766.								
2.7219683	-46.3756131								
0.0000531	20263.								
	-47.5640922								
	20759.								
	-48.7516657								
	21253.								
	-49.9383259								
	21749.								

Pier 11aff.1p70

or maximum developed moment if pile fails at smaller strains.

Load No.	Axial Thrust kips	Nominal Mom. in-kip	Max. Comp. Strain
1	0.000	40395.232	0.00300000

Note note that the values of moment capacity in the table above are not factored by a strength reduction factor (phi-factor).
 In ACI 318-08, the value of the strength reduction factor depends on whether the transverse reinforcing steel bars are tied hoops (0.65) or spirals (0.70).
 The above values should be multiplied by the appropriate strength reduction factor to compute ultimate moment capacity according to ACI 318-08, section 9.3.2.2 or the value required by the design standard being followed.

The following table presents factored moment capacities and corresponding bending stiffnesses computed for common resistance factor values used for reinforced concrete sections.

Axial Load No.	Resistance Factor at Ult. Mom. Cap. for Moment	Bending Stiffness Moment kip-in ²	Nominal Moment Capacity in-kip	Ultimate (Factored) Axial Thrust kips	Ultimate Moment
1	0.65	406260579.288	40395.232	0.000	
1	0.70	404789053.314	40395.232	0.000	
1	0.75	398293409.577	40395.232	0.000	

Pile Section No. 2:

Dimensions and Properties of Drilled shaft (Bored pile) with Permanent Casing:

Length of Section	=	104.00000 ft
Outer Diameter of Casing	=	49.00000 in
Concrete Cover Thickness Inside Casing	=	4.50000 in
Casing Wall Thickness	=	0.50000 in
Moment of Inertia of Steel Casing	=	22403. in ⁴
Yield Stress of Casing	=	36000. psi
Elastic Modulus of Casing	=	290000000. psi
Number of Reinforcing Bars	=	30 bars
Area of Single Reinforcing Bar	=	0.79000 sq. in.
Edge-to-Edge Bar Spacing	=	2.59000 in
Maximum Concrete Aggregate Size	=	0.37500 in
Ratio of Bar Spacing to Aggregate Size	=	0.60000 in
Offset of Center of Rebar Cage from Center of Pile	=	6.00000. psi
Yield Stress of Reinforcing Bars	=	2900000. psi
Modulus of Elasticity of Reinforcing Bars	=	188574000. psi
Gross Area of Pile	=	1970.01737 sq. in.
Area of Concrete	=	76.18362 sq. in.
Cross-sectional Area of Steel Casing	=	

Pier 11aff.1p70

Summary of Results for Nominal (Unfactored) Moment Capacity for Section 1

254539263.	13.2620016	0.0019810	-0.0051890
38022.	13.1787297	0.0020345	-0.0053755
-60.0000000	13.0959086	0.0020872	-0.0055628
4.4965333	13.0163967	0.0021396	-0.0057504
0.0001544	12.9406891	0.0021918	-0.0059382
4.4998779	12.8709600	0.0022444	-0.0061256
0.0001594	12.8035616	0.0022966	-0.0063134
4.4991008	12.7393054	0.0023488	-0.0065012
0.0001644	12.6749886	0.0024003	-0.0066897
4.4961694	12.6125107	0.0024516	-0.0068784
0.0001694	12.5515567	0.0025025	-0.0070675
4.4983350	12.4946057	0.0025536	-0.0072564
0.0001744	12.4414757	0.0026049	-0.0074451
4.4996772	12.3892958	0.0026560	-0.0076340
0.0001844	12.3398762	0.0027071	-0.0078229
4.4990003	12.2917083	0.0027580	-0.0080120
0.0001944	12.2454771	0.0028088	-0.0082012
4.4956386	12.1978486	0.0028589	-0.0083911
0.0001994	12.1516759	0.0029088	-0.0085812
4.4933210	12.1063441	0.0029585	-0.0087715
0.0002044	12.0632455	0.0030083	-0.0089617
4.4949946	12.0224625	0.0030582	-0.0091518
0.0002094	11.9837750	0.0031083	-0.0093417
4.4972998	11.9459332	0.0031582	-0.0095318
0.0002144	11.9101831	0.0032083	-0.0097217
4.4986503	11.8759269	0.0032585	-0.0099115
0.0002244	11.8448054.	0.0033083	-0.01010495
4.4945873	11.81224625	0.0033582	-0.0102988
0.0002294	11.7837750	0.0034083	-0.0104927
4.497195	11.7516759	0.0034582	-0.01068715
0.0002344	11.7201831	0.0035082	-0.0108815
4.4982677	11.68868185.	0.0035582	-0.0110760
0.0002394	11.6584525.	0.0036083	-0.0112705
4.4998905	11.62828002.	0.0036582	-0.0114650
0.0002444	11.5984525.	0.0037083	-0.0116600
4.4926204	11.5693441	0.0037582	-0.0118550
0.0002494	11.54028002.	0.0038083	-0.0120500
4.4936508	11.511868.	0.0038582	-0.0122450
0.0002544	11.4840647.	0.0039083	-0.0124400
4.4974059	11.4579269	0.0039582	-0.0126350
0.0002594	11.43201338.	0.0040083	-0.0128300
4.4995166	11.406090.	0.0040582	-0.0130250
0.0002644	11.379923.	0.0041083	-0.0132200
4.495184	11.34448054.	0.0041582	-0.0134150
0.0002694	11.318448054.	0.0042083	-0.0136100
4.4903477	11.2874980.	0.0042582	-0.0138050
0.0002744	11.2574980.	0.0043083	-0.0140000
4.4867102	11.2274980.	0.0043582	-0.0141950

Moment values interpolated at maximum compressive strain = 0.003

Pier 11aff.1p70
 Area of All Steel (Casing and Bars) = 115.68362 sq. in.
 Area Ratio of All Steel to Gross Area of Pile = 6.13 percent

Pier 11aff.1p70
 Axial Structural Capacities:

11883.080 kips
 Nom. Axial Structural Capacity = 0.85 Fc Ac + FY As = 11883.080 kips
 Tensile Load for Cracking of Concrete = -1165.721 kips
 Nominal Axial Tensile Capacity = -5112.610 kips

Pier 11aff.1p70
 48 1.00000 16.88491 -8.71205
 49 0.79000 18.27238 -5.20771
 50 1.00000 18.52104 -4.23924

NOTE: The positions of the above rebars were computed by LPIIe
 Minimum spacing between any two bars not equal to zero = -0.0001154 inches between
 Bars 1 and 2
 Spacing to aggregate size ratio = -0.0003078

Concrete Properties:
 Compressive Strength of Concrete = 4500.00000 psi
 Modulus of Elasticity of Concrete = 3823676. psi
 Modulus of Rupture of Concrete = -503.11528 psi
 Compression Strain at Peak Stress = 0.00200
 Tensile Strain at Fracture of Concrete = -0.0001152
 Maximum Coarse Aggregate Size = 0.37500 in

Number of Axial Thrust Force Values Determined from Pile-head Loadings = 1

Number Axial Thrust Force
 kips
 1 0.000

Definitions of Run Messages and Notes:

C = concrete in section has cracked in tension.
 Y = stress in reinforcing steel has reached yield stress.
 T = ACI 318-08 criteria for tension-controlled section met, tensile strain in
 reinforcement exceeds 0.005 while simultaneously compressive strain in
 concrete more than 0.003. See ACI 318-08, Section 10.3.4.
 Z = depth of tensile zone in concrete section is less than 10 percent of section
 depth.
 Bending Stiffness (EI) = Computed Bending Moment / Curvature.
 Position of neutral axis is measured from edge of compression side of pile.
 Compressive stresses and strains are positive in sign.
 Tensile stresses and strains are negative in sign.

Axial Thrust Force = 0.000 kips

Bending Curvature rad/in.	Bending Moment in-kip	Max Steel Stress ksi	Bending Stress in-ksi	Max Casing Stress ksi	Depth to Run N Axis in	Max Comp Strain in/in	Max Tens Strain in/in
0.000000625	1246.1877906	1993900465	24.5001275	1993900465	24.5001275	0.0000153	-0.0000153
0.0679356	0.4396324	0.4396324	0.4396324	0.4396324	0.4396324	0.0000306	-0.0000306
0.00001250	2488.7459054	1990986724	24.5001279	1990986724	24.5001279	0.0000306	-0.0000306
0.13335544	0.8792484	0.8792484	0.8792484	0.8792484	0.8792484	0.0000306	-0.0000306

Reinforcing Bar Dimensions and Positions Used in Computations:

Bar Number	Bar Diam. inches	Bar Area sq. in.	X inches	Y inches
1	1.00000	0.79000	18.99342	-0.49994
2	1.00000	0.79000	18.99342	0.49994
3	1.00000	0.79000	18.52104	4.23924
4	1.00000	0.79000	18.27238	5.20771
5	1.00000	0.79000	16.88491	8.71205
6	1.00000	0.79000	16.40321	9.58825
7	1.00000	0.79000	14.18784	12.63745
8	1.00000	0.79000	13.50337	13.36633
9	1.00000	0.79000	10.59930	15.76879
10	1.00000	0.79000	9.75507	16.30456
11	1.00000	0.79000	6.34476	17.90933
12	1.00000	0.79000	5.39382	18.21831
13	1.00000	0.79000	1.69156	18.92455
14	1.00000	0.79000	0.69365	18.98733
15	1.00000	0.79000	-3.06793	18.75068
16	1.00000	0.79000	-4.05010	18.56332
17	1.00000	0.79000	-7.63464	17.39863
18	1.00000	0.79000	-8.53937	16.97290
19	1.00000	0.79000	-11.72165	14.95336
20	1.00000	0.79000	-12.49207	14.31601
21	1.00000	0.79000	-15.07214	11.56851
22	1.00000	0.79000	-15.65986	10.75959
23	1.00000	0.79000	-17.47560	7.45678
24	1.00000	0.79000	-17.84388	6.52711
25	1.00000	0.79000	-18.78099	2.87651
26	1.00000	0.79000	-18.90631	1.88451
27	1.00000	0.79000	-18.90631	-1.88451
28	1.00000	0.79000	-18.78099	-2.87651
29	1.00000	0.79000	-17.84388	-6.52711
30	1.00000	0.79000	-17.47560	-7.45678
31	1.00000	0.79000	-15.65986	-10.75959
32	1.00000	0.79000	-15.07214	-11.56851
33	1.00000	0.79000	-12.49207	-14.31601
34	1.00000	0.79000	-11.72165	-14.95336
35	1.00000	0.79000	-6.53937	-16.97290
36	1.00000	0.79000	-7.63464	-17.39863
37	1.00000	0.79000	-4.05010	-18.56332
38	1.00000	0.79000	-3.06793	-18.75068
39	1.00000	0.79000	0.69365	-18.98733
40	1.00000	0.79000	1.69156	-18.92455
41	1.00000	0.79000	5.39382	-18.21831
42	1.00000	0.79000	9.75507	-16.30456
43	1.00000	0.79000	13.50337	-15.76879
44	1.00000	0.79000	17.90933	-13.36633
45	1.00000	0.79000	18.21831	-12.63745
46	1.00000	0.79000	18.52104	-11.56851
47	1.00000	0.79000	18.99342	-9.58825

0.00001875	3727.6743445	1988092984.	24.5001283	0.0000459	-0.0000459	1.5883554	-18.5445778	18.6682387	0.0004084	-0.0006655
0.202256	1.3188726	1.3188726				0.0000219	1176301169.			
0.00002500	4962.9710777	1985189243.	24.5001286	0.0000613	-0.0000612	1.6303186	-19.0862892	18.6741116	0.0004202	-0.0006823
0.2686421	1.7584968	1.7584968				0.0000225	1175869930.			
0.00003125	6194.441952	1982285502.	24.5001290	0.0000766	-0.0000766	1.6720045	-19.6277796	18.6799978	0.0004320	-0.0007012
0.3345108	2.1981210	2.1981210				0.0000231	1175437855.			
0.00003750	7422.6816068	1979381762.	24.5001294	0.0000919	-0.0000919	1.7134124	-20.1690483	18.6858973	0.0004438	-0.0007200
0.3998628	2.6377453	2.6377453				0.0000238	1175004942.			
0.00004375	8647.0913427	1976478021.	24.5001298	0.0001072	-0.0001072	1.7545419	-20.7100945	18.6918101	0.0004556	-0.0007388
0.00005000	8647.0913427	1976478021.	24.5001298	0.0000926	-0.0000926	0.0000244	1174571186.			
0.000005625	8647.0913427	1976478021.	24.5001298	0.0000926	-0.0000926	1.7953924	-21.2509174	18.7036758	0.0004793	-0.0007763
0.4505457	-4.3848797	-4.3848797				0.0000256	1173701123.			
0.000006250	8647.0913427	1976478021.	24.5001298	0.0001042	-0.0001042	1.8762546	-22.3318905	18.7155957	0.0005030	-0.0008139
0.000006875	8647.0913427	1976478021.	24.5001298	0.0001158	-0.0001158	0.0000269	1172827657.			
0.000007500	8894.972711	197599948	18.5255374	0.0001390	-0.0001390	1.9559948	-23.4119610	18.7275700	0.0005267	-0.0008514
0.5477623	-6.0258903	-6.0258903				2.0346089	-24.4911229	18.7395995	0.0005505	-0.0008889
0.5959719	-6.5724864	-6.5724864				2.1120926	-25.5693697	18.7516845	0.0005743	-0.0009264
0.00008125	9632.8701085	1185584013.	18.5422569	0.0001507	-0.0001507	2.1884416	-26.6466950	18.7638256	0.0005981	-0.0009638
0.6439151	-7.1188776	-7.1188776				2.2636516	-27.7230922	18.7760234	0.0006220	-0.0010012
0.000008750	10370.	1185170297.	18.5478538	0.0001623	-0.0001623	2.3377183	-28.7985549	18.7882783	0.0006458	-0.0010385
0.000009375	11107.	1184755819.	18.5534628	0.0001739	-0.0001739	2.4106371	-29.8730762	18.8005910	0.0006698	-0.0010759
0.0000100	11843.	1184340574.	18.5590837	0.0001856	-0.0001856	2.4824038	-30.9466494	18.8129619	0.0006937	-0.0011131
0.0000106	12579.	118568157	18.5647167	0.0001973	-0.0001973	2.5530137	-32.0192676	18.8253917	0.0007177	-0.0011504
0.8330144	-9.3023810	-9.3023810				2.6242464	-33.0902939	18.8378808	0.0007417	-0.0011876
0.0000113	13314.	1183507775.	18.5703619	0.0002089	-0.0002089	2.6907451	-34.1616112	18.8504300	0.0007658	-0.0012248
0.7861415	-8.7568157	-8.7568157				2.7578573	-35.2313223	18.8589255	0.0007897	-0.0012622
0.0000125	14049.	1182527533.	18.5816888	0.0002206	-0.0002206	2.8233213	-36.3050459	18.8708550	0.0008128	-0.0013003
0.9259536	-9.847382	-9.847382				2.8832227	-37.4036257	18.8740541	0.0008353	-0.0013391
0.9720190	-10.3928865	-10.3928865				2.9444397	-38.5186780	18.8828946	0.0008573	-0.0013783
0.0000131	14783.	1182671874.	18.5873707	0.0002440	-0.0002440	3.0014606	-39.6463092	18.8946464	0.0008791	-0.0014178
1.0178143	15517.	1182252753.	18.5930649	0.0002557	-0.0002557	3.0586932	-40.7819777	18.9090000	0.0009006	-0.0014575
1.0633390	16250.	118182847.	18.5987715	0.0002674	-0.0002674	3.1102262	-41.9213324	18.9233249	0.0009219	-0.0014974
1.085926	16983.	118142154.	18.6044906	0.0002791	-0.0002791	3.1622450	-43.0713692	18.9326300	0.0009431	-0.0015376
1.4535747	-13.1154716	-13.1154716				3.2127711	-44.2283680	18.9460000	0.0009640	-0.0015779
1.4982848	-13.6593524	-13.6593524				3.2600019	-45.3826269	18.9592000	0.0009848	-0.0016183
1.2427224	-14.2030196	-14.2030196				3.3088531	-46.5532591	18.9723199	0.0010055	-0.0016589
1.2868870	-14.7464723	-14.7464723				3.3564715	-47.7220884	18.9812920	0.0010260	-0.0016996
0.0000175	20638.	119296752.	18.6217231	0.0003142	-0.0003142	3.4018904	-48.8938485	18.9900000	0.0010464	-0.0017404
0.0000181	21367.	119296752.	18.6274926	0.0003260	-0.0003260	3.4461531	-50.0687283	18.9988175		
1.3743934	-15.8327318	-15.8327318								
0.0000188	1178444960.	1178444960.	18.6332748	0.0003377	-0.0003377					
1.4177383	-16.3755370	-16.3755370								
0.0000194	22824.	1178017845.	18.6390698	0.0003495	-0.0003495					
1.4680862	-16.9181250	-16.9181250								
0.0000200	23532.	1177589311.	18.6448776	0.0003612	-0.0003612					
1.5035986	-17.4604949	-17.4604949								
0.0000206	24279.	1177604349.	18.6506984	0.0003730	-0.0003730					
1.9461132	-18.0026461	-18.0026461								
0.0000213	25006.	11767315177.	18.6565321	0.0003848	-0.0003848					
			18.6623788	0.0003966	-0.0003966					

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Load No.	Pier 11a		Pier 11a		Pier 11a		Pier 11a		Pier 11a		Pier 11a		Pier 11a	
	11a		11a		11a		11a		11a		11a		11a	
0.0000581	60910.	1047913654.	18.3524698	0.0010667	-0.0017814	60.0000000	36.0000000	15.9198154	0.0026964	-0.0036030				
3.4892404	-51.2472648	-36.0000000	CY	0.0011694	-0.0018225	60.0000000	501939766.	CY	0.0026964	-0.0036030				
0.0000594	61682.	1038848112.	18.3060172	0.0010869	-0.0018225	60.0000000	36.0000000	CY	0.0026964	-0.0036030				
3.5311716	-52.4293420	-36.0000000	CY	0.0011744	-0.0018636	60.0000000	85250.	CY	0.0026964	-0.0036030				
0.0000606	62440.	1029943371.	18.2600628	0.0011070	-0.0018636	60.0000000	36.0000000	CY	0.0026964	-0.0036030				
3.5720391	-53.6130913	-36.0000000	CY	0.0011794	-0.0019048	60.0000000	85470.	CY	0.0026964	-0.0036030				
0.0000619	63187.	1021207548.	18.2146955	0.0011270	-0.0019048	60.0000000	36.0000000	CY	0.0026964	-0.0036030				
3.6118689	-54.8007587	-36.0000000	CY	0.0011844	-0.0019461	60.0000000	464662001.	CY	0.0026964	-0.0036030				
0.0000631	63923.	1012646783.	18.1699929	0.0011470	-0.0019461	60.0000000	36.0000000	CY	0.0026964	-0.0036030				
3.6506854	-55.9896785	-36.0000000	CY	0.0011894	-0.0019875	60.0000000	453401426.	CY	0.0026964	-0.0036030				
0.0000644	64650.	1004265562.	18.1260229	0.0011669	-0.0019875	60.0000000	36.0000000	CY	0.0026964	-0.0036030				
3.6885113	-57.1804715	-36.0000000	CY	0.0011944	-0.0020289	60.0000000	442646666.	CY	0.0026964	-0.0036030				
0.0000656	65367.	996065543.	18.0828308	0.0011867	-0.0020289	60.0000000	36.0000000	CY	0.0026964	-0.0036030				
3.7253656	-58.3729718	-36.0000000	CY	0.0012064	-0.0020704	60.0000000	432367621.	CY	0.0026964	-0.0036030				
0.0000669	66074.	988019719.	18.0401664	0.0012064	-0.0020704	60.0000000	36.0000000	CY	0.0026964	-0.0036030				
3.7612310	-59.5675802	-36.0000000	CY	0.0012261	-0.0021120	60.0000000	422528550.	CY	0.0026964	-0.0036030				
0.0000681	66773.	980156974.	17.9983515	0.0012458	-0.0021536	60.0000000	86203.	CY	0.0026964	-0.0036030				
3.7961596	-60.0000000	-36.0000000	CY	0.0012458	-0.0021536	60.0000000	413145390.	CY	0.0026964	-0.0036030				
0.0000694	67466.	972477926.	17.9574311	0.0012656	-0.0021951	60.0000000	86628.	CY	0.0026964	-0.0036030				
3.8301685	-60.0000000	-36.0000000	CY	0.0012855	-0.0022364	60.0000000	404097559.	CY	0.0026964	-0.0036030				
0.0000706	68142.	964843635.	17.9194255	0.0012855	-0.0022364	60.0000000	36.0000000	CY	0.0026964	-0.0036030				
3.8635106	-60.0000000	-36.0000000	CY	0.0013056	-0.0022775	60.0000000	86741.	CY	0.0026964	-0.0036030				
0.0000719	68792.	957107775.	17.8855537	0.0013056	-0.0022775	60.0000000	36.0000000	CY	0.0026964	-0.0036030				
3.8963346	-60.0000000	-36.0000000	CY	0.0013258	-0.0023186	60.0000000	379011338.	CY	0.0026964	-0.0036030				
0.0000731	69423.	949380920.	17.8542977	0.0013258	-0.0023186	60.0000000	36.0000000	CY	0.0026964	-0.0036030				
3.9284606	-60.0000000	-36.0000000	CY	0.0014075	-0.0024819	60.0000000	371267093.	CY	0.0026964	-0.0036030				
0.0000744	70040.	941712434.	17.8260522	0.0014075	-0.0024819	60.0000000	86936.	CY	0.0026964	-0.0036030				
3.9599353	-60.0000000	-36.0000000	CY	0.0014875	-0.0026469	60.0000000	4097559.	CY	0.0026964	-0.0036030				
0.0000754	72378.	911849904.	17.7921611	0.0014875	-0.0026469	60.0000000	36.0000000	CY	0.0026964	-0.0036030				
4.0700360	-60.0000000	-36.0000000	CY	0.0015647	-0.0028147	60.0000000	87016.	CY	0.0026964	-0.0036030				
4.1795572	-60.0000000	-36.0000000	CY	0.0015647	-0.0028147	60.0000000	36.0000000	CY	0.0026964	-0.0036030				
4.2643087	73780.	887889856.	17.5073060	0.0015647	-0.0028147	60.0000000	36.0000000	CY	0.0026964	-0.0036030				
0.0000844	77018.	816087263.	17.3824668	0.0016405	-0.0029839	60.0000000	87214.	CY	0.0026964	-0.0036030				
4.3347927	-60.0000000	-36.0000000	CY	0.0016405	-0.0029839	60.0000000	36.0000000	CY	0.0026964	-0.0036030				
0.0000944	80774.	85668532.	17.2557305	0.0017148	-0.0031546	60.0000000	345075082.	CY	0.0026964	-0.0036030				
4.3917872	-60.0000000	-36.0000000	CY	0.0017882	-0.0033262	60.0000000	87270.	CY	0.0026964	-0.0036030				
0.0001044	78992.	736814015.	17.1323516	0.0017882	-0.0033262	60.0000000	36.0000000	CY	0.0026964	-0.0036030				
4.4362794	-60.0000000	-36.0000000	CY	0.0018608	-0.0034985	60.0000000	85950.433	CY	0.0026964	-0.0036030				
0.0001094	78603.	729607333.	17.0132920	0.0018608	-0.0034985	60.0000000	0.0000000	CY	0.0026964	-0.0036030				
4.4687739	-60.0000000	-36.0000000	CY	0.0019329	-0.0036715	60.0000000	85950.433	CY	0.0026964	-0.0036030				
0.0001144	80517.	705973353.	16.8993985	0.0019329	-0.0036715	60.0000000	0.0000000	CY	0.0026964	-0.0036030				
4.4992440	-60.0000000	-36.0000000	CY	0.0020040	-0.0038454	60.0000000	85950.433	CY	0.0026964	-0.0036030				
0.0001194	81153.	679836432.	16.7874938	0.0020040	-0.0038454	60.0000000	0.0000000	CY	0.0026964	-0.0036030				
4.4992440	-60.0000000	-36.0000000	CY	0.0020746	-0.0040198	60.0000000	85950.433	CY	0.0026964	-0.0036030				
0.0001244	81729.	671141404.	16.6801722	0.0020746	-0.0040198	60.0000000	0.0000000	CY	0.0026964	-0.0036030				
4.4992440	-60.0000000	-36.0000000	CY	0.0021448	-0.0041946	60.0000000	85950.433	CY	0.0026964	-0.0036030				
0.0001294	82710.	653688352.	16.5782931	0.0021448	-0.0041946	60.0000000	0.0000000	CY	0.0026964	-0.0036030				
4.4992440	-60.0000000	-36.0000000	CY	0.0022149	-0.0043695	60.0000000	85950.433	CY	0.0026964	-0.0036030				
0.0001344	83710.	615540993.	16.4830044	0.0022149	-0.0043695	60.0000000	0.0000000	CY	0.0026964	-0.0036030				
4.4992440	-60.0000000	-36.0000000	CY	0.0022846	-0.0045448	60.0000000	85950.433	CY	0.0026964	-0.0036030				
0.0001394	83139.	596511359.	16.3914553	0.0022846	-0.0045448	60.0000000	0.0000000	CY	0.0026964	-0.0036030				
4.4992440	-60.0000000	-36.0000000	CY	0.0023536	-0.0047208	60.0000000	85950.433	CY	0.0026964	-0.0036030				
0.0001444	83570.	578295131.	16.3016668	0.0023536	-0.0047208	60.0000000	0.0000000	CY	0.0026964	-0.0036030				
4.4992440	-60.0000000	-36.0000000	CY	0.0024224	-0.0048969	60.0000000	85950.433	CY	0.0026964	-0.0036030				
0.0001494	83870.	561472182.	16.2171924	0.0024224	-0.0048969	60.0000000	0.0000000	CY	0.0026964	-0.0036030				
4.4992440	-60.0000000	-36.0000000	CY	0.0024912	-0.0050732	60.0000000	85950.433	CY	0.0026964	-0.0036030				
0.0001544	84197.	545405022.	16.1373405	0.0024912	-0.0050732	60.0000000	0.0000000	CY	0.0026964	-0.0036030				
4.4999984	-60.0000000	-36.0000000	CY	0.0025599	-0.0052495	60.0000000	85950.433	CY	0.0026964	-0.0036030				
0.0001594	84492.	530143855.	16.0618326	0.0025599	-0.0052495	60.0000000	0.0000000	CY	0.0026964	-0.0036030				
4.4992081	-60.0000000	-36.0000000	CY	0.0026282	-0.0054261	60.0000000	85950.433	CY	0.0026964	-0.0036030				
0.0001644	84764.	515674732.	15.9893153	0.0026282	-0.0054261	60.0000000	0.0000000	CY	0.0026964	-0.0036030				

 Summary of Results for Nominal (Unfactored) Moment Capacity for section 2

 Moment values interpolated at maximum compressive strain = 0.003
 or maximum developed moment if pile fails at smaller strains.
 Load No. Axial Thrust Nominal Mom. Cap. Max. Comp. Strain

 I 0.000 kips ----- 85950.433 ----- 0.00300000

 Note note that the values of moment capacity in the table above are not factored by a strength reduction factor (phi-factor).
 In ACI 318-08, the value of the strength reduction factor depends on whether the transverse reinforcing steel bars are tied hoops (0.65) or spirals (0.70). The above values should be multiplied by the appropriate strength reduction factor to compute ultimate moment capacity according to ACI 318-08. Section 9.3.2.2 or the value required by the design standard being followed.
 The following table presents factored moment capacities and corresponding bending stiffnesses computed for common resistance factor values used for

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reinforced concrete sections.				Ultimate (Factored)		Ultimate
Axial Load Capacity	Resistance Factor	Nominal Moment Capacity	Axial Thrust	Moment		
in-kip		kip-in ²	kip	Moment		
55867.779	0.65	1105241617.673	0.000			
60165.302	0.70	1056639830.845	0.000			
64462.825	0.75	1006420922.590	0.000			

Computed Values of Pile Loading and Deflection						
for Lateral Loading for Load Case Number 1						

Pile-head conditions are Displacement and Moment (Loading Type 4)						
Displacement of pile head = 0.50000 inches						
Moment at pile head = 5499600.0 in.-lbs						
Axial load at pile head = 0.0 lbs						

Depth X	Deflect. y	Bending Moment	Shear Force	Slope S	Total Stress	Soil p
feet	inches	in.-lbs	lbs	radians	psi*	lb-in ²
Lat. Load	DistriB.					
lb/inch	lb/inch					
0.000	0.000	5499600.	22344.	-0.002739	0.000	1.337E+12
1.113	0.4638	5797894.	22344.	-0.002683	0.000	1.337E+12
2.225	0.4284	6096188.	22344.	-0.002557	0.000	4.190E+11
3.337	0.3955	6394482.	21791.	-0.002358	0.000	4.188E+11
4.450	0.3654	6678012.	20650.	-0.002149	0.000	4.187E+11
5.562	0.3381	6945837.	19440.	-0.001932	0.000	4.185E+11
6.675	0.3138	7197068.	18165.	-0.001707	0.000	4.184E+11
7.787	0.2926	7430851.	16820.	-0.001567	0.000	1.979E+12
8.900	0.2730	7646158.	15407.	-0.001516	0.000	1.979E+12
10.012	0.2571	7842279.	13940.	-0.001464	0.000	1.978E+12
11.125	0.2439	8018368.	12424.	-0.001410	0.000	1.978E+12
12.237	0.2325	8173950.	10863.	-0.001355	0.000	1.977E+12

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-118.4604	7374.1527	0.000	9263.8001	-0.001300	0.000	1.977E+12
13.350	0.1967	8308419.	7630.7868	-0.001243	0.000	1.977E+12
-121.1731	8222.6590	0.000	5969.8891	-0.001186	0.000	1.977E+12
-123.4731	9170.0733	0.000	4286.8211	-0.001128	0.000	1.977E+12
15.575	0.4635	8512161.	2587.4473	-0.001068	0.000	1.832E+12
-125.3505	10233.	0.000	877.6590	-0.001002	0.000	1.680E+12
16.688	0.1481	8580689.	-836.8740	-0.000937	0.000	1.889E+12
-126.7945	11431.	0.000	-2550.3844	-0.000878	0.000	1.977E+12
-127.7934	12788.	0.000	-4256.6602	-0.000819	0.000	1.977E+12
18.912	0.1196	8649774.	-5949.2121	-0.000762	0.000	1.977E+12
-128.3547	14331.	0.000	-7621.3346	-0.000704	0.000	1.977E+12
20.025	0.1067	8650053.	-9266.0702	-0.000648	0.000	1.977E+12
-128.5042	16085.	0.000	-12301.	-0.000592	0.000	1.977E+12
21.137	0.0945	8627429.	-16451.	-0.000538	0.000	1.978E+12
-128.2015	18102.	0.000	-19944.	-0.000485	0.000	1.979E+12
22.250	0.0832	8581958.	-23010.	-0.000434	0.000	1.979E+12
-127.4203	20440.	0.000	-25912.	-0.000384	0.000	1.980E+12
23.362	0.0727	8513777.	-28564.	-0.000338	0.000	1.981E+12
-126.1455	23174.	0.000	-30881.	-0.000293	0.000	1.982E+12
24.475	0.0629	8423114.	-32681.	-0.000252	0.000	1.983E+12
-124.3597	26400.	0.000	-33851.	-0.000214	0.000	1.984E+12
25.588	0.0539	8310287.	-34433.	-0.000178	0.000	1.985E+12
-122.0426	30250.	0.000	-34480.	-0.000146	0.000	1.986E+12
26.700	0.0456	8175709.	-34047.	-0.000117	0.000	1.987E+12
-332.6686	97428.	0.000	-33193.	-9.075E-05	0.000	1.988E+12
27.812	0.0380	7981843.	-31977.	-6.765E-05	0.000	1.989E+12
-289.0102	101413.	0.000	-30462.	-4.743E-05	0.000	1.990E+12
28.925	0.0312	7736469.	-28705.	-2.995E-05	0.000	1.991E+12
-234.2469	100153.	0.000	-26764.	-1.504E-05	0.000	1.992E+12
30.073	0.0251	7495816.	-24692.	-2.531E-06	0.000	1.992E+12
-225.1673	119736.	0.000	-22538.	7.763E-06	0.000	1.993E+12
31.150	0.0196	7122093.	0.000			
-209.3576	142391.	0.000				
32.232	0.0166	6757490.				
-187.7582	168934.	0.000				
33.315	0.0106	6359425.				
-159.2705	199961.	0.000				
34.487	0.007002	5922974.				
-110.4830	2106510.	0.000				
35.560	0.003903	5486832.				
-64.7207	221349.	0.000				
-22.5623	232042.	0.000				
15.5596	242735.	0.000				
49.3514	253429.	0.000				
78.6459	264127.	0.000				
103.3930	274815.	0.000				
123.6434	285509.	0.000				
139.5363	296202.	0.000				
151.2855	306895.	0.000				
159.1636	317589.	0.000				
163.4901	328282.	0.000				

Pier 11aff.1p7o		Pier 11aff.1p7o	
47.837	-0.006483	1092.595	1.994E+12
164.6189	338975	0.000	0.000
48.950	-0.006220	835619	1.994E+12
162.9250	349669	0.000	0.000
158.7937	-0.005883	607681	1.994E+12
158.7937	360362	0.000	0.000
151.175	-0.005491	408043	1.994E+12
152.6118	371056	0.000	0.000
144.7591	-0.005062	235604	1.994E+12
144.7591	381749	0.000	0.000
135.6010	-0.004613	88965	1.994E+12
135.6010	392442	0.000	0.000
125.4826	-0.004155	-33508	1.994E+12
125.4826	403136	0.000	0.000
114.7244	-0.003701	-133616	1.994E+12
114.7244	413829	0.000	0.000
103.6179	-0.003258	-213278	1.994E+12
103.6179	424522	0.000	0.000
92.4240	-0.002835	-274474	1.994E+12
92.4240	435216	0.000	0.000
81.3712	-0.002436	-319197	1.994E+12
81.3712	445909	0.000	0.000
70.6552	-0.002066	-349418	1.994E+12
70.6552	456602	0.000	0.000
60.4392	-0.001727	-367046	1.994E+12
60.4392	467296	0.000	0.000
50.8545	-0.001420	-373903	1.994E+12
50.8545	477989	0.000	0.000
42.0025	-0.001147	-371697	1.994E+12
42.0025	488682	0.000	0.000
33.9561	-0.000908	-362004	1.994E+12
33.9561	499576	0.000	0.000
26.7620	-0.000700	-346260	1.994E+12
26.7620	510069	0.000	0.000
20.4431	-0.000524	-325747	1.994E+12
20.4431	520762	0.000	0.000
15.0007	-0.000377	-301590	1.994E+12
15.0007	531456	0.000	0.000
10.4172	-0.000257	-274759	1.994E+12
10.4172	542149	0.000	0.000
6.6580	-0.000161	-246072	1.994E+12
6.6580	552842	0.000	0.000
3.6735	-8.1703E-05	-185670	1.994E+12
3.6735	563536	0.000	0.000
18.2524	-7.1261E-05	-151869	1.994E+12
18.2524	574230	0.000	0.000
-7.2891	-3.8687E-06	131889	1.994E+12
-7.2891	585479	0.000	0.000
-17.2450	-7.8245E-05	-119407	1.994E+12
-17.2450	596724	0.000	0.000
-20.9250	-5.0305E-05	-90015	1.994E+12
-20.9250	607969	0.000	0.000
-22.7654	-1.2339E-05	-64360	1.994E+12
-22.7654	619214	0.000	0.000
-22.7170	-6.1863E-05	412673	1.994E+12
-22.7170	630459	0.000	0.000
-21.2656	-4.4202E-05	-24946	1.994E+12
-21.2656	641704	0.000	0.000
-19.7042	-3.8027E-05	-11010	1.994E+12
-19.7042	652949	0.000	0.000
-17.8121	-3.0775E-05	-5852394	1.994E+12
-17.8121	664194	0.000	0.000
-17.7275	-7.6911E-05	6679.7625	1.994E+12
-17.7275	675439	0.000	0.000
-82.325	-2.347E-05	440.8602	1.994E+12
-82.325	686684	0.000	0.000
-15.4808	8807462	0.000	0.000
83.438	1.676E-05	11186	1.994E+12
-13.0823	10422505	0.000	0.000
84.550	1.105E-05	13360	1.994E+12
-10.6229	12835934	0.000	0.000
85.663	6.534E-06	13641	1.994E+12
-8.1694	16691622	0.000	0.000
86.775	3.239E-06	12467	1.994E+12
-5.7519	23708766	0.000	0.000
87.887	1.058E-06	10267	1.994E+12
-3.2880	41486227	0.000	0.000
89.000	-2.050E-07	7480.6948	1.994E+12
1.0466	68139446	0.000	0.000
90.112	-7.995E-07	4881.3048	1.994E+12
2.8572	47709716	0.000	0.000
91.225	-9.576E-07	2791.1318	1.994E+12
3.1273	43596065	0.000	0.000
92.337	-8.663E-07	1238.3072	1.994E+12
2.9745	45838752	0.000	0.000
93.450	-6.625E-07	255.6043	1.994E+12
2.6012	52419909	0.000	0.000
94.562	-4.358E-07	-283.4986	1.994E+12
2.1099	64632934	0.000	0.000
95.675	-2.345E-07	-446.5667	1.994E+12
1.2006	6835313	0.000	0.000
0.005775	1054980	0.000	0.000
96.788	-7.307E-08	-395.6658	1.994E+12
-0.004274	1077257	0.000	0.000
97.900	5.297E-08	-343.7357	1.994E+12
-0.0122	1099535	-292.5674	1.994E+12
99.012	1.483E-07	-243.5757	1.994E+12
100.125	-2.175E-07	-197.8406	1.994E+12
-0.0183	1121813	0.000	0.000
101.237	2.648E-07	-156.1507	1.994E+12
-0.0227	1144091	0.000	0.000
102.350	2.946E-07	-119.0472	1.994E+12
0.0257	1166369	0.000	0.000
103.462	3.103E-07	-86.8679	1.994E+12
-0.0276	1186646	0.000	0.000
104.575	3.154E-07	-59.7877	1.994E+12
-0.0286	1210924	0.000	0.000
105.688	3.128E-07	-37.8567	1.994E+12
-0.0289	1233202	0.000	0.000
106.800	3.048E-07	-18.0339	1.994E+12
-0.0287	1255480	0.000	0.000
107.913	2.958E-07	-9.2158	1.994E+12
-0.0285	1277736	0.000	0.000
109.025	2.809E-07	0.2059	1.994E+12
-0.0273	1300036	0.000	0.000
110.137	2.646E-07	0.2596	1.994E+12
-0.0264	1322312	0.000	0.000
111.250	2.418E-07	0.000	1.994E+12
-0.0234	672296	0.000	0.000

* This analysis computed pile response using nonlinear moment-curvature

relationships. Values of total stress due to combined axial and bending stresses are computed only.

elastic sections only and do not equal the actual stresses in concrete and steel. Stresses in concrete and steel may be interpolated from the output for nonlinear bending properties relative to the magnitude of bending moment developed in the pile.

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Output Summary for Load Case No. 1:

File-head deflection = 0.5000000 inches
 Computed slope at pile head = -0.0027392 radians
 Maximum bending moment = 8650053. inch-lbs
 Maximum shear force = -34480. lbs
 Depth of maximum bending moment = 20.0250000 feet below pile head
 Depth of maximum shear force = 37.8250000 feet below pile head
 Number of iterations = 43
 Number of zero deflection points = 4

Computed values of Pile Loading and Deflection for Lateral Loading for Load Case Number 2

Pile-head conditions are Displacement and Moment (Loading Type 4)
 Displacement of pile head = 1.000000 inches
 Moment at pile head = 5499600.0 in-lbs
 Axial load at pile head = 0.0 lbs

Res. X	Depth	Deflect.	Bending	Shear	Slope	Total	Bending	Soil
feet	ft	inches	in-lbs	lbs	radians	Stress	stiffness	p
lb/inch	lb/inch	lb/inch	lb/inch	psi*	lb-in/2	lb-in/2	lb/in	lb/in
0.00	0.00	1.0000	5499600.	36070.	-0.004610	0.000	1.337E+12	0.000
0.000	0.000	0.9388	5981138.	36070.	-0.004553	0.000	1.337E+12	0.000
0.000	1.113	0.0000	0.000	36070.	-0.004420	0.000	4.188E+11	0.000
0.000	2.225	0.0000	0.000	35365.	-0.004206	0.000	4.185E+11	0.000
0.000	3.337	0.8208	6944214.	33907.	-0.003977	0.000	4.183E+11	0.000
-105.6647	1718.5636	0.000	0.000	32356.	-0.003734	0.000	4.180E+11	0.000
-112.7815	1965.7096	0.000	0.000	30719.	-0.003476	0.000	4.178E+11	0.000
-119.4935	2232.2630	0.000	0.000	28989.	-0.003298	0.000	4.1750E+12	0.000
-125.8309	2520.5482	0.000	0.000	27173.	-0.003200	0.000	4.186E+12	0.000
-133.2843	2861.5185	0.000	0.000	25286.	-0.003097	0.000	4.186E+12	0.000
-138.8043	3203.6485	0.000	0.000	23336.	-0.002989	0.000	4.186E+12	0.000
-143.8363	3580.0203	0.000	0.000	21328.	-0.002878	0.000	4.185E+12	0.000
-148.3689	3995.5135	0.000	0.000	19271.	-0.002763	0.000	4.185E+12	0.000
-152.3920	4455.8955	0.000	0.000	17170.	-0.002646	0.000	4.185E+12	0.000
-157.8884	4968.0298	0.000	0.000	15033.	-0.002526	0.000	4.185E+12	0.000
-158.7816	5540.0328	0.000	0.000					
-161.2661	6182.0782	0.000	0.000					

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16.688	0.3153	10934216.	0.000	12868.	-0.002404	0.000	1.185E+12	0.000
-163.1202	6905.9178	0.000	0.000	10681.	-0.002280	0.000	1.185E+12	0.000
17.800	0.2841	11091463.	0.000	8482.1245	-0.002154	0.000	1.185E+12	0.000
-164.4002	7726.3604	0.000	0.000	6277.5408	-0.002027	0.000	1.185E+12	0.000
18.912	0.2545	11219411.	0.000	4075.8732	-0.001899	0.000	1.185E+12	0.000
-165.0923	8661.5848	0.000	0.000	1885.4603	-0.001771	0.000	1.185E+12	0.000
20.025	0.2265	11317936.	0.000	-285.1513	-0.001642	0.000	1.185E+12	0.000
-165.1824	9734.2555	0.000	0.000	-2427.2020	-0.001513	0.000	1.185E+12	0.000
21.137	0.2003	11387022.	0.000	-4531.7183	-0.001385	0.000	1.185E+12	0.000
-164.6555	10973.	0.000	0.000	-8682.2025	-0.001257	0.000	1.185E+12	0.000
22.250	0.1758	11426762.	0.000	-14581.	-0.001131	0.000	1.185E+12	0.000
-163.4963	12414.	0.000	0.000	-19724.	-0.001006	0.000	1.185E+12	0.000
23.362	0.1530	11437363.	0.000	-24359.	-0.000885	0.000	1.185E+12	0.000
-161.6890	14104.	0.000	0.000	-28800.	-0.000768	0.000	1.185E+12	0.000
24.475	0.1320	11419148.	0.000	-32932.	-0.000654	0.000	1.185E+12	0.000
-159.2175	16105.	0.000	0.000	-36696.	-0.000546	0.000	1.186E+12	0.000
25.588	0.1126	11372557.	0.000	-40126.	-0.000444	0.000	1.200E+12	0.000
-156.0659	18497.	0.000	0.000	-43081.	-0.000367	0.000	1.977E+12	0.000
26.700	0.0950	11298151.	0.000	-45245.	-0.000313	0.000	1.979E+12	0.000
-465.7295	65441.	0.000	0.000	-46524.	-0.000263	0.000	1.980E+12	0.000
27.812	0.0791	11140742.	0.000	-46992.	-0.000217	0.000	1.982E+12	0.000
-418.0541	70576.	0.000	0.000	-46734.	-0.000175	0.000	1.983E+12	0.000
28.925	0.0648	10908826.	0.000	-45835.	-0.000138	0.000	1.984E+12	0.000
-352.2911	72554.	0.000	0.000	-44386.	-0.000105	0.000	1.986E+12	0.000
30.037	0.0522	10614124.	0.000	-42474.	-7.593E-05	0.000	1.987E+12	0.000
-342.2108	87507.	0.000	0.000	-40188.	-5.066E-05	0.000	1.988E+12	0.000
31.150	0.0412	10558433.	0.000	-37611.	-2.900E-05	0.000	1.990E+12	0.000
-323.1151	104727.	0.000	0.000	-34820.	-1.072E-05	0.000	1.991E+12	0.000
32.262	0.0317	9845155.	0.000	-31891.	4.435E-06	0.000	1.992E+12	0.000
-295.8540	124544.	0.000	0.000	-28888.	1.673E-05	0.000	1.993E+12	0.000
33.375	0.0237	9379149.	0.000	-25872.	2.643E-05	0.000	1.994E+12	0.000
-268.0010	150853.	0.000	0.000	-22894.	3.382E-05	0.000	1.994E+12	0.000
34.487	0.0171	8865379.	0.000	-22894.	3.382E-05	0.000	1.994E+12	0.000
-245.9383	191656.	0.000	0.000					
35.600	0.0119	8307778.	0.000					
-196.6747	221349.	0.000	0.000					
36.712	0.007341	7715125.	0.000					
-127.6054	232042.	0.000	0.000					
37.825	0.003516	7099729.	0.000					
-63.9302	242735.	0.000	0.000					
38.938	0.000330	6472940.	0.000					
-6.2577	253429.	0.000	0.000					
40.050	-0.002275	5845035.	0.000					
45.0010	264122.	0.000	0.000					
41.163	0.004353	5225131.	0.000					
89.6176	274813.	0.000	0.000					
42.275	0.003963	4621839.	0.000					
127.3258	285309.	0.000	0.000					
53.587	0.001158	4040055.	0.000					
158.8162	296202.	0.000	0.000					
63.6200	306807.	0.000	0.000					
183.6820	3088750.	0.000	0.000					
202.45213	317588.	0.000	0.000					
215.52725	3208297.	0.000	0.000					
215.52725	3208297.	0.000	0.000					
223.3501	338975.	0.000	0.000					
226.4669	349669.	0.000	0.000					
225.3948	360362.	0.000	0.000					
51.175	-0.0007941	940701.	0.000					

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220.7025	371056.	0.000	0.000
52.287	-0.007447	654728.	1.994E+12
212.9500	381749.	0.000	0.000
53.400	-0.006895	406707.	1.994E+12
202.6865	392442.	0.000	0.000
54.512	-0.006307	194809.	1.994E+12
190.4408	403136.	0.000	0.000
55.625	-0.005701	168852.	1.994E+12
176.7126	413829.	0.000	0.000
56.738	-0.005093	-129611.	1.994E+12
161.9661	424522.	0.000	0.000
57.850	-0.004498	-247208.	1.994E+12
146.6243	435216.	0.000	0.000
131.0661	445909.	0.000	0.000
115.6244	-0.003924	-338673.	1.994E+12
60.075	-0.003381	-406779.	1.994E+12
61.188	-0.002874	-454278.	1.994E+12
100.5848	456602.	0.000	0.000
86.1869	477989.	0.000	0.000
72.6249	488682.	0.000	0.000
60.0503	499376.	0.000	0.000
48.5743	510069.	0.000	0.000
38.2714	520762.	0.000	0.000
29.1825	531456.	0.000	0.000
21.3183	542149.	0.000	0.000
14.6635	552842.	0.000	0.000
9.1796	563536.	0.000	0.000
33.7722	4033127.	0.000	0.000
18.5218	7345301.	0.000	0.000
-14.6124	9349640.	0.000	0.000
-23.9271	5700172.	0.000	0.000
-27.9363	4898105.	0.000	0.000
-29.2855	4635016.	0.000	0.000
-29.2129	4666131.	0.000	0.000
-28.1048	4847705.	0.000	0.000
-26.8793	5166057.	0.000	0.000
-23.9725	5698195.	0.000	0.000
-21.2447	6413570.	0.000	0.000
-18.3557	7422838.	0.000	0.000
-15.3601	8669171.	0.000	0.000
28.0784	-5.454E-07	20461.	0.000
-116.6502	-4.108E-07	0.000	0.000
-221.3913	-2.867E-07	19736.	0.000
-283.9853	-1.823E-07	0.000	0.000
-283.7840	-1.034E-07	17347.	0.000
-234.2961	-4.975E-08	13825.	0.000
-173.2906	-1.709E-08	9764.1903	0.000
-108.9283	8.419E-11	6248.2182	0.000
-44.5957	7.521E-09	3508.4841	0.000
-11.5788	1.097E-08	1621.3581	0.000
-9.4171	1.339E-08	600.0975	0.000
-7.4050	1.496E-08	430.6532	0.000
-5.5735	1.587E-08	290.9444	0.000
-3.9455	1.629E-08	179.2158	0.000
-2.5366	1.635E-08	93.2317	0.000
-1.3574	1.618E-08	50.4026	0.000
-0.4152	1.590E-08	-12.1120	0.000
0.2853	1.557E-08	-37.3233	0.000
0.7399	1.527E-08	0.000	0.000
0.9444	1.504E-08	-48.3556	0.000
0.8937	1.489E-08	-48.4088	0.000
0.5814	1.483E-08	-407.7388	0.000
0.000	1.481E-08	-28.6544	0.000
0.000	1.994E+12	-51.0244	0.000
0.000	1.994E+12	0.47933	0.000
0.000	1.994E+12	0.000	0.000
0.000	1.994E+12	672296.	0.000

* This analysis computed pile response using nonlinear moment-curvature relationships.
 Values of total stress due to combined axial and bending stresses are computed only for elastic sections only and do not equal the actual stresses in concrete and steel in concrete and steel may be interpolated from the output for nonlinear bending properties relative to the magnitude of bending moment developed in the pile.

Pier 11a1ff.lp7o
 = -46992. lbs
 = 23.3625000 feet below pile head
 = 38.9375000 feet below pile head
 = 18
 = 4

Computed values of Pile Loading and Deflection
 for Lateral Loading for Load Case Number 3

Pile-head conditions are Displacement and Moment (Loading Type 4)
 Displacement of pile head = 1.500000 inches
 Moment at pile head = 5499600.0 in-lbs
 Axial load at pile head = 0.0 lbs

Res.	Soil	Deflect.	Bending	Shear	Slope	Total	Bending	Soil
X	spr.	y	Moment	Force	S	Stress	stiffness	p
feet	inches	inches	in-lbs	lbs	radians	psi*	lb-in ²	lb/in
0.00	0.00	1.5000	5499600.	52450.	-0.006195	0.000	1.337E+12	0.000
0.000	1.113	0.000	0.000	52450.	-0.006137	0.000	1.337E+12	0.000
0.000	1.113	0.000	0.000	52450.	-0.005996	0.000	4.186E+11	0.000
0.000	2.225	0.000	0.000	51637.	-0.005765	0.000	4.182E+11	0.000
-121.8122	1293.1286	0.000	8278736.	49954.	-0.005511	0.000	4.178E+11	0.000
-130.3267	1471.6828	0.000	8934010.	48160.	-0.005236	0.000	4.170E+11	0.000
-138.4028	1663.9438	0.000	9364618.	46262.	-0.004940	0.000	4.170E+11	0.000
-146.0638	1870.5880	0.000	10169194.	44252.	-0.004730	0.000	1.185E+12	0.000
-155.0287	2115.0590	0.000	10746141.	42137.	-0.004612	0.000	1.185E+12	0.000
-161.7988	2357.7143	0.000	11294531.	39935.	-0.004488	0.000	1.185E+12	0.000
-168.0473	2622.7038	0.000	11824412.	37654.	-0.004357	0.000	1.184E+12	0.000
-173.7612	2913.0922	0.000	12299604.	35299.	-0.004221	0.000	1.184E+12	0.000
-178.9270	3232.1063	0.000	12754907.	32880.	-0.004080	0.000	1.184E+12	0.000
-183.5311	3584.0940	0.000	13177502.	30403.	-0.003934	0.000	1.184E+12	0.000
-187.4462	4065.0501	0.000	13566669.	27876.	-0.003783	0.000	1.183E+12	0.000
-190.3775	4407.0326	0.000	13921905.	25307.	-0.003628	0.000	1.183E+12	0.000
-193.1898	4890.1741	0.000	14242377.	22705.	-0.003469	0.000	1.183E+12	0.000
-196.0446	5433.1581	0.000	14528019.	20077.	-0.003307	0.000	1.183E+12	0.000
-197.6216	6044.5486	0.000	1478440.	17433.	-0.003141	0.000	1.183E+12	0.000
-20.025	0.3934	0.000	1478440.	17433.	-0.003141	0.000	1.183E+12	0.000

Pier 11a1ff.lp7o

-198.5437	6737.3612	0.000	14993476.	14781.	-0.002973	0.000	1.183E+12	0.000
-198.5437	6737.3612	0.000	14993476.	14781.	-0.002973	0.000	1.183E+12	0.000
-198.7994	7327.0449	0.000	15173082.	12130.	-0.002803	0.000	1.182E+12	0.000
-198.7994	7327.0449	0.000	15173082.	12130.	-0.002803	0.000	1.182E+12	0.000
-198.3642	8432.9230	0.000	15317353.	9488.9898	-0.002631	0.000	1.182E+12	0.000
-197.2209	9479.4259	0.000	15426438.	6868.5860	-0.002457	0.000	1.182E+12	0.000
-195.2495	10696.	0.000	15500726.	4278.1791	-0.002283	0.000	1.182E+12	0.000
-195.2495	10696.	0.000	15500726.	4278.1791	-0.002283	0.000	1.182E+12	0.000
-192.7270	12129.	0.000	15540663.	-1204.2089	-0.002108	0.000	1.182E+12	0.000
-192.7270	12129.	0.000	15540663.	-1204.2089	-0.002108	0.000	1.182E+12	0.000
-628.6046	45900.	0.000	15468574.	-9329.9981	-0.001932	0.000	1.182E+12	0.000
-588.7421	50426.	0.000	15291555.	-16747.	-0.001759	0.000	1.182E+12	0.000
-522.4576	53148.	0.000	1502422.	-23712.	-0.001588	0.000	1.183E+12	0.000
-522.4576	53148.	0.000	1502422.	-23712.	-0.001588	0.000	1.183E+12	0.000
-521.0029	63866.	0.000	14658433.	-30572.	-0.001420	0.000	1.183E+12	0.000
-506.6019	76126.	0.000	14205160.	-37153.	-0.001257	0.000	1.183E+12	0.000
-32.262	90145.	0.000	11591793.	-43345.	-0.001100	0.000	1.183E+12	0.000
-479.3380	90145.	0.000	13666456.	-43345.	-0.001100	0.000	1.183E+12	0.000
-33.375	108283.	0.000	13047850.	-49154.	-0.000949	0.000	1.184E+12	0.000
-34.487	108283.	0.000	13047850.	-49154.	-0.000949	0.000	1.184E+12	0.000
-421.9728	135364.	0.000	12354039.	-54534.	-0.000806	0.000	1.184E+12	0.000
-383.9600	171305.	0.000	11591793.	-59322.	-0.000671	0.000	1.184E+12	0.000
-333.4040	221243.	0.000	10770130.	-63005.	-0.000545	0.000	1.185E+12	0.000
-218.2705	240336.	0.000	9009820.	-65163.	-0.000429	0.000	1.185E+12	0.000
-38.398	2502536.	0.000	9030268.	-65939.	-0.000322	0.000	1.186E+12	0.000
-105.1008	2670958.	0.000	819003.	-65591.	-0.000244	0.000	1.186E+12	0.000
-11.0439	2670958.	0.000	819003.	-65591.	-0.000244	0.000	1.186E+12	0.000
63.0311	278193063.	0.000	7178976.	-64321.	-0.000192	0.000	1.186E+12	0.000
127.2408	285509.	0.000	6431635.	-62260.	-0.000145	0.000	1.186E+12	0.000
181.5132	2962081.	0.000	5616635.	-59540.	-0.000105	0.000	1.186E+12	0.000
226.0475	306895.	0.000	4841914.	-56287.	-6.974E-05	0.000	1.186E+12	0.000
45.1613	317589.	0.000	4113767.	-52623.	-3.964E-05	0.000	1.186E+12	0.000
261.2618	328382.	0.000	3436878.	-48663.	-1.428E-05	0.000	1.186E+12	0.000
287.6075	338975.	0.000	2814476.	-44510.	6.695E-06	0.000	1.186E+12	0.000
47.837	338975.	0.000	2814476.	-44510.	6.695E-06	0.000	1.186E+12	0.000
305.7777	349669.	0.000	2248452.	-40262.	2.367E-05	0.000	1.186E+12	0.000
316.3321	349669.	0.000	1739493.	-36001.	3.704E-05	0.000	1.186E+12	0.000
320.1912	360362.	0.000	1287229.	-31802.	4.718E-05	0.000	1.186E+12	0.000
51.175	371056.	0.000	890377.	-27728.	5.447E-05	0.000	1.186E+12	0.000
318.1119	371056.	0.000	890377.	-27728.	5.447E-05	0.000	1.186E+12	0.000
52.287	381749.	0.000	546888.	-23831.	5.928E-05	0.000	1.186E+12	0.000
310.9154	381749.	0.000	546888.	-23831.	5.928E-05	0.000	1.186E+12	0.000
53.400	392442.	0.000	403136.	284.4192	0.000	0.000	1.186E+12	0.000
299.4195	392442.	0.000	403136.	284.4192	0.000	0.000	1.186E+12	0.000
54.512	403136.	0.000	403136.	284.4192	0.000	0.000	1.186E+12	0.000
284.4192	403136.	0.000	403136.	284.4192	0.000	0.000	1.186E+12	0.000

Pier 11a1ff.jp7o		Pier 11a1ff.jp7o	
-20152.	6.196E-05	0.000	1.994E+12
55.625	-0.008603	254089.	0.000
266.6750	413829.	0.000	0.000
56.738	0.007764	8817.3164	0.000
246.9018	424522.	0.000	0.000
57.850	-0.006925	-192451.	0.000
225.7195	435216.	0.000	0.000
58.962	-0.006103	-353483.	0.000
203.8472	445909.	0.000	0.000
60.075	-0.005312	-478186.	0.000
181.6986	456602.	0.000	0.000
61.188	-0.004565	-570505.	0.000
159.7797	467296.	0.000	0.000
62.300	-0.003868	-634349.	0.000
138.4888	477989.	0.000	0.000
63.412	-0.003228	-673510.	0.000
118.1571	488682.	0.000	0.000
64.525	-0.002648	-691613.	0.000
99.0520	499376.	0.000	0.000
81.3799	510069.	0.000	0.000
66.750	-0.001674	-678009.	0.000
67.862	-0.001278	-652319.	0.000
50.8836	531456.	0.000	0.000
68.975	-0.000941	-617561.	0.000
38.2105	542149.	0.000	0.000
70.087	-0.000659	-575992.	0.000
27.2830	552842.	0.000	0.000
18.0769	563536.	0.000	0.000
50.0075	5725131.	0.000	0.000
32.6708	4169043.	0.000	0.000
74.537	-1.917E-06	-421343.	0.000
4.3233	30101639.	0.000	0.000
-26.5371	5143531.	0.000	0.000
-34.0691	4004096.	0.000	0.000
-37.4964	3637351.	0.000	0.000
-38.5963	3533260.	0.000	0.000
-38.1485	3574390.	0.000	0.000
-36.6079	3724492.	0.000	0.000
-34.2811	3976928.	0.000	0.000
-31.3937	4342267.	0.000	0.000
-28.1201	4847166.	0.000	0.000
-24.5993	5540052.	0.000	0.000
-20.9413	6506420.	0.000	0.000
-17.2276	7906602.	0.000	0.000
-13.5013	10083781.	0.000	0.000
90.112	9.288E-06	265600.	0.000
277.4356	-5.542E-07	0.000	0.000
491.1147	1.212E-05	0.000	0.000
4604.9926	9.103E-06	0.000	0.000
4851.9286	6.498E-06	0.000	0.000
4703.6516	4.326E-06	0.000	0.000
4299.1050	2.575E-06	0.000	0.000
3821.4050	1.208E-06	0.000	0.000
3313.4862	1.820E-07	0.000	0.000
2801.2143	-5.474E-07	0.000	0.000
2302.2149	-1.026E-06	0.000	0.000
1829.0307	-1.300E-06	0.000	0.000
1390.6515	-1.409E-06	0.000	0.000
993.3971	-1.395E-06	0.000	0.000
641.4947	-1.291E-06	0.000	0.000
337.5108	-1.131E-06	0.000	0.000
82.7335	-9.398E-07	0.000	0.000
-122.3817	-7.416E-07	0.000	0.000
-277.4356	-5.542E-07	0.000	0.000

Pier 11a1ff.jp7o		Pier 11a1ff.jp7o	
-20152.	6.196E-05	0.000	1.994E+12
91.225	3.076E-06	21989.	0.000
-5.5881	24249677.	0.000	0.000
92.337	-1.170E-06	16422.	0.000
3.4789	39687963.	0.000	0.000
93.450	-3.949E-06	11476.	0.000
6.3591	21497972.	0.000	0.000
94.562	-5.702E-06	7662.7563	0.000
7.6356	17877589.	0.000	0.000
95.675	-6.770E-06	5210.4018	0.000
8.3173	1640581.	0.000	0.000
96.788	-7.372E-06	4240.3778	0.000
0.5826	1054980.	0.000	0.000
97.900	-7.595E-06	3374.1824	0.000
0.6129	1077257.	0.000	0.000
99.012	-7.517E-06	2617.2188	0.000
0.6191	1099533.	0.000	0.000
100.125	-7.205E-06	1970.5960	0.000
0.6054	1121813.	0.000	0.000
101.237	-6.716E-06	1431.8726	0.000
0.5756	1144091.	0.000	0.000
102.350	-6.100E-06	995.7316	0.000
0.5329	1166369.	0.000	0.000
103.462	-5.394E-06	654.5722	0.000
0.4803	1188646.	0.000	0.000
104.575	-4.631E-06	399.0149	0.000
0.4200	1210924.	0.000	0.000
105.688	-3.831E-06	218.3147	0.000
0.3539	1233202.	0.000	0.000
106.800	-3.012E-06	100.6850	0.000
0.2832	1255480.	0.000	0.000
107.913	-2.184E-06	33.5365	0.000
0.2090	1277758.	0.000	0.000
109.025	-1.353E-06	3.6392	0.000
0.1317	1300036.	0.000	0.000
0.0516	1322313.	-2.7814	0.000
111.250	3.099E-07	0.000	0.000
-0.0312	672296.	0.000	0.000

* This analysis computed pile response using nonlinear moment-curvature relationships.

Values of total stress due to combined axial and bending stresses are computed only for elastic sections only and do not equal the actual stresses in concrete and steel. Stresses in concrete and steel may be interpolated from the output for nonlinear bending properties relative to the magnitude of bending moment developed in the pile.

Output Summary for Load Case No. 3:

Pile-head deflection	=	1.500000 inches
Computed slope at pile head	=	-0.006464 radians
Maximum bending moment	=	13548693. lbf-in
Maximum shear force	=	26.700000 lbf
Depth of maximum bending moment	=	26.700000 feet below pile head
Number of iterations	=	40.050000
Number of zero deflection points	=	13

Computed Values of Pile Loading and Deflection
for Lateral Loading for Load Case Number 4

Pile-head conditions are Displacement and Moment (Loading Type 4)
Displacement of pile head = 2.000000 inches
Moment at pile head = 5499600.0 in-lbs
Axial load at pile head = 0.0 lbs

Res. X	Depth	Deflect.	Bending	Shear	Slope	Total	Bending	Soil
feet	inches	lb/inch	in-lbs	lbs	radians	Stress	Stiffness	P
	lb/inch	lb/inch	in-lbs	lbs		psi*	lb-in ²	lb/in
0.000	0.000	2.0000	5499600.	67787.	-0.007738	0.000	1.337E+12	0.000
0.000	1.113	1.8971	6404562.	67787.	-0.007678	0.000	1.337E+12	0.000
0.000	2.225	1.7950	7309524.	67787.	-0.007529	0.000	4.183E+11	0.000
0.000	3.337	1.6960	8214486.	66889.	-0.007282	0.000	4.178E+11	0.000
-134.	5835	1059.3483	9095463.	65028.	-0.007005	0.000	4.173E+11	0.000
-144.	1756	1202.5325	9950743.	63043.	-0.006700	0.000	4.168E+11	0.000
-153.	3013	1356.2409	10778703.	60938.	-0.006368	0.000	4.163E+11	0.000
-161.	4301	1521.0358	11577793.	58708.	-0.006130	0.000	1.184E+12	0.000
-172.	5589	1716.0099	12346210.	56359.	-0.005995	0.000	1.184E+12	0.000
-179.	6884	1908.4295	13082575.	53910.	-0.005852	0.000	1.184E+12	0.000
-187.	8172	2117.7242	13785610.	51369.	-0.005700	0.000	1.183E+12	0.000
-193.	9460	2346.0586	14454137.	48744.	-0.005541	0.000	1.182E+12	0.000
-199.	10748	2595.9509	15087083.	46043.	-0.005374	0.000	1.182E+12	0.000
-205.	12036	2870.3452	15683478.	43273.	-0.005200	0.000	1.182E+12	0.000
-209.	13324	3172.7025	16242462.	40442.	-0.005020	0.000	1.182E+12	0.000
-214.	14612	3507.1146	16763288.	37560.	-0.004833	0.000	1.181E+12	0.000
-217.	15900	3878.4492	17245322.	34635.	-0.004641	0.000	1.181E+12	0.000
-220.	17188	4292.5351	17688048.	31676.	-0.004444	0.000	1.181E+12	0.000
-222.	18476	4736.4017	18091070.	28692.	-0.004242	0.000	1.181E+12	0.000
-224.	19764	5278.5903	18454114.	25692.	-0.004035	0.000	1.181E+12	0.000
-225.	21052	5869.5651	18777037.	22686.	-0.003825	0.000	1.180E+12	0.000
-225.	22340	6542.2591	19059822.	19684.	-0.003611	0.000	1.180E+12	0.000
-224.	23628	7312.8086	0.000	0.000				

24.475	0.3632	18302588.	16696.	-0.003394	0.000	1.180E+12
-223.1042	8201.5533	0.000				
25.588	0.3193	19505592.	13732.	-0.003174	0.000	1.180E+12
-220.8713	9234.4139	0.000				
26.700	0.2784	19669233.	7170.1746	-0.002952	0.000	1.180E+12
-762.1729	36547.	0.000				
-732.2781	40677.	0.000				
28.925	0.2055	19594250.	-2808.3444	-0.002730	0.000	1.180E+12
-671.2753	43603.	0.000				
-679.9847	52312.	0.000				
-673.2540	62216.	0.000				
-650.6952	73450.	0.000				
-622.6635	87616.	0.000				
-599.7408	107909.	0.000				
-562.8360	133869.	0.000				
-510.9338	168219.	0.000				
-442.4604	216216.	0.000				
-309.2784	253429.	0.000				
-144.5141	264122.	0.000				
-3.8368	274815.	0.000				
42.275	-0.005236	1012361.	-55729.	-0.001451	0.000	1.181E+12
111.9783	285509.	0.000				
202.7107	296202.	0.000				
268.6230	306895.	0.000				
321.6863	317389.	0.000				
362.5248	328282.	0.000				
391.9295	338975.	0.000				
410.8202	349669.	0.000				
420.2078	360362.	0.000				
421.1652	371056.	0.000				
414.75287	381750.	0.000				
402.18151	392444.	0.000				
384.42712	403138.	0.000				
362.524625	413832.	0.000				
337.5760	424526.	0.000				
310.3748	435220.	0.000				
58.962	-0.008437	-362163.	-15803.	7.998E-05	0.000	1.994E+12

STR - A
Δ = 2.0"
LATERAL
RESISTANCE
= 67.79 K

Pier 11aflff.lp70		Pier 11aflff.lp70	
281.7954	445909	0.000	1.994E+12
60.075	-0.007385	-54802.3	0.000
252.5868	456602	0.000	1.994E+12
61.188	-0.006382	-688866.	0.000
223.4081	467296	0.000	1.994E+12
62.300	-0.005441	-783983.	0.000
194.8280	477989	0.000	1.994E+12
63.412	-0.004571	-856198.	0.000
167.3247	488682	0.000	1.994E+12
64.525	-0.003777	-892681.	0.000
141.2899	499376	0.000	1.994E+12
65.638	-0.003063	-903983.	0.000
117.0318	510069	0.000	1.994E+12
66.750	-0.002430	-894427.	0.000
94.7817	520762	0.000	1.994E+12
67.862	-0.001876	-867980.	0.000
74.6997	531456	0.000	1.994E+12
68.975	-0.001401	-828219.	0.000
56.8820	542149	0.000	1.994E+12
70.087	-0.000999	-778320.	0.000
41.3677	552842	0.000	1.994E+12
71.200	-0.000667	-721049.	0.000
28.1466	563536	0.000	1.994E+12
72.312	-0.000399	-658761.	0.000
63.8246	2135081.	0.000	1.994E+12
73.425	-0.000190	-585099.	0.000
44.0568	3091532.	0.000	1.994E+12
74.537	-3.372E-05	-503584.	0.000
18.5080	7327625	0.000	1.994E+12
75.650	7.780E-05	-418771.	0.000
-28.2173	4842072.	0.000	1.994E+12
76.763	0.000152	-338987.	0.000
-39.4039	3463475	0.000	1.994E+12
77.875	0.000196	-266226.	0.000
-44.7175	3050981.	0.000	1.994E+12
78.987	0.000216	-201434.	0.000
-46.9426	2905934.	0.000	1.994E+12
80.100	0.000218	-145009.	0.000
-47.1559	2892528.	0.000	1.994E+12
81.212	0.000207	-96987.	0.000
-45.9498	2968257.	0.000	1.994E+12
82.325	0.000187	-57155.	0.000
-43.7099	3120188.	0.000	1.994E+12
83.438	0.000162	-25113.	0.000
-40.7132	3349666.	0.000	1.994E+12
84.550	0.000135	-327.4969	0.000
-37.1708	3668676.	0.000	1.994E+12
85.663	0.000108	17834.	0.000
-33.2489	4101124.	0.000	1.994E+12
86.775	8.280E-05	30069.	0.000
-29.0794	4688714.	0.000	1.994E+12
87.887	6.052E-05	37122.	0.000
-24.7650	5305260.	0.000	1.994E+12
89.000	4.062E-05	39762.	0.000
-20.5641	6592743.	0.000	1.994E+12
90.112	857343.	38972.	0.000
-15.8913	77323.	34950.	0.000
91.225	17.232.	0.000	1.994E+12
-11.2146	1313738.	0.000	1.994E+12
92.337	3.045E-06	29129.	0.000
-5.4506	2434971	0.000	1.994E+12
93.450	-3.635E-06	0.000	1.994E+12
6.1095	22447345.	0.000	1.994E+12

Pier 11aflff.lp70		Pier 11aflff.lp70	
94.562	-8.321E-06	16595.	0.000
9.2298	14808315.	0.000	1.994E+12
95.675	-1.152E-05	12517.	0.000
10.8581	12577598.	0.000	1.994E+12
96.788	-1.361E-05	10374.	0.000
1.0755	1054980.	0.000	1.994E+12
97.900	-1.477E-05	8422.8150	0.000
1.1917	1077257.	0.000	1.994E+12
99.012	-1.517E-05	6684.1260	0.000
1.2497	1099535.	0.000	1.994E+12
100.125	-1.498E-05	5168.1639	0.000
1.2589	1121813.	0.000	1.994E+12
1.01.237	-1.433E-05	3876.5614	0.000
1.2278	1144091.	0.000	1.994E+12
102.350	-1.333E-05	2803.7814	0.000
1.1643	1166369.	0.000	1.994E+12
103.462	-1.207E-05	1938.5022	0.000
1.0751	1188646.	0.000	1.994E+12
104.575	-1.065E-05	1264.8298	0.000
0.9660	1210924.	0.000	1.994E+12
105.688	-9.112E-06	763.3252	0.000
0.8418	1233202.	0.000	1.994E+12
106.800	-7.506E-06	411.8404	0.000
0.7059	1253480.	0.000	1.994E+12
107.913	-5.864E-06	186.1693	0.000
0.5612	1277758.	0.000	1.994E+12
109.025	-4.204E-06	60.5228	0.000
0.4094	1300036.	0.000	1.994E+12
110.137	-2.540E-06	7.8456	0.000
0.2515	1322513.	0.000	1.994E+12
111.250	-8.741E-07	0.000	1.994E+12
0.0880	672296.	0.000	1.994E+12

* This analysis computed pile response using nonlinear moment-curvature relationships.

Values of total stress due to combined axial and bending stresses are computed only for elastic sections only and do not equal the actual stresses in concrete and steel.

Stresses in concrete and steel may be interpolated from the output for nonlinear bending properties relative to the magnitude of bending moment developed in the pile.

Output Summary for Load Case No. 4:

Pile-head deflection	=	2.0000000 inches
Computed slope at pile head	=	-0.007275 radians
Maximum bending moment	=	19897036 lbf-ft
Maximum shear force	=	86056 lbf
Depth of maximum bending moment	=	27.8125000 feet below pile head
Depth of maximum shear force	=	41.1625000 feet below pile head
Number of iterations	=	17
Number of zero deflection points	=	4

----- Pile-head Deflection vs. Pile Length for Load Case 4 -----

Boundary Condition Type 4, Deflection and Moment

Deflection =		2.00000 in		Pier 11aff.1p70		Pier 11aff.1p70		0.000 1.986E+12			
Moment =		5499600 in-lb						32055. -0.001535			
Axial Load =		0. lb						0.000 1.985E+12			
Pile Length feet	Pile Head Deflection inches	Maximum Moment in-lbs	Maximum Shear lbs	Res. X feet	Depth Soil X feet	Deflect. Lat. Load in-lbs	Bending Moment in-lbs	Total Stress psi*	Slope S radians	Bending Stiffness lb-in ²	Soil P lb/in
111.2500	2.0000000	19697036.	-86058.	0.000	0.000	0.500000	783600.	0.000	-0.001738	0.000	1.354E+12
105.6875	2.0000000	19852396.	-86562.	0.000	0.000	0.4769	1308425.	0.000	-0.001728	0.000	1.354E+12
100.1250	2.0000000	19544590.	-85185.	0.000	0.000	0.4539	1083249.	0.000	-0.001712	0.000	1.350E+12
94.5625	2.0000000	19771668.	-86245.	0.000	0.000	0.4311	9358074.	0.000	-0.001691	0.000	1.348E+12
89.0000	2.0000000	19606694.	-85794.	0.000	0.000	0.4087	7867704.	0.000	-0.001665	0.000	1.346E+12
83.4375	2.0000000	19661879.	-85972.	0.000	0.000	0.3863	6377004.	0.000	-0.001635	0.000	1.345E+12
77.8750	2.0000000	19682032.	-86145.	0.000	0.000	0.3639	4886303.	0.000	-0.001599	0.000	1.343E+12
72.3125	2.0000000	19548374.	-85340.	0.000	0.000	0.3415	3395600.	0.000	-0.001565	0.000	1.987E+12
66.7500	2.0000000	19650220.	-85215.	0.000	0.000	0.3191	19304330.	0.000	-0.001599	0.000	1.987E+12
61.1875	2.0000000	19753534.	-86408.	0.000	0.000	0.2967	18056391.	0.000	-0.001599	0.000	1.987E+12
55.6250	2.0000000	19304330.	-92511.	0.000	0.000	0.2743	13862172.	0.000	-0.001599	0.000	1.987E+12
50.0625	2.0000000	18056391.	-100440.	0.000	0.000	0.2519	9309965.	0.000	-0.001599	0.000	1.987E+12
44.5000	2.0000000	16766511.	-46727.	0.000	0.000	0.2295	66766511.	0.000	-0.001599	0.000	1.987E+12
38.9375	2.0000000	9309965.	-33074.	0.000	0.000	0.2071	5499600.	0.000	-0.001599	0.000	1.987E+12
33.3750	2.0000000	66766511.	-33074.	0.000	0.000	0.1847	4294633.	0.000	-0.001599	0.000	1.987E+12
27.8125	2.0000000	5499600.	-30204.	0.000	0.000	0.1623	33549.	0.000	-0.001565	0.000	1.987E+12
22.2500	2.0000000	4294633.	-38714.	0.000	0.000	0.1399	0.000	0.000	-0.001565	0.000	1.987E+12
16.6875	2.0000000	5499600.	-38714.	0.000	0.000	0.1175	0.000	0.000	-0.001565	0.000	1.987E+12

Computed Values of Pile Loading and Deflection for Lateral Loading for Load Case Number 5

Pile-head conditions are Displacement and Moment (Loading Type 4)
 Displacement of pile head = 0.500000 inches
 Moment at pile head = 783600.0 in-lbs
 Axial load at pile head = 0.0 lbs

Res. X feet	Depth Soil X feet	Deflect. Lat. Load in-lbs	Bending Moment in-lbs	Total Stress psi*	Slope S radians	Bending Stiffness lb-in ²	Soil P lb/in
0.00	0.5000	783600.	39313.	0.000	1.354E+12	0.000	0.000
0.000	1.113	0.4769	1308425.	0.000	1.354E+12	0.000	0.000
0.000	2.225	0.4539	1083249.	0.000	1.350E+12	0.000	0.000
0.000	3.337	0.4311	9358074.	0.000	1.348E+12	0.000	0.000
-85.2330	2639.8793	2867704.	37564.	0.000	1.346E+12	0.000	0.000
-91.4600	2987.6819	2867704.	37564.	0.000	1.345E+12	0.000	0.000
-97.3711	3361.7803	36303.	36303.	0.000	1.345E+12	0.000	0.000
-102.9566	3764.9201	3837007.	34966.	0.000	1.343E+12	0.000	0.000
-109.4129	4246.3072	4294633.	33549.	0.000	1.987E+12	0.000	0.000

Pier 11aff.1p70		Pier 11aff.1p70	
99.7861	296202	0.000	0.000
44.500	3123197	0.000	1.989E+12
124.5750	306895	0.000	1.989E+12
45.613	-0.006061	0.000	1.990E+12
144.1835	317589	0.000	1.991E+12
46.725	-0.006461	0.000	1.992E+12
158.8893	328282	0.000	1.993E+12
47.837	-0.006657	0.000	1.994E+12
169.0335	338975	0.000	1.994E+12
175.0059	349669	0.000	1.994E+12
177.2310	360362	0.000	1.994E+12
176.1549	371056	0.000	1.994E+12
52.287	-0.006023	0.000	1.994E+12
53.400	-0.005644	0.000	1.994E+12
165.9114	392442	0.000	1.994E+12
157.6367	403136	0.000	1.994E+12
55.625	-0.004769	0.000	1.994E+12
56.738	-0.004305	0.000	1.994E+12
136.8863	424522	0.000	1.994E+12
125.1747	435216	0.000	1.994E+12
58.962	-0.003384	0.000	1.994E+12
113.0277	445909	0.000	1.994E+12
60.075	-0.002945	0.000	1.994E+12
100.7477	456602	0.000	1.994E+12
88.5796	467296	0.000	1.994E+12
76.610	-0.002144	0.000	1.994E+12
65.4724	488682	0.000	1.994E+12
64.525	-0.001467	0.000	1.994E+12
54.8643	499376	0.000	1.994E+12
45.0535	510069	0.000	1.994E+12
36.1258	520762	0.000	1.994E+12
28.1387	531456	0.000	1.994E+12
21.1243	542149	0.000	1.994E+12
15.9924	552842	0.000	1.994E+12
10.0331	563536	0.000	1.994E+12
37.5029	3637880	0.000	1.994E+12
25.1582	5426772	0.000	1.994E+12
8.7847	1567488	0.000	1.994E+12
-17.1900	7915680	0.000	1.994E+12
-22.6279	5966093	0.000	1.994E+12
-25.1586	5417771	0.000	1.994E+12
78.987	6.468E-05	-64348.	0.000
-25.7019	5305109.	0.000	1.994E+12
80.100	6.161E-05	-41018.	0.000
-25.0892	5436541.	0.000	1.994E+12
81.212	5.487E-05	-22159.	0.000
-23.6831	5761643.	0.000	1.994E+12
82.325	4.616E-05	-7520.4835	0.000
-21.7268	6283642.	0.000	1.994E+12
83.438	3.677E-05	3245.4380	0.000
-19.3987	7042541.	0.000	1.994E+12
84.550	2.768E-05	10554.	0.000
-16.8371	8121799.	0.000	1.994E+12
85.663	1.952E-05	14862.	0.000
-14.1511	9677203.	0.000	1.994E+12
-11.4253	12013295.	0.000	1.994E+12
86.775	1.270E-05	16648.	0.000
-8.7162	15811564.	0.000	1.994E+12
87.887	7.359E-06	16397.	0.000
89.000	3.488E-06	14594.	0.000
-6.0282	23074663.	0.000	1.994E+12
90.112	9.205E-07	11715.	0.000
-3.1645	45895789.	0.000	1.994E+12
2.3928	53279129.	8273.1479	0.000
92.337	-1.380E-06	5257.4135	0.000
3.7186	35971213.	2904.4215	0.000
4.1401	32690635.	1289.2875	0.000
94.562	-1.742E-06	425.7634	0.000
4.2173	32324757.	0.000	1.994E+12
95.675	-1.677E-06	302.0123	0.000
4.1508	33034032.	0.000	1.994E+12
96.788	-1.575E-06	200.4461	0.000
97.900	-1.446E-06	119.6737	0.000
0.1167	1077257.	0.000	1.994E+12
99.012	-1.299E-06	0.000	1.994E+12
0.1070	1099535.	0.000	1.994E+12
100.125	-1.141E-06	57.9646	0.000
0.0959	1121813.	0.000	1.994E+12
101.237	-9.777E-07	13.3400	0.000
0.0838	1144091.	0.000	1.994E+12
102.350	-8.134E-07	-16.3515	0.000
0.0711	1166369.	-33.3771	0.000
0.0579	1188646.	0.000	1.994E+12
104.575	-4.908E-07	-40.0785	0.000
0.0445	1210924.	0.000	1.994E+12
105.688	-3.345E-07	-38.8460	0.000
0.0309	1233202.	0.000	1.994E+12
106.800	-1.818E-07	-32.1060	0.000
0.0171	1255480.	-22.3197	0.000
0.003049	1277758.	0.000	1.994E+12
109.025	-1.161E-07	-11.9899	0.000
-0.0113	1300036.	-3.6745	0.000
-0.0260	1322313.	0.000	1.994E+12
111.250	4.094E-07	0.000	1.994E+12
-0.0412	672296.	0.000	1.994E+12

* This analysis computed pile response using nonlinear moment-curvature relationships.

Pier 11aiff,lp7o
 Values of total stress due to combined axial and bending stresses are computed only for elastic sections only and do not equal the actual stresses in concrete and steel.
 Stresses in concrete and steel may be interpolated from the output for nonlinear bending properties relative to the magnitude of bending moment developed in the pile.

Output summary for Load Case No. 5:
 Pile-head deflection = 0.5000000 inches
 Computed slope at pile head = -0.0017379 radians
 Maximum bending moment = 8583608. inch-lbs
 Maximum shear force = 39313. lbs
 Depth of maximum bending moment = 26.7000000 feet below pile head
 Depth of maximum shear force = II
 Number of iterations = 4
 Number of zero deflection points = 4

Computed Values of Pile Loading and Deflection for Lateral Loading for Load Case Number 6

Pile-head conditions are Displacement and Moment (Loading Type 4)
 Displacement of pile head = 1.000000 inches
 Moment at pile head = 783600.0 in-lbs
 Axial load at pile head = 0.0 lbs

Res. X	Depth feet	Deflect. inches	Bending Moment in-lbs	Shear Force lbs	Slope radians	Total Stress psi*	Bending Stiffness lb-in^2	Soil p lb/in
0.000	0.00	1.0000	783600.	52667.	-0.003343	0.000	1.354E+12	0.000
0.000	1.113	0.9554	1486709.	52667.	-0.003332	0.000	1.354E+12	0.000
0.000	2.225	0.9110	2189818.	52667.	-0.003314	0.000	1.349E+12	0.000
0.000	3.337	0.8669	2892926.	51949.	-0.003289	0.000	1.346E+12	0.000
-107.	6079.	1657.0487	0.000	50460.	-0.003257	0.000	1.344E+12	0.000
-115.	5156.	1873.2702	0.000	48867.	-0.003218	0.000	1.342E+12	0.000
-123.	0.506.	2105.7538	4400.000	47177.	-0.003172	0.000	1.339E+12	0.000
-130.	1406.	2356.3458	4861616.	45385.	-0.003129	0.000	1.984E+12	0.000
-138.	3306.	2656.1803	5499930.	43497.	-0.003090	0.000	1.982E+12	0.000
-144.	5660.	2952.0638	6093306.	41528.	-0.003047	0.000	1.981E+12	0.000
-150.	8649.	3275.8328	6661205.	39485.	-0.003001	0.000	1.980E+12	0.000
-155.	16474.	3630.2663	7202205.	37376.	-0.002950	0.000	1.979E+12	0.000
-160.	24246.	4020.6756	7836000.	37376.	-0.002950	0.000	1.979E+12	0.000

SEK-1"
 A=1.0
 LATERAL
 RESISTANCE K
 = 5267

Res. X	Depth feet	Deflect. inches	Bending Moment in-lbs	Shear Force lbs	Slope radians	Total Stress psi*	Bending Stiffness lb-in^2	Soil p lb/in
-160.	4246.	4020.6756	8200132.	35206.	-0.002897	0.000	1.977E+12	0.000
-164.	6541.	4453.0521	8655455.	32983.	-0.002823	0.000	1.975E+12	0.000
-168.	3100.	4934.8241	9080782.	30715.	-0.002726	0.000	1.986E+12	0.000
-171.	4178.	5471.4006	9475558.	28410.	-0.002621	0.000	1.986E+12	0.000
-173.	9707.	6071.1737	9839328.	26074.	-0.002512	0.000	1.985E+12	0.000
-175.	9537.	6744.8011	10171740.	23716.	-0.002400	0.000	1.985E+12	0.000
-177.	3514.	7505.2782	10472543.	21343.	-0.002284	0.000	1.985E+12	0.000
-178.	1480.	8368.5829	10741597.	18963.	-0.002164	0.000	1.985E+12	0.000
-178.	3271.	9354.5362	10978869.	16586.	-0.002042	0.000	1.985E+12	0.000
-177.	8720.	10488.	11184439.	14219.	-0.001917	0.000	1.985E+12	0.000
-176.	7658.	11800.	11358507.	11871.	-0.001790	0.000	1.985E+12	0.000
-174.	9914.	13332.	11501386.	9550.9588	-0.001661	0.000	1.985E+12	0.000
-172.	3317.	15134.	11613517.	4799.1485	-0.001531	0.000	1.984E+12	0.000
-539.	3500.	55013.	0.000	-2117.1007	-0.001400	0.000	1.984E+12	0.000
-496.	7922.	59576.	0.000	-8319.0175	-0.001269	0.000	1.984E+12	0.000
-432.	3339.	61721.	0.000	-14067.	-0.001140	0.000	1.985E+12	0.000
-428.	3794.	73910.	11407406.	-19696.	-0.001012	0.000	1.985E+12	0.000
-414.	6409.	87749.	1181412.	-25070.	-0.000888	0.000	1.985E+12	0.000
-390.	4965.	103418.	10881520.	-30112.	-0.000768	0.000	1.985E+12	0.000
-364.	7650.	123683.	1071032.	-34851.	-0.000652	0.000	1.985E+12	0.000
-345.	2769.	154063.	1007533.	-39280.	-0.000541	0.000	1.986E+12	0.000
-318.	2374.	193120.	981531.	-43199.	-0.000436	0.000	1.986E+12	0.000
-268.	9742.	232045.	902871.	-46247.	-0.000357	0.000	1.977E+12	0.000
-187.	7885.	2473103.	842801.	-48254.	-0.000302	0.000	1.978E+12	0.000
-112.	8273.	253429.	7793964.	-49306.	-0.000252	0.000	1.980E+12	0.000
-44.	7368.	264172.	7139719.	-49497.	-0.000206	0.000	1.982E+12	0.000
16.	0235.	274815.	6477500.	-48929.	-0.000164	0.000	1.983E+12	0.000
69.	1936.	285509.	5818137.	-47701.	-0.000127	0.000	1.985E+12	0.000
114.	6980.	296202.	5171106.	-45917.	-9.482E-05	0.000	1.986E+12	0.000
152.	6255.	306895.	4544517.	-43675.	-6.629E-05	0.000	1.987E+12	0.000
183.	2057.	317589.	3945129.	-41072.	-4.170E-05	0.000	1.989E+12	0.000
206.	7876.	328282.	3378392.			0.000		

Pier 11aff.lp7o		Pier 11aff.lp7o	
47.837	-0.008815	2848510.	0.000
223.8162	338975.	0.000	1.994E+12
48.950	-0.008965	2358517.	0.000
234.8120	349669.	0.000	1.991E+12
230.0662	-0.008904	19103372.	0.000
240.3501	360362.	0.000	1.992E+12
51.175	-0.008672	1505063.	0.000
241.0397	371056.	0.000	1.993E+12
52.287	-0.008306	1142713.	0.000
237.5092	381749.	0.000	1.994E+12
53.400	-0.007837	8226693.	0.000
230.3892	392442.	0.000	1.994E+12
54.512	-0.007295	543733.	0.000
220.2980	403136.	0.000	1.994E+12
55.625	-0.006705	3040335.	0.000
207.8319	413829.	0.000	1.994E+12
56.738	-0.006087	101377.	0.000
193.5554	424522.	0.000	1.994E+12
57.850	-0.005460	-66784.	0.000
177.9937	435216.	0.000	1.994E+12
58.962	-0.004839	-203224.	0.000
161.6271	445909.	0.000	1.994E+12
60.075	-0.004236	-310857.	0.000
144.8870	456602.	0.000	1.994E+12
61.188	-0.003661	-392669.	0.000
128.1539	467296.	0.000	1.994E+12
62.300	-0.003121	-451640.	0.000
111.7564	477989.	0.000	1.994E+12
63.412	-0.002622	-490694.	0.000
95.9717	488682.	-512644.	0.000
64.525	-0.002166	-520153.	0.000
81.0274	499376.	0.000	1.994E+12
65.638	-0.001756	-515702.	0.000
67.1040	510069.	0.000	1.994E+12
66.750	-0.001393	-501568.	0.000
54.3376	520762.	0.000	1.994E+12
67.862	-0.001076	-479801.	0.000
42.8242	531436.	-452219.	0.000
68.975	-0.000803	-420403.	0.000
32.6232	542149.	-385693.	0.000
70.087	-0.000574	-342286.	0.000
23.7618	552842.	-292743.	0.000
16.2389	563536.	-240097.	0.000
71.200	-0.000385	-190604.	0.000
72.312	-0.000233	-143658.	0.000
48.7960	2793763.	0.000	1.994E+12
73.425	-0.000116	0.000	1.994E+12
34.4343	3958757.	0.000	1.994E+12
17.4023	7830897.	0.000	1.994E+12
74.537	-2.967E-05	0.000	1.994E+12
75.650	3.062E-05	0.000	1.994E+12
-17.6870	7711039.	0.000	1.994E+12
-26.6333	61945E-05	0.000	1.994E+12
-30.7262	4466338.	0.000	1.994E+12
-31.8366	9.293E-05	0.000	1.994E+12
-31.8366	4663394.	0.000	1.994E+12
-30.6409	444960E	0.000	1.994E+12
-82.325	8.062E-05	-22528.	0.000
-38198.	-2.081E-05	1492.0868	-9.229E-07
-35136.	-3.348E-06	3529.5640	2.270E-06
-31965.	1.096E-05	3148.0243	1.144E-06
-28751.	2.240E-05	2730.9514	2.990E-07
-25557.	3.127E-05	2305.1562	-3.019E-07
-22434.	3.785E-05	1888.1433	-6.968E-07
-19425.	4.242E-05	1492.0868	-9.229E-07
-16568.	4.526E-05	0.000	1.994E+12
-13888.	4.662E-05	0.000	1.994E+12
-11408.	4.674E-05	0.000	1.994E+12
-9141.3044	4.583E-05	0.000	1.994E+12
-7095.3226	4.411E-05	0.000	1.994E+12
-5272.7741	4.176E-05	0.000	1.994E+12
-3671.3726	3.893E-05	0.000	1.994E+12
-2284.7874	3.577E-05	0.000	1.994E+12
-1103.3180	3.242E-05	0.000	1.994E+12
-114.5408	2.896E-05	0.000	1.994E+12
696.0817	2.549E-05	0.000	1.994E+12
1344.6365	2.208E-05	0.000	1.994E+12
1848.2475	1.880E-05	0.000	1.994E+12
2224.6171	1.568E-05	0.000	1.994E+12
2491.6219	1.276E-05	0.000	1.994E+12
2925.7300	1.006E-05	0.000	1.994E+12
3481.2923	7.622E-06	0.000	1.994E+12
3827.3018	5.496E-06	0.000	1.994E+12
3825.4017	3.712E-06	0.000	1.994E+12
3529.5640	2.270E-06	0.000	1.994E+12
3148.0243	1.144E-06	0.000	1.994E+12
2730.9514	2.990E-07	0.000	1.994E+12
2305.1562	-3.019E-07	0.000	1.994E+12
1888.1433	-6.968E-07	0.000	1.994E+12
1492.0868	-9.229E-07	0.000	1.994E+12

* This analysis computed pile response using nonlinear moment-curvature relations.
Values of total stress due to combined axial and bending stresses are computed for elastic sections only and do not equal the actual stresses in concrete and steel.
Stresses in concrete and steel may be interpolated from the output for nonlinear bending properties relative to the magnitude of bending moment developed in the pile.

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Output Summary for Load Case No. 6:

Pile-head deflection = 1.0000000 inches
 Computed slope at pile head = -0.0033432 radians
 Maximum bending moment = 11629524. inch-lbs
 Maximum shear force = 52667. lbs
 Depth of maximum bending moment = 27.8125000 feet below pile head
 Depth of maximum shear force = 17.0000000 feet below pile head
 Number of iterations = 17
 Number of zero deflection points = 4

Pile-head deflection vs. Pile Length for Load Case 6

Boundary Condition Type 4, Deflection and Moment

Deflection = 1.00000 in
 Moment = 783600. in-lb
 Axial Load = 0. lb

Pile Length feet	Pile Head Deflection inches	Maximum Moment in-lbs	Maximum Shear lbs
111.2500	1.0000000	11629524.	52667.
105.6875	1.0000000	11686281.	51859.
100.1250	1.0000000	11541827.	51544.
94.5625	1.0000000	11696125.	52316.
89.0000	1.0000000	11622885.	52264.
83.4375	1.0000000	11658876.	52592.
77.8750	1.0000000	11668888.	51995.
72.3125	1.0000000	11603785.	52031.
66.7500	1.0000000	11593421.	52298.
61.1875	1.0000000	11673728.	52197.
55.6250	1.0000000	11468015.	-34030.
50.0625	1.0000000	10926863.	-63572.
44.5000	1.0000000	9023654.	-66867.
38.9375	1.0000000	5282115.	-48031.
33.3750	1.0000000	3246390.	-28544.
27.8125	1.0000000	2039742.	-17677.
22.2500	1.0000000	1435919.	11386.
16.6875	1.0000000	788231.	-8811.8996282
11.1250	1.0000000	783600.	-8237.6272468
11.1250	0.0000000	7.746642E+11	-2.901365E+11

Computed Values of Pile Loading and Deflection
 For Lateral Loading For Load Case Number 7

Pile-head conditions are Displacement and Moment (Loading Type 4)
 Displacement of pile head = 500000. inches
 Moment at pile head = 783600.0 in-lbs
 Axial load at pile head = 0.0 lbs

Depth Deflect. Bending Shear Slope Total Bending Soil

Res. X feet	Soil Spr. Es*h lb/inch	y inches	Distrib. Lat. Load lb/inch	Moment in-lbs	Force lbs	S radians	Stress psi*	Stiffness lb-in^2	P lb/in
0.000	0.00	1.5000	1.5000	783600.	68040.	-0.004975	0.000	1.354E+12	0.000
0.000	1.113	1.4336	1.4336	1691929.	68040.	-0.004963	0.000	1.354E+12	0.000
0.000	2.225	1.3675	1.3675	2600259.	68040.	-0.004942	0.000	1.347E+12	0.000
0.000	3.337	1.3017	1.3017	3508588.	67217.	-0.004911	0.000	1.344E+12	0.000
-123.2207	1263.7341	0.000	0.000	0.000	65512.	-0.004872	0.000	1.341E+12	0.000
-132.2863	1428.4031	0.000	0.000	0.000	63688.	-0.004824	0.000	1.338E+12	0.000
-140.8998	1605.4903	0.000	0.000	0.000	61753.	-0.004701	0.000	4.190E+11	0.000
-149.0448	1796.5086	0.000	0.000	0.000	59700.	-0.004580	0.000	1.980E+12	0.000
-158.5187	2022.9509	0.000	0.000	0.000	57535.	-0.004531	0.000	1.979E+12	0.000
-165.7698	2246.1055	0.000	0.000	0.000	55277.	-0.004477	0.000	1.977E+12	0.000
-172.4956	2489.1785	0.000	0.000	0.000	52933.	-0.004396	0.000	1.186E+12	0.000
-178.6704	2755.1250	0.000	0.000	0.000	50510.	-0.004289	0.000	1.185E+12	0.000
-184.3077	3046.1373	0.000	0.000	0.000	48016.	-0.004175	0.000	1.185E+12	0.000
-189.3923	3365.6833	0.000	0.000	0.000	45457.	-0.004053	0.000	1.185E+12	0.000
-193.9086	3717.8442	0.000	0.000	0.000	42842.	-0.003924	0.000	1.184E+12	0.000
-197.8408	4107.4516	0.000	0.000	0.000	40179.	-0.003788	0.000	1.184E+12	0.000
-201.1727	4540.2610	0.000	0.000	0.000	37475.	-0.003647	0.000	1.184E+12	0.000
-203.8876	5023.1750	0.000	0.000	0.000	34739.	-0.003500	0.000	1.184E+12	0.000
-205.9683	5564.5313	0.000	0.000	0.000	31980.	-0.003348	0.000	1.183E+12	0.000
-207.3975	6174.4789	0.000	0.000	0.000	29206.	-0.003190	0.000	1.183E+12	0.000
-208.1570	6865.4748	0.000	0.000	0.000	26427.	-0.003029	0.000	1.183E+12	0.000
-208.2250	7652.9332	0.000	0.000	0.000	23651.	-0.002863	0.000	1.183E+12	0.000
-207.38862	8556.1379	0.000	0.000	0.000	20889.	-0.002694	0.000	1.182E+12	0.000
-206.27075	9599.1576	0.000	0.000	0.000	18150.	-0.002521	0.000	1.182E+12	0.000
-204.10338	10813.2620	0.000	0.000	0.000	12226.	-0.002346	0.000	1.182E+12	0.000
-683.4697	41575.	0.000	0.000	0.000	3328.6771	-0.002169	0.000	1.182E+12	0.000
-649.4334	45785.	0.000	0.000	0.000	-4923.0640	-0.001992	0.000	1.182E+12	0.000
-586.7825	48491.	0.000	0.000	0.000	-12791.	-0.001815	0.000	1.182E+12	0.000
-591.9076	58042.	0.000	0.000	0.000					

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31.150	0.1131	15371250.	0.000	1.182E+12	0.000	1.182E+12	0.000	1.994E+12
-583.4010	68871.	0.000	0.000	0.000	0.000	0.000	0.000	0.000
32.262	15043772.	0.000	0.000	1.183E+12	0.000	1.183E+12	0.000	1.994E+12
-561.1102	81115.	0.000	0.000	0.000	0.000	0.000	0.000	0.000
33.375	14616291.	0.000	0.000	1.183E+12	0.000	1.183E+12	0.000	1.994E+12
-534.8125	96642.	0.000	0.000	0.000	0.000	0.000	0.000	0.000
34.487	14093495.	0.000	0.000	1.183E+12	0.000	1.183E+12	0.000	1.994E+12
-514.2209	119161.	0.000	0.000	0.000	0.000	0.000	0.000	0.000
35.600	0.0435	13479053.	0.000	1.183E+12	0.000	1.183E+12	0.000	1.994E+12
-481.7983	147983.	0.000	0.000	0.000	0.000	0.000	0.000	0.000
36.712	0.0313	12778743.	0.000	1.184E+12	0.000	1.184E+12	0.000	1.994E+12
-436.9464	186069.	0.000	0.000	0.000	0.000	0.000	0.000	0.000
37.825	0.0212	12000560.	0.000	1.184E+12	0.000	1.184E+12	0.000	1.994E+12
-378.7871	238995.	0.000	0.000	0.000	0.000	0.000	0.000	0.000
38.938	0.0128	11154869.	0.000	1.185E+12	0.000	1.185E+12	0.000	1.994E+12
-242.4831	253425.	0.000	0.000	0.000	0.000	0.000	0.000	0.000
40.050	0.006066	10265962.	0.000	1.185E+12	0.000	1.185E+12	0.000	1.994E+12
-120.0183	264122.	0.000	0.000	0.000	0.000	0.000	0.000	0.000
41.163	0.00903	9353664.	0.000	1.186E+12	0.000	1.186E+12	0.000	1.994E+12
-18.5862	274815.	0.000	0.000	0.000	0.000	0.000	0.000	0.000
42.275	-0.002854	8442054.	0.000	1.977E+12	0.000	1.977E+12	0.000	1.994E+12
61.0438	285509.	0.000	0.000	0.000	0.000	0.000	0.000	0.000
43.387	-0.005850	7539324.	0.000	1.979E+12	0.000	1.979E+12	0.000	1.994E+12
129.8067	296202.	0.000	0.000	0.000	0.000	0.000	0.000	0.000
44.500	-0.008168	6659728.	0.000	1.981E+12	0.000	1.981E+12	0.000	1.994E+12
187.7615	306895.	0.000	0.000	0.000	0.000	0.000	0.000	0.000
45.613	-0.009886	5813595.	0.000	1.983E+12	0.000	1.983E+12	0.000	1.994E+12
235.1755	317389.	0.000	0.000	0.000	0.000	0.000	0.000	0.000
46.725	-0.0111	5009376.	0.000	1.985E+12	0.000	1.985E+12	0.000	1.994E+12
272.4957	328282.	0.000	0.000	0.000	0.000	0.000	0.000	0.000
47.837	-0.0118	4253722.	0.000	1.987E+12	0.000	1.987E+12	0.000	1.994E+12
300.3073	338975.	0.000	0.000	0.000	0.000	0.000	0.000	0.000
48.950	-0.0122	3551589.	0.000	1.988E+12	0.000	1.988E+12	0.000	1.994E+12
319.3207	349669.	0.000	0.000	0.000	0.000	0.000	0.000	0.000
50.062	-0.0122	2906366.	0.000	1.990E+12	0.000	1.990E+12	0.000	1.994E+12
330.5246	360362.	0.000	0.000	0.000	0.000	0.000	0.000	0.000
334.1665	371036.	0.000	0.000	1.991E+12	0.000	1.991E+12	0.000	1.994E+12
331.7269	381749.	0.000	0.000	0.000	0.000	0.000	0.000	0.000
332.8951	392442.	0.000	0.000	1.992E+12	0.000	1.992E+12	0.000	1.994E+12
311.5316	403138.	0.000	0.000	0.000	0.000	0.000	0.000	0.000
295.55625	-0.009534	361171.	0.000	1.994E+12	0.000	1.994E+12	0.000	1.994E+12
276.6738	413823.	0.000	0.000	0.000	0.000	0.000	0.000	0.000
255.75650	-0.0098701	259421.	0.000	1.994E+12	0.000	1.994E+12	0.000	1.994E+12
233.47162	431264.	0.000	0.000	0.000	0.000	0.000	0.000	0.000
210.3199	456605343	0.000	0.000	1.994E+12	0.000	1.994E+12	0.000	1.994E+12
187.0212	467296.	0.000	0.000	0.000	0.000	0.000	0.000	0.000
164.0681	-0.004581	587340.	0.000	1.994E+12	0.000	1.994E+12	0.000	1.994E+12
141.6956	-0.003871	652551.	0.000	0.000	0.000	0.000	0.000	0.000
120.4279	499376.	0.000	0.000	1.994E+12	0.000	1.994E+12	0.000	1.994E+12
65.638	-0.002630	-711003.	0.000	0.000	0.000	0.000	0.000	0.000

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100.4815	510069.	0.000	0.000	503.8918	3.702E-05	503.8918	3.702E-05	1.994E+12
66.750	-0.002104	-711589.	0.000	0.000	0.000	0.000	0.000	0.000
82.0698	520762.	0.000	0.000	1487.9025	3.230E-05	1487.9025	3.230E-05	1.994E+12
67.862	-0.001642	-697549.	0.000	0.000	0.000	0.000	0.000	0.000
65.3475	531456.	0.000	0.000	2260.6273	2.772E-05	2260.6273	2.772E-05	1.994E+12
68.975	-0.001241	-671862.	0.000	0.000	0.000	0.000	0.000	0.000
50.4165	542149.	0.000	0.000	2846.3453	2.333E-05	2846.3453	2.333E-05	1.994E+12
70.087	-0.000901	-637190.	0.000	0.000	0.000	0.000	0.000	0.000
37.3315	552842.	0.000	0.000	3269.7913	1.921E-05	3269.7913	1.921E-05	1.994E+12
71.200	-0.000618	-595865.	0.000	0.000	0.000	0.000	0.000	0.000
26.1061	563536.	0.000	0.000	3864.5944	1.537E-05	3864.5944	1.537E-05	1.994E+12
63.0030	2164006.	0.000	0.000	4592.8307	1.188E-05	4592.8307	1.188E-05	1.994E+12
46.0961	2957847.	0.000	0.000	5080.8731	8.801E-06	5080.8731	8.801E-06	1.994E+12
74.537	-7.147E-05	-427258.	0.000	0.000	0.000	0.000	0.000	0.000
27.0189	5047143.	-357021.	0.000	5150.5693	6.175E-06	5150.5693	6.175E-06	1.994E+12
75.650	2.693E-05	0.000	0.000	8333.7695	4.010E-06	8333.7695	4.010E-06	1.994E+12
-16.5775	8218726.	0.000	0.000	0.000	0.000	0.000	0.000	0.000
76.763	9.341E-05	-289738.	0.000	0.000	0.000	0.000	0.000	0.000
-30.8831	4413775.	0.000	0.000	4380.7172	2.277E-06	4380.7172	2.277E-06	1.994E+12
77.875	-0.000134	-227959.	0.000	0.000	0.000	0.000	0.000	0.000
-36.9899	3685347.	0.000	0.000	3868.9330	9.353E-07	3868.9330	9.353E-07	1.994E+12
-39.6819	3435438.	-172773.	0.000	3335.1152	-6.037E-08	3335.1152	-6.037E-08	1.994E+12
80.100	0.000159	-124659.	0.000	2802.6806	-7.580E-07	2802.6806	-7.580E-07	1.994E+12
-40.2908	3383589.	0.000	0.000	0.000	0.000	0.000	0.000	0.000
81.212	0.000153	-83725.	0.000	2287.9439	-1.205E-06	2287.9439	-1.205E-06	1.994E+12
-39.4747	3453597.	0.000	0.000	1802.6268	-1.448E-06	1802.6268	-1.448E-06	1.994E+12
-37.6394	3622045.	0.000	0.000	1355.1580	-1.529E-06	1355.1580	-1.529E-06	1.994E+12
-35.0673	3887776.	0.000	0.000	0.000	0.000	0.000	0.000	0.000
84.550	-0.000100	-1697.1110	0.000	951.4617	-1.489E-06	951.4617	-1.489E-06	1.994E+12
-31.5692	4264394.	0.000	0.000	595.5012	-1.365E-06	595.5012	-1.365E-06	1.994E+12
85.663	7.1539E-05	13545.	0.000	289.7177	-1.187E-06	289.7177	-1.187E-06	1.994E+12
-28.5096	4762188.	0.000	0.000	35.4681	-9.830E-07	35.4681	-9.830E-07	1.994E+12
-24.8178	5459690.	0.000	0.000	0.000	0.000	0.000	0.000	0.000
87.887	4.534E-05	29445.	0.000	-166.3646	-7.760E-07	-166.3646	-7.760E-07	1.994E+12
-20.5825	6494352.	0.000	0.000	-314.0465	-5.838E-07	-314.0465	-5.838E-07	1.994E+12
-17.0571	7774949.	0.000	0.000	0.000	0.000	0.000	0.000	0.000
13.13925	1031599E-05	30392.	0.000	-398.4986	-4.198E-07	-398.4986	-4.198E-07	1.994E+12
-8.98425	1517887E-06	0.000	0.000	-384.2022	-2.913E-07	-384.2022	-2.913E-07	1.994E+12
-8.98425	3173645E-06	0.000	0.000	0.000	0.000	0.000	0.000	0.000
-3.6571	3723966E-06	0.000	0.000	-291.1996	-1.972E-07	-291.1996	-1.972E-07	1.994E+12
5.8085	-4534580106E-06	0.000	0.000	-174.5214	-1.292E-07	-174.5214	-1.292E-07	1.994E+12
8.1241	56778897E-06	0.000	0.000	0.000	0.000	0.000	0.000	0.000
91.675	781572E-06	8585.4984	0.000	-106.8426	-7.668E-08	-106.8426	-7.668E-08	1.994E+12
9.3558	14571113.	0.000	0.000	-95.8941	-3.376E-08	-95.8941	-3.376E-08	1.994E+12
96.788	9.912E-06	7089.3480	0.000	0.000	0.000	0.000	0.000	0.000
0.7833	1054980.	0.000	0.000	-84.2294	5.975E-10	-84.2294	5.975E-10	1.994E+12
97.900	1.063E-05	5732.8022	0.000	0.000	0.000	0.000	0.000	0.000
0.8569	1077257.	0.000	0.000	-72.3370	2.742E-08	-72.3370	2.742E-08	1.994E+12
99.012	-1.081E-05	4528.9747	0.000	0.000	0.000	0.000	0.000	0.000
0.8906	1099535.	0.000	0.000	0.000	0.000	0.000	0.000	0.000
100.125	-1.060E-05	3483.8775	0.000	0.000	0.000	0.000	0.000	0.000
0.8910	1121813.	0.000	0.000	0.000	0.000	0.000	0.000	0.000

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Res. X	Soil Spr. Y	Res. X	Soil Spr. Y
101.237	-1.008E-05	2597.5761	0.000
0.8640	1144091.	0.000	0.000
102.350	-9.327E-06	1865.2544	0.000
0.8149	1166369.	0.000	0.000
103.462	-8.407E-06	1278.1704	0.000
0.7485	1188646.	824.4885	0.000
104.575	-7.372E-06	824.4885	0.000
0.6687	1210924.	489.9781	0.000
105.688	-6.263E-06	258.5800	0.000
0.5786	1233202.	112.8413	0.000
106.800	-5.111E-06	34.2295	0.000
0.4806	1255480.	0.000	0.000
107.913	-3.935E-06	34.2295	0.000
0.3766	1277758.	0.000	0.000
109.025	-2.750E-06	34.2295	0.000
0.2678	1300036.	3.3378	0.000
110.137	-1.561E-06	0.000	0.000
0.1546	1322313.	0.000	0.000
111.250	-3.719E-07	0.000	0.000
0.0375	672296.	0.000	0.000

Pier 11a1ff. 1p7o		Pier 11a1ff. 1p7o	
Res. X	Soil Spr. Y	Res. X	Soil Spr. Y
-60.6226	4.778E-08	82566.	-0.006600
-49.4159	6.272E-08	82566.	-0.006587
-38.9800	7.324E-08	82566.	-0.006563
-29.5203	8.028E-08	81660.	-0.006528
-21.1951	8.468E-08	79783.	-0.006482
-14.1250	8.719E-08	77775.	-0.006357
-8.4026	8.843E-08	75644.	-0.006142
-4.1013	8.893E-08	73382.	-0.005999
-1.2820	8.905E-08	70996.	-0.005919
0.0000	8.906E-08	68506.	-0.005810
		65920.	-0.005691
		63244.	-0.005562
		60486.	-0.005423
		57655.	-0.005275
		54758.	-0.005118
		51805.	-0.004953
		48803.	-0.004781
		45761.	-0.004600
		42689.	-0.004413
		39595.	-0.004219
		36491.	-0.004020
		33384.	-0.003814
		30286.	-0.003604
		27208.	-0.003389
		20288.	-0.003170
		9672.0969	-0.002948
		-405.3678	-0.002724
		-10202.	-0.002500
		-20091.	-0.002278
		-29858.	-0.002059
		-39354.	-0.001845
		-48579.	-0.001636

Computed Values of Pile Loading and Deflection for Lateral Loading for Load Case Number 8	
Depth	26
Soil Deflect.	1.500000 inches
Soil Spr. Y	-0.0049750 radians
Distrib. Moment	15726199. inch-lbs
Lat. Load	27.8125000 feet below pile head
Max. Bending Moment	41.1625000 feet below pile head
Max. Shear Force	
Number of Iterations	4
Number of zero deflection points	4

Computed Values of Pile Loading and Deflection for Lateral Loading for Load Case Number 8	
Displacement of pile head	2.000000 inches
Moment at pile head	783600.0 in-lbs
Axial load at pile head	0.0 lbs

Res. X	Soil Spr. Y	Distrib. Moment	Lat. Load	Soil Deflect.	Slope	Total Stress	Bending Stiffness
feet	inches	in-lbs	lbs	radians	psi*	lb-in^2	lb/in
101.237	-1.008E-05	2597.5761	0.000	1.994E+12	0.000	1.994E+12	0.000
102.350	-9.327E-06	1865.2544	0.000	1.994E+12	0.000	1.994E+12	0.000
103.462	-8.407E-06	1278.1704	0.000	1.994E+12	0.000	1.994E+12	0.000
104.575	-7.372E-06	824.4885	0.000	1.994E+12	0.000	1.994E+12	0.000
105.688	-6.263E-06	489.9781	0.000	1.994E+12	0.000	1.994E+12	0.000
106.800	-5.111E-06	258.5800	0.000	1.994E+12	0.000	1.994E+12	0.000
107.913	-3.935E-06	112.8413	0.000	1.994E+12	0.000	1.994E+12	0.000
109.025	-2.750E-06	34.2295	0.000	1.994E+12	0.000	1.994E+12	0.000
110.137	-1.561E-06	3.3378	0.000	1.994E+12	0.000	1.994E+12	0.000
111.250	-3.719E-07	0.000	0.000	1.994E+12	0.000	1.994E+12	0.000

* This analysis computed pile response using nonlinear moment-curvature relationships.
 Values of total stress due to combined axial and bending stresses are computed only for elastic sections only and do not equal the actual stresses in concrete and steel.
 Stresses in concrete and steel may be interpolated from the output for nonlinear bending properties relative to the magnitude of bending moment developed in the pile.

Pier 11aff.1p70		Pier 11aff.1p70	
-682.2933	99301.	0.000	0.000
35.600	0.0713	17433060.	0.000
-650.7096	121916.	0.000	0.000
36.712	0.0534	16607764.	0.000
-604.1089	150999.	0.000	0.000
37.825	0.0381	15674801.	0.000
-541.3834	189839.	0.000	0.000
38.938	0.0251	14645352.	0.000
-460.6407	245040.	0.000	0.000
40.050	0.0143	13333806.	0.000
-283.4616	264122.	0.000	0.000
41.163	0.005597	12371741.	0.000
-115.2206	274815.	0.000	0.000
42.275	-0.001271	11189142.	0.000
27.1803	285509.	0.000	0.000
43.387	-0.006456	10011386.	0.000
143.2370	296202.	0.000	0.000
232.9968	306895.	0.000	0.000
45.613	-0.0125	7748456.	0.000
297.3533	317589.	0.000	0.000
46.725	-0.0142	6690749.	0.000
348.3335	328282.	0.000	0.000
386.6985	338975.	0.000	0.000
48.950	-0.0158	4768414.	0.000
413.3636	349669.	0.000	0.000
429.3600	360362.	0.000	0.000
435.7971	371056.	0.000	0.000
433.8290	381749.	0.000	0.000
424.6265	392442.	0.000	0.000
409.3474	403136.	0.000	0.000
389.1176	413829.	0.000	0.000
365.0080	424522.	0.000	0.000
338.0227	435216.	0.000	0.000
309.0873	445909.	0.000	0.000
279.0401	456602.	0.000	0.000
248.6295	467296.	0.000	0.000
218.4970	477989.	0.000	0.000
189.2087	488682.	0.000	0.000
161.2172	499376.	0.000	0.000
134.8074	510070.	0.000	0.000
110.6750	520764.	0.000	0.000
88.3655	531458.	0.000	0.000
68.9875	542152.	0.000	0.000
68.4971	542149.	0.000	0.000
70.087	-0.001232	832570.	0.000
51.0194	552842.	0.000	0.000
71.200	-0.000852	779504.	0.000
35.9546	563536.	0.000	0.000
72.312	-0.000541	720031.	0.000
74.3183	183332.	0.000	0.000
73.425	-0.000295	647311.	0.000
54.8573	2482950.	0.000	0.000
74.537	-0.000107	564816.	0.000
32.9584	4128076.	0.000	0.000
75.650	3.129E-05	476446.	0.000
-17.9257	7647408.	0.000	0.000
76.763	0.000127	391271.	0.000
-35.9730	3793818.	0.000	0.000
77.875	0.000187	312507.	0.000
-43.7001	3121376.	0.000	0.000
-47.3301	2881385.	0.000	0.000
78.987	0.000219	241531.	0.000
80.100	0.000230	178991.	0.000
-48.4784	2812805.	0.000	0.000
81.212	0.000225	125091.	0.000
-47.9253	2845041.	0.000	0.000
82.325	0.000209	79732.	0.000
83.438	0.000185	42597.	0.000
-43.4647	3136669.	0.000	0.000
84.550	0.000158	13208.	0.000
-40.1264	3397458.	0.000	0.000
85.663	0.000129	9028.7164	0.000
-36.3186	3753469.	0.000	0.000
86.775	0.000101	24793.	0.000
-32.1904	4234591.	0.000	0.000
87.887	7.601E-05	34820.	0.000
-27.8577	4892864.	0.000	0.000
89.000	5.365E-05	39882.	0.000
-23.4025	5823792.	0.000	0.000
90.112	3.485E-05	40774.	0.000
-18.8605	7225257.	0.000	0.000
91.225	1.970E-05	38304.	0.000
-14.1770	9609633.	0.000	0.000
92.337	7.966E-06	33308.	0.000
-9.0123	15104134.	0.000	0.000
93.450	7.867E-07	26705.	0.000
2.8533	48420300.	0.000	0.000
94.562	7.152E-06	20611.	0.000
8.5513	15962005.	0.000	0.000
95.675	1.166E-05	16040.	0.000
10.9224	12489341.	0.000	0.000
96.788	1.476E-05	13417.	0.000
1.1668	10349801.	0.000	0.000
97.900	1.165E-05	11001.	0.000
1.3439	1077277.	0.000	0.000
99.012	1.756E-05	8823.1017	0.000
1.4464	1099535.	0.000	0.000
100.12	1.619E-05	6906.7762	0.000
1.4656	1121613.	0.000	0.000
101.23	1.461E-05	5233.2177	0.000
1.4705	11406231E-05	3623.0000	0.000
1.4162	1166369.	0.000	0.000
1.4103	462.480E-05	2733.3130	0.000
1.3362	1188646.	0.000	0.000
104.575	-1.334E-05	1820.9553	0.000
3634.4256	3.127E-05	832570.	0.000
4214.9772	2.587E-05	779504.	0.000
4951.0493	2.085E-05	720031.	0.000
5813.2968	1.628E-05	647311.	0.000
6399.4668	1.222E-05	564816.	0.000
6499.8099	8.733E-06	476446.	0.000
6140.0360	5.828E-06	391271.	0.000
5608.2183	3.472E-06	312507.	0.000
5000.5922	1.617E-06	241531.	0.000
4361.0708	2.095E-07	178991.	0.000
3717.5760	-8.084E-07	125091.	0.000
3089.6553	-1.494E-06	79732.	0.000
2491.5095	-1.904E-06	42597.	0.000
1933.5395	-2.090E-06	13208.	0.000
1423.2695	-2.104E-06	9028.7164	0.000
965.9719	-1.991E-06	24793.	0.000
565.1509	-1.792E-06	34820.	0.000
222.9890	-1.542E-06	39882.	0.000
-59.1168	-1.272E-06	40774.	0.000
-279.6421	-1.007E-06	38304.	0.000
-434.4304	-7.671E-07	33308.	0.000
-475.5417	-5.662E-07	26705.	0.000
-399.4158	-4.078E-07	20611.	0.000
-269.4285	-2.851E-07	16040.	0.000
-188.7333	-1.865E-07	13417.	0.000
-171.9746	-1.048E-07	11001.	0.000
-153.3494	-3.838E-08	8823.1017	0.000
-133.7784	1.429E-08	6906.7762	0.000
-114.0345	5.500E-08	5233.2177	0.000
-94.7530	8.551E-08	3623.0000	0.000
-76.4457	1.076E-07	2733.3130	0.000
-59.5161	1.228E-07	1820.9553	0.000

Pier 11aiff.jp7o		Pier 11aiff.jp7o		Pier 11aiff.jp7o				
Res. X	Soil Spr. y	Depth Deflect. in-lbs	Bending Moment in-lbs	Shear Force lbs	Slope radians	Total Stress psi*	Bending Stiffness lb-in ²	Soil p
1.2099	1210924.	0.000	0.000	0.000	1.994E+12	0.000	1.994E+12	0.000
105.688	-1.162E+05	1134.2337	-44.2758	1.327E-07	0.000	1.994E+12	0.000	1.994E+12
1.0733	1233202.	0.000	0.000	0.000	1.994E+12	0.000	1.994E+12	0.000
106.800	-9.797E+06	638.7922	-30.9618	1.386E-07	0.000	1.994E+12	0.000	1.994E+12
0.9213	1255480.	0.000	0.000	0.000	1.994E+12	0.000	1.994E+12	0.000
107.913	-7.918E+06	307.5528	-19.7533	1.418E-07	0.000	1.994E+12	0.000	1.994E+12
0.7579	1277758.	0.000	0.000	0.000	1.994E+12	0.000	1.994E+12	0.000
109.025	-6.012E+06	111.3796	-10.7869	1.432E-07	0.000	1.994E+12	0.000	1.994E+12
0.5854	1300036.	0.000	0.000	0.000	1.994E+12	0.000	1.994E+12	0.000
110.137	-4.095E+06	19.5421	-4.1715	1.436E-07	0.000	1.994E+12	0.000	1.994E+12
0.4056	1322313.	0.000	0.000	0.000	1.994E+12	0.000	1.994E+12	0.000
111.250	-2.177E+06	0.000	0.000	1.437E-07	0.000	1.994E+12	0.000	1.994E+12
0.2193	6722296.	0.000	0.000	0.000	1.994E+12	0.000	1.994E+12	0.000

* This analysis computed pile response using nonlinear moment-curvature relationships.
Values of total stress due to combined axial and bending stresses are computed only for elastic sections only and do not equal the actual stresses in concrete and steel.
Stresses in concrete and steel may be interpolated from the output for nonlinear bending properties relative to the magnitude of bending moment developed in the pile.

output summary for Load Case No. 8:

Pile-head deflection = 2.000000 inches
Computed slope at pile head = -0.0066004 radians
Maximum bending moment = 19799712. inch-lbs
Maximum shear force = -88403. lbs
Depth of maximum bending moment = 28.9250000 feet below pile head
Depth of maximum shear force = 42.2750000 feet below pile head
Number of iterations = 23
Number of zero deflection points = 3

Computed Values of Pile Loading and Deflection
for Lateral Loading for Load Case Number 9

Pile-head conditions are Shear and Moment (Loading Type 1)

Shear force at pile head	=	13600.0 lbs
Applied moment at pile head	=	5499600.0 in-lbs
AXIAL thrust load on pile head	=	0.0 lbs

Res. X	Soil Spr. y	Depth Deflect. in-lbs	Bending Moment in-lbs	Shear Force lbs	Slope radians	Total Stress psi*	Bending Stiffness lb-in ²	Soil p
0.000	0.3540	5499600.	13600.	-0.002118	0.000	1.337E+12	0.000	1.337E+12
0.000	1.113	0.000	0.000	-0.002062	0.000	1.337E+12	0.000	1.337E+12
0.000	2.225	0.000	0.000	-0.002001	0.000	1.199E+12	0.000	1.199E+12
0.000	0.000	0.000	0.000					

Pier 11aff, lp70				Pier 11aff, lp70			
62.6082	242735.	0.000	1.994E+12	-74028.	1639.5537	7.129E-07	0.000
38.938	-0.004227	2464817.	0.000	0.000	1422.9244	2.860E-07	0.000
80.2457	253429.	0.000	1.991E+12	-53499.	1190.4602	-1.372E-08	0.000
40.050	-0.004790	2145638.	0.000	0.000	958.7240	-2.071E-07	0.000
94.7738	264122.	0.000	1.992E+12	-36036.	738.2154	-3.147E-07	0.000
41.163	-0.005161	1843349.	0.000	0.000	535.9097	-3.563E-07	0.000
106.2513	274815.	0.000	1.993E+12	-21713.	356.3844	-3.501E-07	0.000
42.275	-0.005368	1559997.	0.000	0.000	202.4443	-3.120E-07	0.000
114.7963	285509.	0.000	1.994E+12	-0.000	75.5337	-2.558E-07	0.000
120.5761	296202.	0.000	1.994E+12	-10438.	-23.9256	-1.928E-07	0.000
44.500	-0.005385	1055701.	0.000	0.000	-96.1236	-1.320E-07	0.000
123.7971	306895.	0.000	1.994E+12	-2003.1250	-140.7550	-7.977E-08	0.000
45.613	-0.005242	836361.	0.000	0.000	-147.9145	-4.013E-08	0.000
124.6945	317589.	0.000	1.994E+12	3870.9484	-123.8549	-1.371E-08	0.000
46.725	-0.005023	639245.	0.000	0.000	-91.3426	1.643E-09	0.000
123.5235	328282.	0.000	1.994E+12	7512.3393	-59.4702	8.830E-09	0.000
47.837	-0.004748	464143.	0.000	0.000	-31.5910	1.070E-08	0.000
120.5519	338975.	0.000	1.994E+12	9276.2099	-11.2332	9.748E-09	0.000
48.950	-0.004431	310526.	0.000	0.000	0.2519	7.791E-09	0.000
116.0523	349669.	0.000	1.994E+12	9529.0888	4.6392	5.857E-09	0.000
50.062	-0.004086	177592.	0.000	0.000	3.6861	4.337E-09	0.000
110.2956	360362.	0.000	1.994E+12	8637.3952	2.0230	3.147E-09	0.000
103.5455	371056.	0.000	1.994E+12	6962.5876	1.9014	2.138E-09	0.000
52.287	-0.003359	381749.	0.000	0.000	1.7463	1.298E-09	0.000
96.0533	381749.	0.000	1.994E+12	6289.0571	1.5688	6.150E-10	0.000
53.400	-0.002995	53.400	0.000	0.000	1.3786	7.193E-11	0.000
88.0543	392442.	0.000	1.994E+12	5689.0571	1.1835	-3.479E-10	0.000
54.512	-0.002641	170221.	0.000	0.000	0.9901	-6.620E-10	0.000
79.7849	403136.	0.000	1.994E+12	5151.4685	0.8037	-8.875E-10	0.000
55.625	-0.002303	218015.	0.000	0.000	0.6283	-1.041E-09	0.000
71.3801	413829.	0.000	1.994E+12	4689.0571	0.4671	-1.139E-09	0.000
56.738	-0.001983	253088.	0.000	0.000	0.3222	-1.195E-09	0.000
63.0722	424522.	0.000	1.994E+12	4229.0571	0.2222	-1.195E-09	0.000
57.850	-0.001687	276920.	0.000	0.000	0.1071	1.066E-07	0.000
54.9904	435216.	0.000	1.994E+12	3817.49	107.913	1.066E-07	0.000
58.962	-0.001415	290952.	0.000	0.000	-15.2500	8939410.	-74028.
47.2602	445903.	0.000	1.994E+12	3515.4685	-17.4537	2.898E-05	0.000
39.9838	456602.	0.000	1.994E+12	3262.3324	-17.2038	7924201.	-53499.
60.075	-0.001169	296560.	0.000	0.000	75.650	3.041E-05	0.000
33.2414	-0.000950	293043.	0.000	0.000	-17.6223	7736007.	-36036.
82.300	-0.000757	287601.	0.000	0.000	76.763	2.862E-05	0.000
27.0919	477969.	0.000	1.994E+12	2622.8008	-17.0947	7974766.	-21713.
63.412	-0.000589	273531.	0.000	0.000	77.875	2.488E-05	0.000
21.5741	486682.	0.000	1.994E+12	2469.0571	-15.9403	8552306.	-10438.
64.525	-0.000447	259216.	0.000	0.000	78.987	2.072E-05	0.000
16.7089	493576.	0.000	1.994E+12	2315.4685	-14.3677	9488410.	-2003.1250
12.5004	510069.	0.000	1.994E+12	2161.466	80.100	1.557E-05	0.000
8.9979	520760.	0.000	1.994E+12	2003.1250	-12.5275	1.0882165.	0.000
5.9965	531956.	0.000	1.994E+12	1870.9484	81.212	1.087E-05	0.000
67.862	541956.	0.000	1.994E+12	1712.3393	-10.5347	12940694.	0.000
68.975	552149.	0.000	1.994E+12	1572.3124	-10.5347	12940694.	0.000
3.6405	562149.	0.000	1.994E+12	1429.0571	82.325	7.039E-06	0.000
70.087	572643.	0.000	1.994E+12	1272.584	-8.4781	16079783.	0.000
1.8232	582643.	0.000	1.994E+12	1129.0571	83.438	4.039E-06	0.000
71.200	1.157E-05	0.000	1.994E+12	1000.000	-6.4222	2127502.	0.000
0.4885	1.157E-05	0.000	1.994E+12	889.0571	84.550	1.891E-06	0.000
72.312	9.948E-06	0.000	1.994E+12	789.0571	-4.3940	31025389.	0.000
40.0790	13525740.	0.000	1.994E+12	689.0571	-2.2923	59471039.	0.000

MOMENT FIXITY @ 72.31

EL 7.25-72.31 = -65.06

-0.0102 1277758. 0.000
 109.025 9.041E-08 -2.3390 0.1953 -1.222E-09 0.000 1.994E+12
 -0.008804 1300036. 0.000
 110.137 7.400E-08 -0.5164 0.0876 -1.231E-09 0.000 1.994E+12
 -0.007329 1322313. 0.000
 111.250 5.754E-08 0.000 -1.233E-09 0.000 1.994E+12
 -0.005795 672296. 0.000

* This analysis computed pile response using nonlinear moment-curvature relationships.
 Values of total stress due to combined axial and bending stresses are computed only for elastic sections only and do not equal the actual stresses in concrete and steel.
 Stresses in concrete and steel may be interpolated from the output for nonlinear bending properties relative to the magnitude of bending moment developed in the pile.

Output Summary for Load Case No. 9:

Pile-head deflection = 0.3539704 inches
 Computed slope at pile head = -0.0021179 radians
 Maximum bending moment = 7025520. inch-lbs
 Maximum shear force = -26560. lbs
 Depth of maximum bending moment = 15.5750000 feet below pile head
 Depth of maximum shear force = 34.4875000 feet below pile head
 Number of iterations = 39
 Number of zero deflection points = 4

Pile-head Deflection vs. Pile Length for Load Case 9

Boundary Condition Type 1, Shear and Moment

Shear Moment = 13600. lb
 Axial Load = 5499600. in-lb

Pile Length feet	Pile Head Deflection inches	Maximum Moment in-lbs	Maximum Shear lbs
111.2500	0.3539704	7025520.	-26560.
105.6875	0.3587023	7134252.	-27299.
100.1250	0.3682543	7106117.	-26907.
94.5625	0.3585636	7087886.	-27006.
89.0000	0.3641047	7063670.	-26773.
83.4375	0.3663132	7041701.	-26650.
77.8750	0.3642149	7109677.	-27410.
72.3125	0.3639302	7078240.	-26806.
66.7500	0.3561247	7039086.	-26392.
61.1875	0.3375334	7029396.	-26835.
55.6250	0.3736279	7026583.	-26816.
50.0625	0.4203716	7038352.	-32135.
44.5000	0.4673460	6864307.	-43185.
38.9375	1.9170195	6634521.	-41991.
33.3750	7.3014206	6431518.	-43664.
27.8125			

Computed Values of Pile Loading and Deflection for Lateral Loading for Load Case Number 10

Pile-head conditions are Shear and Moment (Loading Type 1)

Shear force at pile head = 9900.0 lbs
 Applied moment at pile head = 783600.0 in-lbs
 Axial thrust load on pile head = 0.0 lbs

Res. X	Depth, feet	Soil spr. Est ^h lb/inch	Deflect. Lat. Load lb/inch	Bending Moment in-lbs	Shear Force lbs	Slope S radians	Total Stress psi*	Bending Stiffness lb-in ²	Soil P lb/in
0.000	0.000	0.0780	0.000	783600.	9900.0000	-0.000377	0.000	1.354E+12	0.000
0.000	1.113	0.000	0.0730	915765.	9900.0000	-0.000369	0.000	1.354E+12	0.000
0.000	2.225	0.000	0.0661	1047930.	9900.0000	-0.000359	0.000	1.352E+12	0.000
0.000	3.337	0.000	0.0634	1180095.	9599.6620	-0.000348	0.000	1.352E+12	0.000
-44.9945	4.450	9479.4161	0.000	1304241.	8979.3960	-0.000336	0.000	1.351E+12	0.000
-47.9293	5.562	10883.	0.0544	1419845.	8321.4260	-0.000323	0.000	1.351E+12	0.000
-50.6430	6.675	12430.	0.0502	1526423.	7628.7001	-0.000308	0.000	1.351E+12	0.000
-53.1362	7.788	14137.	0.0462	1623551.	6900.0749	-0.000295	0.000	1.993E+12	0.000
-56.0212	8.900	16201.	0.0423	1710655.	6138.6655	-0.000284	0.000	1.992E+12	0.000
-58.0476	10.012	18322.	0.0386	1787434.	5351.8782	-0.000272	0.000	1.992E+12	0.000
-59.8231	11.125	20700.	0.0350	1853550.	4543.1035	-0.000260	0.000	1.992E+12	0.000
-61.3416	12.237	23360.	0.0316	1908734.	3715.8108	-0.000247	0.000	1.992E+12	0.000
-62.5973	13.350	26444.	0.0284	1952762.	2873.5493	-0.000235	0.000	1.992E+12	0.000
-63.5842	14.462	29863.	0.0254	1985058.	2019.9504	-0.000221	0.000	1.992E+12	0.000
-64.2958	15.575	33633.	0.0225	2006695.	1158.7311	-0.000208	0.000	1.992E+12	0.000
-64.7258	16.688	37801.	0.0198	2016396.	293.7008	-0.000194	0.000	1.992E+12	0.000
-64.8668	17.800	43682.	0.0173	2014537.	-571.2297	-0.000181	0.000	1.992E+12	0.000
-64.7108	18.912	49882.	0.0150	2001144.	-1432.0335	-0.000167	0.000	1.992E+12	0.000
-64.2485	20.025	57207.	0.0128	1976302.	-2284.5460	-0.000154	0.000	1.992E+12	0.000
-63.4687	21.137	65955.	0.0109	1940147.	-3124.4332	-0.000141	0.000	1.992E+12	0.000
-62.3571	22.250	76533.	0.009081	1892879.	-3947.1427	-0.000128	0.000	1.992E+12	0.000
-60.8953	23.362	89520.	0.000	0.000					

Pier 11laff.p70		Pier 11laff.p70		Pier 11laff.p70	
23.362	0.007455	1834758.	0.000	1.992E+12	0.000
-59.0578	105764.	-4747.8296	-0.000116	0.000	1.992E+12
24.475	0.005992	1766112.	-5521.2382	-0.000104	0.000
-56.8086	126566.	0.000	0.000	0.000	1.992E+12
25.588	0.004688	1687341.	-6261.5077	-9.206E-05	0.000
-54.0932	154053.	0.000	0.000	0.000	1.992E+12
26.700	0.003534	1598930.	-6862.5476	-8.105E-05	0.000
-35.9503	135802.	0.000	0.000	0.000	1.993E+12
27.812	0.002524	1504111.	-7287.3606	-7.066E-05	0.000
-27.6921	146495.	0.000	0.000	0.000	1.993E+12
18.925	0.001648	1404357.	-7601.6936	-6.092E-05	0.000
-19.3989	157189.	0.000	0.000	0.000	1.993E+12
30.037	0.000897	1301146.	-7806.4853	-5.186E-05	0.000
-11.2814	167882.	0.000	0.000	0.000	1.994E+12
31.150	0.000263	1195924.	-7905.2690	-4.350E-05	0.000
-3.5176	178575.	0.000	0.000	0.000	1.994E+12
32.262	0.000264	1090075.	-7903.7408	-3.584E-05	0.000
3.7466	189269.	0.000	0.000	0.000	1.994E+12
33.375	0.000694	984894.	-7809.3394	-2.890E-05	0.000
10.3960	199962.	0.000	0.000	0.000	1.994E+12
34.487	0.001036	881566.	-7630.8450	-2.265E-05	0.000
16.3448	210655.	0.000	0.000	0.000	1.994E+12
35.600	0.001299	781151.	-7378.0001	-1.708E-05	0.000
21.5346	221349.	0.000	0.000	0.000	1.994E+12
25.9321	232042.	0.000	0.000	0.000	1.994E+12
37.825	0.001624	592518.	-6690.9744	-7.900E-06	0.000
29.5264	242735.	0.000	0.000	0.000	1.994E+12
32.3266	253429.	0.000	0.000	0.000	1.994E+12
34.3586	264122.	0.000	0.000	0.000	1.994E+12
41.163	0.001732	350184.	-5365.5896	1.489E-06	0.000
35.6627	274815.	0.000	0.000	0.000	1.994E+12
36.2907	285509.	0.000	0.000	0.000	1.994E+12
43.387	0.001636	219746.	-4400.7383	5.283E-06	0.000
36.3030	296202.	0.000	0.000	0.000	1.994E+12
35.7665	306895.	0.000	0.000	0.000	1.994E+12
45.613	0.001461	115091.	-3448.9631	7.503E-06	0.000
34.7521	317589.	0.000	0.000	0.000	1.994E+12
46.725	0.001356	72144.	-2994.4989	8.130E-06	0.000
33.3325	328282.	0.000	0.000	0.000	1.994E+12
31.5804	338975.	0.000	0.000	0.000	1.994E+12
29.4890	0.001129	3759.8898	-2561.2056	8.489E-06	0.000
50.062	0.001014	-22349.	-1773.0558	8.557E-06	0.000
27.3605	360362.	0.000	0.000	0.000	1.994E+12
51.175	0.000900	-43381.	-1423.3836	8.337E-06	0.000
25.0249	371056.	0.000	0.000	0.000	1.994E+12
22.6192	381749.	0.000	0.000	0.000	1.994E+12
53.400	0.000687	-73094.	-819.5612	7.542E-06	0.000
20.1970	392442.	0.000	0.000	0.000	1.994E+12
54.512	0.000590	-82235.	-565.8946	7.022E-06	0.000
17.8055	403136.	0.000	0.000	0.000	1.994E+12
35.625	0.000500	-88203.	-343.6750	6.451E-06	0.000
15.4836	413829.	0.000	0.000	0.000	1.994E+12
16.738	0.000417	0.000	0.000	0.000	1.994E+12
13.7252	425222.	0.000	0.000	0.000	1.994E+12
57.850	-0.000343	-92254.	11.6012	5.235E-06	0.000

Pier 11laff.p70		Pier 11laff.p70		Pier 11laff.p70	
11.1940	435216.	0.000	0.000	0.000	1.994E+12
58.962	-0.000278	-91102.	148.2134	4.621E-06	0.000
9.2723	445909.	0.000	0.000	0.000	1.994E+12
60.075	-0.000220	-88297.	260.3266	4.021E-06	0.000
7.5237	456602.	0.000	0.000	0.000	1.994E+12
61.188	-0.000170	-84151.	350.3244	3.444E-06	0.000
5.9591	467296.	0.000	0.000	0.000	1.994E+12
62.300	-0.000128	-78943.	420.7004	2.898E-06	0.000
4.5841	477989.	0.000	0.000	0.000	1.994E+12
63.412	-9.288E-05	-72918.	473.9933	2.389E-06	0.000
3.3998	488688.	0.000	0.000	0.000	1.994E+12
64.525	-6.424E-05	-66287.	512.7271	1.923E-06	0.000
2.4030	498376.	0.000	0.000	0.000	1.994E+12
65.638	-4.153E-05	-59228.	539.3584	1.503E-06	0.000
1.5867	510069.	0.000	0.000	0.000	1.994E+12
66.750	-2.411E-05	-51886.	556.2274	1.131E-06	0.000
0.9405	520762.	0.000	0.000	0.000	1.994E+12
67.862	-1.133E-05	-44377.	565.5160	8.088E-07	0.000
0.4510	531456.	0.000	0.000	0.000	1.994E+12
68.975	-2.516E-06	-36787.	569.2089	5.370E-07	0.000
0.1022	542149.	0.000	0.000	0.000	1.994E+12
70.087	3.009E-06	-29179.	569.0593	3.162E-07	0.000
-0.1246	552842.	0.000	0.000	0.000	1.994E+12
71.200	5.926E-06	-21593.	566.5577	1.462E-07	0.000
-0.2502	563536.	0.000	0.000	0.000	1.994E+12
72.312	6.913E-06	-14052.	508.8252	2.691E-08	0.000
-8.3989	16218366.	0.000	0.000	0.000	1.994E+12
73.425	6.645E-06	-8007.6703	397.7944	-4.694E-08	0.000
-8.2349	16545035.	0.000	0.000	0.000	1.994E+12
74.537	5.660E-06	-3430.9403	292.0902	-8.324E-08	0.000
-7.6009	17927597.	0.000	0.000	0.000	1.994E+12
75.650	4.369E-06	-208.8608	196.7774	-9.742E-08	0.000
-6.6782	20406679.	0.000	0.000	0.000	1.994E+12
76.763	3.059E-06	1823.0150	114.8984	-9.202E-08	0.000
-5.5883	24388808.	0.000	0.000	0.000	1.994E+12
77.875	1.912E-06	2858.9270	48.1039	-7.634E-08	0.000
-4.4184	30850176.	0.000	0.000	0.000	1.994E+12
78.987	1.021E-06	3107.3891	-2.9375	-5.637E-08	0.000
-3.2283	42229399.	0.000	0.000	0.000	1.994E+12
80.100	4.069E-07	2780.4964	-38.0953	-3.666E-08	0.000
-2.0388	66892170.	0.000	0.000	0.000	1.994E+12
81.212	4.175E-08	2090.2446	-53.1216	-2.035E-08	0.000
-0.2123	67889935.	0.000	0.000	0.000	1.994E+12
82.325	-1.386E-07	1362.1500	-49.9013	-8.796E-09	0.000
0.6948	67925579.	0.000	0.000	0.000	1.994E+12
83.438	-1.931E-07	757.8804	-38.7020	-1.699E-09	0.000
0.9830	67961224.	0.000	0.000	0.000	1.994E+12
84.550	-1.819E-07	328.8079	-25.9556	1.939E-09	0.000
0.9265	67996868.	0.000	0.000	0.000	1.994E+12
85.663	-1.413E-07	64.8647	-14.9636	3.257E-09	0.000
0.7202	68032513.	0.000	0.000	0.000	1.994E+12
86.775	-9.495E-08	-70.7207	-6.9248	3.237E-09	0.000
0.4841	68068153.	0.000	0.000	0.000	1.994E+12
87.887	-5.489E-08	-120.0269	-1.8243	2.599E-09	0.000
0.2800	68103801.	0.000	0.000	0.000	1.994E+12
89.000	2.536E-08	-113.4296	0.9155	1.797E-09	0.000
0.1304	68139446.	0.000	0.000	0.000	1.994E+12
90.112	6.903E-09	-85.5833	2.0215	1.077E-09	0.000
0.0353	68175091.	0.000	0.000	0.000	1.994E+12
91.222	3.709E-09	-65.0545	2.1474	5.383E-10	0.000
-0.0644	68227073.	0.000	0.000	0.000	1.994E+12
92.337	7.432E-09	-58.2477	1.7831	1.911E-10	0.000
-0.0382	68246380.	0.000	0.000	0.000	1.994E+12

Pier 11aff.1p7o
Boundary Condition Type 1, Shear and Moment

Shear Moment	9900. lb	783600. in-lb
Axial Load	0. lb	0. lb
Pier 11aff.1p7o		
1.2444	3.344E-12	0.000
0.7024	-7.321E-11	0.000
0.2269	-8.699E-11	0.000
0.006913	-8.047E-11	0.000
0.001884	-7.334E-11	0.000
-0.002185	-6.604E-11	0.000
-0.005359	-5.894E-11	0.000
-0.007705	-5.231E-11	0.000
-0.009292	-4.638E-11	0.000
-0.0102	-4.127E-11	0.000
-0.0104	-3.708E-11	0.000
-0.0101	-3.381E-11	0.000
-0.009147	-3.145E-11	0.000
-0.007675	-2.990E-11	0.000
-0.005664	-2.904E-11	0.000
-0.003109	-2.869E-11	0.000
0.000	-2.862E-11	0.000

Pier 11aff.1p7o
Boundary Condition Type 1, Shear and Moment

93.450	8.312E-09	-17.8464	0.000	1.994E+12
-0.0425	68282024.	0.000	0.000	0.000
94.562	7.559E-09	-5.0221	0.000	0.000
-0.0387	68317669.	0.000	0.000	0.000
95.675	6.357E-09	0.9081	0.000	0.000
-0.0325	68353313.	0.000	0.000	0.000
96.788	5.237E-09	1.0373	0.000	0.000
-0.000414	1054980.	0.000	0.000	0.000
97.900	4.209E-09	1.0927	0.000	0.000
-0.000340	1077257.	0.000	0.000	0.000
99.012	3.278E-09	1.0876	0.000	0.000
-0.000270	1099535.	0.000	0.000	0.000
100.125	2.445E-09	1.0344	0.000	0.000
-0.000205	1121813.	0.000	0.000	0.000
101.237	1.705E-09	0.9445	0.000	0.000
-0.000146	1144091.	0.000	0.000	0.000
-9.160E-05	1166369.	0.8286	0.000	0.000
102.350	1.048E-09	0.6964	0.000	0.000
-4.152E-05	1188646.	0.000	0.000	0.000
104.575	5.355E-11	0.5568	0.000	0.000
4.857E-06	1210924.	0.000	0.000	0.000
105.688	5.237E-10	0.4181	0.000	0.000
4.837E-05	1233202.	0.000	0.000	0.000
106.800	9.564E-10	0.2879	0.000	0.000
8.994E-05	1255480.	0.000	0.000	0.000
107.913	1.363E-09	0.1738	0.000	0.000
0.000130	1277758.	0.000	0.000	0.000
109.025	1.755E-09	0.0830	0.000	0.000
0.000171	1300036.	0.000	0.000	0.000
110.137	2.139E-09	0.0226	0.000	0.000
0.000212	1322313.	0.000	0.000	0.000
111.250	2.521E-09	0.000	0.000	0.000
0.000254	672296.	0.000	0.000	0.000

* This analysis computed pile response using nonlinear moment-curvature relationships. Values of total stress due to combined axial and bending stresses are computed only for elastic sections only and do not equal the actual stresses in concrete and steel. Stresses in concrete and steel may be interpolated from the output for nonlinear bending properties relative to the magnitude of bending moment developed in the pile.

Output Summary for Load Case No. 10:

Pile-head deflection	=	0.0779506 inches
Computed slope at pile head	=	-0.0003775 radians
Maximum bending moment	=	2016396. in-lb
Maximum shear force	=	9900.000000 lbs
Depth of maximum bending moment	=	16.6875000 feet below pile head
Depth of maximum shear force	=	2.2250000 feet below pile head
Number of iterations	=	17
Number of zero deflection points	=	5

Pile-head Deflection vs. Pile Length for Load Case 10

Summary of Pile Response(s)

Definitions of Pile-head Loading Conditions:

Load Type 1: Load 1 = Shear, lbs, and Load 2 = Moment, in-lbs
 Load Type 2: Load 1 = Shear, lbs, and Load 2 = Slope, radians
 Load Type 3: Load 1 = Shear, lbs, and Load 2 = Rotational Stiffness, in-lbs/radian
 Load Type 4: Load 1 = Top Deflection, inches, and Load 2 = Moment, in-lbs
 Load Type 5: Load 1 = Top Deflection, inches, and Load 2 = Slope, radians

Load	Load Type	Pile-head		Axial Loading	Pile-head Deflection	Maximum Moment
		Condition 1	Condition 2			
No.	Y	in-lb	in-lb/rad.	lbs	inches	in-lbs
1	Y = 0.5000	M = 5498600.		0.0000000	0.5000000	
2	Y = -34480	M = -0.00273924		0.0000000	1.0000000	
3	Y = -46592	M = 0.00460980		0.0000000	1.5000000	
4	Y = -65939	M = -0.00618546		0.0000000	2.0000000	

```

19697036.  -86058.  -0.00773751  Pier 11aff.1p7o  0.50000000
5          y = 0.5000  M = 783600.  0.00000000
8583608.  39313.  -0.00173790  M = 783600.  1.00000000
6          y = 1.0000  M = 783600.  0.00000000
11629524.  52667.  -0.00334316  M = 783600.  1.50000000
7          y = 1.5000  M = 783600.  0.00000000
15726199.  -68311.  -0.00497502  M = 783600.  2.00000000
8          y = 2.0000  M = 783600.  0.00000000
19799712.  -88403.  -0.00660036  M = 5499600.  0.35397042
9          y = 13600.  M = 5499600.  0.00000000
7025520.  -26560.  -0.00211790  M = 783600.  0.07795055
10         y = 9900.0000  M = 783600.  0.00000000
2016396.  9900.0000  -0.00037748  M = 783600.  0.00000000

```

SER-1, $\Delta = 0.08^{\wedge}$ < 1.0¹¹ SK

The analysis ended normally.

10/28/14

DELDOT BR1-159
 VBENT RESULTANT FORCES
 DESIGNED BY: SBM 10/16/2014

$R_R = 778^k$

PIER 1

Worst Case	Limit State	Load Case	Column	Top/Bot	M _u	P _u	V _u
Max P _u	STR-I	1/2/3	1	T	540.1	777.5	
	SER-I	1/2/3	1	T	248.8	516.1	
Max V _u	STR-I	26	3	T	458.3		13.6
	SER-I	28	4	T	65.3		9.9

PIER 2

Worst Case	Limit State	Load Case	Column	Top/Bot	M _u	P _u	V _u
Max P _u	STR-I	2	4	T	252.0	689.2	
	SER-I	1/3	1	T	132.4	464.8	
Max V _u	STR-V	28	4	T	115.2		8.8
	SER-I	28	4	T	98.6		8.7

PIER 3

Worst Case	Limit State	Load Case	Column	Top/Bot	M _u	P _u	V _u
Max P _u	STR-I	4	4	T	141.4	688.3	
	SER-I	4	1	T	218.4	500.6	
Max V _u	STR-III	25	2	T	651.5		21.3
	SER-I	26	3	T	365.0		11.0

PIER 4

Worst Case	Limit State	Load Case	Column	Top/Bot	M _u	P _u	V _u
Max P _u	STR-I	1/2/3	1	T	377.0	709.1	
	SER-I	1/2/3	1	T	185.3	475.0	
Max V _u	STR-I	26	4	T	316.1		9.8
	SER-I	26	4	T	270.7		8.4

PIER-1

4' Ø, 1/2" STEEL CASING, TOP FLGV = 0.0

DEFLECTION

STR-1
(lbs)

SER 1
(lbs)

0.5

22,344

39,319

1.0

36,070

52,667 ←

1.5

52,450

68,040

→ 2.0

67,787

82,566

GEOTECHNICAL AXIAL CAPACITY

$= 778^k > 777.5^k$ OK

LATERAL CAPACITY, 2" DEFLECTION (STR-1)

$57.79^k > 13.6^k$ OK.

LATERAL CAPACITY, 1" DEFLECTION (SER-1)

$52.67 > 9.9^k$ OK.

PIER 2

LAYER (BELOW DSCAP)

Boring No. JS-5 By: SJM Chk: AT
BELOW BRIDGE DECK OG Elev. = 11.00

RIVER BED @ EL. -9.0

Sample No.	Depth of SS run (ft)	N-Values Field	q' _v (ksf)	C _N	N _{CORR}
1	20	4	0.952	1.250	5
2	22	0	1.047	1.218	0
3	24	0	1.142	1.189	0
4	26	2	1.238	1.162	2
5	33	10	1.571	1.083	11
6	38	13	1.809	1.035	13
7	43	29	2.047	0.994	29
8	48	16	2.285	0.957	15
9	53	17	2.523	0.924	16
10	58	19	2.761	0.894	17
11	63	15	2.999	0.866	13
12	68	22	3.237	0.841	18
13	73	23	3.475	0.817	19
14	78	45	3.713	0.795	36
15	83	82	3.951	0.774	63
16	88	84	4.189	0.755	63
17	93	41	4.427	0.736	30
18	98	80	4.665	0.719	57
19	103	78	4.903	0.702	55
20	108	50	5.141	0.686	34
21	113	50	5.379	0.671	34
22	118	50	5.617	0.656	33

GWT= 5.0
 γ = 110 lb/ft³
 γ' = 47.6 lb/ft³

- ①
- ②
- ③
- ④
- ⑤
- ⑥

N_{avg} (Below BFE) = 26
 (Ref. AASHTO Eqn 10.4.6.2.4-1)

C_N = 0.77xlog(40/q'_v)
 N_{CORR} = N_{Field} x C_N

Boring No. JS-6 By: SJM Chk:
OG Elev. = 11.00

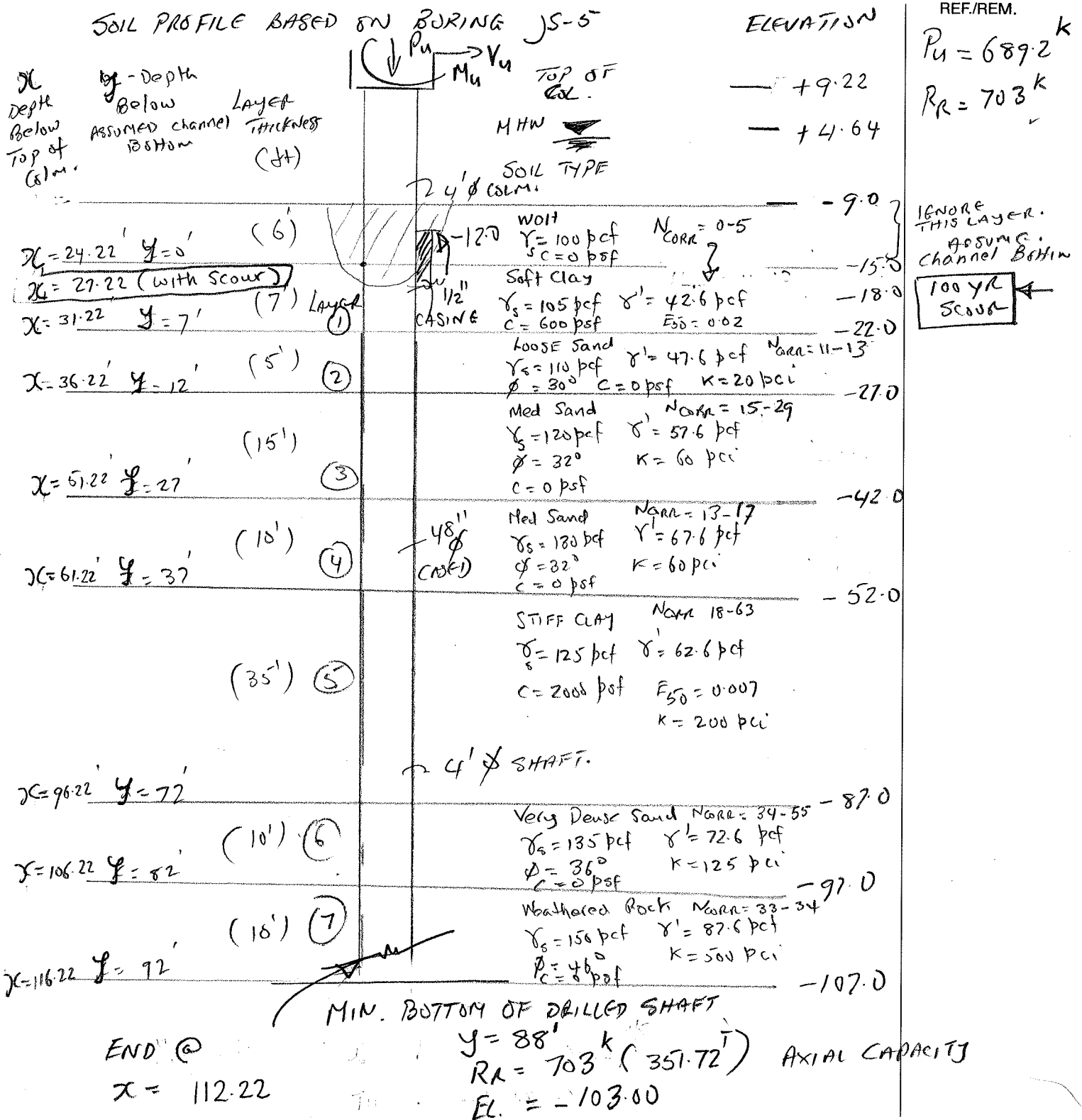
Sample No.	Depth of SS run (ft)	N-Values Field	q' _v (ksf)	C _N	N _{CORR}
1	23	0	1.095	1.203	0
2	25	19	1.190	1.175	22
3	27	0	1.285	1.150	0
4	29	0	1.380	1.126	0
5	31	12	1.476	1.103	13
6	33	9	1.571	1.083	10
7	38	4	1.809	1.035	4
8	43	19	2.047	0.994	19
9	48	15	2.285	0.957	14
10	53	13	2.523	0.924	12
11	58	9	2.761	0.894	8
12	63	23	2.999	0.866	20
13	68	31	3.237	0.841	26
14	73	46	3.475	0.817	38
15	78	33	3.713	0.795	26
16	83	24	3.951	0.774	19
17	88	54	4.189	0.755	41
18	93	50	4.427	0.736	37
19	98	56	4.665	0.719	40
20	103	50	4.903	0.702	35
21	108		5.141	0.686	

GWT= 0.0
 γ = 110 lb/ft³
 γ' = 47.6 lb/ft³

N_{avg} (Below BFE) = 20
 (Ref. AASHTO Eqn 10.4.6.2.4-1)

C_N = 0.77xlog(40/q'_v)
 N_{CORR} = N_{Field} x C_N

PROJECT BR1-159 JOB NO. _____ SHEET NO. 1 OF 1
 LOCATION PER 2
 SUBJECT SOIL PROFILE (AXIAL & LATERAL CAPACITIES)
 DESIGNED BY SJM DATE 7/14 CHECKED BY AT DATE 8/14
 REVISED BY _____ DATE _____ BACK CHECKED BY _____ DATE _____



AXIAL CAPACITY

```

=====
pier 22.sfo
BRIDGE FOUNDATION REPORT SHAFT output
SHAFT for windows, Version 2012.7.11
Serial Number : 228741384
VERTICALLY LOADED DRILLED SHAFT ANALYSIS
(C) Copyright ENSOFT, Inc., 1987-2012
All Rights Reserved
=====

```

```

Path to file locations : Y:\Bridges\DELDOT\BR1-159_JAMES ST
BRIDGE FOUNDATION REPORT SHAFT output
Name of input data file : pier 22.sfo
Name of output file : pier 22.sfo
Name of plot output file : pier 22.sfp
Name of runtime file : pier 22.sfr
=====

```

Time and Date of Analysis

Date: September 10, 2014 Time: 14:03:55

BR1-159 Pier 2

PROPOSED DEPTH = 110.0 FT

NUMBER OF LAYERS = 7

WATER TABLE DEPTH = 0.0 FT.

*****WARNING*****
PLEASE PROVIDE THE SOIL DEPTH THAT IS TWO-DIAMETER DEEPER
THAN THE TIP OF DRILLED SHAFTS

SOIL INFORMATION

LAYER NO 1----CLAY

AT THE TOP

```

STRENGTH REDUCTION FACTOR-ALPHA = 0.550E+00
END BEARING COEFFICIENT-NC      = 0.800E+01
UNDRAINED SHEAR STRENGTH, LB/SQ FT = 0.600E+03
INTERNAL FRICTION ANGLE, DEG.    = 0.000E+00
BLOWS PER FOOT FROM STANDARD PENETRATION TEST
                                     = 0.000E+00

```

Page 1

```

SOIL UNIT WEIGHT, LB/CU FT          pier 22.sfo
MAXIMUM LOAD TRANSFER FOR SOIL, LB/SQ FT
DEPTH, FT                          = 0.105E+03
                                     = 0.100E+11
                                     = 0.000E+00

```

AT THE BOTTOM

```

STRENGTH REDUCTION FACTOR-ALPHA   = 0.550E+00
END BEARING COEFFICIENT-NC        = 0.800E+01
UNDRAINED SHEAR STRENGTH, LB/SQ FT = 0.600E+03
INTERNAL FRICTION ANGLE, DEG.     = 0.000E+00
BLOWS PER FOOT FROM STANDARD PENETRATION TEST
SOIL UNIT WEIGHT, LB/CU FT        = 0.105E+03
MAXIMUM LOAD TRANSFER FOR SOIL, LB/SQ FT
DEPTH, FT                          = 0.100E+11
                                     = 0.700E+01

```

```

LRFD RESISTANCE FACTOR (SIDE FRICTION) = 0.450E+00
LRFD RESISTANCE FACTOR (TIP RESISTANCE) = 0.400E+00

```

LAYER NO 2----SAND

AT THE TOP

```

SKIN FRICTION COEFFICIENT- BETA    = 0.114E+01
UNDRAINED SHEAR STRENGTH, LB/SQ FT = 0.300E+02
INTERNAL FRICTION ANGLE, DEG.      = 0.300E+02
BLOWS PER FOOT FROM STANDARD PENETRATION TEST
SOIL UNIT WEIGHT, LB/CU FT         = 0.110E+03
MAXIMUM LOAD TRANSFER FOR SOIL, LB/SQ FT
DEPTH, FT                          = 0.700E+01

```

AT THE BOTTOM

```

SKIN FRICTION COEFFICIENT- BETA    = 0.103E+01
UNDRAINED SHEAR STRENGTH, LB/SQ FT = 0.100E+00
INTERNAL FRICTION ANGLE, DEG.      = 0.300E+02
BLOWS PER FOOT FROM STANDARD PENETRATION TEST
SOIL UNIT WEIGHT, LB/CU FT         = 0.100E+00
MAXIMUM LOAD TRANSFER FOR SOIL, LB/SQ FT
DEPTH, FT                          = 0.120E+02

```

```

LRFD RESISTANCE FACTOR (SIDE FRICTION) = 0.550E+00
LRFD RESISTANCE FACTOR (TIP RESISTANCE) = 0.500E+00

```

LAYER NO 3----SAND

AT THE TOP

```

SKIN FRICTION COEFFICIENT- BETA    = 0.103E+01
UNDRAINED SHEAR STRENGTH, LB/SQ FT = 0.000E+00
INTERNAL FRICTION ANGLE, DEG.      = 0.320E+02
BLOWS PER FOOT FROM STANDARD PENETRATION TEST
SOIL UNIT WEIGHT, LB/CU FT         = 0.000E+00
MAXIMUM LOAD TRANSFER FOR SOIL, LB/SQ FT
DEPTH, FT                          = 0.100E+11
                                     = 0.120E+02

```

AT THE BOTTOM

Page 2

Pier 22.sfo

DRILLED SHAFT INFORMATION

DIAMETER OF STEM = 4.000 FT.
 DIAMETER OF BASE = 4.000 FT.
 END OF STEM TO BASE = 0.000 FT.
 ANGLE OF BELL = 0.000 DEG.
 IGNORED TOP PORTION = 3.000 FT.
 AREA OF ONE PORTION = 4.000 FT.
 AREA OF ONE PERCENT STEEL = 16.098 SQ.IN.
 ELASTIC MODULUS, EC = 0.312E+07 LB/SQ IN.
 VOLUME OF UNDERREAM = 0.000 CU.YDS.

PREDICTED RESULTS

QS = ULTIMATE SIDE RESISTANCE;
 QB = ULTIMATE BASE RESISTANCE;
 WT = WEIGHT OF DRILLED SHAFT (UPLIFT CAPACITY ONLY);
 QD = TOTAL SIDE FRICTION RESISTANCE;
 LRFQ QS = TOTAL SIDE FRICTION RESISTANCE;
 LRFQ QB = TOTAL BASE BEARING RESISTANCE;
 LRFQ QU = TOTAL CAPACITY WITH LRFQ RESISTANCE FACTOR.

LENGTH (FEET)	QS (TONS)	QB (TONS)	QU (TONS)	LRFQ QS (TONS)	LRFQ QB (TONS)	LRFQ QU (TONS)
10.0	4.65	63.69	65.76	0.93	31.84	32.78
11.0	4.15	67.04	71.19	1.87	33.52	35.39
12.0	6.41	67.04	73.45	3.11	33.52	36.63
13.0	6.05	67.04	75.99	4.51	33.52	38.03
14.0	6.52	67.04	78.80	6.06	33.52	39.58
15.0	6.58	67.04	81.88	7.75	33.52	41.27
16.0	7.45	67.04	85.20	9.58	33.52	43.09
17.0	7.91	67.04	88.80	11.55	33.52	45.07
18.0	8.38	67.04	92.69	13.69	33.52	47.21
19.0	8.84	67.04	96.87	15.99	33.52	49.51
20.0	9.31	67.04	101.32	18.44	33.52	51.96
21.0	9.78	67.04	106.03	21.03	33.52	54.55
22.0	10.24	67.04	111.00	23.77	33.52	57.29
23.0	10.71	67.04	116.22	26.64	33.52	60.15
24.0	11.17	67.04	121.67	29.64	33.52	63.15
25.0	11.64	67.04	127.36	32.76	33.52	66.28
26.0	12.10	67.04	133.26	36.01	33.52	69.52
27.0	12.57	67.04	139.37	39.37	33.52	72.89
28.0	13.03	67.04	145.69	42.84	33.52	76.36
29.0	13.50	67.04	152.20	46.42	33.52	79.94
30.0	13.96	67.04	158.93	50.11	33.52	83.64
31.0	14.43	67.04	165.87	53.89	33.52	87.44
32.0	14.90	67.04	173.01	57.79	33.52	91.33
33.0	15.36	67.04	180.36	61.80	33.52	95.31
34.0	15.83	67.04	187.91	65.92	33.52	99.47
35.0	16.29	67.04	195.66	70.16	33.52	103.79
36.0	16.76	67.04	203.61	74.50	33.52	108.27
37.0	17.22	67.04	211.74	78.93	33.52	112.81
38.0	17.69	67.04	220.05	83.46	33.52	117.41
39.0	18.15	67.04	228.54	88.09	33.52	122.07

LOAD SETTLEMENT RELATIONSHIP

TOP LOAD TONS	TOP MOVEMENT IN.
0.6034E+02	0.4507E-01
0.1207E+03	0.9014E-01
0.1810E+03	0.1352E+00
0.2414E+03	0.1803E+00

Pier 22.sfo

40.0	18.62	169.48	100.54	92.80	40.22
41.0	19.58	198.19	100.54	78.73	40.22
42.0	20.55	206.90	100.54	109.70	40.22
43.0	21.52	215.61	100.54	140.67	40.22
44.0	22.49	224.32	100.54	171.64	40.22
45.0	23.46	233.03	100.54	202.61	40.22
46.0	24.43	241.74	100.54	233.58	40.22
47.0	25.40	250.45	100.54	264.55	40.22
48.0	26.37	259.16	100.54	295.52	40.22
49.0	27.34	267.87	100.54	326.49	40.22
50.0	28.31	276.58	100.54	357.46	40.22
51.0	29.28	285.29	100.54	388.43	40.22
52.0	30.25	294.00	100.54	419.40	40.22
53.0	31.22	302.71	100.54	450.37	40.22
54.0	32.19	311.42	100.54	481.34	40.22
55.0	33.16	320.13	100.54	512.31	40.22
56.0	34.13	328.84	100.54	543.28	40.22
57.0	35.10	337.55	100.54	574.25	40.22
58.0	36.07	346.26	100.54	605.22	40.22
59.0	37.04	354.97	100.54	636.19	40.22
60.0	38.01	363.68	100.54	667.16	40.22
61.0	38.98	372.39	100.54	698.13	40.22
62.0	39.95	381.10	100.54	729.10	40.22
63.0	40.92	389.81	100.54	760.07	40.22
64.0	41.89	398.52	100.54	791.04	40.22
65.0	42.86	407.23	100.54	822.01	40.22
66.0	43.83	415.94	100.54	852.98	40.22
67.0	44.80	424.65	100.54	883.95	40.22
68.0	45.77	433.36	100.54	914.92	40.22
69.0	46.74	442.07	100.54	945.89	40.22
70.0	47.71	450.78	100.54	976.86	40.22
71.0	48.68	459.49	100.54	1007.83	40.22
72.0	49.65	468.20	100.54	1038.80	40.22
73.0	50.62	476.91	100.54	1069.77	40.22
74.0	51.59	485.62	100.54	1100.74	40.22
75.0	52.56	494.33	100.54	1131.71	40.22
76.0	53.53	503.04	100.54	1162.68	40.22
77.0	54.50	511.75	100.54	1193.65	40.22
78.0	55.47	520.46	100.54	1224.62	40.22
79.0	56.44	529.17	100.54	1255.59	40.22
80.0	57.41	537.88	100.54	1286.56	40.22
81.0	58.38	546.59	100.54	1317.53	40.22
82.0	59.35	555.30	100.54	1348.50	40.22
83.0	60.32	564.01	100.54	1379.47	40.22
84.0	61.29	572.72	100.54	1410.44	40.22
85.0	62.26	581.43	100.54	1441.41	40.22
86.0	63.23	590.14	100.54	1472.38	40.22
87.0	64.20	598.85	100.54	1503.35	40.22
88.0	65.17	607.56	100.54	1534.32	40.22
89.0	66.14	616.27	100.54	1565.29	40.22
90.0	67.11	624.98	100.54	1596.26	40.22
91.0	68.08	633.69	100.54	1627.23	40.22

k
Re=703

y=88

Pier_22.sfo
0.2253E+00
0.2704E+00
0.3155E+00
0.3606E+00
0.4056E+00
0.4507E+00
0.9674E+00
0.1484E+01
0.2001E+01
0.2518E+01
0.3021E+01

0.3017E+03
0.3621E+03
0.4224E+03
0.4827E+03
0.5431E+03
0.6034E+03
0.6378E+03
0.6722E+03
0.7066E+03
0.7410E+03
0.77410E+03

PIER 2 LATERAL CAPACITY

Pier 22af.lp7o

Pier 22af.lp7o

Description: Pier 2 Lateral Capacity (4' DIA Colm.&caisson at each beam)

LPile Plus for Windows, Version 2013-07-007
 Analysis of Individual Piles and Drilled Shafts
 Subjected to Lateral Loading using the p-y Method
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This copy of LPile is used by:
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Files Used for Analysis
 Path to file locations: Y:\bridges\DELDOT\BRI-159_JAMES ST BRIDGE\FOUNDATION
 REPORT\LPILE Output\ pier 22af.lp7d
 Name of input data file: pier 22af.lp7o
 Name of output report file: pier 22af.lp7p
 Name of plot output file: pier 22af.lp7p
 Name of runtime message file: Pier 22af.lp7r

Date and Time of Analysis
 Date: October 24, 2014 Time: 14:48:28

Problem Title
 Project Name: BRI-159 Pier 2

Job Number:
 Client: DelDOT
 Engineer: SJM

 Program Options and Settings

Engineering Units of Input Data and Computations:
 - Engineering units are US Customary Units (pounds, feet, inches)

Analysis Control Options:
 - Maximum number of iterations allowed = 600
 - Deflection tolerance for convergence = 1.0000E-05 in
 - Maximum allowable deflection = 100.0000 in
 - Number of pile increments = 100

Loading Type and Number of Cycles of Loading:
 - Static loading specified

Computational Options:
 - Use unfactored loads in computations (conventional analysis)
 - Compute pile response under loading and nonlinear bending properties of pile (only if nonlinear pile properties are input)
 - Use of p-y modification factors for p-y curves not selected
 - Loading by lateral soil movements acting on pile not selected
 - Input of shear resistance at the pile tip not selected
 - Computation of pile-head foundation stiffness matrix not selected
 - Push-over analysis of pile not selected
 - Buckling analysis of pile not selected

Output Options:
 - No p-y curves to be computed and reported for user-specified depths
 - Values of pile-head deflection, bending moment, shear force, and soil reaction are printed for full length of pile.
 - Printing increment (nodal spacing of output points) = 1

 pile Structural Properties and Geometry

Total number of pile sections = 2
 Total length of pile = 112.22 ft
 Depth of ground surface below top of pile = 27.22 ft
 Pile diameter values used for p-y curve computations are defined using 4 points.
 p-y curves are computed using pile diameter values interpolated with depth over the length of the pile.

Point	Depth X ft	Pile Diameter in
1	0.00000	48.0000000
2	21.220000	48.0000000
3	21.220000	49.0000000

4 112.220000 Pier 22af. 1p70 49.000000 Pier 22af. 1p70

Input Structural Properties:

Pile Section No. 1:
Section Type = Drilled shaft (bored pile)
Section Length = 21.22000 ft
Section Diameter = 48.00000 in

Pile Section No. 2:
Section Type = Drilled shaft with
Permanent casing
Section Length = 91.00000 ft
Section Diameter = 49.00000 in

Ground Slope and Pile Batter Angles

Ground Slope Angle = 0.000 degrees
Pile Batter Angle = 0.000 radians

Soil and Rock Layering Information

The soil profile is modelled using 7 layers

Layer 1 is soft clay, p-y criteria by Matlock, 1970

Distance from top of pile to top of layer	=	27.22000 ft
Distance from top of pile to bottom of layer	=	31.22000 ft
Effective unit weight at top of layer	=	42.60000 pcf
Effective unit weight at bottom of layer	=	42.60000 pcf
Undrained cohesion at top of layer	=	600.00000 psf
Undrained cohesion at bottom of layer	=	600.00000 psf
Epsilon-50 at top of layer	=	0.02000
Epsilon-50 at bottom of layer	=	0.02000

Layer 2 is sand, p-y criteria by Reese et al., 1974

Distance from top of pile to top of layer	=	31.22000 ft
Distance from top of pile to bottom of layer	=	36.22000 ft
Effective unit weight at top of layer	=	47.60000 pcf
Effective unit weight at bottom of layer	=	47.60000 pcf
Friction angle at top of layer	=	30.00000 deg.
Friction angle at bottom of layer	=	30.00000 deg.
Subgrade k at top of layer	=	20.00000 pci
Subgrade k at bottom of layer	=	20.00000 pci

Layer 3 is sand, p-y criteria by Reese et al., 1974

Distance from top of pile to top of layer	=	36.22000 ft
Distance from top of pile to bottom of layer	=	41.22000 ft
Effective unit weight at top of layer	=	47.60000 pcf
Effective unit weight at bottom of layer	=	47.60000 pcf
Friction angle at top of layer	=	30.00000 deg.
Friction angle at bottom of layer	=	30.00000 deg.
Subgrade k at top of layer	=	20.00000 pci
Subgrade k at bottom of layer	=	20.00000 pci

Layer 4 is sand, p-y criteria by Reese et al., 1974

Distance from top of pile to top of layer	=	41.22000 ft
Distance from top of pile to bottom of layer	=	46.22000 ft
Effective unit weight at top of layer	=	47.60000 pcf
Effective unit weight at bottom of layer	=	47.60000 pcf
Friction angle at top of layer	=	30.00000 deg.
Friction angle at bottom of layer	=	30.00000 deg.
Subgrade k at top of layer	=	20.00000 pci
Subgrade k at bottom of layer	=	20.00000 pci

Layer 5 is stiff clay with water-induced erosion

Distance from top of pile to top of layer	=	61.22000 ft
Distance from top of pile to bottom of layer	=	91.22000 ft
Effective unit weight at top of layer	=	62.60000 pcf
Effective unit weight at bottom of layer	=	62.60000 pcf
Undrained cohesion at top of layer	=	2000.00000 psf
Undrained cohesion at bottom of layer	=	2000.00000 psf
Epsilon-50 at top of layer	=	0.00700
Epsilon-50 at bottom of layer	=	0.00700
Subgrade k at top of layer	=	200.00000 pci
Subgrade k at bottom of layer	=	200.00000 pci

Layer 6 is sand, p-y criteria by Reese et al., 1974

Distance from top of pile to top of layer	=	96.22000 ft
Distance from top of pile to bottom of layer	=	106.22000 ft
Effective unit weight at top of layer	=	72.60000 pcf
Effective unit weight at bottom of layer	=	72.60000 pcf
Friction angle at top of layer	=	36.00000 deg.
Friction angle at bottom of layer	=	36.00000 deg.
Subgrade k at top of layer	=	125.00000 pci
Subgrade k at bottom of layer	=	125.00000 pci

Layer 7 is sand, p-y criteria by Reese et al., 1974

Distance from top of pile to top of layer	=	106.22000 ft
Distance from top of pile to bottom of layer	=	116.22000 ft
Effective unit weight at top of layer	=	87.60000 pcf
Effective unit weight at bottom of layer	=	87.60000 pcf
Friction angle at top of layer	=	46.00000 deg.
Friction angle at bottom of layer	=	46.00000 deg.
Subgrade k at top of layer	=	500.00000 pci
Subgrade k at bottom of layer	=	500.00000 pci

(Depth of lowest soil layer extends 4.00 ft below pile tip)

Summary of Soil Properties

Layer Num.	Strain Factor (p-y Curve Criteria) Epsilon 50	Soil Type	Layer Depth ft	Effective unit wt. pcf	Undrained Cohesion psf
1	0.02000	Soft Clay	27.220	42.600	600.000
2	0.02000	Sand (Reese, et al.)	31.220	42.600	600.000
3	20.000	Sand (Reese, et al.)	31.220	47.600	--
4	20.000	Sand (Reese, et al.)	36.220	47.600	--
5	60.000	Sand (Reese, et al.)	36.220	57.600	--
6	60.000	Sand (Reese, et al.)	51.220	57.600	--
7	60.000	Sand (Reese, et al.)	51.220	67.600	--
8	60.000	Sand (Reese, et al.)	61.220	67.600	--
9	60.000	Stiff Clay with Free water	61.220	62.600	2000.000
10	200.000	Stiff Clay with Free water	96.220	62.600	2000.000
11	0.00700	Sand (Reese, et al.)	96.220	72.600	--
12	125.000	Sand (Reese, et al.)	106.220	72.600	--
13	125.000	Sand (Reese, et al.)	106.220	87.600	--
14	500.000	Sand (Reese, et al.)	106.220	87.600	--
15	500.000	Sand (Reese, et al.)	116.220	87.600	--

Loading Type

Static loading criteria were used when computing p-y curves for all analyses.

Pile-head Loading and Pile-head Fixity Conditions

Number of loads specified = 10

Load No.	Load Type	Condition	Condition	Axial Thrust Force, lbs
1	Top y vs Pile Length	1	2	

1	4	Y	M	in	in-lbs
2	4	Y	1.00000	in	1382400. in-lbs
3	4	Y	1.50000	in	1382400. in-lbs
4	4	Y	2.00000	in	1382400. in-lbs
5	4	Y	0.50000	in	1183200. in-lbs
6	4	Y	1.00000	in	1183200. in-lbs
7	4	Y	1.50000	in	1183200. in-lbs
8	4	Y	2.00000	in	1183200. in-lbs
9	1	V	8800.00000	lbs	1382400. in-lbs
10	1	V	8700.00000	lbs	1183200. in-lbs

V = perpendicular shear force applied to pile head
M = bending moment applied to pile head
Y = lateral deflection relative to pile axis
S = pile slope relative to original pile batter angle
R = rotational stiffness applied to pile head
Axial thrust is assumed to be acting axially for all pile batter angles.

Computations of Nominal Moment Capacity and Nonlinear Bending Stiffness

Axial thrust force values were determined from pile-head loading conditions

Number of Pile Sections Analyzed = 2

Pile Section No. 1:

Dimensions and Properties of Drilled shaft (Bored Pile):

Length of Section	=	21.22000 ft
Shaft Diameter	=	48.00000 in
Concrete Cover Thickness	=	4.00000 in
Number of Reinforcing Bars	=	30 bars
Yield Stress of Reinforcing Bars	=	60000. psi
Modulus of Elasticity of Reinforcing Bars	=	29000000. psi
Gross Area of Shaft	=	1809.56337 sq. in.
Total Area of Reinforcing Steel	=	39.50000 sq. in.
Area Ratio of Steel Reinforcement	=	2.18438 percent
Edge-to-Edge Bar Spacing	=	2.86438 in
Ratio of Bar Spacing to Aggregate Size	=	0.37500 in
Offset of Center of Rebar Cage from Center of Pile	=	0.00000 in

Axial Structural Capacities:

Nom. Axial Structural Capacity = 0.85 Fc Ac + Fy As	=	9140.470 kips
Tensile Load for Cracking of Concrete	=	-911.303 kips

Nominal Axial Tensile Capacity = -2370.000 kips

Pier 22af.lp7o

Reinforcing Bar Dimensions and Positions Used in Computations:

Bar Number	Bar Diam. Inches	Bar Area Sq. In.	X Inches	Y Inches
1	1.00000	0.79000	19.49359	-0.49995
2	1.00000	0.79000	19.49359	0.49995
3	1.00000	0.79000	19.00549	4.36362
4	1.00000	0.79000	18.75683	5.33210
5	1.00000	0.79000	17.32321	8.95300
6	1.00000	0.79000	16.84151	9.82921
7	1.00000	0.79000	14.55245	12.97984
8	1.00000	0.79000	13.86798	13.70873
9	1.00000	0.79000	10.86731	16.19110
10	1.00000	0.79000	10.02307	16.72687
11	1.00000	0.79000	6.49933	18.38501
12	1.00000	0.79000	5.54837	18.69400
13	1.00000	0.79000	1.72297	19.42373
14	1.00000	0.79000	0.72505	19.48652
15	1.00000	0.79000	-3.16164	19.24199
16	1.00000	0.79000	-4.14382	19.05462
17	1.00000	0.79000	-7.84760	17.85119
18	1.00000	0.79000	-8.75233	17.42546
19	1.00000	0.79000	-12.04047	15.33875
20	1.00000	0.79000	-12.81090	14.70139
21	1.00000	0.79000	-15.47679	11.86251
22	1.00000	0.79000	-16.06451	11.05358
23	1.00000	0.79000	-17.94084	7.64091
24	1.00000	0.79000	-18.30872	6.71123
25	1.00000	0.79000	-19.27722	2.93920
26	1.00000	0.79000	-19.40254	1.94719
27	1.00000	0.79000	-19.40254	-1.94719
28	1.00000	0.79000	-19.27722	-2.93920
29	1.00000	0.79000	-16.30872	-6.71123
30	1.00000	0.79000	-17.94084	-7.64091
31	1.00000	0.79000	-16.06451	-11.05358
32	1.00000	0.79000	-15.47679	-11.86251
33	1.00000	0.79000	-12.81090	-14.70139
34	1.00000	0.79000	-12.04047	-15.33875
35	1.00000	0.79000	-6.35233	-17.42546
36	1.00000	0.79000	-7.84760	-17.85119
37	1.00000	0.79000	-3.16382	-18.24199
38	1.00000	0.79000	-3.16164	-18.38501
39	1.00000	0.79000	1.72507	-18.48652
40	1.00000	0.79000	5.54837	-18.69400
41	1.00000	0.79000	6.49933	-18.72687
42	1.00000	0.79000	10.02307	-16.72687
43	1.00000	0.79000	10.86731	-16.19110
44	1.00000	0.79000	13.86798	-13.70873
45	1.00000	0.79000	14.55245	-12.97984
46	1.00000	0.79000	16.84151	-8.95300
47	1.00000	0.79000	17.32321	-8.35300
48	1.00000	0.79000	18.75683	-5.33210
49	1.00000	0.79000	19.00549	-4.36362
50	1.00000	0.79000	19.49359	-0.49995

NOTE: The positions of the above rebars were computed by LPILE
Minimum spacing between any two bars not equal to zero = -0.0001096 inches between

Bars 1 and 2

Spacing to aggregate size ratio = -0.0002922

Pier 22af.lp7o

Concrete Properties:

Compressive Strength of Concrete = 4500.00000 psi
 Modulus of Elasticity of Concrete = 3823676. psi
 Modulus of Rupture of Concrete = -503.11528 psi
 Compression Strain at Peak Stress = 0.00200
 Tensile Strain at Fracture of Concrete = -0.0001132
 Maximum Coarse Aggregate Size = 0.37500 in

Number of Axial Thrust Force Values Determined from Pile-head Loadings = 1

Number Axial Thrust Force Kips

 1 ----- 0.000

Definitions of Run Messages and Notes:

C = concrete in section has cracked in tension.
 Y = stress in reinforcing steel has reached yield stress.
 T = ACI 318-08 criteria for tension-controlled section met, tensile strain in reinforcement exceeds 0.005 while simultaneously compressive strain in concrete more than 0.003. See ACI 318-08, Section 10.3.4.
 Z = depth of tensile zone in concrete section is less than 10 percent of section depth.
 Bending Stiffness (EI) = Computed Bending Moment / Curvature.
 Position of neutral axis is measured from edge of compression side of pile.
 Compressive stresses and strains are positive in sign.
 Tensile stresses and strains are negative in sign.

Axial Thrust Force = 0.000 kips

Max Concrete Curvature Rad/in.	Bending Moment Max Steel Stress KSI	Bending Moment Run Kip	Bending Stiffness Run kip-in2	Depth to N Axis in	Max Comp Strain in/in	Max Tens Strain in/in
0.00000625	845.9514339	135322294.	24.0001518	0.0000150	-0.0000150	-0.0000150
0.065544	0.4306528	1350625155.	24.0001524	0.0000300	-0.0000300	-0.0000300
0.000001250	1688.281444	1347728017.	24.0001529	0.0000450	-0.0000450	-0.0000450
0.1326129	0.8615055	1344830878.	24.0001534	0.0000600	-0.0000600	-0.0000600
0.000001875	2576.9900314	1341933739.	24.0001540	0.0000750	-0.0000750	-0.0000750
0.1981756	1.291919583	1339036601.	24.0001545	0.0000900	-0.0000900	-0.0000900
0.000002500	3362.0771951	2.3839168				
0.2632425	1.7226111					
0.000003125	4193.5429353					
0.3278135	2.1532639					
0.000003750	5021.3872521					
0.3918887	2.3839168					

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1386139462.	24.0001551	0.0001050	-0.0001050
5845.6101456	14.1767436	0.0000709	-0.0001691
3.0145696	14.1814610	0.0000798	-0.0001902
0.4554681	14.1861892	0.0000887	-0.0002113
0.00005000	14.1909283	0.0000976	-0.0002324
0.3080092	14.1956783	0.0001065	-0.0002535
0.00005625	14.2004394	0.0001154	-0.0002746
0.3458573	14.2052115	0.0001243	-0.0002957
0.00006250	14.2099947	0.0001332	-0.0003168
0.3835595	14.2147891	0.0001421	-0.0003379
0.00006875	14.21925946	0.0001511	-0.0003589
0.4211155	14.2244115	0.0001600	-0.0003800
0.00007500	14.2292396	0.0001690	-0.0004010
0.4585249	14.2340792	0.0001779	-0.0004221
0.00008125	14.2389301	0.0001869	-0.0004431
0.4957876	14.2437926	0.0001959	-0.0004641
0.00008750	14.2486666	0.0002048	-0.0004852
0.5329033	14.2535522	0.0002138	-0.0005062
0.5698716	14.2584494	0.0002228	-0.0005272
0.6066924	14.2633583	0.0002318	-0.0005482
0.0000106	14.2682790	0.0002408	-0.0005692
0.0000106	14.2732116	0.0002498	-0.0005902
0.0000106	14.2781560	0.0002588	-0.0006112
0.6433653	14.2831123	0.0002678	-0.0006322
0.6798902	14.2880807	0.0002768	-0.0006532
0.7162666	14.2930611	0.0002859	-0.0006741
0.7524943	14.2980536	0.0002949	-0.0006951
0.7885732	14.3030584	0.0003039	-0.0007161
0.8245028	14.3080753	0.0003130	-0.0007370
0.8602829	14.3130466	0.0003220	-0.0007580
0.8959132	14.3181462	0.0003311	-0.0007789
0.9313934	14.3232002	0.0003402	-0.0007998
0.9672234			
1.0019026			
1.0369310			
1.0748061			
1.1065338			
1.1410076			
1.1735234			
1.2009986			
1.2349113			
1.2728763			
1.3116888			
1.3515890			
1.3924667			
1.4343466			
1.4772328			
1.5211197			
1.5659966			
1.6118796			
1.6587619			
1.7066410			
1.7545137			
1.8023826			
1.8502510			
1.8981196			
1.9459844			
2.0000000			
2.0500000			
2.1000000			
2.1500000			
2.2000000			
2.2500000			
2.3000000			
2.3500000			
2.4000000			
2.4500000			
2.5000000			
2.5500000			
2.6000000			
2.6500000			
2.7000000			
2.7500000			
2.8000000			
2.8500000			
2.9000000			
2.9500000			
3.0000000			
3.0500000			
3.1000000			
3.1500000			
3.2000000			
3.2500000			
3.3000000			
3.3500000			
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3.6500000			
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3.7500000			
3.8000000			
3.8500000			
3.9000000			
3.9500000			
4.0000000			

Pier 22af.1p7o		Pier 22af.1p7o	
Load No.	Axial Thrust kips	Nominal Mgm. Cap. in-kip	Max. Comp. Strain
1	0.000	40395.232	0.00300000
Note note that the values of moment capacity in the table above are not factored by a strength reduction factor (phi-factor).			
In ACI 318-08, the value of the strength reduction factor depends on whether the transverse reinforcing steel bars are tied hoops (0.65) or spirals (0.70).			
The above values should be multiplied by the appropriate strength reduction factor to compute ultimate moment capacity according to ACI 318-08, Section			
Page 12			

Pier 22af.1p7o		Pier 22af.1p7o	
Load No.	Axial Thrust kips	Nominal Mgm. Cap. in-kip	Max. Comp. Strain
1	0.000	40395.232	0.00300000
Note note that the values of moment capacity in the table above are not factored by a strength reduction factor (phi-factor).			
In ACI 318-08, the value of the strength reduction factor depends on whether the transverse reinforcing steel bars are tied hoops (0.65) or spirals (0.70).			
The above values should be multiplied by the appropriate strength reduction factor to compute ultimate moment capacity according to ACI 318-08, Section			
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1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	31	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48	49	50			
0.79000	0.79000	0.79000	0.79000	0.79000	0.79000	0.79000	0.79000	0.79000	0.79000	0.79000	0.79000	0.79000	0.79000	0.79000	0.79000	0.79000	0.79000	0.79000	0.79000	0.79000	0.79000	0.79000	0.79000	0.79000	0.79000	0.79000	0.79000	0.79000	0.79000	0.79000	0.79000	0.79000	0.79000	0.79000	0.79000	0.79000	0.79000	0.79000	0.79000	0.79000	0.79000	0.79000	0.79000	0.79000	0.79000	0.79000	0.79000	0.79000	0.79000			
18.99342	18.99342	18.52104	18.27238	16.88491	16.40321	14.18784	13.50337	10.59930	9.75507	6.34476	5.39382	1.69156	0.69365	-3.06793	-4.05010	-7.63464	-8.53937	-11.72165	-12.49207	-15.07214	-15.65986	-17.47560	-17.84368	-18.78099	-18.90631	-18.78099	-17.84368	-17.47560	-15.65986	-15.07214	-12.49207	-8.53937	-7.63464	-4.05010	0.69365	1.69156	5.39382	6.34476	9.75507	10.59930	13.50337	14.18784	16.40321	16.88491	18.27238	18.52104	18.99342					
1.00000	1.00000	1.00000	1.00000	1.00000	1.00000	1.00000	1.00000	1.00000	1.00000	1.00000	1.00000	1.00000	1.00000	1.00000	1.00000	1.00000	1.00000	1.00000	1.00000	1.00000	1.00000	1.00000	1.00000	1.00000	1.00000	1.00000	1.00000	1.00000	1.00000	1.00000	1.00000	1.00000	1.00000	1.00000	1.00000	1.00000	1.00000	1.00000	1.00000	1.00000	1.00000	1.00000	1.00000	1.00000	1.00000	1.00000	1.00000	1.00000	1.00000	1.00000		
0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000		
0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000

NOTE: The positions of the above rebars were computed by LPile

Minimum spacing between any two bars not equal to zero = -0.0001154 inches between Bars 1 and 2

Spacing to aggregate size ratio = -0.0003078

Concrete Properties:

Pier 22af.jp7o

9.3.2.2 or the value required by the design standard being followed.

The following table presents factored moment capacities and corresponding bending stiffnesses computed for common resistance factor values used for reinforced concrete sections.

Axial Load Capacity at Ult. Moment	Resistance Factor	Nominal Moment Capacity at Ult. Mom. Cap. for Moment	Ultimate (Factored) Axial Thrust	Ultimate Moment
26256.900	0.65	406260579.288	0.000	
28276.662	0.70	404789053.314	0.000	
30296.424	0.75	398293409.577	0.000	

Pile Section No. 2:

Dimensions and Properties of Drilled shaft (Bored Pile) with Permanent Casing:

Length of Section	=	91.00000 ft
Outer Diameter of Casing	=	49.00000 in
Concrete Cover Thickness	=	4.50000 in
Casing Wall Thickness	=	0.50000 in
Moment of Inertia of Steel Casing	=	22403. in^4
Yield Stress of Casing	=	36000. psi
Elastic Modulus of Casing	=	290000000. psi
Number of Reinforcing Bars	=	50 bars
Area of Single Reinforcing Bar	=	0.79000 sq. in.
Edge-to-Edge Bar Spacing	=	2.76901 in
Maximum Concrete Aggregate Size	=	0.37500 in
Ratio of Bar Spacing to Aggregate Size	=	7.38
Offset of Center of Rebar Cage from Center of Pile	=	0.00000 in
Yield Stress of Reinforcing Bars	=	60000. psi
Modulus of Elasticity of Reinforcing Bars	=	290000000. psi
Gross Area of Pile	=	1895.74099 sq. in.
Area of Concrete	=	1770.03737 sq. in.
Cross-sectional Area of Steel Casing	=	176.18362 sq. in.
Area of All Steel (Casing and Bars)	=	115.68362 sq. in.
Area Ratio of All Steel to Gross Area of Pile	=	6.13 percent

Axial Structural Capacities:

Nom. Axial Structural Capacity = 0.85 Fc Ac + Fy As	=	9626.257 kips
Tensile Load for Cracking of Concrete	=	-1029.818 kips
Nominal Axial Tensile Capacity	=	-5112.610 kips

Reinforcing Bar Dimensions and Positions Used in Computations:

Bar Number	Bar Diam. inches	Bar Area sq. in.	X inches	Y inches

Compressive strength of Concrete = 3000.00000 psi
 Modulus of Elasticity of Concrete = 3122019. psi
 Modulus of Rupture of Concrete = -410.79191 psi
 Compression Strain at Peak Stress = 0.00163
 Tensile Strain at Fracture of Concrete = -0.0001160
 Maximum Coarse Aggregate Size = 0.37500 in

Number of Axial Thrust Force Values Determined from Pile-head Loadings = 1

Number	Axial Thrust Force kips
1	0.000

Definitions of Run Messages and Notes:

C = concrete in section has cracked in tension.
 Y = stress in reinforcing steel has reached yield stress.
 T = ACI 318-08 criteria for tension-controlled section met, tensile strain in reinforcement exceeds 0.005 while simultaneously compressive strain in concrete more than 0.003. See ACI 318-08, Section 10.3.4.
 Z = depth of tensile zone in concrete section is less than 10 percent of section depth.

Bending stiffness (EI) = Computed Bending Moment / Curvature.
 Position of neutral axis is measured from edge of compression side of pile.
 Compressive stresses and strains are positive in sign.
 Tensile stresses and strains are negative in sign.

Axial Thrust Force = 0.000 kips

Bending Curvature rad/in.	Bending Moment in-kip	Bending Stress kpsi	Max Casting Stress kpsi	Max Casting Strain	Depth to Run N Axis in	Max Comp Strain in/in	Max Tens Strain in/in
0.00000625	1115.4130428	1784660668	1784660668	0.0000153	24.5001514	0.0000153	-0.0000153
0.00000120	227.1564098	178177128	178177128	0.0000306	24.5001519	0.0000306	-0.0000306
0.00000125	335.5301009	178853367	178853367	0.0000459	24.5001524	0.0000459	-0.0000459
0.00000250	4439.874163	173598447	173598447	0.0000613	24.5001529	0.0000613	-0.0000613
0.00000375	17584986	17584986	17584986	0.0000766	24.5001534	0.0000766	-0.0000766
0.00000500	5540.684359	175053596	175053596	0.0000919	24.5001539	0.0000919	-0.0000919
0.00000625	6638.973137	176374193	176374193	0.0001072	24.5001544	0.0001072	-0.0001072
0.00000750	7731.073727	176732842	176732842	0.0001491	19.1836393	0.0001491	-0.0001491
0.00000875	7731.073727	154633672	154633672	0.0000959	19.1903888	0.0000959	-0.0000959
0.00001000	7731.073727	137451875	137451875	0.0001079	19.1903888	0.0001079	-0.0001079
0.00001125	7731.073727	1237066897	1237066897	0.0001200	19.1971550	0.0001200	-0.0001200
0.00001250	7731.073727	1237066897	1237066897	0.0001863			

0.4192925	-5.3573594	7866.3604171	7866.3604171	0.00006875	3000.00000	psi
1144197879	-5.3573594	7866.3604171	7866.3604171	0.00006875	3000.00000	psi
1144197879	-5.8917429	8577.8442105	8577.8442105	0.00007500	-410.79191	psi
1143712561	-5.8917429	8577.8442105	8577.8442105	0.00007500	-410.79191	psi
1143712561	-6.4258769	9288.7128352	9288.7128352	0.00008125	0.00163	
1143226195	-6.4258769	9288.7128352	9288.7128352	0.00008125	0.00163	
1142738775	-6.9597604	9938.9642814	9938.9642814	0.00008750	-0.0001160	
1142738775	-6.9597604	9938.9642814	9938.9642814	0.00008750	-0.0001160	
1142738775	-7.4933924	10709.	10709.	0.00009375	0.37500	in
114250296.	-7.4933924	10709.	10709.	0.00009375	0.37500	in
1141760753.	-8.0267719	11418.	11418.	0.000100		
1141760753.	-8.0267719	11418.	11418.	0.000100		
1141760753.	-8.5598981	12126.	12126.	0.000106		
1141760753.	-8.5598981	12126.	12126.	0.000106		
1140778456.	-9.0927699	12834.	12834.	0.000113		
1140778456.	-9.0927699	12834.	12834.	0.000113		
1140778456.	-9.6253864	13541.	13541.	0.000119		
1140778456.	-9.6253864	13541.	13541.	0.000119		
1140285692.	-10.1577466	14247.	14247.	0.000125		
1140285692.	-10.1577466	14247.	14247.	0.000125		
1139791843.	-10.6898495	14953.	14953.	0.000131		
1139791843.	-10.6898495	14953.	14953.	0.000131		
1139296905.	-11.2216941	15659.	15659.	0.000138		
1139296905.	-11.2216941	15659.	15659.	0.000138		
113800871.	-11.7532794	16363.	16363.	0.000144		
113800871.	-11.7532794	16363.	16363.	0.000144		
1138303738.	-12.2846044	17067.	17067.	0.000150		
1138303738.	-12.2846044	17067.	17067.	0.000150		
1137805500.	-12.8156681	17770.	17770.	0.000156		
1137805500.	-12.8156681	17770.	17770.	0.000156		
1137306150.	-13.3464694	18473.	18473.	0.000163		
1137306150.	-13.3464694	18473.	18473.	0.000163		
1136805685.	-13.8770074	19175.	19175.	0.000169		
1136805685.	-13.8770074	19175.	19175.	0.000169		
1136304097.	-14.4072809	19877.	19877.	0.000175		
1136304097.	-14.4072809	19877.	19877.	0.000175		
1135801383.	-14.9372890	20577.	20577.	0.000181		
1135801383.	-14.9372890	20577.	20577.	0.000181		
1135297536.	-15.4670306	21277.	21277.	0.000188		
1135297536.	-15.4670306	21277.	21277.	0.000188		
1134792551.	-15.9965046	22676.	22676.	0.000194		
1134792551.	-15.9965046	22676.	22676.	0.000194		
1134286421.	-16.5257100	23374.	23374.	0.000200		
1134286421.	-16.5257100	23374.	23374.	0.000200		
1133779143.	-17.0546456	24071.	24071.	0.000206		
1133779143.	-17.0546456	24071.	24071.	0.000206		
1133270763.	-17.5833338	24768.	24768.	0.000213		
1133270763.	-17.5833338	24768.	24768.	0.000213		
1132761317.	-18.1117940	25464.	25464.	0.000219		
1132761317.	-18.1117940	25464.	25464.	0.000219		
113250725.	-18.6399854	26854.	26854.	0.000225		
113250725.	-18.6399854	26854.	26854.	0.000225		
1131738979.	-19.1679070	28584.	28584.	0.000231		
1131738979.	-19.1679070	28584.	28584.	0.000231		
1131226073.	-19.6955577	29935.	29935.	0.000238		
1131226073.	-19.6955577	29935.	29935.	0.000238		
1130712000.	-20.2229365	30318.	30318.	0.000244		
1130712000.	-20.2229365	30318.	30318.	0.000244		
1130196756.	-20.7500422	28935.	28935.	0.000250		
1130196756.	-20.7500422	28935.	28935.	0.000250		
1129500422.	-21.8034304	30318.	30318.	0.000256		
1129500422.	-21.8034304	30318.	30318.	0.000256		
112842529.	-22.8557126			0.000269		
112842529.	-22.8557126			0.000269		

Pier 22af. p70		Pier 22af. p70	
0.0000281	31699.	1127080336.	19.4438834
1.6534998	-23.9068801	-23.9068801	C
0.0000294	33077.	1126031888.	C
1.7148669	-24.9569237	-24.9569237	C
0.0000306	34452.	1124978535.	C
1.7730441	-26.0058841	-26.0058841	C
0.0000319	3825.	1123020225.	C
1.8299355	-27.0536017	-27.0536017	C
0.0000331	37195.	112102161.	C
1.885654	-28.1002161	-28.1002161	C
0.0000344	38361.	111788598.	C
1.9399280	-29.1456692	-29.1456692	C
0.0000356	39925.	1120715069.	C
1.9930173	-30.1899502	-30.1899502	C
0.0000369	41287.	1119658414.	C
2.0448273	-31.2330491	-31.2330491	C
0.0000381	42645.	1118325356.	C
2.0935350	-32.2749557	-32.2749557	C
0.0000394	44000.	1117463380.	C
2.1443832	-33.3136395	-33.3136395	C
0.0000406	43352.	1116966890.	C
2.193207	-34.3531700	-34.3531700	C
0.0000419	45008.	111389007.	C
2.2531521	-35.3934163	-35.3934163	C
0.0000431	46008.	111336478.	C
2.2839953	-36.4384689	-36.4384689	C
2.3233319	-37.5086714	-37.5086714	C
2.3657176	-38.5923837	-38.5923837	C
2.4036069	-39.6921668	-39.6921668	C
2.4439917	-40.7975711	-40.7975711	C
2.476489	-41.9113148	-41.9113148	C
0.0000506	54089.	1077128370.	C
2.5079804	-43.0306106	-43.0306106	C
0.0000519	54958.	1059445952.	C
2.5399548	-44.1524278	-44.1524278	C
0.0000531	55805.	105050724.	C
2.5706027	-45.2851505	-45.2851505	C
0.0000544	56630.	1041675325.	C
2.5999562	-46.4202004	-46.4202004	C
0.0000556	57435.	1032534230.	C
2.6280930	-47.5592349	-47.5592349	C
0.0000569	58227.	1023678278.	C
2.6550534	-48.7017720	-48.7017720	C
0.0000581	58992.	1014922893.	C
2.6808669	-49.8475207	-49.8475207	C
0.0000594	59748.	1006284034.	C
2.7055600	-50.9962076	-50.9962076	C
0.0000606	60490.	9977763162.	C
2.7291569	-52.1475779	-52.1475779	C
0.0000619	61220.	989410360.	C
2.7516794	-53.3013873	-53.3013873	C
0.0000631	61938.	981195320.	C
2.7731476	-54.4574027	-54.4574027	C
0.0000644	62646.	973133740.	C
2.7935795	-55.6153994	-55.6153994	C
0.0000656	63344.	965242645.	C
2.8129916	-56.7751596	-56.7751596	C
0.0000669	64026.	957399461.	C
18.8486036	0.0012841	-0.0008313	0.0005469
18.8182436	0.0013055	-0.0008678	0.0005716
18.7906547	0.0013271	-0.0009043	0.0005964
18.7672152	0.0013489	-0.0009407	0.0006212
18.7445517	0.0013707	-0.0009771	0.0006460
18.7249127	0.0013927	-0.0010134	0.0006709
18.6608272	0.0014812	-0.0010498	0.0006959
18.6107997	0.0015703	-0.0010860	0.0007208
18.5316756	0.0016563	-0.0011223	0.0007459
18.4419665	0.0017405	-0.0011585	0.0007709
18.3478736	0.0018233	-0.0011946	0.0007960
18.2534341	0.0019052	-0.0012307	0.0008212
18.1608710	0.0019863	-0.0012671	0.0008461
18.0711279	0.0020669	-0.0013043	0.0008701
17.9848775	0.0021469	-0.0013420	0.0008936
17.9021814	0.0022266	-0.0013802	0.0009167
17.8209154	0.0023056	-0.0014186	0.0009395
17.7417126	0.0023840	-0.0014573	0.0009621
17.6653320	0.0024621	-0.0014962	0.0009844
17.5929514	0.0025400	-0.0015353	0.0010066
17.5227136	0.0026175	-0.0015746	0.0010286
17.4546211	0.0026946	-0.0016140	0.0010504
17.3887355	0.0027713	-0.0016536	0.0010720
17.3238682	0.0028476	-0.0016933	0.0010936
17.2607593	0.0029235	-0.0017331	0.0011150
17.2013139	0.0029995	-0.0017730	0.0011363
17.1447881	0.0030753	-0.0018130	0.0011576
17.0962917	0.0031521	-0.0018531	0.0011787
17.04758580	0.0032289	-0.0018933	0.0011998
17.0000000	0.0033071	-0.0019335	0.0012208
16.95235329	0.0033851	-0.0019738	0.0012418
16.9049000	0.0034627	-0.0020141	0.0012628

Pier 22af.1p7o

Res.	Soil	Deflect.	Bending	Shear	Slope	Total	Soil
X	Spr.	Y	Moment	Force	S	Stress	Stiffness
feet	inches	inches	in-lbs	lbs	radians	psi*	lb-in ²
lb/inch	lb/inch	lb/inch	lb/inch				lb/in
0.000	0.00	0.000	1382400.	10435.	-0.001486	0.000	1.351E+12
0.000	1.122	0.4801	1522928.	10435.	-0.001472	0.000	1.351E+12
0.000	2.244	0.4604	1663456.	10435.	-0.001456	0.000	1.351E+12
0.000	3.367	0.4409	1803984.	10435.	-0.001439	0.000	1.350E+12
0.000	4.489	0.4216	1944511.	10435.	-0.001420	0.000	1.349E+12
0.000	5.611	0.4026	2085039.	10435.	-0.001400	0.000	1.349E+12
0.000	6.733	0.3839	2225567.	10435.	-0.001378	0.000	1.349E+12
0.000	7.855	0.3655	2366095.	10435.	-0.001355	0.000	1.348E+12
0.000	8.978	0.3474	2506623.	10435.	-0.001331	0.000	1.348E+12
0.000	10.100	0.3297	2647151.	10435.	-0.001305	0.000	1.347E+12
0.000	11.222	0.3123	2787678.	10435.	-0.001278	0.000	1.347E+12
0.000	12.344	0.2952	2928206.	10435.	-0.001249	0.000	1.346E+12
0.000	13.466	0.2786	3068734.	10435.	-0.001219	0.000	1.346E+12
0.000	14.589	0.2624	3209262.	10435.	-0.001188	0.000	1.345E+12
0.000	15.711	0.2466	3349790.	10435.	-0.001155	0.000	1.345E+12
0.000	16.833	0.2313	3490318.	10435.	-0.001121	0.000	1.344E+12
0.000	17.955	0.2164	3630846.	10435.	-0.001085	0.000	1.344E+12
0.000	19.077	0.2021	3771373.	10435.	-0.001048	0.000	1.343E+12
0.000	20.200	0.1882	3911901.	10435.	-0.001010	0.000	1.343E+12
0.000	21.322	0.1749	4052429.	10435.	-0.000975	0.000	1.777E+12
0.000	22.444	0.1619	4192957.	10435.	-0.000943	0.000	1.776E+12
0.000	23.566	0.1495	4333485.	10435.	-0.000911	0.000	1.776E+12
0.000	24.688	0.1374	4474013.	10435.	-0.000878	0.000	1.776E+12
0.000	25.811	0.1258	4614540.	10435.	-0.000843	0.000	1.775E+12

Load No.	Axial Thrust kips	Nominal Mom. Cap. in-kip	Max. Comp. Strain
1	0.000	82158.297	0.00300000

Summary of Results for Nominal (Unfactored) Moment Capacity for Section 2

Moment values interpolated at maximum compressive strain = 0.003 or maximum developed moment if pile fails at smaller strains.

Load No.	Axial Thrust kips	Nominal Mom. Cap. in-kip	Max. Comp. Strain
1	0.000	82158.297	0.00300000

Note that the values of moment capacity in the table above are not factored by a strength reduction factor (phi-factor).

In ACI 318-08, the value of the strength reduction factor depends on whether the transverse reinforcing steel bars are tied hoops (0.65) or spirals (0.70). The above values should be multiplied by the appropriate strength reduction factor to compute ultimate moment capacity according to ACI 318-08, section 9.3.2.2 or the value required by the design standard being followed.

The following table presents factored moment capacities and corresponding bending stiffnesses computed for common resistance factor values used for reinforced concrete sections.

Axial Load Capacity for Moment	Resistance Factor	Nominal Bending Stiffness at Ult. Mom. Cap. for Moment	Ultimate (Factored) Axial Thrust	Ultimate Moment
53402.891	0.65	1074989949.193	0.000	
57510.807	0.70	1031678065.076	0.000	
61618.723	0.75	984846872.122	0.000	

Computed Values of Pile Loading and Deflection for Lateral Loading for Load Case Number 1

Pier 22af.jp7c		Pier 22af.jp7o	
0.000	26.933	0.1147	4755068.
0.000	0.000	0.000	0.000
0.000	28.055	0.1041	4895596.
-112.6060	14572.	14572.	0.000
29.177	0.0939	0.0939	5015704.
-116.2977	16674.	16674.	0.000
30.299	0.0843	0.0843	5114721.
-119.3911	19071.	19071.	0.000
89.7042	0.0752	0.0752	5192088.
-89.7042	16062.	16062.	0.000
-97.4332	19689.	19689.	0.000
33.666	0.0586	0.0586	5296618.
-101.4771	23316.	23316.	0.000
-102.2790	26943.	26943.	0.000
-100.2821	30570.	30570.	0.000
-260.7228	92943.	92943.	0.000
-246.0938	103823.	103823.	0.000
-226.5797	114704.	114704.	0.000
40.399	0.0218	0.0218	5009121.
-203.3840	125585.	125585.	0.000
-177.6328	136465.	136465.	0.000
42.644	0.0137	0.0137	4613739.
-150.3626	147346.	147346.	0.000
43.766	0.0104	0.0104	4372675.
-122.5103	158227.	158227.	0.000
44.888	0.007558	0.007558	4109394.
-94.9069	169107.	169107.	0.000
46.010	0.005108	0.005108	3828902.
-68.2735	179988.	179988.	0.000
47.132	0.003049	0.003049	3536030.
-43.2189	190869.	190869.	0.000
48.255	0.001351	0.001351	3235320.
-20.2399	201749.	201749.	0.000
49.377	-1.750E-05	-1.750E-05	2930939.
0.2763	212630.	212630.	0.000
50.499	-0.001087	-0.001087	2626609.
18.0468	223510.	223510.	0.000
51.621	-0.001890	-0.001890	2325551.
31.8665	227100.	227100.	0.000
43.3876	237980.	237980.	0.000
52.0046	-0.002814	-0.002814	1742861.
54.988	-0.002996	-0.002996	1464881.
57.7817	259741.	259741.	1197379.
60.8588	270622.	270622.	0.000
57.232	-0.002939	-0.002939	940914.
61.4446	281503.	281503.	0.000
59.8108	292383.	292383.	695591.
56.2868	303264.	303264.	461115.
51.2572	314145.	314145.	236845.
61.721	-0.001871	-0.001871	21871.
0.000	276.7818	1992118.	0.000
0.000	62.843	-0.001543	-142910.
0.000	251.3764	2194519.	0.000
0.000	63.965	-0.001229	-262106.
0.000	224.4137	2459741.	0.000
0.000	65.088	-0.000941	-340605.
0.000	196.5117	2811339.	0.000
0.000	66.210	-0.000689	-383469.
0.000	168.1729	3288816.	0.000
0.000	67.332	-0.000475	-395835.
0.000	139.7699	3963592.	0.000
0.000	68.454	-0.000301	-382855.
0.000	111.4870	4981792.	0.000
0.000	69.576	-0.000167	-349657.
0.000	83.1297	6713083.	0.000
0.000	70.699	-6.768E-05	-301385.
0.000	37.3076	7422970.	0.000
0.000	71.821	7.697E-07	-246347.
0.000	-0.4263	7459238.	0.000
0.000	72.943	4.419E-05	-191386.
0.000	-24.5961	7495507.	0.000
0.000	74.065	6.816E-05	-140885.
0.000	-38.1229	7531776.	0.000
0.000	75.187	7.782E-05	-97298.
0.000	-43.7334	7568045.	0.000
0.000	76.310	7.759E-05	-61642.
0.000	-43.8131	7604313.	0.000
0.000	77.432	7.109E-05	-33930.
0.000	-40.3377	7640582.	0.000
0.000	78.554	6.115E-05	-13534.
0.000	-34.8619	7676851.	0.000
0.000	-28.5448	7713120.	539.8201
0.000	80.798	3.857E-05	9437.5600
0.000	-22.1983	7749389.	0.000
0.000	81.921	2.827E-05	14310.
0.000	-16.3455	7785657.	0.000
0.000	83.043	1.942E-05	16218.
0.000	-11.2819	7821926.	0.000
0.000	84.165	1.222E-05	16080.
0.000	-7.1323	7858195.	0.000
0.000	85.287	6.655E-06	14649.
0.000	-3.9017	7894464.	0.000
0.000	86.409	2.577E-06	12510.
0.000	-1.5177	7930733.	0.000
0.000	87.532	-2.302E-07	10096.
0.000	0.1362	7967001.	0.000
0.000	88.654	-2.012E-06	7706.6037
0.000	1.1955	8003270.	0.000
0.000	89.776	-3.010E-06	5534.0712
0.000	1.7969	8039539.	0.000
0.000	90.898	-3.446E-06	3687.3888
0.000	-2.0664	8075808.	0.000
0.000	92.020	-3.507E-06	2215.4361
0.000	2.1126	8112076.	0.000
0.000	93.143	-3.343E-06	1126.5874
0.000	2.0229	8148345.	0.000
0.000	94.265	-3.065E-06	408.5752
0.000	1.8627	8184614.	0.000
0.000	95.387	-2.745E-06	20.3551
0.000	1.6760	8220883.	0.000
0.000	96.509	-2.542E-06	-59.9409
0.000	0.1090	605356.	0.000

Pier 22af.jp70		Pier 22af.jp70		Pier 22af.jp70		Pier 22af.jp70		Pier 22af.jp70		Pier 22af.jp70		Pier 22af.jp70	
Res. X	Depth	Deflect.	Bending	Shear	Total	Bending	Soil	Force	Stress	Stiffness	P		
feet	inches	inches	in-lbs	lbs	psi*	lb-in ²	lb/in	lbs	psi*	lb-in ²	lb/in		
Lat. Load	Y	Slope	Moment										
lb/inch	lb/inch	radians	in-lbs										
0.000	0.000	1.0000	1382400.	18562.	0.000	1.351E+12	0.000	18562.	0.000	1.351E+12	0.000		
0.000	1.122	0.9622	1632362.	18562.	0.000	1.351E+12	0.000	18562.	0.000	1.351E+12	0.000		
0.000	2.244	0.9246	1882323.	18562.	0.000	1.350E+12	0.000	18562.	0.000	1.350E+12	0.000		
0.000	3.367	0.8873	2132285.	18562.	0.000	1.349E+12	0.000	18562.	0.000	1.349E+12	0.000		
0.000	4.489	0.8503	2382246.	18562.	0.000	1.348E+12	0.000	18562.	0.000	1.348E+12	0.000		
0.000	5.611	0.8136	2632208.	18562.	0.000	1.347E+12	0.000	18562.	0.000	1.347E+12	0.000		
0.000	6.733	0.7772	2882169.	18562.	0.000	1.346E+12	0.000	18562.	0.000	1.346E+12	0.000		
0.000	7.855	0.7412	3132131.	18562.	0.000	1.345E+12	0.000	18562.	0.000	1.345E+12	0.000		
0.000	8.978	0.7057	3382092.	18562.	0.000	1.345E+12	0.000	18562.	0.000	1.345E+12	0.000		
0.000	10.100	0.6706	3632054.	18562.	0.000	1.344E+12	0.000	18562.	0.000	1.344E+12	0.000		
0.000	11.222	0.6360	3882016.	18562.	0.000	1.343E+12	0.000	18562.	0.000	1.343E+12	0.000		
0.000	12.344	0.6019	4131977.	18562.	0.000	1.342E+12	0.000	18562.	0.000	1.342E+12	0.000		
0.000	13.466	0.5684	4381939.	18562.	0.000	1.341E+12	0.000	18562.	0.000	1.341E+12	0.000		
0.000	14.589	0.5355	4631900.	18562.	0.000	1.340E+12	0.000	18562.	0.000	1.340E+12	0.000		
0.000	15.711	0.5032	4881862.	18562.	0.000	1.339E+12	0.000	18562.	0.000	1.339E+12	0.000		
0.000	16.833	0.4715	5131823.	18562.	0.000	1.339E+12	0.000	18562.	0.000	1.339E+12	0.000		
0.000	17.955	0.4406	5381785.	18562.	0.000	1.338E+12	0.000	18562.	0.000	1.338E+12	0.000		
0.000	19.077	0.4104	5631746.	18562.	0.000	1.337E+12	0.000	18562.	0.000	1.337E+12	0.000		
0.000	20.200	0.3809	5881708.	18562.	0.000	4.240E+11	0.000	18562.	0.000	4.240E+11	0.000		
0.000	21.322	0.3540	6131670.	18562.	0.000	1.771E+12	0.000	18562.	0.000	1.771E+12	0.000		
0.000	22.444	0.3277	6381631.	18562.	0.000	1.771E+12	0.000	18562.	0.000	1.771E+12	0.000		
0.000	23.566	0.3020	6631593.	18562.	0.000	1.770E+12	0.000	18562.	0.000	1.770E+12	0.000		
0.000	24.688	0.2771	6881554.	18562.	0.000	1.769E+12	0.000	18562.	0.000	1.769E+12	0.000		
0.000	25.811	0.2528	7131516.	18562.	0.000	1.769E+12	0.000	18562.	0.000	1.769E+12	0.000		
0.000	26.933	0.2293	7381477.	18562.	0.000	1.768E+12	0.000	18562.	0.000	1.768E+12	0.000		
0.000	28.055	0.2065	7631439.	17609.	0.000	1.767E+12	0.000	17609.	0.000	1.767E+12	0.000		
-141.809	9228.702	7855.900	8053630.	15676.	0.000	1.148E+12	0.000	15676.	0.000	1.148E+12	0.000		
-145.6437	10633.7	16337.0	8053630.	13692.	0.000	1.144E+12	0.000	13692.	0.000	1.144E+12	0.000		
30.299	0.1637	0.1637	8053630.										

Pier 22af.jp70		Pier 22af.jp70		Pier 22af.jp70		Pier 22af.jp70		Pier 22af.jp70		Pier 22af.jp70		Pier 22af.jp70	
Res. X	Depth	Deflect.	Bending	Shear	Total	Bending	Soil	Force	Stress	Stiffness	P		
feet	inches	inches	in-lbs	lbs	psi*	lb-in ²	lb/in	lbs	psi*	lb-in ²	lb/in		
Lat. Load	Y	Slope	Moment										
lb/inch	lb/inch	radians	in-lbs										
0.000	0.000	1.785E+12	0.000	1.785E+12	0.000	1.785E+12	0.000	1.785E+12	0.000	1.785E+12	0.000		
0.000	1.122	1.785E+12	0.000	1.785E+12	0.000	1.785E+12	0.000	1.785E+12	0.000	1.785E+12	0.000		
0.000	2.244	1.785E+12	0.000	1.785E+12	0.000	1.785E+12	0.000	1.785E+12	0.000	1.785E+12	0.000		
0.000	3.367	1.785E+12	0.000	1.785E+12	0.000	1.785E+12	0.000	1.785E+12	0.000	1.785E+12	0.000		
0.000	4.489	1.785E+12	0.000	1.785E+12	0.000	1.785E+12	0.000	1.785E+12	0.000	1.785E+12	0.000		
0.000	5.611	1.785E+12	0.000	1.785E+12	0.000	1.785E+12	0.000	1.785E+12	0.000	1.785E+12	0.000		
0.000	6.733	1.785E+12	0.000	1.785E+12	0.000	1.785E+12	0.000	1.785E+12	0.000	1.785E+12	0.000		
0.000	7.855	1.785E+12	0.000	1.785E+12	0.000	1.785E+12	0.000	1.785E+12	0.000	1.785E+12	0.000		
0.000	8.978	1.785E+12	0.000	1.785E+12	0.000	1.785E+12	0.000	1.785E+12	0.000	1.785E+12	0.000		
0.000	10.100	1.785E+12	0.000	1.785E+12	0.000	1.785E+12	0.000	1.785E+12	0.000	1.785E+12	0.000		
0.000	11.222	1.785E+12	0.000	1.785E+12	0.000	1.785E+12	0.000	1.785E+12	0.000	1.785E+12	0.000		
0.000	12.344	1.785E+12	0.000	1.785E+12	0.000	1.785E+12	0.000	1.785E+12	0.000	1.785E+12	0.000		
0.000	13.466	1.785E+12	0.000	1.785E+12	0.000	1.785E+12	0.000	1.785E+12	0.000	1.785E+12	0.000		
0.000	14.589	1.785E+12	0.000	1.785E+12	0.000	1.785E+12	0.000	1.785E+12	0.000	1.785E+12	0.000		
0.000	15.711	1.785E+12	0.000	1.785E+12	0.000	1.785E+12	0.000	1.785E+12	0.000	1.785E+12	0.000		
0.000	16.833	1.785E+12	0.000	1.785E+12	0.000	1.785E+12	0.000	1.785E+12	0.000	1.785E+12	0.000		
0.000	17.955	1.785E+12	0.000	1.785E+12	0.000	1.785E+12	0.000	1.785E+12	0.000	1.785E+12	0.000		
0.000	19.077	1.785E+12	0.000	1.785E+12	0.000	1.785E+12	0.000	1.785E+12	0.000	1.785E+12	0.000		
0.000	20.200	1.785E+12	0.000	1.785E+12	0.000	1.785E+12	0.000	1.785E+12	0.000	1.785E+12	0.000		
0.000	21.322	1.785E+12	0.000	1.785E+12	0.000	1.785E+12	0.000	1.785E+12	0.000	1.785E+12	0.000		
0.000	22.444	1.785E+12	0.000	1.785E+12	0.000	1.785E+12	0.000	1.785E+12	0.000	1.785E+12	0.000		
0.000	23.566	1.785E+12	0.000	1.785E+12	0.000	1.785E+12	0.000	1.785E+12	0.000	1.785E+12	0.000		
0.000	24.688	1.785E+12	0.000	1.785E+12	0.000	1.785E+12	0.000	1.785E+12	0.000	1.785E+12	0.000		
0.000	25.811	1.785E+12	0.000	1.785E+12	0.000	1.785E+12	0.000	1.785E+12	0.000	1.785E+12	0.000		
0.000	26.933	1.785E+12	0.000	1.785E+12	0.000	1.785E+12	0.000	1.785E+12	0.000	1.785E+12	0.000		
0.000	28.055	1.785E+12	0.000	1.785E+12	0.000	1.785E+12	0.000	1.785E+12	0.000	1.785E+12	0.000		
-141.809	9228.702	7855.900	8053630.	15676.	0.000	1.148E+12	0.000	15676.	0.000	1.148E+12	0.000		
-145.6437	10633.7	16337.0	8053630.	13692.	0.000	1.144E+12	0.000	13692.	0.000	1.144E+12	0.000		
30.299	0.1637	0.1637	8053630.										

* This analysis computed pile response using nonlinear moment-curvature relationships. Values of total stress due to combined axial and bending stresses are computed only for elastic sections only and do not equal the actual stresses in concrete and steel. Stresses in concrete and steel may be interpolated from the output for nonlinear bending properties relative to the magnitude of bending moment developed in the pile.

Output summary for Load Case No. 1:
 Pile-head deflection = 0.5000000 radians
 Computed slope at pile head = -0.0014862 radians
 Maximum bending moment = 5328127. inch-lbs
 Maximum shear force = -22601. lbs
 Depth of maximum bending moment = 35.9104000 feet below pile head
 Depth of maximum shear force = 49.3768000 feet below pile head
 Number of iterations = 7
 Number of zero deflection points = 4

Computed values of Pile Loading and Deflection for Lateral Loading for Load Case Number 2

 Pile-head conditions are Displacement and Moment (Loading Type 4)
 Displacement of pile head = 1382400.0 inches
 Moment at pile head = 1382400.0 lb-ft
 Axial load at pile head = 0.0 lbs

Pier 22af.jp7o		Pier 22af.jp7o	
-148.9554	12251.	0.000	0.000
31.422	0.1443	8224508.	0.000
-172.0553	16062.	0.000	0.000
32.544	0.1261	8364185.	0.000
-184.3309	19689.	0.000	0.000
33.666	0.1092	8470434.	0.000
-189.1118	23316.	0.000	0.000
34.788	0.0937	8542390.	0.000
-187.5033	26943.	0.000	0.000
35.910	0.0796	8580342.	0.000
-180.6164	30570.	0.000	0.000
37.033	0.0668	8585541.	0.000
-460.8503	92943.	8507167.	0.000
38.155	0.0553	8507167.	0.000
-426.6713	103623.	851420.	0.000
39.277	0.0453	851420.	0.000
-385.5094	114704.	8125762.	0.000
40.399	0.0365	8125762.	0.000
-340.4027	125585.	0.000	0.000
41.521	0.0290	7838374.	0.000
-294.1961	136465.	0.000	0.000
42.644	0.0228	7497636.	0.000
-249.2977	147346.	0.000	0.000
43.766	0.0173	7111689.	0.000
-203.3409	158227.	6688868.	0.000
44.888	0.0126	6688868.	0.000
-157.6880	169107.	6237451.	0.000
46.010	0.008493	5765447.	0.000
-113.5205	179988.	5280416.	0.000
47.132	0.005068	4789317.	0.000
-71.8386	190869.	0.000	0.000
48.255	0.002333	4298395.	0.000
-33.4598	201749.	3813095.	0.000
49.377	-6.179E-05	337866.	0.000
0.9756	212630.	2875778.	0.000
50.499	-0.001868	2430124.	0.000
30.9981	223510.	2002641.	0.000
51.621	-0.003235	1394444.	0.000
54.5490	227100.	0.000	0.000
52.743	-0.004213	0.000	0.000
74.4450	237980.	1594444.	0.000
53.866	-0.004850	0.000	0.000
89.6332	248661.	0.000	0.000
54.988	-0.005195	0.000	0.000
100.2002	259741.	0.000	0.000
106.3511	270622.	0.000	0.000
108.6003	281503.	0.000	0.000
106.7577	293383.	0.000	0.000
101.9167	305264.	0.000	0.000
94.4619	317145.	0.000	0.000
61.721	0.003324	0.000	0.000
379.3670	1498623.	0.000	0.000
62.843	0.002982	-112311.	0.000
34.9183	1575923.	0.000	0.000
63.865	0.002453	-313291.	0.000
316.6508	1737805.	0.000	0.000
282.5537	1946574.	-457874.	0.000
		0.000	0.000
66.210	-0.001503	66.210	-550718.
247.7932	2219626.	247.7932	2219626.
67.332	-0.001108	67.332	-598626.
212.7230	2585517.	212.7230	2585517.
68.454	-0.000773	68.454	-607958.
177.7227	3094633.	177.7227	3094633.
69.576	-0.000501	69.576	-585060.
142.9790	3846494.	142.9790	3846494.
70.699	-0.000287	70.699	-536235.
108.3002	5077879.	108.3002	5077879.
71.821	-0.000128	71.821	-467770.
72.943	-1.701E-05	72.943	-386413.
9.4675	7495507.	9.4675	7495507.
74.065	5.506E-05	74.065	-303339.
-30.7956	7531776.	-30.7956	7531776.
75.187	9.631E-05	75.187	-225849.
-54.1244	7568045.	-54.1244	7568045.
76.310	0.000115	76.310	-158175.
-64.7164	7604313.	-64.7164	7604313.
77.432	0.000117	77.432	-102237.
-66.2877	7640382.	-66.2877	7640382.
78.534	0.000109	78.534	-58319.
-61.9487	7676851.	-61.9487	7676851.
79.676	9.458E-05	79.676	-25636.
-54.1715	771320.	-54.1715	771320.
80.798	7.788E-05	80.798	-2776.0811
-44.8194	7749389.	-44.8194	7749389.
81.921	6.091E-05	81.921	11956.
-35.2143	7783657.	-35.2143	7783657.
83.043	4.515E-05	83.043	20302.
-26.2234	7821926.	-26.2234	7821926.
84.165	3.145E-05	84.165	23893.
-18.3514	7858195.	-18.3514	7858195.
85.287	2.018E-05	85.287	24156.
-11.8289	7894464.	-11.8289	7894464.
86.409	1.139E-05	86.409	0.000
-6.6912	7930733.	-6.6912	7930733.
87.532	2.047E-07	87.532	19178.
-2.8450	4.809E-06	-2.8450	4.809E-06
-0.1217	8005270.	-0.1217	8005270.
1.6822	8039339.	1.6822	8039339.
2.775	8075608.	2.775	8075608.
3.3512	8115764E-06	3.3512	8115764E-06
3.573	8148317E-06	3.573	8148317E-06
3.574	8148317E-06	3.574	8148317E-06
3.585	8182419.	3.585	8182419.
3.585	8220883.	3.585	8220883.
3.4698	8220883.	3.4698	8220883.
0.2409	50960535E-06	0.2409	50960535E-06
0.2311	631628024.	0.2311	631628024.
0.2173	754497E-06	0.2173	754497E-06
0.2173	998764004E-06	0.2173	998764004E-06
0.2002	673360.	0.2002	673360.
100.998	-3.494E-06	100.998	-3.494E-06

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0.1806	696028.	0.000	-6.0148	3.796E-08	0.000	1.785E+12	0.000	1.785E+12	0.000	1.351E+12
102.120	-2.980E-06	-54.3881	-4.0276	3.730E-08	0.000	1.785E+12	0.000	1.785E+12	0.000	1.351E+12
0.1591	718696.	0.000	-2.3567	3.623E-08	0.000	1.785E+12	0.000	1.785E+12	0.000	1.349E+12
103.242	-2.472E-06	-120.9643	-1.0135	3.492E-08	0.000	1.785E+12	0.000	1.785E+12	0.000	1.348E+12
0.1361	7411364.	0.000	0.7953	3.350E-08	0.000	1.785E+12	0.000	1.785E+12	0.000	1.347E+12
104.365	-1.976E-06	-162.8636	2.7424	3.217E-08	0.000	1.785E+12	0.000	1.785E+12	0.000	1.346E+12
0.1121	764032.	0.000	3.6834	3.112E-08	0.000	1.785E+12	0.000	1.785E+12	0.000	1.345E+12
105.487	-1.496E-06	-184.4361	3.5762	3.044E-08	0.000	1.785E+12	0.000	1.785E+12	0.000	1.344E+12
0.0874	786700.	0.000	2.3693	3.012E-08	0.000	1.785E+12	0.000	1.785E+12	0.000	1.343E+12
106.609	-1.035E-06	-190.1593	0.0000	3.005E-08	0.000	1.785E+12	0.000	1.785E+12	0.000	1.341E+12
0.1812	2357637.	0.000	0.0000	3.000E-08	0.000	1.785E+12	0.000	1.785E+12	0.000	1.340E+12
0.1079	2448309.	0.000								
0.0318	2538981.	0.000								
108.853	-1.687E-07	-116.2987								
109.976	2.444E-07	-63.8123								
-0.0477	2629653.	0.000								
111.098	6.511E-07	-19.9810								
-0.1315	2720325.	0.000								
112.220	1.056E-06	0.000								
-0.2204	1405499.	0.000								

* This analysis computed pile response using nonlinear moment-curvature relationships.

Values of total stress due to combined axial and bending stresses are computed only for elastic sections only and do not equal the actual stresses in concrete and steel.

Stresses in concrete and steel may be interpolated from the output for nonlinear bending properties relative to the magnitude of bending moment developed in the pile.

Output Summary for Load Case No. 2:

Pile-head deflection	=	1.0000000 inches
Computed slope at pile head	=	-0.0028132 radians
Maximum bending moment	=	8585541. inch-lbs
Maximum shear force	=	-36462. lbs
Depth of maximum bending moment	=	37.0326000 feet below pile head
Depth of maximum shear force	=	49.3768000 feet below pile head
Number of iterations	=	38
Number of zero deflection points	=	4

Computed Values of Pile Loading and Deflection for Lateral Loading for Load Case Number 3

Displacement of pile head	=	1382400.0 in
Moment at pile head	=	8585541.0 in-lb
Axial load at pile head	=	0.0 lbs

Depth	Deflect.	Bending	Shear	Slope	Total	Bending	soil
Res. X	Soil Spr.	y	Force	S	Stress	stiffness	P
feet	inches	in-lbs	lbs	radians	psi*	lb-in ²	lb/in

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0.000	0.000	1.5000	1382400.	24084.	-0.004389	0.000	1.351E+12
0.000	1.122	0.000	1706731.	24084.	-0.004374	0.000	1.351E+12
0.000	2.244	0.000	2031061.	24084.	-0.004355	0.000	1.349E+12
0.000	3.367	0.000	2355392.	24084.	-0.004334	0.000	1.348E+12
0.000	4.489	0.000	2679723.	24084.	-0.004308	0.000	1.347E+12
0.000	5.611	0.000	3004053.	24084.	-0.004280	0.000	1.346E+12
0.000	6.733	0.000	3328384.	24084.	-0.004248	0.000	1.345E+12
0.000	7.855	0.000	3652715.	24084.	-0.004213	0.000	1.344E+12
0.000	8.978	0.000	3977045.	24084.	-0.004175	0.000	1.343E+12
0.000	10.100	0.000	4301376.	24084.	-0.004134	0.000	1.341E+12
0.000	11.222	0.000	4625707.	24084.	-0.004089	0.000	1.340E+12
0.000	12.344	0.000	4950037.	24084.	-0.004041	0.000	1.339E+12
0.000	13.466	0.000	5274368.	24084.	-0.003989	0.000	1.338E+12
0.000	14.589	0.000	5598698.	24084.	-0.003934	0.000	1.337E+12
0.000	15.711	0.000	5923029.	24084.	-0.003812	0.000	4.224E+11
0.000	16.833	0.000	6247360.	24084.	-0.003617	0.000	4.189E+11
0.000	17.955	0.000	6571690.	24084.	-0.003411	0.000	4.187E+11
0.000	19.077	0.000	6896021.	24084.	-0.003194	0.000	4.186E+11
0.000	20.200	0.000	7220352.	24084.	-0.002967	0.000	4.184E+11
0.000	21.322	0.000	7544682.	24084.	-0.002822	0.000	1.768E+12
0.000	22.444	0.000	7869013.	24084.	-0.002747	0.000	1.144E+12
0.000	23.566	0.000	8193344.	24084.	-0.002653	0.000	1.144E+12
0.000	24.688	0.000	8517674.	24084.	-0.002554	0.000	1.144E+12
0.000	25.811	0.000	8842005.	24084.	-0.002452	0.000	1.144E+12
0.000	26.933	0.000	9166336.	24084.	-0.002346	0.000	1.143E+12
0.000	28.055	0.000	9490666.	23026.	-0.002236	0.000	1.143E+12
-157.1463	7482.7252	0.000	9814996.	20878.	-0.002123	0.000	1.143E+12
-161.9173	8602.7435	0.000	10057971.	18672.	-0.002006	0.000	1.143E+12
-165.7687	9893.0267	0.000	10289381.	15954.	-0.001886	0.000	1.143E+12
-173.8750	16062.	0.000	10482654.	12631.	-0.001763	0.000	1.142E+12
-255.6524	19689.	0.000	10629566.	9138.2042	-0.001639	0.000	1.142E+12
-263.0716	23316.	0.000					

Pier 22af, lp7o		Pier 22af, lp7o	
34.788	10728771.	5605.9854	-0.001513
-261.5242	0.1307	2145.5770	-0.001386
35.910	26943.	-3281.7306	-0.001259
-252.4095	0.1112	-10724.	-0.001132
37.033	10780551.	-17929.	-0.001008
-553.6423	0.0000	-24568.	-0.000886
38.155	10786558.	-30379.	-0.000767
-551.7336	0.0000	-35213.	-0.000654
39.277	10692165.	-38985.	-0.000547
-518.3206	10692165.	-41833.	-0.000445
-467.6126	10497718.	-43928.	-0.000353
40.399	10209277.	-45275.	-0.000284
-395.4890	0.0000	-45955.	-0.000231
41.521	9836038.	-46028.	-0.000184
42.644	9991079.	-45567.	-0.000141
43.766	8887640.	-44667.	-0.000104
-237.6596	0.0000	-43411.	-7.017E-05
44.888	8341103.	-41869.	-4.129E-05
-185.2634	169107.	-40117.	-1.671E-05
46.010	0.009420	-38231.	3.772E-06
-125.9083	179988.	0.0000	0.0000
47.132	0.005235	0.0000	0.0000
-74.1947	190869.	0.0000	0.0000
48.255	0.001783	0.0000	0.0000
-26.7128	201749.	0.0000	0.0000
49.377	0.000999	0.0000	0.0000
50.499	-0.003174	0.0000	0.0000
52.6842	223510.	0.0000	0.0000
81.0786	227100.	0.0000	0.0000
52.743	0.005962	0.0000	0.0000
105.3591	237980.	0.0000	0.0000
53.866	-0.006698	0.0000	0.0000
123.7730	248861.	0.0000	0.0000
54.988	-0.007074	0.0000	0.0000
136.4445	259741.	0.0000	0.0000
56.110	-0.007148	0.0000	0.0000
143.6394	270622.	0.0000	0.0000
57.232	0.006972	0.0000	0.0000
145.7524	281503.	0.0000	0.0000
58.354	-0.006600	0.0000	0.0000
143.2928	292383.	0.0000	0.0000
59.477	-0.006078	0.0000	0.0000
136.8729	303284.	0.0000	0.0000
60.599	0.005453	0.0000	0.0000
127.1994	314145.	0.0000	0.0000
441.2678	1246473	0.0000	0.0000
407.5494	1350256	0.0000	0.0000
371.07465	1482083371	0.0000	0.0000
371.07465	1482083371	0.0000	0.0000
333.1811	165073718	0.0000	0.0000
333.66210	0.002122	0.0000	0.0000
294.3770	1868318	0.0000	0.0000
255.1798	2155199	0.0000	0.0000
255.68454	-0.001143	0.0000	0.0000
216.0355	2545607	0.0000	0.0000
69.576	-0.000769	2599.1295	2.495E-05
177.2074	3103203.	0.0000	1.142E+12
138.6777	-0.000471	4726.0475	1.951E-05
99.7315	3965031.	6331.3042	1.455E-05
72.943	-0.000244	7299.5967	1.023E-05
44.0772	5512413.	7476.1165	6.658E-06
-17.8609	7495507.	6976.9689	3.844E-06
75.187	3.193E-05	6097.1905	1.739E-06
-56.2714	7531776.	5074.6169	2.529E-07
76.310	0.000100	4039.6515	-7.172E-07
-74.3913	7568045.	3040.2063	-1.277E-06
-77.4790	7595548.	2136.0333	-1.527E-06
-79.676	0.000147	1381.2890	-1.561E-06
-72.2036	0.000142	787.0492	-1.454E-06
-62.0821	0.000128	343.5526	-1.267E-06
81.921	0.000108	32.4053	-1.046E-06
83.043	8.650E-05	-168.7754	-8.208E-07
-38.2444	7821926.	-283.0464	-6.130E-07
-27.6228	7858195.	-331.9479	-4.339E-07
-18.5882	7894464.	-334.2173	-2.886E-07
-11.2908	7930733.	-305.1937	-1.773E-07
-5.6805	7967001.	12563.	0.0000
-1.5822	8003270.	8731.1226	0.0000
1.2432	8039539.	5648.6428	0.0000
30.898	8075608.	3413.5312	0.0000
32.020	-6.860E-06	2061.2931	0.0000
4.1327	8112076.	1589.3162	0.0000
4.6727	8148345.	1190.9707	0.0000
4.8685	8184614.	831.9662	0.0000
4.8941	8220883.	606.4642	0.0000
0.3454	6055336	502.6992	0.0000
0.3387	631620733E-06	308.4642	0.0000
0.3388	754620733E-06	124.6513	0.0000
0.3035	87650609E-06	124.6513	0.0000
0.3035	87650609E-06	124.6513	0.0000
0.2780	998696028.	124.6513	0.0000
0.2486	120.24.4.659E-06	124.6513	0.0000
0.2161	103.242.3.925E-06	124.6513	0.0000
0.2161	104.365.3.193E-06	124.6513	0.0000
0.1812	764032.	124.6513	0.0000

Pier 22af.lp7o
 -3.9792 5.282E-08 0.000 1.785E+12 0.000 1.7600 2623674. 30725. -0.005906 0.000 1.347E+12
 0.1445 786700. -180.2945 0.000 1.785E+12 0.000 0.000 0.000 30725. -0.005878 0.000 1.346E+12
 0.106 609 -1.770E-06 -220.7826 0.000 1.785E+12 0.000 1.6807 3037431. 30725. -0.005845 0.000 1.344E+12
 0.3100 2357637. 0.000 1.785E+12 0.000 1.6017 3451189. 30725. -0.005809 0.000 1.343E+12
 0.1983 2448309. -205.0597 0.000 1.785E+12 0.000 1.5233 3864947. 30725. -0.005768 0.000 1.342E+12
 0.108 853 -4.318E-07 -153.3754 0.000 1.785E+12 0.000 1.4453 4278705. 30725. -0.005723 0.000 1.340E+12
 0.0814 2538981. 0.000 1.785E+12 0.000 1.3679 4692463. 30725. -0.005673 0.000 1.339E+12
 -0.0413 2629653. 0.000 1.785E+12 0.000 1.2912 5106221. 30725. -0.005620 0.000 1.337E+12
 0.111 098 8.460E-07 -27.9675 0.000 1.785E+12 0.000 1.2151 5519979. 30725. -0.005497 0.000 4.221E+11
 -0.1709 2720325. 0.000 1.785E+12 0.000 1.1398 5933736. 30725. -0.005301 0.000 4.189E+11
 0.112 220 1.478E-06 0.000 1.785E+12 0.000 1.0671 6347494. 30725. -0.005090 0.000 4.186E+11
 -0.3084 1405499. 0.000 1.785E+12 0.000 0.9970 6761252. 30725. -0.004866 0.000 4.184E+11
 0.000 0.000 0.8660 7588768. 30725. -0.004628 0.000 4.182E+11
 0.000 0.000 0.8053 8002526. 30725. -0.004377 0.000 4.179E+11
 0.000 0.000 0.7481 8416284. 30725. -0.004112 0.000 4.177E+11
 0.000 0.000 0.6946 8830042. 30725. -0.003834 0.000 4.175E+11
 0.000 0.000 0.6448 9243799. 30725. -0.003637 0.000 1.143E+12
 0.000 0.000 0.5966 9657557. 30725. -0.003526 0.000 1.143E+12
 0.000 0.000 0.5499 10071315. 30725. -0.003410 0.000 1.143E+12
 0.000 0.000 0.5048 10485073. 30725. -0.003289 0.000 1.142E+12
 0.000 0.000 0.4613 10898831. 30725. -0.003163 0.000 1.142E+12
 0.000 0.000 0.4196 11312589. 30725. -0.003032 0.000 1.142E+12
 0.000 0.000 0.3797 11726347. 29558. -0.002896 0.000 1.142E+12
 -175.3217 6148.8121 0.000 11726347. 29558. -0.002755 0.000 1.141E+12
 -23.177 0.3516 12106668. 27187. -0.002610 0.000 1.141E+12
 -178.84589 7050.3705 12458557. 24748. -0.002461 0.000 1.141E+12
 39.7239 8084.3271 12775190. 21334. -0.002309 0.000 1.141E+12
 -183.3742 0.000 12775190. 21334. -0.002154 0.000 1.141E+12
 -323.5832 1605324 13023748. 16801. -0.002039 0.000 1.140E+12
 -349.6724 19689 13272691. 12009. -0.001997 0.000 1.140E+12
 -362.0426 23116 13356582. 7130.9168 -0.001839 0.000 1.140E+12
 -362.34788 26943 13419748. 2316.5872 -0.001680 0.000 1.140E+12
 -352.5825 30570 13418975. -4244.3384 -0.001523 0.000 1.140E+12
 -37.033 0.000 13418975. -4244.3384 -0.001463 0.000 1.140E+12
 -621.8317 63621 13305436. -12643. -0.001378 0.000 1.140E+12
 38.155 0.1101 13305436. -12643. -0.001264 0.000 1.140E+12

* This analysis computed pile response using nonlinear moment-curvature relationships.
 Values of total stress due to combined axial and bending stresses are computed only for elastic sections only and do not equal the actual stresses in concrete and steel.
 Stresses in concrete and steel may be interpolated from the output for nonlinear bending properties relative to the magnitude of bending moment developed in the pile.

Output Summary for Load Case No. 3:

Pile-head deflection = 1.500000 inches
 Computed slope at pile head = -0.0043895 radians
 Maximum bending moment = 10786558. inch-lbs
 Maximum shear force = -46028. lbs
 Depth of maximum bending moment = 37.0326000 feet below pile head
 Depth of maximum shear force = 49.3768000 feet below pile head
 Number of iterations = 52
 Number of zero deflection points = 4

 Computed values of Pile Loading and Deflection
 For Lateral Loading For Load Case Number 4

Pile-head conditions are Displacement and Moment (Loading Type 4)
 Displacement of pile head = 2.000000 inches
 Moment at pile head = 1382400.0 in-lbs
 Axial load at pile head = 0.0 lbs

Res.	Depth	Deflect.	Bending	Shear	Slope	Total	Bending	Soil
X	Y	Lat.	Moment	Force	S	Stress	Stiffness	P
feet	inches	inches	in-lbs	lbs	radians	psi*	lb-in ²	lb/in
0.000	0.000	2.0000	1382400.	30725.	-0.005966	0.000	1.351E+12	STR-V
0.000	1.122	0.000	1796158.	30725.	-0.005950	0.000	1.351E+12	Δ = 2.0
0.000	2.244	0.000	2209916.	30725.	-0.005930	0.000	1.349E+12	LATERAL RFBST AN (F = 38.73
0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	

Pier 22af.lp7o

0.2077 2538981. 0.0000 5.7801 7.973E-08 0.000 1.785E+12

109.976 -2.199E-08 -118.1490 0.000 1.785E+12

0.004295 2629653. 0.0000 4.3868 7.913E-08 0.000 1.785E+12

111.098 1.046E-06 -39.9217 0.000 7.898E-08 0.000 1.785E+12

-0.2112 2720325. 0.0000 0.000 0.000 0.000 0.000

112.220 2.109E-06 0.0000 0.000 0.000 0.000 0.000

-0.4403 1405499. 0.0000 0.000 0.000 0.000 0.000

* This analysis computed pile response using nonlinear moment-curvature relationships. Values of total stress due to combined axial and bending stresses are computed for elastic sections only and do not equal the actual stresses in concrete and steel. Stresses in concrete and steel may be interpolated from the output for nonlinear bending properties relative to the magnitude of bending moment developed in the pile.

Output Summary for Load Case No. 4:

Pile-head deflection = 2.000000 inches

Computed slope at pile head = -0.0059659 radians

Maximum bending moment = 13419748. inch-lbs

Maximum shear force = -57001. lbs

Depth of maximum bending moment = 35.9104000 feet below pile head

Depth of maximum shear force = 49.3768000 feet below pile head

Number of iterations = 23

Number of zero deflection points = 4

Pile-head Deflection vs. Pile Length for Load Case 4

Pile Length feet	Pile Head Deflection inches	Maximum Moment in-lbs	Maximum Shear lbs
112.2200	2.000000	13419748.	-57001.
106.6980	2.000000	13348659.	-57209.
100.3890	2.000000	13295509.	-56643.
93.7970	2.000000	13258905.	-56833.
87.1460	2.000000	13216880.	-56843.
78.5540	2.000000	13211153.	-56379.
72.0430	2.000000	13269805.	-56102.
67.3370	2.000000	13387068.	-55943.
61.7210	2.000000	13038685.	-64436.
56.1100	2.000000	11581018.	-73071.
50.4990	2.000000	8366688.	-67318.
44.8880	2.000000	4035156.	-42803.
39.2770	2.000000	1522459.	-19126.
33.6660	2.000000	1382400.	-7056.0637015
33.6660	0.000000	1.674739E+11	-20727376688.

Pier 22af.lp7o

33.6660 0.000000 1.674739E+11 -20727376688.

33.6660 0.000000 1.674739E+11 -20727376688.

33.6660 0.000000 1.674739E+11 -20727376688.

33.6660 0.000000 1.674739E+11 -20727376688.

Computed Values of Pile Loading and Deflection for Lateral Loading for Load Case Number 5

Pile-head conditions are Displacement and Moment (Loading Type 4)

Displacement of pile head = 0.500000 inches

Moment at pile head = 1183200.0 in-lbs

Axial load at pile head = 0.0 lbs

Res. X	Soil Spr.	Depth X feet	Soil Deflect. inches	Y Lat. Load lb/inch	Bending Moment in-lbs	Shear Force lbs	Slope S radians	Total Stress psi*	Bending Stiffness lb-in^2	Soil P lb/in
0.00	0.00	0.00	0.5000	1183200.	10961.	-0.001465	0.000	1.352E+12		
0.000	0.000	1.122	0.000	0.4804	1330808.	10961.	-0.001452	0.000	1.352E+12	
0.000	0.000	2.244	0.000	0.4609	1478415.	10961.	-0.001438	0.000	1.351E+12	
0.000	0.000	3.367	0.000	0.4416	1626023.	10961.	-0.001423	0.000	1.351E+12	
0.000	0.000	4.489	0.000	0.4226	1773631.	10961.	-0.001406	0.000	1.350E+12	
0.000	0.000	5.611	0.000	0.4038	1921238.	10961.	-0.001387	0.000	1.350E+12	
0.000	0.000	6.733	0.000	0.3852	2068846.	10961.	-0.001368	0.000	1.349E+12	
0.000	0.000	7.855	0.000	0.3669	2216454.	10961.	-0.001346	0.000	1.349E+12	
0.000	0.000	8.978	0.000	0.3489	2364061.	10961.	-0.001323	0.000	1.348E+12	
0.000	0.000	10.100	0.000	0.3313	2511669.	10961.	-0.001299	0.000	1.348E+12	
0.000	0.000	11.222	0.000	0.3140	2659277.	10961.	-0.001273	0.000	1.347E+12	
0.000	0.000	12.344	0.000	0.2970	2806884.	10961.	-0.001246	0.000	1.347E+12	
0.000	0.000	13.466	0.000	0.2804	2954492.	10961.	-0.001217	0.000	1.346E+12	
0.000	0.000	14.589	0.000	0.2642	3102100.	10961.	-0.001187	0.000	1.346E+12	
0.000	0.000	15.711	0.000	0.2484	3249708.	10961.	-0.001155	0.000	1.345E+12	
0.000	0.000	16.833	0.000	0.2331	3397315.	10961.	-0.001122	0.000	1.345E+12	
0.000	0.000	17.955	0.000	0.2182	3544923.	10961.	-0.001087	0.000	1.344E+12	
0.000	0.000	19.077	0.000	0.2038	3692531.	10961.	-0.001051	0.000	1.344E+12	
0.000	0.000	20.200	0.000	0.1899	3840138.	10961.	-0.001013	0.000	1.343E+12	
0.000	0.000	21.322	0.000	0.1766	3987746.	10961.	-0.000978	0.000	1.777E+12	

Pier 22af.lp7o		Pier 22af.lp7o	
0.000	0.000	57.232	-0.002945
0.000	0.1636	61.5558	281503
0.000	0.000	58.354	-0.002765
0.000	0.1510	60.0409	292383
0.000	0.000	59.477	-0.002513
0.000	0.1389	56.6036	303284
0.000	0.000	60.599	-0.002213
0.000	0.1273	51.6307	314145
0.000	0.000	61.721	-0.001888
0.000	0.1161	278.0183	1983324
0.000	0.1054	57.843	-0.001559
-113.0751	14452	252.7131	2182388
0.000	0.0952	63.965	-0.001244
-116.8022	16530	225.8161	2444352
0.000	0.0855	65.088	-0.000955
-119.9305	18900	197.9517	2730983
0.000	0.0763	169.6282	3260694
-90.9769	16062	67.332	-0.000701
0.000	0.0676	141.2258	3922774
0.000	0.0595	112.9414	4517454
-103.0456	23316	69.576	-0.000509
0.000	0.0519	84.6108	534310
-103.9330	26943	70.699	-0.000473
0.000	0.0449	39.6965	7422970
-101.9832	30570	1.1871	821452336E-06
37.0333	92943	23.615	749230E-05
-265.3771	103823	-37.6315	753177E-05
38.155	92943	-43.5821	756804E-05
-250.9735	103823	-43.8971	760431E-05
39.277	0.0271	-40.5656	764038E-05
-231.1254	114704	-35.19	767685E-05
40.399	0.0223	-28.8691	771312E-05
-207.9562	123583	-22.5109	7749389
41.521	0.0179	-16.6534	7785657
-181.7682	138463	-11.5182	7821926
42.644	0.0141	-7.3214	7858195
-154.2102	147346	-4.0453	7894464
43.786	0.0107	-86.409	2.752E-06
-126.0318	158224	87.532	-1.150E-07
44.888	0.007810	0.0680	7967001
-98.0739	169102	1.1554	8003270
46.010	0.005317	89.776	-2.979E-06
-71.071	179883	1.7785	8039539
47.132	0.003820	2.0641	8075808
-45.689	190667	92.020	-3.522E-06
48.26255	2091488		
-22.286233	227129		
49.377	21630		
-1.407	21630		
50.499	22510		
16.7084	22510		
30.8810	227100		
51.743	236001		
42.6857	2415		
53.866	237800		
51.5553	248661		
54.988	25974		
57.5533	25974		
56.110	270622		
60.8173	270622		

Pier 22af.lp7o		Pier 22af.lp7o	
0.000	1.777E+12	961583.	-18842. 9.691E-06
0.000	1.777E+12	0.000	
0.000	1.777E+12	713435.	-18023. 1.601E-05
0.000	1.777E+12	0.000	
0.000	1.777E+12	476175.	-17238. 2.050E-05
0.000	1.777E+12	249180.	-16509. 2.324E-05
0.000	1.777E+12	0.000	
0.000	1.777E+12	31348.	-14289. 2.429E-05
0.000	1.777E+12	0.000	
0.000	1.777E+12	-135667.	-10716. 2.390E-05
0.000	1.777E+12	9.000	
0.000	1.777E+12	-257055.	-7493.6179 2.242E-05
0.000	1.777E+12	9.000	
0.000	1.777E+12	9.000	
0.000	1.777E+12	-337491.	-4640.3044 2.018E-05
0.000	1.777E+12	9.000	
0.000	1.777E+12	-382031.	-2165.3153 1.746E-05
0.000	1.777E+12	9.000	
0.000	1.777E+12	-598809.	-72.2728 1.453E-05
0.000	1.777E+12	9.000	
0.000	1.777E+12	-363977.	1639.0881 1.159E-05
0.000	1.777E+12	9.000	
0.000	1.777E+12	-351664.	2969.2488 8.810E-06
0.000	1.777E+12	9.000	
0.000	1.777E+12	-30407.	3806.2347 6.336E-06
0.000	1.777E+12	9.000	
0.000	1.777E+12	-23152.	4081.4851 4.249E-06
0.000	1.777E+12	9.000	
0.000	1.777E+12	-194081.	3930.4471 2.577E-06
0.000	1.777E+12	9.000	
0.000	1.777E+12	-143284.	3518.1190 1.304E-06
0.000	1.777E+12	9.000	
0.000	1.777E+12	-98329.	2971.3482 3.887E-07
0.000	1.777E+12	9.000	
0.000	1.777E+12	-63267.	2382.3329 -2.247E-07
0.000	1.777E+12	9.000	
0.000	1.777E+12	-35166.	1813.6285 -5.961E-07
0.000	1.777E+12	9.000	
0.000	1.777E+12	-14421.	1303.7296 -7.832E-07
0.000	1.777E+12	9.000	
0.000	1.777E+12	-52.6276	872.5857 -8.378E-07
0.000	1.777E+12	9080.3413	526.6335 -8.037E-07
0.000	1.777E+12	0.000	
0.000	1.777E+12	14131.	263.1203 -7.162E-07
0.000	1.777E+12	9.000	
0.000	1.777E+12	16167.	73.6238 -6.019E-07
0.000	1.777E+12	16114.	-53.2270 -4.801E-07
0.000	1.777E+12	14733.	-129.7617 -3.637E-07
0.000	1.777E+12	12619.	-167.9110 -2.605E-07
0.000	1.777E+12	0.000	
0.000	1.777E+12	10211.	-178.3643 -1.743E-07
0.000	1.777E+12	0.000	
0.000	1.777E+12	7815.2867	-170.1268 -1.063E-07
0.000	1.777E+12	0.000	
0.000	1.777E+12	5629.0528	-150.3724 -5.562E-08
0.000	1.777E+12	0.000	
0.000	1.777E+12	3765.3366	-124.4992 -2.017E-08
0.000	1.777E+12	0.000	
0.000	1.777E+12	2275.9407	-96.3143 2.620E-09

Pier 22af.lp7o

2.1218	8112076.	0.000	0.000	1.785E+12	0.000
93.143	-3.371E-06	1171.3240	1.563E-08	1.785E+12	0.000
2.0400	8148345.	0.000	0.000	1.785E+12	0.000
94.265	-3.101E-06	436.6473	2.169E-08	1.785E+12	0.000
1.8850	8184614.	0.000	0.000	1.785E+12	0.000
95.387	-2.787E-06	43.8060	2.351E-08	1.785E+12	0.000
1.7015	8220883.	0.000	0.000	1.785E+12	0.000
96.509	-2.468E-06	-40.4803	2.352E-08	1.785E+12	0.000
0.1110	6053556.	0.000	0.000	1.785E+12	0.000
97.631	-2.154E-06	-104.6441	2.297E-08	1.785E+12	0.000
0.1004	628024.	0.000	0.000	1.785E+12	0.000
98.754	-1.850E-06	-150.5930	2.201E-08	1.785E+12	0.000
0.0894	650692.	0.000	0.000	1.785E+12	0.000
99.876	-1.561E-06	-180.3334	2.076E-08	1.785E+12	0.000
0.0781	673360.	0.000	0.000	1.785E+12	0.000
100.998	-1.291E-06	-195.9185	1.934E-08	1.785E+12	0.000
0.0667	696028.	0.000	0.000	1.785E+12	0.000
102.120	-1.040E-06	-199.4060	1.785E+12	1.785E+12	0.000
0.0555	718696.	0.000	0.000	1.785E+12	0.000
103.242	-8.100E-07	-192.8262	1.637E-08	1.785E+12	0.000
0.0446	741364.	0.000	0.000	1.785E+12	0.000
104.365	-5.994E-07	-178.1597	1.497E-08	1.785E+12	0.000
0.0340	764032.	0.000	0.000	1.785E+12	0.000
105.487	-4.069E-07	-157.3264	1.370E-08	1.785E+12	0.000
0.0238	786700.	0.000	0.000	1.785E+12	0.000
106.609	-2.303E-07	-132.1828	1.261E-08	1.785E+12	0.000
0.0403	2357637.	0.000	0.000	1.785E+12	0.000
107.731	-6.724E-08	-99.7262	1.174E-08	1.785E+12	0.000
0.0122	2448309.	0.000	0.000	1.785E+12	0.000
108.853	8.572E-08	-65.0526	1.111E-08	1.785E+12	0.000
-0.0162	2538981.	0.000	0.000	1.785E+12	0.000
109.976	2.321E-07	-33.3100	1.074E-08	1.785E+12	0.000
-0.0453	2629653.	0.000	0.000	1.785E+12	0.000
111.098	3.750E-07	-9.7856	1.058E-08	1.785E+12	0.000
-0.0758	2720325.	0.000	0.000	1.785E+12	0.000
112.220	5.170E-07	0.000	0.000	1.785E+12	0.000
-0.1079	1405499.	0.000	0.000	1.785E+12	0.000

* This analysis computed pile response using nonlinear moment-curvature relationships.
 Values of total stress due to combined axial and bending stresses are computed only for elastic sections only and do not equal the actual stresses in concrete and steel.
 Stresses in concrete and steel may be interpolated from the output for nonlinear bending properties relative to the magnitude of bending moment developed in the pile.

Output Summary for Load Case No. 5:

Pile-head deflection	=	0.5000000 inches
Computed slope at pile head	=	-0.0014648 radians
Maximum bending moment	=	5331271.1 lbs
Maximum shear force	=	533275.1 lbs
Depth of maximum bending moment	=	35.9104000 feet below pile head
Depth of maximum shear force	=	49.3768000 feet below pile head
Number of iterations	=	7
Number of zero deflection points	=	4

Pier 22af.lp7o
 Computed Values of Pile Loading and Deflection
 for Lateral Loading for Load Case Number 6

Res.	Depth ft	Soil X	Deflect. inches	Bending Moment in-lbs	Shear Force lbs	Slope S radians	Total Stress psi*	Bending Stiffness lb-in ²	Soil P lb/in
0.000	0.00	0.00	1.0000	1183200.	19250.	-0.002778	0.000	1.352E+12	0.000
0.000	1.122	0.00	0.9627	14442433.	19250.	-0.002765	0.000	1.352E+12	0.000
0.000	2.244	0.00	0.9255	1701666.	19250.	-0.002749	0.000	1.351E+12	0.000
0.000	3.367	0.00	0.8886	1960899.	19250.	-0.002731	0.000	1.349E+12	0.000
0.000	4.489	0.00	0.8520	2220132.	19250.	-0.002710	0.000	1.349E+12	0.000
0.000	5.611	0.00	0.8156	2479364.	19250.	-0.002687	0.000	1.348E+12	0.000
0.000	6.733	0.00	0.7796	2738597.	19250.	-0.002661	0.000	1.347E+12	0.000
0.000	7.855	0.00	0.7440	2997830.	19250.	-0.002632	0.000	1.346E+12	0.000
0.000	8.978	0.00	0.7087	3257063.	19250.	-0.002601	0.000	1.345E+12	0.000
0.000	10.100	0.00	0.6739	3516296.	19250.	-0.002567	0.000	1.344E+12	0.000
0.000	11.222	0.00	0.6396	3775529.	19250.	-0.002530	0.000	1.343E+12	0.000
0.000	12.344	0.00	0.6058	4034762.	19250.	-0.002491	0.000	1.342E+12	0.000
0.000	13.466	0.00	0.5725	4293995.	19250.	-0.002449	0.000	1.342E+12	0.000
0.000	14.589	0.00	0.5398	4553227.	19250.	-0.002405	0.000	1.341E+12	0.000
0.000	15.711	0.00	0.5077	4812460.	19250.	-0.002358	0.000	1.340E+12	0.000
0.000	16.833	0.00	0.4763	5071693.	19250.	-0.002308	0.000	1.339E+12	0.000
0.000	17.955	0.00	0.4455	5330926.	19250.	-0.002256	0.000	1.338E+12	0.000
0.000	19.077	0.00	0.4155	5590159.	19250.	-0.002201	0.000	1.337E+12	0.000
0.000	20.200	0.00	0.3863	5849392.	19250.	-0.002097	0.000	5.209E+11	0.000
0.000	21.322	0.00	0.3590	6108625.	19250.	-0.001998	0.000	1.771E+12	0.000
0.000	22.444	0.00	0.3324	6367858.	19250.	-0.001951	0.000	1.771E+12	0.000
0.000	23.566	0.00	0.3065	6627090.	19250.	-0.001901	0.000	1.770E+12	0.000
0.000	24.688	0.00	0.2812	6886323.	19250.	-0.001850	0.000	1.769E+12	0.000

SEE-1
 $\Delta = 1.0'$
 LATERAL
 RESISTANCE
 $= 19.25'$

Pier 22af.jp7o			Pier 22af.jp7o		
25.811	0.2567	7145556.	0.000	1.769E+12	0.000
0.000	0.000	0.000	0.000	1.768E+12	0.000
26.933	0.2328	7404789.	0.000	1.767E+12	0.000
0.000	0.000	0.000	0.000	1.144E+12	0.000
28.055	0.2098	7664022.	0.000	1.144E+12	0.000
-142.2466	9131.3560	7897459.	0.000	1.144E+12	0.000
29.177	0.1875	8104343.	0.000	1.144E+12	0.000
-146.4792	105.17	8284064.	0.000	1.144E+12	0.000
30.299	0.1665	8432051.	0.000	1.144E+12	0.000
-149.7787	121.17	8546024.	0.000	1.144E+12	0.000
-174.9995	160.62	8625085.	0.000	1.144E+12	0.000
-187.5650	196.69	8669515.	0.000	1.144E+12	0.000
32.544	0.1283	8680569.	0.000	1.144E+12	0.000
33.666	0.1112	8606416.	0.000	1.144E+12	0.000
34.788	0.0954	8453330.	0.000	1.144E+12	0.000
-192.5163	233.16	8228882.	0.000	1.144E+12	0.000
-190.9699	269.43	7941384.	0.000	1.144E+12	0.000
-184.0493	305.70	7599363.	0.000	1.144E+12	0.000
-469.8642	929.43	7211079.	0.000	1.144E+12	0.000
-435.2673	1038.23	6784993.	0.000	1.144E+12	0.000
-393.5134	1147.04	6329516.	0.000	1.144E+12	0.000
-347.6829	1255.85	5852789.	0.000	1.144E+12	0.000
-300.6621	1364.65	5362502.	0.000	1.144E+12	0.000
-255.1119	1473.46	4865741.	0.000	1.144E+12	0.000
-208.4550	1582.27	4368867.	0.000	1.144E+12	0.000
-162.0758	1691.07	3877434.	0.000	1.144E+12	0.000
-117.1766	1799.88	3395814.	0.000	1.144E+12	0.000
-74.7751	1908.69	2927697.	0.000	1.144E+12	0.000
-35.7046	2017.49	2475909.	0.000	1.144E+12	0.000
-0.6184	2126.30	2042425.	0.000	1.144E+12	0.000
30.0034	2235.10	1628408.	0.000	1.144E+12	0.000
54.1082	2271.00	1234262.	0.000	1.144E+12	0.000
74.4635	2379.80	859714.	0.000	1.144E+12	0.000
90.0448	2488.61	503897.	0.000	1.144E+12	0.000
100.9367	2597.41		0.000	1.144E+12	0.000
107.3447	2706.22		0.000	1.144E+12	0.000
109.5835	2815.03		0.000	1.144E+12	0.000
108.0649	2923.83		0.000	1.144E+12	0.000
103.2930	3032.64		0.000	1.144E+12	0.000
60.599	-0.004109	503897.	0.000	1.144E+12	0.000
95.8522	314145.	0.000	0.000	1.769E+12	0.000
61.721	-0.003580	165463.	0.000	1.785E+12	0.000
382.3884	1438437.	0.000	0.000	1.785E+12	0.000
62.843	-0.003034	-103628.	0.000	1.785E+12	0.000
352.0306	1562480.	0.000	0.000	1.785E+12	0.000
63.965	-0.002499	-308880.	0.000	1.785E+12	0.000
319.4687	1721733.	0.000	0.000	1.785E+12	0.000
65.088	-0.001995	-456198.	0.000	1.785E+12	0.000
285.4419	1926972.	0.000	0.000	1.785E+12	0.000
66.210	-0.001537	-551754.	0.000	1.785E+12	0.000
250.5739	2195109.	0.000	0.000	1.785E+12	0.000
67.332	-0.001136	-601869.	0.000	1.785E+12	0.000
215.3777	2553816.	0.000	0.000	1.785E+12	0.000
68.454	-0.000795	-612527.	0.000	1.785E+12	0.000
180.2384	3051695.	0.000	0.000	1.785E+12	0.000
69.576	-0.000517	-591299.	0.000	1.785E+12	0.000
145.3552	3784032.	0.000	0.000	1.785E+12	0.000
70.699	-0.000299	-543313.	0.000	1.785E+12	0.000
110.5646	4974665.	0.000	0.000	1.785E+12	0.000
71.821	-0.000137	-475276.	0.000	1.785E+12	0.000
74.6721	7365610.	0.000	0.000	1.785E+12	0.000
72.943	-2.204E-05	-393697.	0.000	1.785E+12	0.000
12.2671	7495507.	0.000	0.000	1.785E+12	0.000
74.065	5.244E-05	-309895.	0.000	1.785E+12	0.000
-29.3292	7531776.	0.000	0.000	1.785E+12	0.000
75.187	9.543E-05	-231410.	0.000	1.785E+12	0.000
-53.6299	7568045.	0.000	0.000	1.785E+12	0.000
76.310	0.000115	-162652.	0.000	1.785E+12	0.000
-64.8839	7604313.	0.000	0.000	1.785E+12	0.000
77.432	0.000118	-105659.	0.000	1.785E+12	0.000
-66.8655	7640382.	0.000	0.000	1.785E+12	0.000
-62.7425	7676851.	-60793.	0.000	1.785E+12	0.000
-55.0393	7713120.	-27304.	0.000	1.785E+12	0.000
-45.6644	7749389.	-3796.1655	0.000	1.785E+12	0.000
81.921	6.223E-05	11431.	0.000	1.785E+12	0.000
-35.9762	7785657.	20133.	0.000	1.785E+12	0.000
83.043	4.626E-05	23963.	0.000	1.785E+12	0.000
-26.8705	7821926.	24371.	0.000	1.785E+12	0.000
84.165	3.234E-05	0.000	0.000	1.785E+12	0.000
-18.8725	7858195.	0.000	0.000	1.785E+12	0.000
85.287	2.086E-05	0.000	0.000	1.785E+12	0.000
-12.2271	7894464.	22361.	0.000	1.785E+12	0.000
86.409	1.185E-05	0.000	0.000	1.785E+12	0.000
-6.9782	7930733.	0.000	0.000	1.785E+12	0.000
87.532	5.113E-06	19486.	0.000	1.785E+12	0.000
-3.0370	7967091.	0.000	0.000	1.785E+12	0.000
-0.2364	3.377E-07	15860.	0.000	1.785E+12	0.000
1.6757	8003770.	12191.	0.000	1.785E+12	0.000
1.6757	8039339.	0.000	0.000	1.785E+12	0.000
2.7657	8075686.	8816.9664	0.000	1.785E+12	0.000
3.3761	8112091E-06	5947.980	0.000	1.785E+12	0.000
3.6231	814849E-06	3680.5084	0.000	1.785E+12	0.000
3.6231	81834E-06	2080.1211	0.000	1.785E+12	0.000
3.6231	82183E-06	0.000	0.000	1.785E+12	0.000
3.6231	82532E-06	1138.7719	0.000	1.785E+12	0.000
3.6231	82881E-06	0.000	0.000	1.785E+12	0.000
3.6231	83230E-06	3.5390	8220883.		

Pier 22af.jp7o			Pier 22af.jp7o		
19250.	-0.001797	0.000	0.000	1.769E+12	0.000
19250.	-0.001741	0.000	0.000	1.768E+12	0.000
18293.	-0.001684	0.000	0.000	1.144E+12	0.000
16349.	-0.001608	0.000	0.000	1.144E+12	0.000
14354.	-0.001514	0.000	0.000	1.144E+12	0.000
12168.	-0.001418	0.000	0.000	1.144E+12	0.000
9726.4181	-0.001319	0.000	0.000	1.144E+12	0.000
7167.2548	-0.001219	0.000	0.000	1.144E+12	0.000
4585.1652	-0.001118	0.000	0.000	1.144E+12	0.000
2060.0856	-0.001016	0.000	0.000	1.144E+12	0.000
-2342.8449	-0.000914	0.000	0.000	1.144E+12	0.000
-8437.2765	-0.000812	0.000	0.000	1.144E+12	0.000
-14018.	-0.000712	0.000	0.000	1.144E+12	0.000
-19008.	-0.000614	0.000	0.000	1.144E+12	0.000
-23374.	-0.000519	0.000	0.000	1.144E+12	0.000
-27116.	-0.000443	0.000	0.000	1.768E+12	0.000
-30237.	-0.000386	0.000	0.000	1.769E+12	0.000
-32732.	-0.000333	0.000	0.000	1.770E+12	0.000
-34612.	-0.000283	0.000	0.000	1.771E+12	0.000
-35905.	-0.000237	0.000	0.000	1.772E+12	0.000
-36649.	-0.000194	0.000	0.000	1.773E+12	0.000
-36893.	-0.000156	0.000	0.000	1.775E+12	0.000
-36695.	-0.000121	0.000	0.000	1.776E+12	0.000
-36129.	-8.933E-05	0.000	0.000	1.777E+12	0.000
-35263.	-6.179E-05	0.000	0.000	1.779E+12	0.000
-34156.	-3.785E-05	0.000	0.000	1.780E+12	0.000
-32870.	-1.742E-05	0.000	0.000	1.781E+12	0.000
-31467.	-3.375E-07	0.000	0.000	1.782E+12	0.000
-30007.	1.353E-05	0.000	0.000	1.783E+12	0.000
-28541.	2.434E-05	0.000	0.000	1.784E+12	0.000
-27118.	3.224E-05	0.000	0.000	1.785E+12	0.000
-25777.	3.738E-05	0.000	0.000	1.785E+12	0.000

Pier 22af.lp7o		0. 1b		Pier 22af.lp7o	
Axial Load =	Pile Length	Pile Head Deflection	Maximum Moment	Maximum Shear	
	feet	Inches	In-lbs	Lbs	
96.509	-5.481E-06	838.1964	0.000	1.785E+12	
0.2464	605356.	0.000	0.000	1.785E+12	
97.631	-5.080E-06	582.3013	0.000	1.785E+12	
0.2369	628024.	0.000	0.000	1.785E+12	
98.754	-4.619E-06	369.3652	0.000	1.785E+12	
0.2232	650692.	0.000	0.000	1.785E+12	
99.876	-4.121E-06	196.9034	0.000	1.785E+12	
0.2061	673360.	0.000	0.000	1.785E+12	
100.998	-3.603E-06	61.8095	0.000	1.785E+12	
0.1862	696028.	0.000	0.000	1.785E+12	
102.120	-3.079E-06	-39.5142	0.000	1.785E+12	
0.1643	718696.	0.000	0.000	1.785E+12	
103.242	-2.558E-06	-111.0428	0.000	1.785E+12	
0.1408	741364.	0.000	0.000	1.785E+12	
0.1163	764032.	-157.0313	0.000	1.785E+12	
0.0909	786700.	-181.9363	0.000	1.785E+12	
0.0693	809368.	-190.3561	0.000	1.785E+12	
0.0519	832036.	-164.4400	0.000	1.785E+12	
0.0384	854704.	-117.8777	0.000	1.785E+12	
0.0289	877372.	0.000	0.000	1.785E+12	
0.0224	900040.	0.000	0.000	1.785E+12	
0.0180	922708.	0.000	0.000	1.785E+12	
0.0146	945376.	0.000	0.000	1.785E+12	
0.0120	968044.	0.000	0.000	1.785E+12	
0.0100	990712.	0.000	0.000	1.785E+12	
0.0085	1013380.	0.000	0.000	1.785E+12	
0.0073	1034648.	0.000	0.000	1.785E+12	
0.0064	1055916.	0.000	0.000	1.785E+12	
0.0057	1077184.	0.000	0.000	1.785E+12	
0.0052	1098452.	0.000	0.000	1.785E+12	
0.0048	1119720.	0.000	0.000	1.785E+12	
0.0045	1140988.	0.000	0.000	1.785E+12	
0.0043	1162256.	0.000	0.000	1.785E+12	
0.0041	1183524.	0.000	0.000	1.785E+12	

* This analysis computed pile response using nonlinear moment-curvature relationships. Values of total stress due to combined axial and bending stresses are computed only for elastic sections only and do not equal the actual stresses in concrete and steel. Stresses in concrete and steel may be interpolated from the output for nonlinear bending properties relative to the magnitude of bending moment developed in the pile.

Output Summary for Load Case No. 6:

Pile-head deflection	=	1.000000 inches
Computed slope at pile head	=	-0.002782 radians
Maximum bending moment	=	8650893. In-lb
Maximum shear force	=	37.032800 lbs
Depth of maximum bending moment	=	49.376800 feet below pile head
Depth of maximum shear force	=	81
Number of iterations	=	4

----- Pile-head Deflection vs. Pile Length for Load Case 6 -----

Boundary Condition Type 4, Deflection and Moment
 Deflection = 1.000000 in
 Moment = 1183200. in-lb

Pier 22af.lp7o		0. 1b		Pier 22af.lp7o	
Axial Load =	Pile Length	Pile Head Deflection	Maximum Moment	Maximum Shear	
	feet	Inches	In-lbs	Lbs	
112.2200	1.0000000	8680569.	8680569.	-36893.	
106.6090	1.0000000	8696609.	8696609.	-36696.	
100.9980	1.0000000	8360408.	8360408.	-36121.	
95.3870	1.0000000	8690727.	8690727.	-36512.	
89.7760	1.0000000	8670054.	8670054.	-36761.	
84.1650	1.0000000	8617068.	8617068.	-36723.	
78.5540	1.0000000	8537347.	8537347.	-36367.	
72.9430	1.0000000	8595186.	8595186.	-36183.	
67.3320	1.0000000	8649093.	8649093.	-35743.	
61.7210	1.0000000	8560604.	8560604.	-41994.	
56.1100	1.0000000	8025547.	8025547.	-44323.	
50.4990	1.0000000	5484685.	5484685.	-46336.	
44.8880	1.0000000	2399184.	2399184.	-46336.	
39.2770	1.0000000	1183500.	1183500.	-5703.	
33.6660	0.0000000	8380702875.	8380702875.	-103758325.	
33.6660	0.0000000	8380702875.	8380702875.	-103758325.	
33.6660	0.0000000	8380702875.	8380702875.	-103758325.	
33.6660	0.0000000	8380702875.	8380702875.	-103758325.	
33.6660	0.0000000	8380702875.	8380702875.	-103758325.	

----- Computed values of pile Loading and Deflection For Lateral Loading for Load Case Number 7 -----

Pile-head conditions are Displacement and Moment (Loading Type 4)
 Displacement of pile head = 500000 inches
 Moment at pile head = 1183200.0 in-lb
 Axial load at pile head = 0.0 lbs

Depth	Deflect. X	Bending Moment	Shear Force	Slope S	Total Stress	Bending Stiffness
res. Soil	spr. Y	Distrib. Moment	lbs	radians	psi*	lb-in ²
feet	inches	in-lb	lbs			lb/in
0.000	1.5000	1183200.	24710.	-0.004346	0.000	1.352E+12
0.000	1.122	1.4416	24710.	-0.004332	0.000	1.352E+12
0.000	2.244	1.3833	24710.	-0.004316	0.000	1.350E+12
0.000	3.367	1.3253	24710.	-0.004296	0.000	1.349E+12
0.000	4.489	1.2676	24710.	-0.004272	0.000	1.348E+12
0.000	5.611	1.2103	24710.	-0.004245	0.000	1.346E+12
0.000	6.733	1.1533	24710.	-0.004215	0.000	1.345E+12
0.000	7.855	1.0967	24710.	-0.004182	0.000	1.344E+12

Pier 22af.jp7o		Pier 22af.jp7o	
0.000	8.978	0.000	1.343E+12
0.000	10.100	0.000	1.342E+12
0.000	0.000	0.000	1.341E+12
0.000	11.222	0.000	1.340E+12
0.000	12.344	0.000	1.338E+12
0.000	13.466	0.000	1.337E+12
0.000	14.589	0.000	5.073E+11
0.000	15.711	0.000	4.190E+11
0.000	16.833	0.000	4.188E+11
0.000	17.955	0.000	4.186E+11
0.000	19.077	0.000	4.184E+11
0.000	20.200	0.000	1.768E+12
0.000	21.322	0.000	1.162E+12
0.000	22.444	0.000	1.144E+12
0.000	23.566	0.000	1.144E+12
0.000	24.688	0.000	1.143E+12
0.000	25.811	0.000	1.143E+12
0.000	26.933	0.000	1.142E+12
0.000	28.055	0.000	1.142E+12
-157.8048	7420.1772	0.000	1.142E+12
-162.6123	8528.5134	0.000	1.142E+12
-166.5091	9804.8294	0.000	1.142E+12
-241.1988	16062.0	0.000	1.142E+12
-259.3549	19689.0	0.000	1.142E+12
-267.0278	23316.0	0.000	1.142E+12
-265.6167	26943.0	0.000	1.142E+12
-256.5729	30700.0	0.000	1.142E+12
-555.38119	78952.463	0.000	1.142E+12
-555.38115	9046.0	0.000	1.142E+12
-522.70377	109728.41	0.000	1.142E+12
-473.5625	124701.1	0.000	1.143E+12
-403.83721	136465.0	0.000	1.143E+12
-329.7033	147346.0	0.000	1.143E+12
43.766	0.0219	8964033.0	1.143E+12
-240.8109	147956.0	0.000	1.343E+12
44.888	0.0151	8415705.0	1.342E+12
-189.9278	169107.0	0.000	1.342E+12
46.010	0.009665	7832934.0	1.341E+12
-129.1844	179988.0	0.000	1.340E+12
47.132	0.005425	7226736.0	1.340E+12
-76.8867	190869.0	0.000	1.338E+12
-28.8381	201749.0	0.000	1.337E+12
49.377	-0.000898	5981225.0	1.337E+12
14.1795	212630.0	0.000	5.073E+11
51.5978	223510.0	0.000	4.190E+11
51.621	-0.004772	4744984.0	4.190E+11
52.743	-0.005950	4146134.0	4.188E+11
105.1415	237980.0	0.000	4.188E+11
53.866	-0.006704	3566351.0	4.186E+11
123.8975	248861.0	0.000	4.184E+11
54.988	-0.007095	3009037.0	4.184E+11
136.8577	259741.0	0.000	1.768E+12
56.110	-0.007180	2476540.0	1.768E+12
144.2875	270622.0	0.000	1.162E+12
57.232	-0.007012	1970209.0	1.162E+12
146.5822	281503.0	0.000	1.144E+12
58.354	-0.006644	1490460.0	1.144E+12
144.2528	292383.0	0.000	1.144E+12
59.477	-0.006124	1036870.0	1.144E+12
137.9150	303264.0	0.000	1.143E+12
60.599	-0.005499	608291.0	1.143E+12
128.2794	314145.0	0.000	1.143E+12
61.721	-0.004812	202974.0	1.143E+12
443.3469	1240716.0	0.000	1.143E+12
62.843	-0.004104	-221945.0	1.143E+12
409.4546	1343416.0	0.000	1.143E+12
63.965	-0.003409	-372611.0	1.143E+12
373.1700	1474042.0	0.000	1.143E+12
65.088	-0.002752	-555606.0	1.143E+12
335.2687	1640680.0	0.000	1.143E+12
66.210	-0.002151	-677801.0	1.143E+12
296.4127	1855755.0	0.000	1.142E+12
67.332	-0.001619	-746244.0	1.142E+12
257.1558	2139053.0	0.000	1.142E+12
68.454	-0.001163	-768053.0	1.142E+12
217.9357	2524028.0	0.000	1.142E+12
69.576	-0.000785	-750342.0	1.142E+12
179.0223	3072646.0	0.000	1.142E+12
70.699	-0.000483	-700165.0	1.142E+12
140.4180	3917404.0	0.000	1.142E+12
71.821	-0.000252	-624325.0	1.142E+12
101.4473	5424903.0	0.000	1.142E+12
72.943	-8.563E-05	-930488.0	1.142E+12
47.1131	7453875.0	0.000	1.142E+12
73.065	-0.000175	-427006.0	1.142E+12
-16.071	753176.0	0.000	1.142E+12
-75.187	98645.0	0.000	1.143E+12
-55.4361	7568045.0	0.000	1.143E+12
-78.310	74020135.0	0.000	1.143E+12
-77.7432	602013.0	0.000	1.143E+12
-77.6216	7086504.0	0.000	1.143E+12
-78.554	0.000143	-100423.0	1.143E+12
-76.5077	7189696.0	0.000	1.143E+12

Pier 22af.jp7o

Pier 22af.jp7o

Res. X	Depth	Est ^h	Y	Lat. Load	Bending	Shear	Slope	Total	Bending
lb/inch	ft	lb/inch	inches	in-lbs	in-lbs	lbs	radians	stress	stiffness
								psi*	lb-in ²
0.000	1.785E+12	0.000	2.0000	1183200.	31438.	-0.005894	0.000	1.352E+12	
0.000	1.785E+12	0.000	1.122	0.000	31438.	-0.005880	0.000	1.352E+12	
0.000	1.785E+12	0.000	2.244	0.000	31438.	-0.005862	0.000	1.349E+12	
0.000	1.785E+12	0.000	3.367	0.000	31438.	-0.005840	0.000	1.348E+12	
0.000	1.785E+12	0.000	4.489	0.000	31438.	-0.005813	0.000	1.346E+12	
0.000	1.785E+12	0.000	5.611	0.000	31438.	-0.005782	0.000	1.345E+12	
0.000	1.785E+12	0.000	6.733	0.000	31438.	-0.005747	0.000	1.342E+12	
0.000	1.785E+12	0.000	7.855	0.000	31438.	-0.005707	0.000	1.340E+12	
0.000	1.785E+12	0.000	8.978	0.000	31438.	-0.005664	0.000	1.340E+12	
0.000	1.785E+12	0.000	10.100	0.000	31438.	-0.005616	0.000	1.339E+12	
0.000	1.785E+12	0.000	11.222	0.000	31438.	-0.005563	0.000	1.338E+12	
0.000	1.785E+12	0.000	12.344	0.000	31438.	-0.005477	0.000	6.654E+11	

Values of total stress due to combined axial and bending stresses are computed only for elastic sections only and do not equal the actual stresses in concrete and steel.

Stresses in concrete and steel may be interpolated from the output for nonlinear bending properties relative to the magnitude of bending moment developed in the pile.

Output Summary for Load Case No. 7:

Pile-head deflection = 1.5000000 inches
 Computed slope at pile head = -0.0043459 radians
 Maximum bending moment = 10852463. inch-lbs
 Maximum shear force = -46344. lbs
 Depth of maximum bending moment = 37.0326000 feet below pile head
 Depth of maximum shear force = 49.3768000 feet below pile head
 Number of iterations = 109
 Number of zero deflection points = 4

Computed Values of Pile Loading and Deflection for Lateral Loading for Load Case Number 8

Pile-head conditions are Displacement and Moment (Loading Type 4)
 Displacement of pile head = 2.000000 inches
 Moment at pile head = 1183200.0 in-lbs
 Axial load at pile head = 0.0 lbs

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moment-curvature

using nonlinear

relationships.

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Pier 22af.lp7o		Pier 22af.lp7o	
0.000	0.000	48.255	0.003992
0.000	1.0762	-59.8049	201749
13.466	0.000	49.377	0.000178
0.000	6763434.	-2.8104	212630
0.000	0.000	50.499	-0.002848
14.589	1.0059	47.2670	223510
0.000	6686787.	87.1145	227100
0.000	0.000	51.621	-0.005166
15.711	0.9386	52.743	-0.006855
0.000	7110139.	121.1356	237980
0.000	0.000	53.866	-0.007992
16.833	0.8743	147.6921	248861
0.000	7533492.	54.988	-0.008652
0.000	0.000	166.8901	259741
17.955	0.8133	56.110	-0.008908
0.000	7956845.	179.0188	270622
0.000	0.000	57.232	-0.008828
19.077	0.7557	184.5331	281503
0.000	8380198.	58.354	-0.008476
0.000	0.000	184.0331	292383
20.200	0.7018	178.2513	303264
0.000	8803551.	60.599	-0.007203
0.000	0.000	168.0368	314145
21.322	0.6518	61.721	-0.006395
0.000	9226904.	511.0882	1076263
0.000	0.000	62.843	-0.005542
22.444	0.6031	475.7748	1156147
0.000	9650256.	63.965	-0.004666
0.000	0.000	437.4982	1257299
23.566	0.5560	65.088	-0.003861
0.000	10073609.	397.1199	1385140
0.000	0.000	66.210	-0.003092
24.688	0.5105	355.3801	1547828
0.000	10496962.	67.332	-0.002397
0.000	0.000	312.9104	1757909
25.811	0.4667	68.454	-0.001788
0.000	10920315.	270.2336	2035531
0.000	0.000	227.7448	2415291
26.933	0.4246	70.699	-0.000844
0.000	11343668.	185.6524	2962912
0.000	0.000	143.8106	3824992
28.055	0.3843	101.1434	-6.564E-05
0.000	11767021.	37.2726	-7531776.
-174.0611	6098.8331	75.187	5.650E-05
29.177	0.3459	-31.7516	7568045
0.000	12458808.	76.310	0.000131
-179.5956	6991.7259	-73.1716	7517320
0.000	0.000	-82.9899	6628041
30.299	0.3094	-85.5718	6428085
0.000	12518028.	-83.7407	6586665
-184.1630	8015.0495	-79.8298	6960318
0.000	0.000	-72.8121	81000128
31.422	0.2749	-72.8303	7538007
0.000	12843850.	83.043	0.000102
0.000	0.000		
32.544	0.2425		
0.000	13110208.		
-354.4971	19689.		
0.000	0.000		
33.666	0.2121		
0.000	13312280.		
-367.2077	23316.		
0.000	0.000		
34.788	0.1838		
0.000	13447761.		
-367.9233	26943.		
0.000	0.000		
35.910	0.1577		
0.000	13516545.		
-358.0102	30570.		
0.000	0.000		
37.033	0.1337		
0.000	13520406.		
-625.1939	62952.		
0.000	0.000		
38.155	0.1119		
0.000	13410892.		
-629.1935	75705.		
0.000	0.000		
39.277	0.0922		
0.000	13187278.		
-600.0923	87616.		
0.000	0.000		
40.399	0.0746		
0.000	12854840.		
-554.3230	100005.		
0.000	0.000		
41.521	0.0591		
0.000	12421879.		
-491.0954	111905.		
0.000	0.000		
42.644	0.0455		
0.000	11899862.		
-405.7999	120037.		
0.000	0.000		
43.766	0.0338		
0.000	11304234.		
-306.8850	122092.		
0.000	0.000		
44.888	0.0240		
0.000	10653005.		
-268.8777	151139.		
0.000	0.000		
46.010	0.0158		
0.000	992995.		
-210.6618	179888.		
0.000	0.000		
47.132	0.009146		
0.000	190869.		
-129.6319	0.000		

Pier 22af.1p70

Pier 22af.1p70

-59.4777	7821926.	0.000	0.000	1.785E+12	0.000
84.165	7.746E-05	27003.	886.1050	-1.750E-06	0.000
-45.1992	7858195.	0.000	363.6487	-1.517E-06	0.000
85.287	5.526E-05	34837.	0.3885	-1.247E-06	0.000
-32.3949	7894464.	0.000	0.000	0.000	0.000
86.409	3.660E-05	36797.	-231.1252	-9.764E-07	0.000
-21.5577	7930733.	0.000	0.000	0.000	0.000
87.532	2.168E-05	34847.	-358.7385	-7.295E-07	0.000
-12.8282	7967001.	0.000	-408.1546	-5.192E-07	0.000
88.654	1.031E-05	30572.	-401.4819	-3.503E-07	0.000
-6.1247	8003270.	0.000	-356.6165	-2.222E-07	0.000
-1.2145	8039539.	0.000	-287.2356	-1.303E-07	0.000
90.898	3.678E-06	19579.	-203.2201	-6.767E-08	0.000
2.2055	8075808.	0.000	-111.3621	-2.565E-08	0.000
92.020	7.400E-06	14373.	-60.6426	5.051E-09	0.000
4.4578	8112076.	0.000	-53.5674	2.959E-08	0.000
93.143	-9.662E-06	9974.4837	-46.4885	4.869E-08	0.000
5.8465	8148345.	0.000	-39.5939	6.307E-08	0.000
94.265	-1.091E-05	6636.5657	-33.0455	7.342E-08	0.000
6.6313	8184614.	0.000	-26.9801	8.042E-08	0.000
95.387	-1.148E-05	4501.1980	-21.5112	8.467E-08	0.000
7.0112	8220883.	0.000	-16.7308	8.674E-08	0.000
96.509	-1.160E-05	3637.2718	-12.7120	8.711E-08	0.000
0.5215	605356.	0.000	-6.8535	8.618E-08	0.000
0.5293	628024.	0.000	-0.0114	8.456E-08	0.000
98.754	-1.080E-05	2194.5519	4.2507	8.294E-08	0.000
0.5221	650692.	0.000	5.7829	8.175E-08	0.000
99.876	-1.004E-05	1615.8571	4.4251	8.115E-08	0.000
0.5019	673360.	0.000	0.000	0.000	0.000
100.998	-9.106E-06	1128.1786	0.000	0.000	0.000
0.4707	696028.	0.000	0.000	0.000	0.000
102.120	-8.060E-06	725.8504	0.000	0.000	0.000
0.4302	718696.	0.000	0.000	0.000	0.000
103.242	-6.940E-06	401.5280	0.000	0.000	0.000
0.3821	741364.	0.000	0.000	0.000	0.000
104.365	-5.779E-06	146.4923	0.000	0.000	0.000
0.3279	764032.	0.000	0.000	0.000	0.000
105.487	-4.604E-06	-49.0796	0.000	0.000	0.000
0.2690	786700.	0.000	0.000	0.000	0.000
106.609	-3.433E-06	-195.8766	0.000	0.000	0.000
0.6011	2357637.	0.000	0.000	0.000	0.000
0.4150	2448309.	-233.6640	0.000	0.000	0.000
108.853	-1.156E-06	-196.1847	0.000	0.000	0.000
0.2180	2538961.	0.000	0.000	0.000	0.000
109.976	-4.910E-08	-119.1798	0.000	0.000	0.000
0.0095888	2629633.	0.000	0.000	0.000	0.000
111.098	1.046E-06	-40.4361	0.000	0.000	0.000
-0.2112	2720323.	0.000	0.000	0.000	0.000
112.220	2.136E-06	0.000	0.000	0.000	0.000
-0.4460	1405499.	0.000	0.000	0.000	0.000

* This analysis computed pile response using nonlinear moment-curvature relationships. Values of total stress due to combined axial and bending stresses are computed only for elastic sections only and do not equal the actual stresses in concrete and steel. Stresses in concrete and steel may be interpolated from the output for nonlinear bending properties relative to the magnitude of bending moment developed in the pile.

Output Summary for Load Case No. 8:

File-head deflection	=	2.0000000 inches
Computed slope at pile head	=	-0.0058940 radians
Maximum bending moment	=	13520406. inch-lbs
Maximum shear force	=	-57389. lbs
Depth of maximum bending moment	=	37.0326000 feet below pile head
Depth of maximum shear force	=	49.3768000 feet below pile head
Number of iterations	=	197
Number of zero deflection points	=	4

Computed Values of Pile Loading and Deflection for Lateral Loading for Load Case Number 9

Pile-head conditions are Shear and Moment (Loading Type I)

Shear force at pile head	=	8800.0 lbs
Applied moment at pile head	=	1382400.0 in-lbs
Axial thrust load on pile head	=	0.0 lbs

Res. X	Depth X	Soil	Deflect. Spr.	Lat. Load	Bending Moment	Shear Force	Slope	Total Stress	Bending stiffness	p
			inches	in-lbs	in-lbs	lbs	radians	psi*	lb-in ²	lb/in
0.00	0.00	0.4387	1382400.	8800.0000	-0.001324	0.000	1.351E+12	0.000	1.351E+12	
0.000	1.122	0.000	0.4210	1500904.	8800.0000	-0.001310	0.000	1.351E+12	0.000	1.351E+12
0.000	2.244	0.000	0.4034	1619409.	8800.0000	-0.001294	0.000	1.351E+12	0.000	1.351E+12
0.000	3.367	0.000	0.3861	1737913.	8800.0000	-0.001278	0.000	1.350E+12	0.000	1.350E+12
0.000	4.489	0.000	0.3690	1856417.	8800.0000	-0.001260	0.000	1.350E+12	0.000	1.350E+12
0.000	5.611	0.000	0.3522	1974922.	8800.0000	-0.001241	0.000	1.349E+12	0.000	1.349E+12
0.000	6.733	0.000	0.3356	2093426.	8800.0000	-0.001220	0.000	1.349E+12	0.000	1.349E+12
0.000	7.855	0.000	0.3193	2211930.	8800.0000	-0.001199	0.000	1.349E+12	0.000	1.349E+12
0.000	8.978	0.000	0.3033	2330435.	8800.0000	-0.001176	0.000	1.348E+12	0.000	1.348E+12
0.000	10.100	0.000	0.2876	2448939.	8800.0000	-0.001152	0.000	1.348E+12	0.000	1.348E+12
0.000	11.222	0.000	0.2723	2567443.	8800.0000	-0.001127	0.000	1.348E+12	0.000	1.348E+12
0.000	12.344	0.000	0.2573	2685948.	8800.0000	-0.001101	0.000	1.347E+12	0.000	1.347E+12
0.000	13.466	0.000	0.2426	2804452.	8800.0000	-0.001074	0.000	1.347E+12	0.000	1.347E+12
0.000	14.589	0.000	0.2284	2922956.	8800.0000	-0.001045	0.000	1.346E+12	0.000	1.346E+12
0.000	15.711	0.000	0.2145	3041460.	8800.0000	-0.001015	0.000	1.346E+12	0.000	1.346E+12

Pier 22af.1p70

0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	1.345E+12	0.000	1.345E+12	0.000	1.785E+12
16.833	0.000	0.2010	3159965.	8800.0000	-0.000984	0.000	1.345E+12	28.763	227100.	2000521.	-19301. -4.233E-05	0.000	1.785E+12
17.955	0.000	0.1880	3278469.	8800.0000	-0.000952	0.000	1.345E+12	52.743	-0.002175	0.000	-18849. -2.819E-05	0.000	1.785E+12
19.077	0.000	0.1754	3396973.	8800.0000	-0.000918	0.000	1.345E+12	38.4300	237980.	0.000	-18283. -1.597E-05	0.000	1.785E+12
20.200	0.000	0.1632	3515478.	8800.0000	-0.000884	0.000	1.344E+12	45.5632	-0.002466	1492877.	-17638. -5.608E-06	0.000	1.785E+12
21.322	0.000	0.1516	3633982.	8800.0000	-0.000852	0.000	1.778E+12	54.988	-0.002605	1250802.	-16946. 2.953E-06	0.000	1.785E+12
22.444	0.000	0.1403	3752486.	8800.0000	-0.000824	0.000	1.778E+12	56.110	-0.002617	1017838.	-16236. 9.790E-06	0.000	1.785E+12
23.566	0.000	0.1294	3870991.	8800.0000	-0.000796	0.000	1.777E+12	57.232	-0.002525	794409.	-15537. 1.498E-05	0.000	1.785E+12
24.688	0.000	0.1189	3989495.	8800.0000	-0.000766	0.000	1.777E+12	58.354	-0.002353	580552.	-14871. 1.859E-05	0.000	1.785E+12
25.811	0.000	0.1088	4107999.	8800.0000	-0.000735	0.000	1.777E+12	59.477	-0.002122	375959.	-14258. 2.068E-05	0.000	1.785E+12
26.933	0.000	0.0991	4226504.	8800.0000	-0.000704	0.000	1.776E+12	60.599	-0.001852	180031.	-12264. 2.133E-05	0.000	1.785E+12
28.055	0.000	0.0898	4345008.	8078.1293	-0.000671	0.000	1.776E+12	61.721	-0.001565	8060.3036	-9021.1476 2.074E-05	0.000	1.785E+12
29.177	0.000	0.0810	4444070.	6610.9328	-0.000638	0.000	1.776E+12	62.843	-0.001278	150275.	-6115.1742 1.922E-05	0.000	1.785E+12
30.299	0.000	0.0726	4523059.	5100.6824	-0.000604	0.000	1.776E+12	63.965	-0.001006	251025.	-3560.8544 1.709E-05	0.000	1.785E+12
31.422	0.000	0.0647	4581446.	3815.8905	-0.000569	0.000	1.775E+12	65.088	-0.000760	314974.	-1365.8248 1.459E-05	0.000	1.785E+12
32.544	0.000	0.0573	4625832.	2731.9203	-0.000534	0.000	1.775E+12	66.210	-0.000546	346929.	467.5866 1.195E-05	0.000	1.785E+12
33.666	0.000	0.0503	465024.	1580.9209	-0.000499	0.000	1.775E+12	67.332	-0.000367	351759.	1939.7972 9.364E-06	0.000	1.785E+12
34.788	0.000	0.0439	4668410.	403.1654	-0.000464	0.000	1.775E+12	68.454	-0.000224	3324336.	3010.3882 6.973E-06	0.000	1.785E+12
35.910	0.000	0.0379	4658883.	-766.2925	-0.000428	0.000	1.775E+12	69.576	-0.000115	299515.	3569.7105 4.887E-06	0.000	1.785E+12
37.033	0.000	0.0323	464772.	-2847.0913	-0.000393	0.000	1.775E+12	70.699	-3.629E-05	253258.	3642.2911 3.164E-06	0.000	1.785E+12
38.155	0.000	0.0273	4589202.	-5764.9652	-0.000358	0.000	1.775E+12	71.821	1.665E-05	203373.	3396.7830 1.812E-06	0.000	1.785E+12
39.277	0.000	0.0227	4492505.	-8481.6738	-0.000323	0.000	1.776E+12	72.943	4.839E-05	153161.	2966.9173 8.042E-07	0.000	1.785E+12
40.399	0.000	0.0186	4360757.	-10948.	-0.000290	0.000	1.776E+12	74.065	6.137E-05	111888.	2453.3196 9.813E-08	0.000	1.785E+12
41.521	0.000	0.0149	4197644.	-13128.	-0.000257	0.000	1.776E+12	75.187	7.560E-05	75253.	1927.2996 -3.586E-07	0.000	1.785E+12
42.644	0.000	0.0116	4007183.	-15000.	-0.000226	0.000	1.777E+12	76.310	8.680E-05	23346.	1435.6194 -6.196E-07	0.000	1.785E+12
43.766	0.000	0.008779	3793659.	-16551.	-0.000197	0.000	1.777E+12	77.432	9.608E-05	1007.8385	1005.5190 -7.346E-07	0.000	1.785E+12
44.888	0.000	0.006522	3561429.	-17780.	-0.000169	0.000	1.778E+12	78.554	1.082E-05	375.0747	649.5104 -7.475E-07	0.000	1.785E+12
46.010	0.000	0.004228	3314803.	-18695.	-0.000143	0.000	1.779E+12	79.676	1.137E-05	1005.	369.6412 -6.944E-07	0.000	1.785E+12
47.132	0.000	0.002472	3057929.	-19311.	-0.000119	0.000	1.779E+12	80.798	7.149E-05	10845.	161.0785 -6.037E-07	0.000	1.785E+12
48.255	0.000	0.001027	2794703.	-19651.	-9.669E-05	0.000	1.780E+12	81.921	2.785E-05	13691.	14.9676 -4.966E-07	0.000	1.785E+12
49.377	0.000	0.00032	2528685.	-19740.	-7.656E-05	0.000	1.781E+12	83.043	1.501E-05	14684.	-79.4052 -3.880E-07	0.000	1.785E+12
50.499	0.000	0.000135	2263046.	-19610.	-5.844E-05	0.000	1.782E+12	84.165	7821926.	14094.	-133.0702 -2.875E-07	0.000	1.785E+12
17.1708	212630.	0.000	0.000	0.000	0.000	0.000	0.000	85.287	4.564E-06	12545.	-156.3563 -2.005E-07	0.000	1.785E+12
	223510.	0.000	0.000	0.000	0.000	0.000	0.000	86.409	1.329E-06	10510.	Page 54	0.000	1.785E+12

As Meant Fixity
Co 71.82
FL -62.60

Pier 22af.lp7o

Maximum bending moment = 4668410. inch-lbs
 Maximum shear force = -19740. lbs
 Depth of maximum bending moment = 34.7882000 feet below pile head
 Depth of maximum shear force = 49.3768000 feet below pile head
 Number of iterations = 8
 Number of zero deflection points = 4

Pile-head Deflection vs. Pile Length for Load Case 9

Boundary Condition Type 1, Shear and Moment

Shear Moment = 8800. lb
 Axial Load = 1382400. in-lb

Pile Length feet	Pile Head Deflection inches	Maximum Moment in-lbs	Maximum Shear lbs
112.2200	0.4387188	4668410.	-19740.
106.6090	0.4287418	4629756.	-19387.
100.9980	0.4286872	4597442.	-19273.
95.3870	0.4319256	4637781.	-19431.
89.7760	0.4371260	4655294.	-19605.
84.1650	0.4369732	4639748.	-19589.
78.5540	0.4354110	4623470.	-19540.
72.9430	0.4360957	4653207.	-19551.
67.3320	0.4334746	4638945.	-19011.
61.7210	0.4499110	4647651.	-22126.
56.1100	0.4994044	4588656.	-27718.
50.4990	0.7610424	4507667.	-35619.
44.8880	2.3833130	4438163.	-47500.
39.2770	72.4346727	4331232.	-68348.

Computed Values of Pile Loading and Deflection for Lateral Loading for Load Case Number 10

Pile-head conditions are Shear and Moment (Loading Type 1)

Shear force at pile head = 8700.0 lbs
 Applied moment at pile head = 1183200.0 in-lbs
 AXIAL thrust load on pile head = 0.0 lbs

Res. X	Depth of Soil	Soil Sph. X	Lat. Load inches	Bending Moment in-lbs	Shear Force lbs	Slope S radians	Total Stress psi*	Bending Stiffness lb-in^2
0.000	0.00	0.00	0.4153	1183200.	8700.0000	-0.001241	0.000	1.352E+12
0.000	1.122	0.000	0.3987	1300358.	8700.0000	-0.001229	0.000	1.352E+12
0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000

Pier 22af.lp7o

-0.7829	7930733.	0.000	0.000	0.000	1.785E+12	0.000	1.785E+12
87.532	-8.374E-07	8333.8728	-158.2917	-1.295E-07	0.000	0.000	0.000
0.4954	7967001.	0.000	-146.3236	-7.444E-08	0.000	0.000	0.000
88.654	-2.157E-06	6247.1731	-126.2657	-3.430E-08	0.000	0.000	0.000
1.2821	8003270.	0.000	-102.3997	-6.985E-09	0.000	0.000	0.000
89.776	-2.842E-06	4392.9696	-77.6677	9.923E-09	0.000	0.000	0.000
1.6969	8039539.	0.000	-53.9127	1.894E-08	0.000	0.000	0.000
1.8477	8075808.	0.000	-32.1353	2.248E-08	0.000	0.000	0.000
90.898	-3.081E-06	2846.4830	-12.7442	2.275E-08	0.000	0.000	0.000
92.020	-3.030E-06	1635.0579	-3.0896	2.173E-08	0.000	0.000	0.000
1.8255	8112076.	0.000	-2.0025	2.039E-08	0.000	0.000	0.000
93.143	-2.814E-06	754.6757	-1.0509	1.885E-08	0.000	0.000	0.000
1.7025	8148345.	0.000	-0.2334	1.720E-08	0.000	0.000	0.000
1.5318	8184614.	0.000	0.4536	1.553E-08	0.000	0.000	0.000
95.387	-2.208E-06	183.0378	1.0156	1.391E-08	0.000	0.000	0.000
1.3481	8220883.	0.000	1.4590	1.239E-08	0.000	0.000	0.000
96.509	-1.908E-06	-160.1994	1.7908	1.102E-08	0.000	0.000	0.000
0.0858	605356.	0.000	2.0176	9.824E-09	0.000	0.000	0.000
97.631	-1.623E-06	-194.0301	2.2222	8.839E-09	0.000	0.000	0.000
0.0757	628024.	0.000	2.3212	8.079E-09	0.000	0.000	0.000
98.754	-1.358E-06	-214.1336	2.1529	7.554E-09	0.000	0.000	0.000
0.0656	650692.	0.000	1.7159	7.249E-09	0.000	0.000	0.000
0.0558	673360.	0.000	1.0025	7.118E-09	0.000	0.000	0.000
0.0463	696028.	0.000	0.000	7.088E-09	0.000	0.000	0.000
100.998	-8.951E-07	-220.4196	0.000	7.088E-09	0.000	0.000	0.000
0.0372	718696.	0.000	0.000	7.088E-09	0.000	0.000	0.000
102.120	-6.971E-07	-210.1160	0.000	7.088E-09	0.000	0.000	0.000
0.0287	741364.	0.000	0.000	7.088E-09	0.000	0.000	0.000
103.242	-5.204E-07	-193.0659	0.000	7.088E-09	0.000	0.000	0.000
0.0206	764032.	0.000	0.000	7.088E-09	0.000	0.000	0.000
104.365	-3.634E-07	-170.8199	0.000	7.088E-09	0.000	0.000	0.000
0.0131	786700.	0.000	0.000	7.088E-09	0.000	0.000	0.000
106.609	-9.882E-08	-144.8348	0.000	7.088E-09	0.000	0.000	0.000
0.0173	2357637.	0.000	0.000	7.088E-09	0.000	0.000	0.000
-0.002597	2448309.	0.000	0.000	7.088E-09	0.000	0.000	0.000
-0.0224	2538981.	0.000	0.000	7.088E-09	0.000	0.000	0.000
109.976	-2.177E-07	-116.4790	0.000	7.088E-09	0.000	0.000	0.000
-0.0425	2629653.	0.000	0.000	7.088E-09	0.000	0.000	0.000
111.098	-3.140E-07	-7.7495	0.000	7.088E-09	0.000	0.000	0.000
-0.0634	2720325.	0.000	0.000	7.088E-09	0.000	0.000	0.000
112.220	4.094E-07	0.000	0.000	7.088E-09	0.000	0.000	0.000
-0.0855	1405499.	0.000	0.000	7.088E-09	0.000	0.000	0.000

* This analysis computed pile response using nonlinear moment-curvature relationships.
 Values of total stress due to combined axial and bending stresses are computed only for elastic sections only and do not equal the actual stresses in concrete and steel.
 Stresses in concrete and steel may be interpolated from the output for nonlinear bending properties relative to the magnitude of bending moment developed in the pile.

Output Summary for Load Case No. 9:

Pile-head deflection = 0.4387188 inches
 Computed slope at pile head = -0.0013244 radians

Pier 22af.1p7o		Pier 22af.1p7o	
0.000	2.244	0.000	-213.4025
0.000	0.000	0.000	38.155
0.000	3.367	0.000	-201.2195
0.000	0.000	0.000	103823.
0.000	0.3660	0.000	39.277
0.000	0.000	0.000	4276645.
0.000	0.3499	0.000	-185.0446
0.000	0.000	0.000	114704.
0.000	0.000	0.000	4152786.
0.000	0.3340	0.000	-165.8720
0.000	0.000	0.000	125585.
0.000	0.3184	0.000	-144.6313
0.000	0.000	0.000	136465.
0.000	0.3031	0.000	-122.1772
0.000	0.000	0.000	147346.
0.000	0.2880	0.000	43.766
0.000	0.000	0.000	0.008450
0.000	0.2732	0.000	-99.2818
0.000	0.000	0.000	158227.
0.000	0.2587	0.000	-76.6286
0.000	0.000	0.000	169107.
0.000	0.2445	0.000	-54.888
0.000	0.000	0.000	0.006102
0.000	0.2307	0.000	-46.010
0.000	0.000	0.000	0.004101
0.000	0.2172	0.000	-47.132
0.000	0.000	0.000	179988.
0.000	0.2041	0.000	-34.3242
0.000	0.000	0.000	190869.
0.000	0.1913	0.000	-15.5796
0.000	0.000	0.000	201749.
0.000	0.1789	0.000	-49.377
0.000	0.000	0.000	-7.018E-05
0.000	0.1670	0.000	1.1081
0.000	0.000	0.000	212630.
0.000	0.1555	0.000	50.499
0.000	0.000	0.000	-0.000934
0.000	0.1444	0.000	15.5101
0.000	0.000	0.000	223510.
0.000	0.1337	0.000	51.621
0.000	0.000	0.000	-0.001579
0.000	0.1233	0.000	26.6257
0.000	0.000	0.000	227100.
0.000	0.1133	0.000	52.743
0.000	0.000	0.000	-0.002029
0.000	0.1037	0.000	35.8527
0.000	0.000	0.000	237980.
0.000	0.0945	0.000	53.866
0.000	0.000	0.000	-0.002309
0.000	0.0857	0.000	42.6759
0.000	0.000	0.000	248861.
0.000	0.0773	0.000	54.988
0.000	0.000	0.000	-0.002445
0.000	0.0689	0.000	47.1544
0.000	0.000	0.000	259741.
0.000	0.0618	0.000	56.110
0.000	0.000	0.000	-0.002459
0.000	0.0547	0.000	49.4100
0.000	0.000	0.000	270622.
0.000	0.0481	0.000	57.232
0.000	0.000	0.000	-0.002374
0.000	0.0419	0.000	49.6217
0.000	0.000	0.000	281503.
0.000	0.0362	0.000	58.354
0.000	0.000	0.000	-0.002212
0.000	0.0309	0.000	48.0210
0.000	0.000	0.000	292383.
0.000	0.0259	0.000	59.477
0.000	0.000	0.000	-0.001993
0.000	0.0200	0.000	44.8892
0.000	0.000	0.000	303264.
0.000	0.0144	0.000	60.599
0.000	0.000	0.000	-0.001738
0.000	0.0133	0.000	40.5541
0.000	0.000	0.000	314145.
0.000	0.0107	0.000	61.721
0.000	0.000	0.000	-0.001466
0.000	0.0094	0.000	244.9006
0.000	0.000	0.000	2249336.
0.000	0.0089	0.000	62.783
0.000	0.000	0.000	-0.001195
0.000	0.0083	0.000	221.1177
0.000	0.000	0.000	2491994.
0.000	0.00783	0.000	63.965
0.000	0.000	0.000	-0.000938
0.000	0.00756	0.000	195.9886
0.000	0.000	0.000	2812369.
0.000	0.00728	0.000	63.088
0.000	0.000	0.000	-0.000706
0.000	0.00699	0.000	170.0275
0.000	0.000	0.000	3242605.
0.000	0.00669	0.000	143.86210
0.000	0.000	0.000	383909505
0.000	0.00639	0.000	67.332
0.000	0.000	0.000	-0.000337
0.000	0.00607	0.000	117.6462
0.000	0.000	0.000	4655700204
0.000	0.00575	0.000	68.624
0.000	0.000	0.000	-0.000204
0.000	0.00542	0.000	91.4991
0.000	0.000	0.000	6047494.
0.000	0.00509	0.000	69.576
0.000	0.000	0.000	-0.000102
0.000	0.00476	0.000	56.0897
0.000	0.000	0.000	386701.
0.000	0.00442	0.000	70.699
0.000	0.000	0.000	-0.00046E-05
0.000	0.00408	0.000	16.2387
0.000	0.000	0.000	7422970.
0.000	0.00375	0.000	71.821
0.000	0.000	0.000	-1.919E-05
0.000	0.0309	0.000	-10.6312
0.000	0.000	0.000	7459238.

Pier 22af.1p7a		Pier 22af.1p7b		Pier 22af.1p7c	
-0.004910	2448309.	0.000	1.785E+12	0.000	1.785E+12
108.853	1.206E-07	-50.5825	2.0389	6.757E-09	0.000
-0.0227	2538981.	0.000	1.785E+12	0.000	1.785E+12
109.976	2.090E-07	-25.1869	1.6111	6.472E-09	0.000
-0.0408	2629653.	0.000	1.785E+12	0.000	1.785E+12
111.098	2.949E-07	-7.1924	0.9352	6.349E-09	0.000
-0.0536	2720325.	0.000	1.785E+12	0.000	1.785E+12
112.220	3.800E-07	0.000	1.785E+12	0.000	1.785E+12
-0.0793	1405499.	0.000	1.785E+12	0.000	1.785E+12

Pier 22af.1p7a		Pier 22af.1p7b		Pier 22af.1p7c	
72.943	4.854E-05	3210.4850	1.635E-06	0.000	1.785E+12
-27.077	7495507.	0.000	1.785E+12	0.000	1.785E+12
74.065	6.322E-05	-103522.	2290.4765	6.998E-07	0.000
-35.3611	7531776.	0.000	1.785E+12	0.000	1.785E+12
75.187	6.739E-05	-69150.	2297.3845	4.837E-08	0.000
-37.8719	7568045.	0.000	1.785E+12	0.000	1.785E+12
76.310	6.435E-05	-41647.	1797.0460	-3.696E-07	0.000
-36.4373	7604313.	0.000	1.785E+12	0.000	1.785E+12
77.432	5.743E-05	-20751.	1332.2962	-6.051E-07	0.000
-32.5863	7640382.	0.000	1.785E+12	0.000	1.785E+12
78.554	4.823E-05	-5784.0545	927.7565	-7.051E-07	0.000
-27.4951	7676851.	0.000	1.785E+12	0.000	1.785E+12
79.676	3.844E-05	4236.4547	594.3700	-7.109E-07	0.000
-22.0188	7713220.	0.000	1.785E+12	0.000	1.785E+12
80.798	2.909E-05	10244.	333.4163	-6.562E-07	0.000
-16.7375	7749389.	0.000	1.785E+12	0.000	1.785E+12
81.921	2.077E-05	13216.	139.8697	-5.677E-07	0.000
-12.0076	7785657.	0.000	1.785E+12	0.000	1.785E+12
83.043	1.380E-05	14011.	5.0670	-4.650E-07	0.000
-8.0130	7821926.	0.000	1.785E+12	0.000	1.785E+12
84.165	8.246E-06	13353.	-81.2835	-3.617E-07	0.000
-4.8116	7858195.	0.000	1.785E+12	0.000	1.785E+12
85.287	4.032E-06	11822.	-129.6769	-2.668E-07	0.000
-2.3757	7894464.	0.000	1.785E+12	0.000	1.785E+12
86.409	1.061E-06	9860.1964	-149.8789	-1.850E-07	0.000
-0.6247	7930733.	0.000	1.785E+12	0.000	1.785E+12
87.532	-9.292E-07	7785.2264	-150.3836	-1.184E-07	0.000
0.5497	7967001.	0.000	1.785E+12	0.000	1.785E+12
88.654	-2.128E-06	5809.9438	-138.1670	-6.710E-08	0.000
1.2647	8003270.	0.000	1.785E+12	0.000	1.785E+12
89.776	-2.736E-06	4064.0013	-118.6522	-2.985E-08	0.000
1.6336	8039539.	0.000	1.785E+12	0.000	1.785E+12
90.898	-2.932E-06	2614.3081	-95.8142	-4.652E-09	0.000
1.7382	8075608.	0.000	1.785E+12	0.000	1.785E+12
92.020	-2.862E-06	1483.4579	-72.3687	1.081E-08	0.000
1.7238	8112076.	0.000	1.785E+12	0.000	1.785E+12
93.143	-2.641E-06	665.2161	-50.0029	1.891E-08	0.000
1.5979	8148345.	0.000	1.785E+12	0.000	1.785E+12
94.265	-2.332E-06	136.7391	-29.6181	2.194E-08	0.000
1.4206	8184614.	0.000	1.785E+12	0.000	1.785E+12
95.388	-2.150E-06	132.4825	-11.5665	2.196E-08	0.000
1.2534	8220893.	0.000	1.785E+12	0.000	1.785E+12
96.509	-1.961E-06	174.7779	-2.6078	2.080E-08	0.000
1.0782	8260336.	0.000	1.785E+12	0.000	1.785E+12
97.631	-1.800E-06	209.7188	-1.6071	1.937E-08	0.000
0.8697	8300290E-06	218.0611	-0.7362	1.779E-08	0.000
0.6979	-1.656E-06	226.5459	0.007238	1.612E-08	0.000
0.5505	8340311E-06	232.0000	0.6276	1.446E-08	0.000
0.4161	8380328E-06	237.8662	1.1309	1.286E-08	0.000
0.2922	-1.520E-06	245.6426	1.5241	1.138E-08	0.000
0.1803	-1.374E-06	187.4072	1.8142	1.005E-08	0.000
0.0819	-1.241E-06	164.5954	2.0082	8.909E-09	0.000
0.0000	-1.120E-06	138.5463	2.1701	7.970E-09	0.000
0.0000	-1.010E-06	110.5093	2.2250	7.250E-09	0.000
0.0000	-9.000E-07	80.1007	2.2250	7.250E-09	0.000
0.0000	-8.000E-07	60.1007	2.2250	7.250E-09	0.000

* This analysis computed pile response using nonlinear moment-curvature relationships. Values of total stress due to combined axial and bending stresses are computed only for elastic sections only and do not equal the actual stresses in concrete and steel. Stresses in concrete and steel may be interpolated from the output for nonlinear bending properties relative to the magnitude of bending moment developed in the pile.

Output Summary for Load Case No. 10:

Pile-head deflection = 0.4152266 inches
 Computed slope at pile head = -0.0012412 radians
 Maximum bending moment = 4436084. inch-lbs
 Maximum shear force = -18796. lbs
 Depth of maximum bending moment = 34.7682000 feet below pile head
 Depth of maximum shear force = 49.3768000 feet below pile head
 Number of iterations = 8
 Number of zero deflection points = 4

----- Pile-head Deflection vs. Pile Length for Load Case 10 -----

Boundary Condition Type 1, Shear and Moment

Shear = 8700. lb
 Moment = 1183200. in-lb
 Axial Load = 0. lb

Pile Length feet	Pile Head Deflection inches	Maximum Moment in-lbs	Maximum Shear lbs
112.2200	0.4152266	4436084.	-18796.
106.9980	0.4036266	4362596.	-18340.
101.7760	0.4036266	4362596.	-18340.
96.5540	0.4036266	4362596.	-18340.
91.3320	0.4134076	4406792.	-18694.
86.1100	0.4119681	4391173.	-18598.
80.8880	0.4119681	4391173.	-18598.
75.6660	0.4101166	4407047.	-18058.
70.4440	0.4238757	4415141.	-21049.
65.2220	0.4238757	4415141.	-21049.
60.0000	0.7160300	4356017.	-56370.
54.7780	0.7160300	4275003.	-33844.
49.5560	2.1909835	4206973.	-45071.
44.3340	52.6904141	4105439.	-65504.

Summary of Pile Response(s)

Definitions of Pile-head Loading Conditions:

- Load Type 1: Load 1 = Shear, lbs, and Load 2 = Moment, in-lbs
- Load Type 2: Load 1 = Shear, lbs, and Load 2 = Slope, radians
- Load Type 3: Load 1 = Shear, lbs, and Load 2 = Rotational Stiffness, in-lbs/radian
- Load Type 4: Load 1 = Top Deflection, inches, and Load 2 = Moment, in-lbs
- Load Type 5: Load 1 = Top Deflection, inches, and Load 2 = Slope, radians

Case No.	Maximum Load in Pile	Pile-head Condition 1	Pile-head Condition 2	Axial Loading	Pile-head Deflection	Maximum Moment in Pile
No.	No.	Y (inches) or V (lbs)	Y (inches) or M (in-lb)	lbs	inches	in-lbs
1	4	Y = 0.5000	M = 1382400.	0.0000000	0.50000000	
5328127.	4	Y = -22601.	M = 1382400.	0.0000000	1.00000000	
8585541.	4	Y = -36462.	M = 1382400.	0.0000000	1.50000000	
10786558.	4	Y = -46028.	M = 1382400.	0.0000000	2.00000000	
13419748.	4	Y = -57001.	M = 1382400.	0.0000000	0.50000000	
5331271.	4	Y = -22731.	M = 1183200.	0.0000000	1.00000000	
8690569.	4	Y = -36813.	M = 1183200.	0.0000000	1.50000000	
10852463.	4	Y = -46344.	M = 1183200.	0.0000000	2.00000000	
13520406.	4	Y = -57389.	M = 1183200.	0.0000000	0.43871878	
4668410.	1	V = 8700.0000	M = 1183200.	0.0000000	0.41532658	
4436084.	1	V = -18796.	M = 1183200.	0.0000000		

ser-1 $\Delta = 0.42'' < 1.0$ ok.

The analysis ended normally.

PIER 1

Worst Case	Limit State	Load Case	Column	Top/Bot	M _u (k-ft)	P _u (k)	V _u (k)
Max P _u	STR-I	1/2/3	1	T	540.1	777.5	
	SER-I	1/2/3	1	T	248.8	516.1	
Max V _u	STR-I	26	3	T	458.3		13.6
	SER-I	28	4	T	65.3		9.9

PIER 2

$P_R = 703^k$ OK

Worst Case	Limit State	Load Case	Column	Top/Bot	M _u	P _u	V _u
Max P _u	STR-I	2	4	T	252.0	689.2	
	SER-I	1/3	1	T	132.4	464.8	
Max V _u	STR-V	28	4	T	115.2		8.8
	SER-I	28	4	T	98.6		8.7

PIER 3

Worst Case	Limit State	Load Case	Column	Top/Bot	M _u	P _u	V _u
Max P _u	STR-I	4	4	T	141.4	688.3	
	SER-I	4	1	T	218.4	500.6	
Max V _u	STR-III	25	2	T	651.5		21.3
	SER-I	26	3	T	365.0		11.0

PIER 4

Worst Case	Limit State	Load Case	Column	Top/Bot	M _u	P _u	V _u
Max P _u	STR-I	1/2/3	1	T	377.0	709.1	
	SER-I	1/2/3	1	T	185.3	475.0	
Max V _u	STR-I	26	4	T	316.1		9.8
	SER-I	26	4	T	270.7		8.4

PIER 2

4' Ø, 1/2" STEEL CASING @ EL -12.0

DEFLECTION	STR-V (lbs)	SER-1 (lbs)	
0.5	10,435	10,961	OK
1.0	18,562	19,250	←
1.5	24,084	24,710	
→ 2.0	30,725	31,438	

OK

GEOTECHNICAL AXIAL CAPACITY
 = 703^k > 689.2^k OK

LATERAL CAPACITY, 2" DEFLECTION (STR-V)
 = 30.73^k > 8.8^k

LATERAL CAPACITY, 1" DEFLECTION (SER-1)
 = 19.25^k > 8.7^k

Boring No. JS-5

By: SJM

Chk:
 OG Elev. = 11.00

Sample No.	Depth of SS run (ft)	N-Values Field	q'_v (ksf)	C_N	N_{CORR}
1	20	4	0.952	1.250	5
2	22	0	1.047	1.218	0
3	24	0	1.142	1.185	0
4	26	2	1.238	1.162	2
5	33	10	1.571	1.083	11
6	38	13	1.809	1.035	13
7	43	29	2.047	0.994	29
8	48	16	2.285	0.957	15
9	53	17	2.523	0.924	16
10	58	19	2.761	0.894	17
11	63	15	2.999	0.866	13
12	68	22	3.237	0.841	18
13	73	23	3.475	0.817	19
14	78	45	3.713	0.795	36
15	83	82	3.951	0.774	63
16	88	84	4.189	0.755	63
17	93	41	4.427	0.736	30
18	98	80	4.665	0.719	57
19	103	78	4.903	0.702	55
20	108	50	5.141	0.686	34
21	113	50	5.379	0.671	34
22	118	50	5.617	0.656	33

GWT= 5.0
 $\gamma = 110$ lb/ft³
 $\gamma' = 47.6$ lb/ft³

$C_N = 0.77 \times \log(40/q'_v)$
 $N_{CORR} = N_{Field} \times C_N$

N_{avg} (Below BFE) = 26
 (Ref. AASHTO Eqn 10.4.6.2.4-1)

PIER 3

Boring No. JS-6

By: SJM

Chk: AT LAYER
 OG Elev. = 11.00

Sample No.	Depth of SS run (ft)	N-Values Field	q'_v (ksf)	C_N	N_{CORR}
1	23	0	1.095	1.203	0
2	25	19	1.190	1.175	22
3	27	0	1.285	1.150	0
4	29	0	1.380	1.126	0
5	31	12	1.476	1.103	13
6	33	9	1.571	1.083	10
7	38	4	1.809	1.035	4
8	43	19	2.047	0.994	19
9	48	15	2.285	0.957	14
10	53	13	2.523	0.924	12
11	58	9	2.761	0.894	8
12	63	23	2.999	0.866	20
13	68	31	3.237	0.841	26
14	73	46	3.475	0.817	38
15	78	33	3.713	0.795	26
16	83	24	3.951	0.774	19
17	88	54	4.189	0.755	41
18	93	50	4.427	0.736	37
19	98	56	4.665	0.719	40
20	103	50	4.903	0.702	35
21	108	50	5.141	0.686	35

GWT= 0.0
 $\gamma = 110$ lb/ft³
 $\gamma' = 47.6$ lb/ft³

$C_N = 0.77 \times \log(40/q'_v)$
 $N_{CORR} = N_{Field} \times C_N$

N_{avg} (Below BFE) = 20
 (Ref. AASHTO Eqn 10.4.6.2.4-1)

①
 ②
 ③
 ④

PROJECT BRI-159 JOB NO. _____ SHEET NO. 1 OF 1
 LOCATION PIER 3 (AXIAL & LATERAL CAPACITIES)
 SUBJECT SOIL PROFILE (JS-6)
 DESIGNED BY SJM DATE 7/14 CHECKED BY AT DATE 8/14
 REVISED BY _____ DATE _____ BACK CHECKED BY _____ DATE _____

PROFILE BASED ON
 BORING JS-6
 X - DEPTH BELOW TOP OF CDM
 X = 0'



ELEVATION
 TOP OF CDM. — 8.83
 MHW — 4.63
 SOIL TYPE

REF./REM.

$P_u = 688.3^k$
 $R_R = 695^k$

DEPTH BELOW RIVER BED (ft)
 LAYER THICKNESS (ft)
 Y = 0

(8')
 Y = 8'
 X = 28.83'
 X = 30.83'

SOFT SILT $N_{CORR} = 0-22$
 $\gamma_s = 105$ $\gamma'_s = 42.6$
 $\phi = 0$ $E_{50} = 0.02$
 $C = 600$ psf

(27')
 Y = 35'

MED SAND
 $\gamma_s = 120$ pcf $\gamma'_s = 57.6$ pcf
 $\phi = 32^\circ$ $K = 60$ pci
 $C = 0$ psf

100 YR SCOUR.

(45')
 Y = 80'

48" ϕ CASED

HARD SANDY CLAY $N_{CORR} = 19-41$
 $\gamma_s = 125$ pcf $\gamma'_s = 62.6$ pcf
 $C = 2000$ psf $E_{50} = 0.007$
 $\phi = 0^\circ$ $K = 200$ pci

(15')
 Y = 95'

4" ϕ CASED

Very Dense Sand
 $\gamma_s = 135$ pcf $\gamma'_s = 72.6$ pcf
 $\phi = 36^\circ$ $K = 125$ pci
 $C = 0$ psf

X = 107.83
 X = 115.83

MIN END BORING.
 BOTTOM OF DRILLED SHAFT

END @

X = 107.83

Y = 87'
 $R_R = 695^k$ (347.44) AXIAL CAPACITY

EL = -99.0

AXIAL CAPACITY

Pier 32.sfo

SHAFT for Windows, Version 2012.7.11

Serial Number : 228741384

VERTICALLY LOADED DRILLED SHAFT ANALYSIS
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Path to file locations : Y:\Bridges\DELDOT\BRI-159_JAMES ST
Name of input data file : Pier 32.sfd
Name of output file : Pier 32.sfo
Name of plot output file : Pier 32.sfp
Name of runtime file : Pier 32.sfr

Time and Date of Analysis

Date: October 21, 2014 Time: 14:41:44

BRI-159 Pier 3

PROPOSED DEPTH = 95.0 FT

NUMBER OF LAYERS = 4

WATER TABLE DEPTH = 0.0 FT.

SOIL INFORMATION

LAYER NO 1----CLAY

AT THE TOP

STRENGTH REDUCTION FACTOR-ALPHA = 0.550E+00
END BEARING COEFFICIENT-NC = 0.800E+01
UNDRAINED SHEAR STRENGTH, LB/SQ FT = 0.600E+03
INTERNAL FRICTION ANGLE, DEG = 0.000E+00
BLOWS PER FOOT FROM STANDARD PENETRATION TEST = 0.000E+00
SOIL UNIT WEIGHT, LB/CU FT = 0.105E+03
MAXIMUM LOAD TRANSFER FOR SOIL, LB/SQ FT = 0.100E+11
DEPTH, FT = 0.000E+00

AT THE BOTTOM

Page 1

Pier 32.sfo

STRENGTH REDUCTION FACTOR-ALPHA = 0.550E+00
END BEARING COEFFICIENT-NC = 0.800E+01
UNDRAINED SHEAR STRENGTH, LB/SQ FT = 0.600E+03
INTERNAL FRICTION ANGLE, DEG. = 0.000E+00
BLOWS PER FOOT FROM STANDARD PENETRATION TEST = 0.000E+00
SOIL UNIT WEIGHT, LB/CU FT = 0.105E+03
MAXIMUM LOAD TRANSFER FOR SOIL, LB/SQ FT = 0.100E+11
DEPTH, FT = 0.800E+01

LRFD RESISTANCE FACTOR (SIDE FRICTION) = 0.450E+00
LRFD RESISTANCE FACTOR (TIP RESISTANCE) = 0.400E+00

LAYER NO 2----SAND

AT THE TOP

SKIN FRICTION COEFFICIENT- BETA = 0.112E+01
UNDRAINED SHEAR STRENGTH, LB/SQ FT = 0.900E+00
INTERNAL FRICTION ANGLE, DEG. = 0.320E+02
BLOWS PER FOOT FROM STANDARD PENETRATION TEST = 0.900E+00
SOIL UNIT WEIGHT, LB/CU FT = 0.120E+03
MAXIMUM LOAD TRANSFER FOR SOIL, LB/SQ FT = 0.100E+11
DEPTH, FT = 0.800E+01

AT THE BOTTOM

SKIN FRICTION COEFFICIENT- BETA = 0.701E+00
UNDRAINED SHEAR STRENGTH, LB/SQ FT = 0.000E+00
INTERNAL FRICTION ANGLE, DEG. = 0.320E+02
BLOWS PER FOOT FROM STANDARD PENETRATION TEST = 0.000E+00
SOIL UNIT WEIGHT, LB/CU FT = 0.100E+03
MAXIMUM LOAD TRANSFER FOR SOIL, LB/SQ FT = 0.100E+11
DEPTH, FT = 0.350E+02

LRFD RESISTANCE FACTOR (SIDE FRICTION) = 0.550E+00
LRFD RESISTANCE FACTOR (TIP RESISTANCE) = 0.500E+00

LAYER NO 3----CLAY

AT THE TOP

STRENGTH REDUCTION FACTOR-ALPHA = 0.550E+00
END BEARING COEFFICIENT-NC = 0.800E+01
UNDRAINED SHEAR STRENGTH, LB/SQ FT = 0.200E+04
INTERNAL FRICTION ANGLE, DEG = 0.000E+00
BLOWS PER FOOT FROM STANDARD PENETRATION TEST = 0.000E+00
SOIL UNIT WEIGHT, LB/CU FT = 0.125E+03
MAXIMUM LOAD TRANSFER FOR SOIL, LB/SQ FT = 0.100E+11
DEPTH, FT = 0.350E+02

AT THE BOTTOM

STRENGTH REDUCTION FACTOR-ALPHA = 0.550E+00
END BEARING COEFFICIENT-NC = 0.800E+01
UNDRAINED SHEAR STRENGTH, LB/SQ FT = 0.200E+04
INTERNAL FRICTION ANGLE, DEG. = 0.000E+00
BLOWS PER FOOT FROM STANDARD PENETRATION TEST = 0.000E+00

Page 2

Pier 32.sfo

SOIL UNIT WEIGHT, LB/CU FT = 0.125E+03
 MAXIMUM LOAD TRANSFER FOR SOIL, LB/SQ FT = 0.100E+11
 DEPTH, FT = 0.800E+02

LRFD RESISTANCE FACTOR (SIDE FRICTION) = 0.450E+00
 LRFD RESISTANCE FACTOR (TIP RESISTANCE) = 0.400E+00

LAYER NO 4-----SAND

AT THE TOP

SKIN FRICTION COEFFICIENT- BETA = 0.293E+00
 UNDRAINED SHEAR STRENGTH, LB/SQ FT = 0.000E+00
 INTERNAL FRICTION ANGLE, DEG. = 0.360E+02
 BLOWS PER FOOT FROM STANDARD PENETRATION TEST = 0.000E+00
 SOIL UNIT WEIGHT, LB/CU FT = 0.135E+03
 MAXIMUM LOAD TRANSFER FOR SOIL, LB/SQ FT = 0.100E+11
 DEPTH, FT = 0.800E+02

AT THE BOTTOM

SKIN FRICTION COEFFICIENT- BETA = 0.250E+00
 UNDRAINED SHEAR STRENGTH, LB/SQ FT = 0.000E+00
 INTERNAL FRICTION ANGLE, DEG. = 0.360E+02
 BLOWS PER FOOT FROM STANDARD PENETRATION TEST = 0.000E+00
 SOIL UNIT WEIGHT, LB/CU FT = 0.135E+03
 MAXIMUM LOAD TRANSFER FOR SOIL, LB/SQ FT = 0.110E+03

LRFD RESISTANCE FACTOR (SIDE FRICTION) = 0.550E+00
 LRFD RESISTANCE FACTOR (TIP RESISTANCE) = 0.500E+00

DRILLED SHAFT INFORMATION

DIAMETER OF STEM = 4.000 FT.
 DIAMETER OF BASE = 4.000 FT.
 END OF STEM TO BASE = 0.000 FT.
 ANGLE OF BELL = 0.000 DEG.
 IGNORED TOP PORTION = 10.000 FT.
 IGNORED BOTTOM PORTION = 4.000 FT.
 AREA OF ONE PERCENT STEEL = 18.098 SQ.IN.
 ELASTIC MODULUS, EC = 0.312E+07 LB/SQ IN.
 VOLUME OF UNDERREAM = 0.000 CU.YDS.

PREDICTED RESULTS

QS = ULTIMATE SIDE RESISTANCE;
 QB = ULTIMATE BASE RESISTANCE;
 WT = WEIGHT OF DRILLED SHAFT (UPLIFT CAPACITY ONLY);
 QU = TOTAL ULTIMATE RESISTANCE;
 LRFD QS = TOTAL SIDE FRICTION USING LRFD RESISTANCE FACTOR

LENGTH (FEET)	VOLUME (CU.YDS)	QS (TONS)	QB (TONS)	QU (TONS)	LRFD QS (TONS)	LRFD QB (TONS)	LRFD QU (TONS)
15.0	6.98	4.00	67.04	71.04	2.20	33.52	35.72
16.0	7.45	8.30	67.04	75.33	4.56	33.52	38.08
17.0	7.91	12.68	67.04	79.92	7.08	33.52	40.60
18.0	8.38	17.74	67.04	84.78	9.76	33.52	43.28
19.0	8.84	22.87	67.04	89.91	12.58	33.52	46.10
20.0	9.31	28.26	67.04	95.29	15.54	33.52	49.06
21.0	9.78	33.89	67.04	100.93	18.64	33.52	52.16
22.0	10.24	39.76	67.04	106.80	21.87	33.52	55.39
23.0	10.71	45.87	67.04	112.91	25.23	33.52	58.75
24.0	11.17	52.19	67.04	119.23	28.71	33.52	62.23
25.0	11.64	58.73	67.04	125.77	32.30	33.52	65.82
26.0	12.10	65.48	67.04	132.52	36.01	33.52	69.53
27.0	12.57	72.42	67.04	139.46	39.83	33.52	73.35
28.0	13.03	79.56	72.06	151.62	43.76	36.03	79.79
29.0	13.50	86.87	77.65	164.52	47.78	38.82	86.60
30.0	13.96	94.36	83.79	178.15	51.90	41.90	93.80
31.0	14.43	102.02	90.49	192.51	56.11	45.25	101.36
32.0	14.90	109.84	95.52	205.36	60.41	47.76	108.17
33.0	15.36	117.82	98.87	216.69	64.80	49.43	114.23
34.0	15.83	125.94	100.54	226.48	69.27	50.27	119.54
35.0	16.29	134.20	100.54	234.74	73.81	40.22	114.03
36.0	16.76	142.60	100.54	243.14	78.43	40.22	118.65
37.0	17.22	151.12	100.54	251.66	83.11	40.22	123.33
38.0	17.69	159.76	100.54	260.31	87.87	40.22	128.09
39.0	18.15	168.52	100.54	269.06	92.69	40.22	132.90
40.0	18.62	175.43	100.54	275.98	95.80	40.22	136.01
41.0	19.08	182.34	100.54	282.89	98.91	40.22	139.12
42.0	19.55	189.26	100.54	289.80	102.02	40.22	142.23
43.0	20.02	196.17	100.54	296.71	105.13	40.22	145.35
44.0	20.48	203.08	100.54	303.63	108.24	40.22	148.46
45.0	20.95	209.99	100.54	310.54	111.35	40.22	151.57
46.0	21.41	216.91	100.54	317.45	114.46	40.22	154.68
47.0	21.88	223.82	100.54	324.36	117.57	40.22	157.79
48.0	22.34	230.73	100.54	331.27	120.68	40.22	160.90
49.0	22.81	237.64	100.54	338.19	123.79	40.22	164.01
50.0	23.27	244.56	100.54	345.10	126.90	40.22	167.12
51.0	23.74	251.47	100.54	352.01	130.01	40.22	170.23
52.0	24.21	258.38	100.54	358.92	133.12	40.22	173.34
53.0	24.67	265.29	100.54	365.84	136.23	40.22	176.45
54.0	25.14	272.21	100.54	372.75	139.34	40.22	179.56
55.0	25.60	279.12	100.54	379.66	142.45	40.22	182.67
56.0	26.07	286.03	100.54	386.57	145.57	40.22	185.78
57.0	26.53	292.94	100.54	393.49	148.68	40.22	188.89
58.0	27.00	299.85	100.54	400.40	151.79	40.22	192.00
59.0	27.46	306.77	100.54	407.31	154.90	40.22	195.11
60.0	27.93	313.68	100.54	414.22	158.01	40.22	198.22
61.0	28.39	320.59	100.54	421.13	161.12	40.22	201.33
62.0	28.86	327.50	100.54	428.04	164.23	40.22	204.44
63.0	29.32	334.41	100.54	434.95	167.34	40.22	207.55
64.0	29.79	341.32	100.54	441.87	170.45	40.22	210.66
65.0	30.25	348.23	100.54	448.78	173.56	40.22	213.77
66.0	30.72	355.14	100.54	455.70	176.67	40.22	216.88
67.0	31.18	362.05	100.54	462.61	179.78	40.22	220.00
68.0	31.65	368.96	100.54	469.52	182.89	40.22	223.11
69.0	32.12	375.87	100.54	476.44	186.00	40.22	226.22
70.0	32.58	382.80	100.54	483.35	189.11	40.22	229.33

Pier 32.sfo

0.5388E+03 0.2210E+00 0.2093E+02 0.1000E+00
 0.6231E+03 0.3972E+00 0.5221E+02 0.2300E+00
 0.6673E+03 0.9659E+00 0.9572E+02 0.5000E+00
 0.6797E+03 0.7972E+00 0.1196E+03 0.6230E+00
 0.6929E+03 0.1381E+01 0.1528E+03 0.1200E+01
 0.7572E+03 0.2607E+01 0.2172E+03 0.2400E+01

RESULT FROM LOWER-BOUND LINE

TOP LOAD Ton	TIP MOVEMENT IN.	TIP LOAD Ton	TIP MOVEMENT IN.
0.3742E-01	0.1803E-04	0.8380E-03	0.1000E-04
0.1671E+00	0.9013E-04	0.4380E-02	0.5000E-04
0.3742E+00	0.1803E-03	0.8380E-02	0.1000E-03
0.1671E+02	0.9013E-02	0.4380E-01	0.5000E-02
0.2807E+02	0.1532E-01	0.5385E+00	0.7500E-02
0.3742E+02	0.1803E-01	0.8380E+00	0.1000E-01
0.9383E+02	0.5100E-01	0.2093E+01	0.2500E-01
0.1604E+03	0.8910E-01	0.4380E+01	0.5000E-01
0.3244E+03	0.1300E+00	0.8380E+01	0.1000E-01
0.4965E+03	0.1652E+00	0.2172E+02	0.2500E-01
0.5462E+03	0.3623E+00	0.5317E+02	0.5000E+00
0.5436E+03	0.5284E+00	0.1046E+03	0.1200E+01
0.5691E+03	0.7311E+00	0.1046E+03	0.2400E+01
0.6941E+03	0.2579E+01	0.1911E+03	0.2400E+01

Pier 32.sfo

33.05 389.72 100.54 490.26 192.22 40.22 232.44
 33.51 396.63 100.54 497.17 195.33 40.22 235.55
 33.98 403.54 115.63 519.17 198.45 46.25 244.70
 34.45 410.45 132.39 542.84 201.56 52.96 254.51
 34.91 417.37 150.83 568.19 204.67 60.33 265.00
 35.38 424.28 170.94 595.22 207.78 68.38 276.15
 35.84 431.19 186.03 617.22 210.89 74.41 285.30
 36.31 438.10 196.08 634.19 214.00 78.43 292.43
 36.77 445.02 201.11 646.13 217.11 80.45 297.55
 37.24 451.93 201.11 653.04 220.22 100.56 320.78
 37.70 458.84 201.11 659.95 223.33 100.56 323.89
 38.17 465.75 201.11 666.87 226.44 100.56 327.00
 38.63 472.67 201.11 673.78 229.55 100.56 330.11
 39.10 479.58 201.11 680.69 232.66 100.56 333.22
 39.57 486.50 201.11 687.61 235.77 100.56 336.33
 40.03 493.42 201.11 694.52 238.88 100.56 339.44
 40.50 500.33 201.11 701.44 242.00 100.56 342.55
 40.96 507.24 201.11 708.35 245.11 100.56 345.66
 41.43 514.15 201.11 715.26 248.22 100.56 348.77
 41.89 521.06 201.11 722.17 251.33 100.56 351.88
 42.36 527.97 201.11 729.08 254.44 100.56 354.99
 42.82 534.88 201.11 736.00 257.55 100.56 358.10
 43.29 541.79 201.11 742.91 260.66 100.56 361.21
 43.76 548.70 201.11 749.82 263.77 100.56 364.32
 44.22 555.61 201.11 756.73 266.88 100.56 367.43
 44.68 562.52 201.11 763.64 270.00 100.56 370.54
 45.14 569.43 201.11 770.55 273.11 100.56 373.65
 45.60 576.34 201.11 777.46 276.22 100.56 376.76
 46.06 583.25 201.11 784.37 279.33 100.56 379.87
 46.52 590.16 201.11 791.28 282.44 100.56 382.98
 46.98 597.07 201.11 798.19 285.55 100.56 386.09
 47.44 603.98 201.11 805.10 288.66 100.56 389.20
 47.90 610.89 201.11 812.01 291.77 100.56 392.31
 48.36 617.80 201.11 818.92 294.88 100.56 395.42
 48.82 624.71 201.11 825.83 298.00 100.56 398.53
 49.28 631.62 201.11 832.74 301.11 100.56 401.64
 49.74 638.53 201.11 839.65 304.22 100.56 404.75
 50.20 645.44 201.11 846.56 307.33 100.56 407.86
 50.66 652.35 201.11 853.47 310.44 100.56 410.97
 51.12 659.26 201.11 860.38 313.55 100.56 414.08
 51.58 666.17 201.11 867.29 316.66 100.56 417.19
 52.04 673.08 201.11 874.20 319.77 100.56 420.30
 52.50 679.99 201.11 881.11 322.88 100.56 423.41
 52.96 686.90 201.11 888.02 326.00 100.56 426.52
 53.42 693.81 201.11 894.93 329.11 100.56 429.63
 53.88 700.72 201.11 901.84 332.22 100.56 432.74
 54.34 707.63 201.11 908.75 335.33 100.56 435.85
 54.80 714.54 201.11 915.66 338.44 100.56 438.96
 55.26 721.45 201.11 922.57 341.55 100.56 442.07
 55.72 728.36 201.11 929.48 344.66 100.56 445.18
 56.18 735.27 201.11 936.39 347.77 100.56 448.29
 56.64 742.18 201.11 943.30 350.88 100.56 451.40
 57.10 749.09 201.11 950.21 354.00 100.56 454.51
 57.56 756.00 201.11 957.12 357.11 100.56 457.62
 58.02 762.91 201.11 964.03 360.22 100.56 460.73
 58.48 769.82 201.11 970.94 363.33 100.56 463.84
 58.94 776.73 201.11 977.85 366.44 100.56 466.95
 59.40 783.64 201.11 984.76 369.55 100.56 470.06
 59.86 790.55 201.11 991.67 372.66 100.56 473.17
 60.32 797.46 201.11 998.58 375.77 100.56 476.28
 60.78 804.37 201.11 1005.49 378.88 100.56 479.39
 61.24 811.28 201.11 1012.40 382.00 100.56 482.50
 61.70 818.19 201.11 1019.31 385.11 100.56 485.61
 62.16 825.10 201.11 1026.22 388.22 100.56 488.72
 62.62 832.01 201.11 1033.13 391.33 100.56 491.83
 63.08 838.92 201.11 1040.04 394.44 100.56 494.94
 63.54 845.83 201.11 1046.95 397.55 100.56 498.05
 64.00 852.74 201.11 1053.86 400.66 100.56 501.16
 64.46 859.65 201.11 1060.77 403.77 100.56 504.27
 64.92 866.56 201.11 1067.68 406.88 100.56 507.38
 65.38 873.47 201.11 1074.59 410.00 100.56 510.49
 65.84 880.38 201.11 1081.50 413.11 100.56 513.60
 66.30 887.29 201.11 1088.41 416.22 100.56 516.71
 66.76 894.20 201.11 1095.32 419.33 100.56 519.82
 67.22 901.11 201.11 1102.23 422.44 100.56 522.93
 67.68 908.02 201.11 1109.14 425.55 100.56 526.04
 68.14 914.93 201.11 1116.05 428.66 100.56 529.15
 68.60 921.84 201.11 1122.96 431.77 100.56 532.26
 69.06 928.75 201.11 1129.87 434.88 100.56 535.37
 69.52 935.66 201.11 1136.78 438.00 100.56 538.48
 69.98 942.57 201.11 1143.69 441.11 100.56 541.59
 70.44 949.48 201.11 1150.60 444.22 100.56 544.70
 70.90 956.39 201.11 1157.51 447.33 100.56 547.81
 71.36 963.30 201.11 1164.42 450.44 100.56 550.92
 71.82 970.21 201.11 1171.33 453.55 100.56 554.03
 72.28 977.12 201.11 1178.24 456.66 100.56 557.14
 72.74 984.03 201.11 1185.15 459.77 100.56 560.25
 73.20 990.94 201.11 1192.06 462.88 100.56 563.36
 73.66 997.85 201.11 1198.97 466.00 100.56 566.47
 74.12 1004.76 201.11 1205.88 469.11 100.56 569.58
 74.58 1011.67 201.11 1212.79 472.22 100.56 572.69
 75.04 1018.58 201.11 1219.70 475.33 100.56 575.80
 75.50 1025.49 201.11 1226.61 478.44 100.56 578.91
 75.96 1032.40 201.11 1233.52 481.55 100.56 582.02
 76.42 1039.31 201.11 1240.43 484.66 100.56 585.13
 76.88 1046.22 201.11 1247.34 487.77 100.56 588.24
 77.34 1053.13 201.11 1254.25 490.88 100.56 591.35
 77.80 1060.04 201.11 1261.16 494.00 100.56 594.46
 78.26 1066.95 201.11 1268.07 497.11 100.56 597.57
 78.72 1073.86 201.11 1274.98 500.22 100.56 600.68
 79.18 1080.77 201.11 1281.89 503.33 100.56 603.79
 79.64 1087.68 201.11 1288.80 506.44 100.56 606.90
 80.10 1094.59 201.11 1295.71 509.55 100.56 610.01
 80.56 1101.50 201.11 1302.62 512.66 100.56 613.12
 81.02 1108.41 201.11 1309.53 515.77 100.56 616.23
 81.48 1115.32 201.11 1316.44 518.88 100.56 619.34
 81.94 1122.23 201.11 1323.35 522.00 100.56 622.45
 82.40 1129.14 201.11 1330.26 525.11 100.56 625.56
 82.86 1136.05 201.11 1337.17 528.22 100.56 628.67
 83.32 1142.96 201.11 1344.08 531.33 100.56 631.78
 83.78 1149.87 201.11 1351.00 534.44 100.56 634.89
 84.24 1156.78 201.11 1357.91 537.55 100.56 638.00
 84.70 1163.69 201.11 1364.82 540.66 100.56 641.11
 85.16 1170.60 201.11 1371.73 543.77 100.56 644.22
 85.62 1177.51 201.11 1378.64 546.88 100.56 647.33
 86.08 1184.42 201.11 1385.55 550.00 100.56 650.44
 86.54 1191.33 201.11 1392.46 553.11 100.56 653.55
 87.00 1198.24 201.11 1399.37 556.22 100.56 656.66
 87.46 1205.15 201.11 1406.28 559.33 100.56 659.77
 87.92 1212.06 201.11 1413.19 562.44 100.56 662.88
 88.38 1218.97 201.11 1420.10 565.55 100.56 665.99
 88.84 1225.88 201.11 1427.01 568.66 100.56 669.10
 89.30 1232.79 201.11 1433.92 571.77 100.56 672.21
 89.76 1239.70 201.11 1440.83 574.88 100.56 675.32
 90.22 1246.61 201.11 1447.74 578.00 100.56 678.43
 90.68 1253.52 201.11 1454.65 581.11 100.56 681.54
 91.14 1260.43 201.11 1461.56 584.22 100.56 684.65
 91.60 1267.34 201.11 1468.47 587.33 100.56 687.76
 92.06 1274.25 201.11 1475.38 590.44 100.56 690.87
 92.52 1281.16 201.11 1482.29 593.55 100.56 693.98
 92.98 1288.07 201.11 1489.20 596.66 100.56 697.09
 93.44 1294.98 201.11 1496.11 599.77 100.56 700.20
 93.90 1301.89 201.11 1503.02 602.88 100.56 703.31
 94.36 1308.80 201.11 1509.93 606.00 100.56 706.42
 94.82 1315.71 201.11 1516.84 609.11 100.56 709.53
 95.28 1322.62 201.11 1523.75 612.22 100.56 712.64
 95.74 1329.53 201.11 1530.66 615.33 100.56 715.75
 96.20 1336.44 201.11 1537.57 618.44 100.56 718.86
 96.66 1343.35 201.11 1544.48 621.55 100.56 721.97
 97.12 1350.26 201.11 1551.39 624.66 100.56 725.08
 97.58 1357.17 201.11 1558.30 627.77 100.56 728.19
 98.04 1364.08 201.11 1565.21 630.88 100.56 731.30
 98.50 1370.99 201.11 1572.12 634.00 100.56 734.41
 98.96 1377.90 201.11 1579.03 637.11 100.56 737.52
 99.42 1384.81 201.11 1585.94 640.22 100.56 740.63
 99.88 1391.72 201.11 1592.85 643.33 100.56 743.74
 100.34 1398.63 201.11 1600.00 646.44 100.56 746.85
 100.80 1405.54 201.11 1607.11 649.55 100.56 749.96
 101.26 1412.45 201.11 1614.22 652.66 100.56 753.07
 101.72 1419.36 201.11 1621.33 655.77 100.56 756.18
 102.18 1426.27 201.11 1628.44 658.88 100.56 759.29
 102.64 1433.18 201.11 1635.55 662.00 100.56 762.40
 103.10 1440.09 201.11 1642.66 665.11 100.56 765.51
 103.56 1447.00 201.11 1649.77 668.22 100.56 768.62
 104.02 1453.91 201.11 1656.88 671.33 100.56 771.73
 104.48 1460.82 201.11 1663.99 674.44 100.56 774.84
 104.94 1467.73 201.11 1671.10 677.55 100.56 777.95
 105.40 1474.64 201.11 1678.21 680.66 100.56 781.06
 105.86 1481.55 201.11 1685.32 683.77 100.56 784.17
 106.32 1488.46 201.11 1692.43 686.88 100.56 787.28
 106.78 1495.37 201.11 1700.00 690.00 100.56 790.39
 107.24 1502.28 201.11 1707.11 693.11 100.56 793.50
 107.70 1509.19 201.11 1714.22 696.22 100.56 796.61
 108.16 1516.10 201.11 1721.33 699.33 100.56 799.72
 108.62 1523.01 201.11 1728.44 702.44 100.56 802.83
 109.08 1529.92 201.11 1735.55 705.55 100.56 805.94
 109.54 1536.83 201.11 1742.66 708.66 100.56 809.05
 110.00 1543.74 201.11 1749.77 711.77 100.56 812.16
 110.46 1550.65 201.11 1756.88 714.88 100.56 815.27
 110.92 1557.56 201.11 1763.99 718.00 100.56 818.38
 111.38 1564.47 201.11 1771.10 721.11 100.56 821.49
 111.84 1571.38 201.11 1778.21 724.22 100.56 824.60
 112.30 1578.29 201.11 1785.32 727.33 100.56 827.71
 112.76 1585.20 201.11 1792.43 730.44 100.56 830.82
 113.22 1592.11 201.11 1799.54 733.55 100.56 833.93
 113.68 1599.02 201.11 1806.65 736.66 100.56 837.04
 114.14 1605.93 201.11 1813.76 739.77 100.56 840.15
 114.60 1612.84 201.11 1820.87 742.88 100.56 843.26
 115.06 1619.75 201.11 1827.98 746.00 100.56 846.37
 115.52 1626.66 201.11 1835.09 749.11 100.56 849.48
 115.98 1633.57 201.11 1842.20 752.22 100.56 852.59
 116.44 1640.48 201.11 1849.31 755.33 100.56 855.70
 116.90 1647.39 201.11 1856.42 758.44 100.56 858.81
 117.36 1654.30 201.11 1863.53 761.55 100.56 861.92
 117.82 1661.21 201.11 1870.64 764.66 100.56 865.03
 118.28 1668.12 201.11 1877.75 767.77 100.56 868.14
 118.74 1675.03 201.11 1884.86 770.88 100.56 871.25
 119.20 1681.94 201.11 1891.97 774.00 100.56 874.36
 119.66 1688.85 201.11 1899.08 777.11 100.56 877.47
 120.12 1695.76 201.11 1906.19 780.22 100.56 880.58
 120.58 1702.67 201.11 1913.30 783.33 100.56 883.69
 121.04 1709.58 201.11 1920.41 786.44 100.56 886.80
 121.50 1716.49 201.11 1927.52 789.55 100.56 889.91
 121.96 1723.40 201.11 1934.63 792.66 100.56 893.02
 122.42 1730.31 201.11 1941.74 795.77 100.56 896.13
 122.88 1737.22 201.11 1948.85 798.88 100.56 899.24
 123.34 1744.13 201.11 1955.96 802.00 100.56 902.35
 123.80 1751.04 201.11 1963.07 805.11 100.56 905.46
 124.26 1757.95 201.11 1970.18 808.22 100.56 908.57
 124.72 1764.86 201.11 1977.29 811.33 100.56 911.68
 125.18 1771.77 201.11 1984.40 814.44 100.56 914.79
 125.64 1778.68 201.11 1991.51 817.55 100.56 917.90
 126.10 1785.59 201.11 1998.62 820.66 100.56 921.01
 126.56 1792.50 20

PIER 3 LATERAL CAPACITY

Pier 32aff.lp7o

Pier 32aff.lp7o

LPILE Plus for Windows, Version 2013-07.007

Analysis of Individual Piles and Drilled Shafts
Subjected to Lateral Loading Using the P-y Method

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Description: Pier 3 Lateral Capacity

Program Options and Settings

Engineering Units of Input Data and Computations:
- Engineering units are US Customary Units (pounds, feet, inches)

Analysis Control Options:
- Maximum number of iterations allowed = 600
- Deflection tolerance for convergence = 1.0000E-05 in
- Maximum allowable deflection = 100.0000 in
- Number of pile increments = 100

Loading Type and Number of Cycles of Loading:
- Static loading specified

Computational Options:
- Use unfactored loads in computations (conventional analysis)
- Compute pile response under loading and nonlinear bending properties of pile (only if nonlinear pile properties are input)
- Use of p-y modification factors for p-y curves not selected
- Loading by lateral soil movements acting on pile not selected
- Input of shear resistance at the pile tip not selected
- Computation of pile-head foundation stiffness matrix not selected
- Push-over analysis of pile not selected
- Compute buckling analysis of pile for specified loading

Output Options:
- No p-y curves to be computed and reported for user-specified depths
- Values of pile-head deflection, bending moment, shear force, and soil reaction are printed for full length of pile.
- Printing Increment (nodal spacing of output points) = 1

Pile Structural Properties and Geometry

Total number of pile sections = 2
Total length of pile = 107.83 ft
Depth of ground surface below top of pile = 30.83 ft

Pile diameter values used for p-y curve computations are defined using 4 points.
p-y curves are computed using pile diameter values interpolated with depth over the length of the pile.

Point	Depth ft	Pile Diameter in
1	0.00000	48.000000
2	9.830000	48.000000
3	9.830000	49.5000000

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Files used for Analysis

Path to file locations: Y:\Bridges\DELDOT\BRI-159_JAMES ST BRIDGE\FOUNDATION
REPORT\LPILE Output: Pier 32aff.lp7d
Name of input data file: pier 32aff.lp7o
Name of output report file: pier 32aff.lp7o
Name of plot output file: pier 32aff.lp7p
Name of runtime message file: pier 32aff.lp7r

Date and Time of Analysis

Date: October 24, 2014 Time: 15:04:42

Problem Title

Project Name: BRI-159 Pier 3

Job Number:

Client: DeLDOT

Engineer: SJM

4 107.830000 Pier 32aff.1p7o 49.5000000

Input Structural Properties:

Pier 32aff.1p7o
 = 100.83000 ft
 = 62.60000 pcf
 = 62.60000 pcf
 = 2000.00000 psf
 = 2000.00000 psf
 = 0.00700
 = 0.00700
 = 200.00000 pci
 = 200.00000 pci

Pile Section No. 1:
 Section Type = Drilled Shaft (Bored Pile)
 Section Length = 9.83000 ft
 Section Diameter = 48.00000 in

Pile Section No. 2:
 Section Type = Drilled Shaft with
 Permanent Casing
 Section Length = 98.00000 ft
 Section Diameter = 49.50000 in

Control Data for Pile Buckling Analysis

Pile-head fixity condition for pile buckling analysis = shear and moment
 Number of axial loads for buckling analysis = 50
 Pile-head shear force for buckling analysis = 14000. lbs
 Pile-head moment for buckling analysis = 9502800. in-lb
 Maximum compression load for buckling analysis = 698600. lbs

Ground Slope and Pile Batter Angles

Ground Slope Angle = 0.000 degrees
 = 0.000 radians

Pile Batter Angle = 0.000 degrees
 = 0.000 radians

Soil and Rock Layering Information

The soil profile is modelled using 3 layers
 Layer 1 is sand, p-y criteria by Reese et al., 1974

Distance from top of pile to top of layer = 30.83000 ft
 Distance from top of pile to bottom of layer = 55.83000 ft
 Effective unit weight at top of layer = 57.60000 pcf
 Effective unit weight at bottom of layer = 57.60000 pcf
 Friction angle at top of layer = 32.00000 deg.
 Friction angle at bottom of layer = 32.00000 deg.
 Subgrade k at top of layer = 60.00000 pci
 Subgrade k at bottom of layer = 60.00000 pci

Layer 2 is stiff clay with water-induced erosion
 Distance from top of pile to top of layer = 55.83000 ft
 Page 3

Pier 32aff.1p7o
 = 100.83000 ft
 = 62.60000 pcf
 = 62.60000 pcf
 = 2000.00000 psf
 = 2000.00000 psf
 = 0.00700
 = 0.00700
 = 200.00000 pci
 = 200.00000 pci

Layer 3 is sand, p-y criteria by Reese et al., 1974

Distance from top of pile to top of layer = 100.83000 ft
 Distance from top of pile to bottom of layer = 115.83000 ft
 Effective unit weight at top of layer = 72.60000 pcf
 Effective unit weight at bottom of layer = 72.60000 pcf
 Friction angle at top of layer = 36.00000 deg.
 Friction angle at bottom of layer = 36.00000 deg.
 Subgrade k at top of layer = 125.00000 pci
 Subgrade k at bottom of layer = 125.00000 pci

(Depth of lowest soil layer extends 8.00 ft below pile tip)

Summary of Soil Properties

Layer Num.	Soil Type	Strain Factor (p-y curve Criteria)	Layer Depth ft	Effective Unit wt. pcf	Undrained Cohesion psf
1	Sand (Reese, et al.)	60.000	30.830	57.600	--
2	Stiff Clay with Free water	200.000	55.830	57.600	--
3	Sand (Reese, et al.)	125.000	100.830	62.600	2000.000
			100.830	62.600	2000.000
			100.830	72.600	--
			115.830	72.600	--

Loading Type
 Static loading criteria were used when computing p-y curves for all analyses.
 Page 4

Pile-head Loading and Pile-head Fixity Conditions

Number of loads specified = 10

Load No.	Load Type	Condition	Condition	Axial Thrust Force, lbs
1	4	Y = 0.50000 in	M = 7818000. in-lbs	0.0000000
2	4	Y = 1.00000 in	M = 7818000. in-lbs	0.0000000
3	4	Y = 1.50000 in	M = 7818000. in-lbs	0.0000000
4	4	Y = 2.00000 in	M = 7818000. in-lbs	0.0000000
5	4	Y = 0.50000 in	M = 4380000. in-lbs	0.0000000
6	4	Y = 1.00000 in	M = 4380000. in-lbs	0.0000000
7	4	Y = 1.50000 in	M = 4380000. in-lbs	0.0000000
8	4	Y = 2.00000 in	M = 4380000. in-lbs	0.0000000
9	1	V = 21300. lbs	M = 7818000. in-lbs	0.0000000
10	1	V = 11000. lbs	M = 4380000. in-lbs	0.0000000

V = perpendicular shear force applied to pile head
M = bending moment applied to pile head
Y = lateral deflection relative to pile axis
S = pile slope relative to original pile batter angle
R = rotational stiffness applied to pile head
Axial thrust is assumed to be acting axially for all pile batter angles.

Computations of Nominal Moment Capacity and Nonlinear Bending Stiffness

Axial thrust force values were determined from pile-head loading conditions

Number of Pile Sections Analyzed = 2

Pile Section No. 1:

Dimensions and Properties of Drilled Shaft (Bored Pile):

Length of Section	=	9.83000 ft
Shaft Diameter	=	48.00000 in
Concrete Cover Thickness	=	4.00000 in
Number of Reinforcing Bars	=	50 bars
Yield Stress of Reinforcing Bars	=	60000. psi
Modulus of Elasticity of Reinforcing Bars	=	29000000. psi
Gross Area of Shaft	=	1809.3737 sq. in.
Total Area of Reinforcing Steel	=	39.50000 sq. in.
Area Ratio of Steel Reinforcement	=	2.18 percent

Edge-to-Edge Bar Spacing = 2.89438 in
Maximum Concrete Aggregate Size = 0.50000 in
Ratio of Bar Spacing to Aggregate Size = 5.79
Offset of Center of Rebar Cage from Center of Pile = 0.0000 in
Axial Structural Capacities:

Nom. Axial Structural Capacity = 0.85 Fc Ac + Fy As = 9140.470 kips
Tensile Load for Cracking of Concrete = -911.303 kips
Nominal Axial Tensile Capacity = -2370.000 kips

Reinforcing Bar Dimensions and Positions Used in Computations:

Bar Number	Bar Diam. inches	Bar Area sq. in.	X inches	Y inches
1	1.00000	0.79000	19.49359	-0.49995
2	1.00000	0.79000	19.49359	0.49995
3	1.00000	0.79000	19.00549	4.36362
4	1.00000	0.79000	18.75683	5.32110
5	1.00000	0.79000	17.32321	8.95300
6	1.00000	0.79000	16.84111	9.82921
7	1.00000	0.79000	14.52445	12.97984
8	1.00000	0.79000	13.86798	13.70873
9	1.00000	0.79000	10.86731	16.19110
10	1.00000	0.79000	10.02307	16.72687
11	1.00000	0.79000	6.49933	18.38501
12	1.00000	0.79000	5.54837	18.69400
13	1.00000	0.79000	1.72297	19.42373
14	1.00000	0.79000	0.72505	19.48652
15	1.00000	0.79000	-3.16164	19.24199
16	1.00000	0.79000	-4.14382	19.05462
17	1.00000	0.79000	-7.84760	17.85119
18	1.00000	0.79000	-8.75233	17.42546
19	1.00000	0.79000	-12.04047	15.33875
20	1.00000	0.79000	-12.81090	14.70139
21	1.00000	0.79000	-15.47679	11.86251
22	1.00000	0.79000	-16.06451	11.05358
23	1.00000	0.79000	-17.94064	7.64091
24	1.00000	0.79000	-18.30872	6.71123
25	1.00000	0.79000	-19.27722	2.93920
26	1.00000	0.79000	-19.40254	1.94719
27	1.00000	0.79000	-19.40254	-1.94719
28	1.00000	0.79000	-19.27722	-2.93920
29	1.00000	0.79000	-18.30872	-6.71123
30	1.00000	0.79000	-17.94064	-7.64091
31	1.00000	0.79000	-16.06451	-11.05358
32	1.00000	0.79000	-15.47679	-11.86251
33	1.00000	0.79000	-12.81090	-14.70139
34	1.00000	0.79000	-12.04047	-15.33875
35	1.00000	0.79000	-8.75233	-17.42546
36	1.00000	0.79000	-7.84760	-17.85119
37	1.00000	0.79000	-4.14382	-19.05462
38	1.00000	0.79000	-3.16164	-19.24199
39	1.00000	0.79000	0.72505	-19.48652
40	1.00000	0.79000	1.72297	-19.42373
41	1.00000	0.79000	5.54837	-18.69400
42	1.00000	0.79000	6.49933	-18.38501
43	1.00000	0.79000	10.02307	-16.72687
44	1.00000	0.79000	10.86731	-16.19110
45	1.00000	0.79000	13.86798	-13.70873

46 1.00000 14.55245 -12.97984
 47 1.00000 16.84151 -9.82921
 48 1.00000 17.32321 -8.95300
 49 1.00000 18.75683 -5.33210
 50 1.00000 19.00549 -4.36362

Pier 32aff.1p7o
 1350625155. 24.0001524
 1347728017. 24.0001529
 1344830878. 24.0001534
 1341933739. 24.0001540
 1339036601. 24.0001545
 1336139462. 24.0001551
 1169122029. 14.1767436
 1039219581. 14.1814610
 935297623. 14.1861892
 850270567. 14.1909283
 779414686. 14.1956783
 719459710. 14.2004394
 668069731. 14.2052115
 623531749. 14.2099947
 584561015. 14.2147891
 550175073. 14.2195946
 519609791. 14.2244115
 492261907. 14.2292396
 467648812. 14.2340792
 445379821. 14.2389301
 425135283. 14.2437926
 419046578. 14.2486666
 418901006. 14.2535522
 418755135. 14.2584494
 418608964. 14.2633583
 418462492. 14.2682790
 418315718. 14.2732116
 418168640. 14.2781560
 418021256. 14.2831123
 417873566. 14.2880807
 417725568. 14.2930611
 41755294. 14.2980536
 8612.5309914

0.000001250 1688.2814444
 0.1326129 0.8613055
 0.000001875 2526.9900314
 0.1981756 1.2919583
 0.000002500 3362.0771951
 0.2632425 1.7226111
 0.000003125 4193.5429353
 0.3278135 2.1532639
 0.000003750 5021.3872521
 0.3918887 2.5839168
 0.000004375 5845.6101456
 0.4554681 3.0145696
 0.000005000 5845.6101456
 0.5290933 -8.5145276
 0.3080092 -4.8695722
 0.000005625 5845.6101456
 0.3458573 -5.4774992
 0.000006250 5845.6101456
 0.3835595 -6.0852532
 0.000006875 5845.6101456
 0.4211155 -6.6928337
 0.000007500 5845.6101456
 0.4585249 -7.3002399
 0.000008125 5845.6101456
 0.4957876 -7.9074713
 0.000008750 5845.6101456
 0.5329033 -8.5145276
 0.000009375 5845.6101456
 0.5698716 -9.1214077
 0.000010000 5845.6101456
 0.6066924 -9.7281112
 0.0000106 5845.6101456
 0.6433653 -10.3346374
 0.0000113 5845.6101456
 0.6798902 -10.9409857
 0.0000119 5845.6101456
 0.7162666 -11.5471536
 0.0000125 5845.6101456
 0.7524943 -12.1531463
 0.0000131 5845.6101456
 0.7885732 -12.7589572
 0.0000138 5845.6101456
 0.8245028 -13.3643877
 0.0000144 6023.7945632
 0.8602829 13.9700371
 0.0000150 6283.5150883
 0.8959132 14.5753048
 0.0000156 6543.0489845
 0.9313334 15.1803201
 0.0000163 6802.2856202
 0.9662169 15.7854546
 1.0019016 16.3900109
 1.0000175 17.0000000
 1.0369310 17.6094451
 1.0714081 17.9045976
 1.0000188 7837.8985655
 1.1085338 -18.2030577
 1.0000194 8096.3003444
 1.1411076 -18.8070346
 1.0000200 8354.5113583
 1.1755294 -19.4108248
 0.0000206 8612.5309914

NOTE: The positions of the above rebars were computed by LPILE
 Minimum spacing between any two bars not equal to zero = -0.0001096 inches between
 Bars 1 and 2
 Spacing to aggregate size ratio = -0.0002191

Concrete Properties:

 Compressive Strength of Concrete = 4500.00000 psi
 Modulus of Elasticity of Concrete = 3823676. psi
 Modulus of Rupture of Concrete = -503.11528 psi
 Compression Strain at Peak Stress = 0.00200
 Tensile Strain at Fracture of Concrete = -0.0001152
 Maximum Coarse Aggregate Size = 0.50000 in

Number of Axial Thrust Force Values Determined from Pile-head Loadings = 1
 Number Axial Thrust Force
 kips

 1 0.000

Definitions of Run Messages and Notes:

 C = concrete in section has cracked in tension.
 Y = stress in reinforcing steel has reached yield stress.
 T = ACI 318-08 criteria for tension-controlled section met, tensile strain in
 reinforcement exceeds 0.005 while simultaneously compressive strain in
 concrete more than 0.003. See ACI 318-08, Section 10.3.4.
 Z = depth of tensile zone in concrete section is less than 10 percent of section
 depth.

Bending Stiffness (EI) = Computed Bending Moment / Curvature.
 Position of neutral axis is measured from edge of compression side of pile.
 Compressive stresses and strains are positive in sign.
 Tensile stresses and strains are negative in sign.

Axial Thrust Force = 0.000 kips		Depth to		Max Tens	
Bending	Bending	Run	Bending	Max Comp	Max Tens
Concrete	Steel	Msg	Stiffness	Strain	Strain
Curvature	Moment		N Axis		
Stress	in-kip		in	in/in	in/in
rad/in.	ksi				
-----	-----	-----	-----	-----	-----
0.00000625	845.9514339	1335352294.	24.0001518	0.0000150	-0.0000150
0.0665544	0.4306528				

	Pier 32aff. 1p70		Pier 32aff. 1p70		Pier 32aff. 1p70							
1.2097988	-20.0144267	C	417428642.	14.3030584	0.0003039	-0.0007161	0.0000569	23227.	408391538.	14.6106719	0.0008310	-0.0018990
0.0000213	8870.3586334	C	417279711.	14.3080753	0.0003130	-0.0007370	2.9257055	-54.6756728	408052124.	14.6223538	0.0008499	-0.0019401
1.2439155	-20.6178403	C	417130466.	14.3131046	0.0003220	-0.0007580	0.0000581	23718.	407711031.	14.6341029	0.0008689	-0.0019811
0.0000219	9127.9936698	C	416980906.	14.3181462	0.0003311	-0.0007789	2.9749169	-55.8576448	407368552.	14.6457265	0.0008879	-0.0020221
1.2778793	-21.2210647	C	416831029.	14.3232002	0.0003402	-0.0007998	0.0000594	24208.	407024713.	14.6572221	0.0009069	-0.0020631
0.0000225	9385.4354826	C	416680834.	14.3282668	0.0003493	-0.0008207	3.0234323	-57.0386538	406679201.	14.6687831	0.0009260	-0.0021040
1.3116898	-21.8240993	C	4166379475.	14.3384375	0.0003674	-0.0008626	3.0712187	-58.2190319	406331998.	14.6804101	0.0009451	-0.0021449
0.0000231	9642.6834300	C	416076834.	14.3486590	0.0003856	-0.0009044	0.0000619	25185.	4059833085.	14.6921039	0.0009642	-0.0021858
1.3453467	-22.4269432	C	415772890.	14.3589318	0.0004038	-0.0009462	3.1182718	-59.3987969	405632443.	14.7038654	0.0009833	-0.0022267
1.3788497	-23.0295958	C	415467630.	14.3692563	0.0004221	-0.0009879	0.0000631	25672.	405280053.	14.7156953	0.010025	-0.0022675
0.0000244	-23.6320564	C	4154543834.	14.4005458	0.0004770	-0.0011130	3.1646176	-60.0000000	404925896.	14.7275946	0.010217	-0.0023083
1.4121986	-23.6320564	C	4154161043.	14.4110828	0.0004954	-0.0011546	3.2102527	-60.0000000	404569952.	14.7395639	0.010410	-0.0023490
0.0000256	10670.	C	4148531116.	14.4216743	0.0005138	-0.0011962	0.0000644	26158.	404091673.	14.7500835	0.010602	-0.0023898
1.4784325	-24.8363989	C	4145437818.	14.4537818	0.0005691	-0.0013209	3.2551736	-60.0000000	403072266.	14.7537205	0.010789	-0.0024311
0.0000269	11182.	C	4143921159.	14.4645973	0.0005876	-0.0013624	3.2993766	-60.0000000	401455043.	14.7495436	0.010970	-0.0024730
1.5440460	-26.0399641	C	413921159.	14.4754703	0.0006062	-0.0014038	3.3428584	-60.0000000	392246336.	14.6948027	0.011664	-0.0026436
1.6090366	-27.2427466	C	413607737.	14.4864015	0.0006247	-0.0014453	3.3856151	-60.0000000	381149774.	14.6090319	0.012326	-0.0028174
1.6734018	-28.4447402	C	413292908.	14.5084408	0.0006619	-0.0015281	3.4276432	-60.0000000	369362560.	14.5055975	0.012964	-0.0029936
1.7311390	-29.6459388	C	412976658.	14.5373579	0.0006806	-0.0015694	3.4687035	-60.0000000	357505362.	14.3951856	0.013585	-0.0031715
1.8002456	-30.8463362	C	412658972.	14.5532459	0.0007368	-0.0016932	3.5079550	-60.0000000	345931693.	14.2834974	0.014194	-0.0033506
1.8627191	-32.0459262	C	412339835.	14.5646025	0.0007555	-0.0017345	3.5452601	-60.0000000	334703122.	14.1715893	0.014792	-0.0035308
1.9245567	-33.2447024	C	412019235.	14.595502	0.0007744	-0.0017756	3.5813494	-60.0000000	323940666.	14.0579740	0.015376	-0.0037124
1.9857559	-34.4426584	C	411697154.	14.624203	0.0008062	-0.0018168	3.6216000	-60.0000000	313627073.	13.9461294	0.015951	-0.0038949
2.0463138	-35.6397875	C	411373579.	14.6597205	0.0008693	-0.0019107	3.6613803	-60.0000000	303860741.	13.8392296	0.016521	-0.0040779
2.1062279	-36.8360832	C	411048519.	14.707205	0.0009322	-0.0020050	3.7013803	-60.0000000	294530941.	13.7351344	0.017083	-0.0042617
2.1654952	-38.0315387	C	410721909.	14.7519521	0.0009780	-0.00206520	3.7413803	-60.0000000	285688006.	13.6338565	0.017639	-0.0044461
2.2241131	-39.2261471	C	410393756.	14.8119521	0.0010167	-0.0021375	3.7813803	-60.0000000	277303670.	13.5348499	0.018187	-0.0046313
2.2820786	-40.4199016	C	410064046.	14.8646025	0.0010692	-0.0022043	3.8213803	-60.0000000	269310170.	13.4391679	0.018731	-0.0048169
2.3393890	-41.6127951	C	409732761.	14.9195502	0.0011309	-0.0022761	3.8613803	-60.0000000	261702218.	13.3473027	0.019270	-0.0050030
2.3960413	-42.8048205	C	409399885.	14.973914	0.0011962	-0.0023485	3.9013803	-60.0000000	254539263.	13.2620016	0.019810	-0.0051890
2.4520326	-44.000444	C	409065400.	15.0284408	0.0012635	-0.0024213	3.9413803	-60.0000000	247698346.	13.1787297	0.020345	-0.0053755
2.5073600	-45.1862362	C	408732761.	15.084408	0.0013309	-0.0024941	3.9813803	-60.0000000	241162765.	13.0959086	0.020872	-0.0055628
2.5620203	-46.3756131	C	408400406.	15.1395502	0.0013972	-0.0025669	4.0213803	-60.0000000				
2.6160105	-47.5640922	C	408064046.	15.195502	0.0014646	-0.0026400	4.0613803	-60.0000000				
2.6695276	-48.7516657	C	407732761.	15.252459	0.0015320	-0.0027132	4.1013803	-60.0000000				
2.7219685	-49.9383259	C	407400406.	15.3097205	0.0016007	-0.0027864	4.1413803	-60.0000000				
2.7735299	-51.1240649	C	407064046.	15.367205	0.0016692	-0.0028596	4.1813803	-60.0000000				
2.8252088	-52.3088745	C	406732761.	15.4246025	0.0017377	-0.0029328	4.2213803	-60.0000000				
2.8758017	-53.4927466	C	406400406.	15.4819521	0.0018062	-0.0030060	4.2613803	-60.0000000				

Note note that the values of moment capacity in the table above are not factored by a strength reduction factor (phi-factor).

In ACI 318-08, the value of the strength reduction factor depends on whether the transverse reinforcing steel bars are tied hoops (0.65) or spirals (0.70). The above values should be multiplied by the appropriate strength reduction factor to compute ultimate moment capacity according to ACI 318-08, section 9.3.2.2 or the value required by the design standard being followed.

The following table presents factored moment capacities and corresponding bending stiffnesses computed for common resistance factor values used for reinforced concrete sections.

Load No.	Axial Thrust in-kip	Nominal Moment Capacity at Ult. Mom. Cap. for Moment kip-in ²	Resistance Factor	Nominal Moment Capacity at Ult. Mom. Cap. for Moment kip-in ²	Ultimate (Factored) Axial Thrust kips	Ultimate Moment
1	0.65	406260579.288	0.65	40395.232	0.000	
1	0.70	404789053.314	0.70	40395.232	0.000	
1	0.75	398293409.577	0.75	40395.232	0.000	

Pile Section No. 2:

Dimensions and Properties of Drilled Shaft (Bored Pile) with Permanent Casing:

Length of Section	=	98.00000 ft
Outer Diameter of Casing	=	49.50000 in
Concrete Cover Thickness	=	4.50000 in
Casing Wall Thickness	=	0.75000 in
Moment of Inertia of Steel Casing	=	34131. in ⁴
Yield Stress of Casing	=	36000. psi
Elastic Modulus of Casing	=	29000000. psi
Number of Reinforcing Bars	=	50 bars
Area of Single Reinforcing Bar	=	0.79000 sq. in.
Edge-to-Edge Bar Spacing	=	2.76901 in
Maximum Concrete Aggregate Size	=	0.50000 in
Ratio of Bar Spacing to Aggregate Size	=	5.54
Offset of Center of Rebar Cage from Center of Pile	=	60000. in
Yield Stress of Reinforcing Bars	=	29000000. psi
Modulus of Elasticity of Reinforcing Bars	=	1924.42185 sq. in.
Gross Area of Pile	=	1770.05737 sq. in.
Area of Concrete	=	114.86448 sq. in.
Cross-sectional Area of Steel Casing	=	154.36448 sq. in.
Area of All Steel (Casing and Bars)	=	8.02 percent
Area Ratio of All Steel to Gross Area of Pile	=	

Axial Structural Capacities:

Load No.	Axial Thrust kips	Nominal Mom. Cap. in-kip	Moment Capacity for Section 1	Max. Comp. Strain
4.4991008	-60.0000000	CY	234919408.	13.0163967
0.0001644	60.0000000	CY	228965876.	12.9406891
4.4961694	60.0000000	CY	223333425.	12.8709600
4.4983350	60.0000000	CY	217937643.	12.8035616
0.0001744	60.0000000	CY	212773812.	12.7393054
4.4972710	60.0000000	CY	207826445.	12.6749886
4.4999672	60.0000000	CY	198527530.	12.5155567
0.0001894	60.0000000	CY	194183848.	12.4946057
4.4990003	60.0000000	CY	190038278.	12.4414757
4.4956386	60.0000000	CY	186045078.	12.3892958
4.4983210	60.0000000	CY	182216468.	12.3398762
4.4949946	60.0000000	CY	178526610.	12.2917083
4.4972998	60.0000000	CY	174983396.	12.2454771
4.4997925	60.0000000	CY	171561779.	12.1978486
4.4921838	60.0000000	CY	168266185.	12.1516759
4.4971340	60.0000000	CY	165084525.	12.1063441
4.4996503	60.0000000	CY	162028002.	12.0632455
4.4945873	60.0000000	CY	159086090.	12.0224625
4.4947195	60.0000000	CY	156254980.	11.9837750
4.4982677	60.0000000	CY	153511868.	11.9459332
0.0002494	60.0000000	CY	150860647.	11.9101831
4.4998905	60.0000000	CY	148301338.	11.8759269
4.4926204	60.0000000	CY	134448054.	11.6976495
4.4936508	60.0000000	CY	122436952.	11.6093256
0.0002644	60.0000000	CY		
4.4974059	60.0000000	CY		
0.0002694	60.0000000	CY		
4.4995166	60.0000000	CY		
0.0002744	60.0000000	CY		
4.4975184	60.0000000	CY		
0.0003044	60.0000000	CY		
4.4903477	60.0000000	CY		
0.0003344	60.0000000	CY		
4.4867102	60.0000000	CY		

Summary of Results for Nominal (Unfactored) Moment Capacity for Section 1

Moment values interpolated at maximum compressive strain = 0.003 or maximum developed moment if pile fails at smaller strains.

Load No.	Axial Thrust kips	Nominal Mom. Cap. in-kip	Max. Comp. Strain
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Nom. Axial Structural Capacity = 0.85 Fc Ac + FY AS = 13275.591 Kips
 Tensile Load for Cracking of Concrete = -1294.896 Kips
 Nominal Axial Tensile Capacity = -6505.121 Kips

Reinforcing Bar Dimensions and Positions Used in Computations:

Bar Number	Bar Diam. inches	Bar Area sq. in.	X inches	Y inches
1	1.00000	0.79000	18.99342	-0.49994
2	1.00000	0.79000	18.99342	0.49994
3	1.00000	0.79000	18.52104	4.23924
4	1.00000	0.79000	18.27238	5.20771
5	1.00000	0.79000	16.88491	8.71205
6	1.00000	0.79000	16.40321	9.58825
7	1.00000	0.79000	14.18784	12.63745
8	1.00000	0.79000	13.36633	13.36633
9	1.00000	0.79000	10.59930	15.76879
10	1.00000	0.79000	16.30456	16.30456
11	1.00000	0.79000	17.90933	17.90933
12	1.00000	0.79000	18.21831	18.21831
13	1.00000	0.79000	18.92455	18.92455
14	1.00000	0.79000	18.98733	18.98733
15	1.00000	0.79000	-3.06793	18.75068
16	1.00000	0.79000	-4.05010	18.56332
17	1.00000	0.79000	-7.63464	17.39863
18	1.00000	0.79000	-8.53937	16.97290
19	1.00000	0.79000	-11.72165	14.95336
20	1.00000	0.79000	-12.49207	14.31601
21	1.00000	0.79000	-15.07214	11.56851
22	1.00000	0.79000	-15.65986	10.75959
23	1.00000	0.79000	-17.47560	7.45678
24	1.00000	0.79000	-17.84368	6.52711
25	1.00000	0.79000	-18.78099	2.87651
26	1.00000	0.79000	-18.90631	1.88451
27	1.00000	0.79000	-18.90631	-1.88451
28	1.00000	0.79000	-18.78099	-2.87651
29	1.00000	0.79000	-17.84368	-6.52711
30	1.00000	0.79000	-17.47560	-7.45678
31	1.00000	0.79000	-15.65986	-10.75959
32	1.00000	0.79000	-15.07214	-11.56851
33	1.00000	0.79000	-12.49207	-14.31601
34	1.00000	0.79000	-11.72165	-14.95336
35	1.00000	0.79000	-8.53937	-16.97290
36	1.00000	0.79000	-7.63464	-17.39863
37	1.00000	0.79000	-4.05010	-18.56332
38	1.00000	0.79000	-3.06793	-18.75068
39	1.00000	0.79000	0.69365	-18.98733
40	1.00000	0.79000	1.69156	-18.92455
41	1.00000	0.79000	5.39382	-18.21831
42	1.00000	0.79000	6.34476	-17.90933
43	1.00000	0.79000	9.75507	-16.30456
44	1.00000	0.79000	10.59930	-15.76879
45	1.00000	0.79000	13.36633	-13.36633
46	1.00000	0.79000	14.18784	-12.63745
47	1.00000	0.79000	16.40321	-9.58825
48	1.00000	0.79000	16.88491	-8.71205
49	1.00000	0.79000	18.27238	-5.20771
50	1.00000	0.79000	18.52104	-4.23924

NOTE: The positions of the above rebars were computed by LPILE
 Minimum spacing between any two bars not equal to zero = -0.0001154 inches between Bars 1 and 2

Spacing to aggregate size ratio = -0.0002308

Concrete Properties:

Compressive Strength of Concrete	=	4500.00000 psi
Modulus of Elasticity of Concrete	=	3823676. psi
Modulus of Rupture of Concrete	=	-503.11528 psi
Compression Strain at Peak Stress	=	0.00200
Tensile Strain at Fracture of Concrete	=	-0.0001152
Maximum Coarse Aggregate Size	=	0.50000 in

Number of Axial Thrust Force Values Determined from Pile-head Loadings = 1

Number	Axial Thrust Force kips
1	0.000

Definitions of Run Messages and Notes:

C = concrete in section has cracked in tension.
 Y = stress in reinforcing steel has reached yield stress.
 T = ACI 318-08 criteria for tension-controlled section met, tensile strain in reinforcement exceeds 0.005 while simultaneously compressive strain in concrete more than 0.003. See ACI 318-08, Section 10.3.4.
 Z = depth of tensile zone in concrete section is less than 10 percent of section depth.

Bending stiffness (EI) = Computed Bending Moment / Curvature.
 Position of neutral axis is measured from edge of compression side of pile.
 Compressive stresses and strains are positive in sign.
 Tensile stresses and strains are negative in sign.

Axial Thrust Force = 0.000 kips

Bending Curvature rad/in. Ks1	Bending Max Steel Moment in-Kip Ks1	Bending Max Casting Stress Kip-in2 Ks1	Depth to Run N Axis in	Max Comp Strain in/in	Max Tens Strain in/in
0.00000025	1438.6794421	2333887107.	24.7501135	0.0000155	-0.0000155
0.0686251	0.4441099	0.4441099	24.7501139	0.0000309	-0.0000309
0.00001250	2913.7289969	2350963197.	24.7501139	0.0000309	-0.0000309
0.1367249	0.8682197	0.8682197	24.7501142	0.0000464	-0.0000464
0.00001875	4363.3789643	2328973288.	24.7501142	0.0000464	-0.0000464
0.2042984	1.3532296	232712378	24.7501145	0.0000619	-0.0000619
0.09022500	5817.7283944	232712378	24.7501148	0.0000773	-0.0000773
0.00003125	7237.0983372	2322271468.	24.7501148	0.0000773	-0.0000773

Pier 32aff.1p70			Pier 32aff.1p70		
0.3378574	2.2205494	0.0000231	35753.	154606622.	0.0004591
0.000003750	8697.2205494	0.0000928	-19.7159388	-19.7159388	0.00007040
0.4038469	2.6646594	0.0001083	36706.	19.8588825	-0.0007224
0.000004375	2316463648.	0.00011083	-20.2448541	19.8646264	-0.0005093
0.4693092	3.1087693	0.0000985	37659.	19.8761504	-0.0007958
0.000005000	2026905692.	0.0001490	-20.7735531	19.8872228	-0.0008325
0.4267214	-4.2862866	0.0001676	39562.	19.8934440	-0.0009058
0.00005625	1801693949.	0.0001108	-21.8303000	19.9345047	-0.0009424
0.4786965	-4.8211906	0.0001231	41463.	19.9463254	-0.0009790
0.00006250	162124554.	0.0001862	-22.8861734	19.9581971	-0.0010155
0.00006875	5.3558966	0.0001355	43361.	19.9701203	-0.0010520
0.5817317	155971372.	0.0001479	-23.9411681	19.9820952	-0.0010885
0.6327907	-5.8904042	0.0001602	47148.	19.9941226	-0.0011249
0.00008125	1559716860.	0.0001726	-26.0484983	20.0062027	-0.0011613
0.00008750	6.9588215	0.0001850	49038.	20.0183361	-0.0011977
0.00009375	-7.4927301	0.0002097	-27.1008222	20.0303233	-0.0012340
0.00010000	1557668055.	0.0002221	50924.	20.0368732	-0.0013082
0.7841278	8.0264378	0.0002346	-28.1522443	20.046438	-0.0013465
0.8339586	-8.5599440	0.0002470	52808.	20.055058	-0.0013852
0.8834811	16539.	0.0002594	-29.2027586	20.0640431	-0.0014244
0.9326948	-9.0932482	0.0002718	32.3487941	20.072888	-0.0014638
0.0000119	9.6263497	0.0002843	-32.3487941	20.0810491	-0.0015035
0.0000125	18473.	0.0002967	36.537934	20.089883	-0.0015435
1.0301939	-10.1592480	0.0003091	-37.6206368	20.099119	-0.0015836
1.0784783	10.6919423	0.0003216	38.7278053	20.009351	-0.0016240
1.1264520	-11.2244322	0.0003341	-39.8371501	20.009351	-0.0016638
1.1741144	11.7367169	0.0003465	40.9610890	20.010024	-0.0017035
1.2214650	-12.2887959	0.0003590	-42.0956668	20.015435	-0.0017431
1.2685034	12.8206684	0.0003715	44.3879083	20.020446	-0.0017828
1.3132290	-13.3523340	0.0003840	-45.5437360	20.025453	-0.0018225
1.3616413	13.5233340	0.0003965	46.7049440	20.030460	-0.0018620
1.4077397	15.4769133	0.0004090	-47.8711305	20.035467	-0.0019017
1.4532339	-16.0075248	0.0004215	49.0402307	20.040474	-0.0019414
1.4989932	16.0075248	0.0004340	-50.2100156	20.045481	-0.0019811
1.5464113	-14.4150415	0.0004465	51.4009240	20.050488	-0.0020208
1.5938857	14.9460822	0.0004590	-52.5915292	20.055495	-0.0020605
1.6414181	14.9460822	0.0004715	53.7816722	20.060502	-0.0021002
1.6890036	-15.4769133	0.0004840	-54.9737361	20.065509	-0.0021399
1.7365857	16.0075248	0.0004965	56.1678222	20.070516	-0.0021796
1.7841670	16.0075248	0.0005090	-57.3619872	20.075523	-0.0022193
1.8317483	-17.0682092	0.0005215	58.5570000	20.080530	-0.0022590
1.8793296	17.0682092	0.0005340	-59.7519872	20.085537	-0.0022987
1.9269109	17.0682092	0.0005465	60.9470000	20.090544	-0.0023384
1.9744922	-18.1276023	0.0005590	-62.1420000	20.095551	-0.0023781
2.0220735	18.1276023	0.0005715	63.3370000	20.100558	-0.0024178
2.0696548	18.1276023	0.0005840	-64.5320000	20.105565	-0.0024575
2.1172361	-19.1870023	0.0005965	65.7270000	20.110572	-0.0024972
2.1648174	19.1870023	0.0006090	-66.9220000	20.115579	-0.0025369
2.2123987	19.1870023	0.0006215	68.1170000	20.120586	-0.0025766
2.2600000	-18.1276023	0.0006340	-69.3120000	20.125593	-0.0026163
2.3076013	18.1276023	0.0006465	70.5070000	20.130600	-0.0026560
2.3551826	18.1276023	0.0006590	-71.7020000	20.135607	-0.0026957
2.4027639	18.1276023	0.0006715	72.8970000	20.140614	-0.0027354
2.4503452	-17.0682092	0.0006840	-74.0920000	20.145621	-0.0027751
2.4979265	17.0682092	0.0006965	75.2870000	20.150628	-0.0028148
2.5455078	17.0682092	0.0007090	-76.4820000	20.155635	-0.0028545
2.5930891	17.0682092	0.0007215	77.6770000	20.160642	-0.0028942
2.6406704	-16.574622	0.0007340	-78.8720000	20.165649	-0.0029339
2.6882517	16.574622	0.0007465	80.0670000	20.170656	-0.0029736
2.7358330	16.574622	0.0007590	-81.2620000	20.175663	-0.0030133
2.7834143	16.574622	0.0007715	82.4570000	20.180670	-0.0030530
2.8309956	-15.4769133	0.0007840	-83.6520000	20.185677	-0.0030927
2.8785769	15.4769133	0.0007965	84.8470000	20.190684	-0.0031324
2.9261582	15.4769133	0.0008090	-86.0420000	20.195691	-0.0031721
2.9737395	15.4769133	0.0008215	87.2370000	20.200698	-0.0032118
3.0213208	15.4769133	0.0008340	-88.4320000	20.205705	-0.0032515
3.0689021	15.4769133	0.0008465	89.6270000	20.210712	-0.0032912
3.1164834	15.4769133	0.0008590	-90.8220000	20.215719	-0.0033309
3.1640647	15.4769133	0.0008715	92.0170000	20.220726	-0.0033706
3.2116460	15.4769133	0.0008840	-93.2120000	20.225733	-0.0034103
3.2592273	15.4769133	0.0008965	94.4070000	20.230740	-0.0034500
3.3068086	15.4769133	0.0009090	-95.6020000	20.235747	-0.0034897
3.3543899	15.4769133	0.0009215	96.7970000	20.240754	-0.0035294
3.4019712	15.4769133	0.0009340	-97.9920000	20.245761	-0.0035691
3.4495525	15.4769133	0.0009465	99.1870000	20.250768	-0.0036088
3.4971338	15.4769133	0.0009590	-100.3820000	20.255775	-0.0036485
3.5447151	15.4769133	0.0009715	101.5770000	20.260782	-0.0036882
3.5922964	15.4769133	0.0009840	-102.7720000	20.265789	-0.0037279
3.6398777	15.4769133	0.0009965	103.9670000	20.270796	-0.0037676
3.6874590	15.4769133	0.0010090	-105.1620000	20.275803	-0.0038073
3.7350403	15.4769133	0.0010215	106.3570000	20.280810	-0.0038470
3.7826216	15.4769133	0.0010340	-107.5520000	20.285817	-0.0038867
3.8302029	15.4769133	0.0010465	108.7470000	20.290824	-0.0039264
3.8777842	15.4769133	0.0010590	-109.9420000	20.295831	-0.0039661
3.9253655	15.4769133	0.0010715	111.1370000	20.300838	-0.0040058
3.9729468	15.4769133	0.0010840	-112.3320000	20.305845	-0.0040455
4.0205281	15.4769133	0.0010965	113.5270000	20.310852	-0.0040852
4.0681094	15.4769133	0.0011090	-114.7220000	20.315859	-0.0041249
4.1156907	15.4769133	0.0011215	115.9170000	20.320866	-0.0041646
4.1632720	15.4769133	0.0011340	-117.1120000	20.325873	-0.0042043
4.2108533	15.4769133	0.0011465	118.3070000	20.330880	-0.0042440
4.2584346	15.4769133	0.0011590	-119.5020000	20.335887	-0.0042837
4.3060159	15.4769133	0.0011715	120.6970000	20.340894	-0.0043234
4.3535972	15.4769133	0.0011840	-121.8920000	20.345901	-0.0043631
4.4011785	15.4769133	0.0011965	123.0870000	20.350908	-0.0044028
4.4487598	15.4769133	0.0012090	-124.2820000	20.355915	-0.0044425
4.4963411	15.4769133	0.0012215	125.4770000	20.360922	-0.0044822
4.5439224	15.4769133	0.0012340	-126.6720000	20.365929	-0.0045219
4.5915037	15.4769133	0.0012465	127.8670000	20.370936	-0.0045616
4.6390850	15.4769133	0.0012590	-129.0620000	20.375943	-0.0046013
4.6866663	15.4769133	0.0012715	130.2570000	20.380950	-0.0046410
4.7342476	15.4769133	0.0012840	-131.4520000	20.385957	-0.0046807
4.7818289	15.4769133	0.0012965	132.6470000	20.390964	-0.0047204
4.8294102	15.4769133	0.0013090	-133.8420000	20.395971	-0.0047601
4.8769915	15.4769133	0.0013215	135.0370000	20.400978	-0.0047998
4.9245728	15.4769133	0.0013340	-136.2320000	20.405985	-0.0048395
4.9721541	15.4769133	0.0013465	137.4270000	20.410992	-0.0048792
5.0197354	15.4769133	0.0013590	-138.6220000	20.415999	-0.0049189
5.0673167	15.4769133	0.0013715	139.8170000	20.421006	-0.0049586
5.1148980	15.4769133	0.0013840	-141.0120000	20.426013	-0.0049983
5.1624793	15.4769133	0.0013965	142.2070000	20.431020	-0.0050380
5.2100606	15.4769133	0.0014090	-143.4020000	20.436027	-0.0050777
5.2576419	15.4769133	0.0014215	144.5970000	20.441034	-0.0051174
5.3052232	15.4769133	0.0014340	-145.7920000	20.446041	-0.0051571
5.3528045	15.4769133	0.0014465	146.9870000	20.451048	-0.0051968
5.4003858	15.4769133	0.0014590	-148.1820000	20.456055	-0.0052365
5.4479671	15.4769133	0.0014715	149.3770000	20.461062	-0.0052762
5.4955484	15.4769133	0.0014840	-150.5720000	20.466069	-0.0053159
5.5431297	15.4769133	0.0014965	151.7670000	20.471076	-0.0053556
5.5907110	15.4769133	0.0015090	-152.9620000	20.476083	-0.0053953
5.6382923	15.4769133	0.0015215	154.1570000	20.481090	-0.0054350
5.6858736	15.4769133	0.0015340	-155.3520000	20.486097	-0.0054747
5.7334549	15.4769133	0.0015465	156.5470000	20.491104	-0.0055144
5.7810362	15.4769133	0.0015590	-157.7420000	20.496111	-0.0055541
5.8286175	15.4769133	0.0015715	158.9370000	20.501118	-0.0055938
5.8761988	15.4769133	0.0015840	-160.1320000	20.506125	-0.0056335
5.9237801	15.4769133	0.0015965	161.3270000	20.511132	-0.0056732
5.9713614	15.4769133	0.0016090	-162.5220000	20.516139	-0.0057129
6.0189427	15.4769133	0.0016215	163.7170000	20.521146	-0.0057526
6.0665240	15.4769133	0.0016340	-164.9120000	20.526153	-0.0057923
6.1141053	15.4769133	0.0016465	166.1070000	20.531160	-0.0058320
6.1616866	15.4769133	0.0016590	-167.3020000	20.536167	-0.0058717
6.2092679	15.4769133	0.0016715	168.4970000	20.541174	-0.0059114
6.2568492	15.4769133	0.0016840	-169.6920000	20.546181	-0.0059511
6.3044305	15.4769133	0.0016965	170.8870000	20.551188	-0.0059

1 76193.386 0.70 1436332370.413 Pier 32aff.1p70 0.000 0.000 2.324E+12
 108847.697 -6580.0136 -0.000782
 1 81635.773 0.75 1365459673.070 108847.697 0.000 0.000 2.324E+12
 1365459673.070 -6580.0136 -0.000712
 1365459673.070 -6580.0136 -0.000679
 1365459673.070 -6580.0136 -0.000645
 1365459673.070 -6580.0136 -0.000613
 1365459673.070 -6580.0136 -0.000580
 1365459673.070 -6580.0136 -0.000548
 1365459673.070 -6580.0136 -0.000517
 1365459673.070 -6580.0136 -0.000486
 1365459673.070 -6580.0136 -0.000455
 1365459673.070 -6580.0136 -0.000425
 1365459673.070 -6580.0136 -0.000396
 1365459673.070 -6580.0136 -0.000367
 1365459673.070 -6580.0136 -0.000338
 1365459673.070 -6580.0136 -0.000311
 1365459673.070 -6580.0136 -0.000284
 1365459673.070 -6580.0136 -0.000257
 1365459673.070 -6580.0136 -0.000232
 1365459673.070 -6580.0136 -0.000207
 1365459673.070 -6580.0136 -0.000184
 1365459673.070 -6580.0136 -0.000162
 1365459673.070 -6580.0136 -0.000141
 1365459673.070 -6580.0136 -0.000121
 1365459673.070 -6580.0136 -0.000103
 1365459673.070 -6580.0136 -0.000085
 1365459673.070 -6580.0136 -0.000067
 1365459673.070 -6580.0136 -0.000050
 1365459673.070 -6580.0136 -0.000035
 1365459673.070 -6580.0136 -0.000020

 Computed Values of Pile Loading and Deflection
 for Lateral Loading for Load Case Number 1

Pile-head conditions are Displacement and Moment (Loading Type 4)
 Displacement of pile head = 0.500000 inches
 Moment at pile head = 7818000.0 in-lbs
 Axial load at pile head = 0.0 lbs

Res. X	Depth	Deflect.	Bending	Shear	Slope	Total	Bending	Soil
Feet	ft	inches	in-lbs	lbs	radians	Stress	Stiffness	P
lb/inch	inches	lb/inch	in-lbs	lbs	radians	psi*	lb-in ²	lb/in
0.00	0.00	0.5000	7818000.	-6580.0136	-0.003275	0.000	4.180E+11	0.000
0.00	1.078	0.4592	7732857.	-6580.0136	-0.003035	0.000	4.180E+11	0.000
0.00	2.157	0.4215	7647715.	-6580.0136	-0.002797	0.000	4.181E+11	0.000
0.00	3.235	0.3868	7562572.	-6580.0136	-0.002561	0.000	4.182E+11	0.000
0.00	4.313	0.3552	7477429.	-6580.0136	-0.002329	0.000	4.182E+11	0.000
0.00	5.392	0.3265	7392286.	-6580.0136	-0.002099	0.000	4.183E+11	0.000
0.00	6.470	0.3009	7307144.	-6580.0136	-0.001871	0.000	4.183E+11	0.000
0.00	7.548	0.2781	7222001.	-6580.0136	-0.001647	0.000	4.184E+11	0.000
0.00	8.626	0.2583	7136858.	-6580.0136	-0.001425	0.000	4.184E+11	0.000
0.00	9.705	0.2413	7051715.	-6580.0136	-0.001205	0.000	4.185E+11	0.000
0.00	10.783	0.2271	6966573.	-6580.0136	-0.001077	0.000	2.323E+12	0.000
0.00	11.861	0.2134	6881430.	-6580.0136	-0.001038	0.000	2.323E+12	0.000
0.00	12.940	0.2002	6796287.	-6580.0136	-0.001000	0.000	2.323E+12	0.000
0.00	14.018	0.1875	6711144.	-6580.0136	-0.000962	0.000	2.323E+12	0.000
0.00	15.096	0.1753	6626002.	-6580.0136	-0.000925	0.000	2.323E+12	0.000
0.00	16.174	0.1636	6540859.	-6580.0136	-0.000889	0.000	2.324E+12	0.000
0.00	17.253	0.1523	6455716.	-6580.0136	-0.000852	0.000	2.324E+12	0.000
0.00	18.331	0.1415	6370573.	-6580.0136	-0.000817	0.000	2.324E+12	0.000

Pier 32aff.1p7o		Pier 32aff.1p7o	
15.2970	205026.	0.000	0.000
53.915	-0.001092	1141135.	2.334E+12
18.1469	215072.	0.000	0.000
54.993	-0.001136	890487.	2.334E+12
19.7687	225118.	0.000	0.000
56.072	-0.001117	643150.	2.334E+12
214.4529	2484476.	0.000	0.000
57.150	-0.001051	431719.	2.334E+12
208.0612	2560645.	0.000	0.000
58.228	-0.000955	255125.	2.334E+12
198.2733	2686770.	0.000	0.000
185.9607	2864263.	0.000	0.000
60.385	-0.000717	533.1512	2.334E+12
171.8169	3099526.	0.000	0.000
61.463	-0.000595	-84026.	2.334E+12
156.4077	3404234.	0.000	0.000
62.541	-0.000478	-141331.	2.334E+12
140.1970	3797043.	0.000	0.000
63.620	-0.000371	-175163.	2.334E+12
111.2451	3878315.	0.000	0.000
64.698	-0.000277	-190369.	2.334E+12
83.7761	3911802.	0.000	0.000
65.776	-0.000197	-191547.	2.334E+12
59.9843	3945288.	0.000	0.000
66.855	-0.000130	-182682.	2.334E+12
40.0019	3978775.	0.000	0.000
67.933	-7.656E-05	-167120.	2.334E+12
23.7383	4012262.	0.000	0.000
69.011	-3.501E-05	-147583.	2.334E+12
10.9462	4045748.	0.000	0.000
70.090	-4.050E-06	-126213.	2.334E+12
1.2768	4079235.	0.000	0.000
71.168	-1.785E-05	-104629.	2.334E+12
-5.6750	4112722.	0.000	0.000
72.246	-3.223E-05	-83996.	2.334E+12
-10.3349	4146208.	0.000	0.000
73.324	-4.063E-05	-65093.	2.334E+12
-13.1229	4179695.	0.000	0.000
74.403	-4.433E-05	-48387.	2.334E+12
-14.4338	4213182.	0.000	0.000
75.481	-4.456E-05	-34098.	2.334E+12
-14.6246	4246668.	0.000	0.000
76.559	-4.233E-05	-22238.	2.334E+12
-14.9074	4280155.	0.000	0.000
77.638	-3.854E-05	-12763.	2.334E+12
-12.8464	4313641.	0.000	0.000
78.716	-3.581E-05	-5416.5056	2.334E+12
-11.3581	4347128.	0.000	0.000
-9.7738	4380615.	0.000	0.000
80.873	-2.558E-05	3840.0123	2.334E+12
-8.0435	4414101.	0.000	0.000
81.951	-1.576E-05	6308.3081	2.334E+12
-6.4473	4447388.	7000.0786	2.334E+12
-4.9712	4481073E-05	0.000	0.000
84.107	-1.052E-05	8258.5037	2.334E+12
-3.6709	4514561E-05	0.000	0.000
85.186	-7.281E-06	8202.2945	2.334E+12
-2.5590	4548048.	0.000	0.000
-1.8626	4.628E-06	7717.6174	2.334E+12
-1.6387	4581535.	0.000	0.000

87.342	2.529E-06	6958.5634	0.000	2.334E+12
-0.9022	4615021.	0.000	0.000	2.334E+12
88.421	-9.299E-07	6048.4592	0.000	2.334E+12
-0.3341	4648508.	0.000	0.000	2.334E+12
89.499	-2.336E-07	5082.4229	0.000	2.334E+12
0.0853	4681995.	0.000	0.000	2.334E+12
90.577	-1.037E-06	4130.6711	0.000	2.334E+12
0.3778	4715481.	0.000	0.000	2.334E+12
91.656	-1.542E-06	3242.1828	0.000	2.334E+12
0.5658	4748968.	0.000	0.000	2.334E+12
92.734	-1.814E-06	2448.4218	0.000	2.334E+12
0.6703	4782455.	0.000	0.000	2.334E+12
93.812	-1.910E-06	1766.8953	0.000	2.334E+12
0.7109	4815941.	0.000	0.000	2.334E+12
94.890	-1.880E-06	1204.4009	0.000	2.334E+12
0.7045	4849428.	0.000	0.000	2.334E+12
95.969	-1.763E-06	759.8654	0.000	2.334E+12
0.6653	4882915.	0.000	0.000	2.334E+12
97.047	-1.592E-06	426.7303	0.000	2.334E+12
0.6049	4916401.	0.000	0.000	2.334E+12
98.125	-1.390E-06	194.8680	0.000	2.334E+12
0.5318	4949888.	0.000	0.000	2.334E+12
99.204	-1.174E-06	52.0420	0.000	2.334E+12
0.4523	4983374.	0.000	0.000	2.334E+12
100.282	-9.548E-07	-15.0610	0.000	2.334E+12
0.3702	5016861.	0.000	0.000	2.334E+12
101.360	-7.363E-07	-20.1833	0.000	2.334E+12
0.0278	4888539.	0.000	0.000	2.334E+12
102.438	-5.193E-07	-20.6479	0.000	2.334E+12
0.0205	509788.	0.000	0.000	2.334E+12
103.517	-3.105E-07	-17.6869	0.000	2.334E+12
0.0125	530717.	0.000	0.000	2.334E+12
104.595	-8.454E-08	-12.6395	0.000	2.334E+12
0.0058	551567.	0.000	0.000	2.334E+12
105.673	-1.536E-07	-6.9530	0.000	2.334E+12
-0.005476	572376.	-2.1838	0.000	2.334E+12
106.752	-3.525E-07	0.000	0.000	2.334E+12
-0.01574	593205E-07	0.000	0.000	2.334E+12
107.830	-5.2193E-07	0.000	0.000	2.334E+12
-0.0261	307217.	0.000	0.000	2.334E+12

* This analysis computed pile response using nonlinear moment-curvature

relationships. Values of total stress due to combined axial and bending stresses are computed only for elastic sections only and do not equal the actual stresses in concrete and steel. Stresses in concrete and steel may be interpolated from the output for nonlinear bending properties relative to the magnitude of bending moment developed in the pile.

Output Summary for Load Case No. 1:

Pile-head deflection = 0.5000000 inches
 Computed slope at pile head = -0.0032754 radians
 Maximum bending moment = 7818000. inch-lbs
 Maximum shear force = -20013. lbs
 Depth of maximum bending moment = 0.000000 feet below pile head
 Depth of maximum shear force = 49.6018000 feet below pile head
 Number of iterations = 9
 Number of zero deflection points = 4

Computed Values of Pile Loading and Deflection
for Lateral Loading for Load Case Number 2

Pile-head conditions are Displacement and Moment (Loading Type 4)
Displacement of pile head = 1.000000 inches
Moment at pile head = 7818000.0 in-lbs
Axial load at pile head = 0.0 lbs

Res. X	Depth	Deflect.	Bending	Shear	Slope	Total	Soil
feet	ft	inches	Moment	Force	S	Stress	P
lb/inch	lb/inch	lb/inch	in-lbs	lbs	radians	psi*	lb-in ²
							lb/in
0.000	0.00	1.0000	7818000.	6374.9764	-0.004652	0.000	4.180E+11
0.000	1.078	0.9414	7900490.	6374.9764	-0.004409	0.000	4.180E+11
0.000	2.157	0.8859	7982979.	6374.9764	-0.004163	0.000	4.179E+11
0.000	3.235	0.8336	8065469.	6374.9764	-0.003915	0.000	4.179E+11
0.000	4.313	0.7846	8147959.	6374.9764	-0.003664	0.000	4.178E+11
0.000	5.392	0.7388	8230448.	6374.9764	-0.003410	0.000	4.178E+11
0.000	6.470	0.6963	8312938.	6374.9764	-0.003154	0.000	4.177E+11
0.000	7.548	0.6572	8395428.	6374.9764	-0.002895	0.000	4.177E+11
0.000	8.626	0.6214	8477917.	6374.9764	-0.002634	0.000	4.177E+11
0.000	9.705	0.5890	8560407.	6374.9764	-0.002370	0.000	4.176E+11
0.000	10.783	0.5601	8642896.	6374.9764	-0.002213	0.000	2.319E+12
0.000	11.861	0.5318	8725386.	6374.9764	-0.002165	0.000	2.319E+12
0.000	12.940	0.5041	8807876.	6374.9764	-0.002116	0.000	2.319E+12
0.000	14.018	0.4770	8890365.	6374.9764	-0.002066	0.000	2.319E+12
0.000	15.096	0.4506	8972855.	6374.9764	-0.002016	0.000	2.319E+12
0.000	16.174	0.4248	9055345.	6374.9764	-0.001966	0.000	2.318E+12
0.000	17.253	0.3997	9137834.	6374.9764	-0.001915	0.000	2.318E+12
0.000	18.331	0.3753	9220324.	6374.9764	-0.001864	0.000	2.318E+12
0.000	19.409	0.3515	9302814.	6374.9764	-0.001812	0.000	2.318E+12
0.000	20.488	0.3284	9385303.	6374.9764	-0.001760	0.000	2.318E+12
0.000	21.566	0.3059	9467793.	6374.9764	-0.001708	0.000	2.318E+12
0.000	22.644	0.2842	9550283.	6374.9764	-0.001655	0.000	2.318E+12

0.000	23.723	0.2631	9632772.	6374.9764	-0.001601	0.000	2.317E+12
0.000	24.801	0.2427	9715262.	6374.9764	-0.001547	0.000	2.317E+12
0.000	25.879	0.2231	9797751.	6374.9764	-0.001493	0.000	2.317E+12
0.000	26.957	0.2041	9880241.	6374.9764	-0.001438	0.000	2.317E+12
0.000	28.036	0.1859	9962731.	6374.9764	-0.001382	0.000	2.317E+12
0.000	29.114	0.1683	10045220.	6374.9764	-0.001325	0.000	2.203E+12
0.000	30.192	0.1516	10127710.	6374.9764	-0.001261	0.000	1.923E+12
0.000	31.271	0.1357	10210200.	6142.5423	-0.001188	0.000	1.680E+12
-35.9260	32.349	0.1208	10286674.	5081.6989	-0.001107	0.000	1.605E+12
-128.0425	33.427	0.1070	10341710.	2958.2146	-0.001024	0.000	1.599E+12
-200.1723	34.506	0.0943	10363230.	47.9415	-0.000940	0.000	1.596E+12
-249.6519	35.584	0.0827	10342951.	-3399.0072	-0.000856	0.000	1.599E+12
-283.1232	36.662	0.0722	10275267.	-7191.7705	-0.000773	0.000	1.606E+12
-303.1025	37.741	0.0627	10156833.	-11172.	-0.000695	0.000	1.783E+12
-312.0530	38.819	0.0542	9986152.	-15208.	-0.000630	0.000	2.317E+12
-311.7943	39.897	0.0464	9763266.	-19186.	-0.000575	0.000	2.317E+12
-303.0331	40.975	0.0393	9489642.	-23005.	-0.000521	0.000	2.318E+12
-287.3316	42.054	0.0329	9167909.	-26586.	-0.000469	0.000	2.318E+12
-266.1719	43.132	0.0272	8801610.	-29867.	-0.000419	0.000	2.319E+12
-240.9431	44.210	0.0221	8394970.	-32804.	-0.000371	0.000	2.320E+12
-212.9304	45.289	0.0176	7952677.	-35367.	-0.000325	0.000	2.321E+12
-183.3062	46.367	0.0137	7479693.	-37544.	-0.000282	0.000	2.322E+12
-153.1223	47.445	0.0103	6981072.	-39332.	-0.000242	0.000	2.323E+12
-123.3039	48.524	0.007429	6461805.	-40742.	-0.000204	0.000	2.324E+12
-94.6466	49.602	0.005017	5926691.	-41793.	-0.000170	0.000	2.325E+12
-67.8139	50.680	0.003032	5380273.	-42513.	-0.000138	0.000	2.326E+12
-43.3067	51.758	0.001934	4826699.	-42933.	-0.000110	0.000	2.327E+12
-21.6116	52.837	0.001184	4369156.	-43091.	-8.479E-05	0.000	2.328E+12
-2.9058	53.915	0.000760	3711327.	-43029.	-6.262E-05	0.000	2.329E+12
12.6326	54.993	-0.001437	3155612.	-42785.	-4.355E-05	0.000	2.330E+12
24.9984	56.072	-0.001887	2604083.	-40818.	-2.756E-05	0.000	2.331E+12
279.0609	1913590.	0.000					

Pier 32aff. 1p7o		Pier 32aff. 1p7o		Pier 32aff. 1p7o		Pier 32aff. 1p7o	
57.150	-0.002150	2099278.	0.000	2.332E+12	0.000	4715481.	0.000
297.8848	1792728.	0.000	0.000	2.333E+12	0.000	12362.	0.000
58.228	-0.002262	1644349.	0.000	2.333E+12	0.000	-1.6711	4748968.
305.5740	1747665.	0.000	0.000	2.334E+12	0.000	92.734	1.552E-06
59.306	-0.002257	1240584.	0.000	2.334E+12	0.000	-0.5737	4782455.
305.1573	1749865.	0.000	0.000	2.334E+12	0.000	93.812	-6.902E-07
60.385	-0.002162	887918.	0.000	2.334E+12	0.000	0.2569	4815941.
298.7340	1787770.	0.000	0.000	2.334E+12	0.000	94.890	-2.309E-06
61.463	-0.002004	585271.	0.000	2.334E+12	0.000	0.8652	4849428.
287.5922	1857079.	0.000	0.000	2.334E+12	0.000	95.969	-3.435E-06
62.541	-0.001804	330776.	0.000	2.334E+12	0.000	1.2963	4882915.
272.8430	1957522.	0.000	0.000	2.334E+12	0.000	97.047	-4.191E-06
63.620	-0.001579	121963.	0.000	2.334E+12	0.000	1.5925	4916401.
255.3381	2091786.	0.000	0.000	2.334E+12	0.000	98.125	-4.683E-06
64.698	-0.001347	44097.	0.000	2.334E+12	0.000	1.7914	4949888.
235.7758	2265418.	0.000	0.000	2.334E+12	0.000	99.204	-4.997E-06
65.776	-0.001117	170680.	0.000	2.334E+12	0.000	1.9244	4983374.
214.7394	2487437.	0.000	0.000	2.334E+12	0.000	100.282	-5.198E-06
66.855	-0.000900	261309.	0.000	2.334E+12	0.000	2.0154	5016861.
192.7195	2771770.	0.000	0.000	2.334E+12	0.000	101.360	-5.329E-06
67.933	-0.000701	319670.	0.000	2.334E+12	0.000	0.2013	488859.
170.1234	3140084.	0.000	0.000	2.334E+12	0.000	102.438	-5.408E-06
69.011	-0.000525	349546.	0.000	2.334E+12	0.000	0.2131	509788.
147.2730	3627518.	0.000	0.000	2.334E+12	0.000	103.517	-5.450E-06
118.1252	4079235.	0.000	0.000	2.334E+12	0.000	0.2235	530717.
70.090	-0.000375	354765.	0.000	2.334E+12	0.000	104.595	-5.468E-06
71.168	-0.000250	340205.	0.000	2.334E+12	0.000	0.2331	551647.
72.246	-0.000149	312367.	0.000	2.334E+12	0.000	105.673	-5.472E-06
47.6621	4146208.	0.000	0.000	2.334E+12	0.000	0.2421	572576.
73.324	-0.038E-05	276548.	0.000	2.334E+12	0.000	106.752	-5.470E-06
22.7337	4179695.	0.000	0.000	2.334E+12	0.000	0.2509	593505.
74.403	-1.185E-05	236923.	0.000	2.334E+12	0.000	107.830	-5.467E-06
3.8596	4213182.	0.000	0.000	2.334E+12	0.000	0.2596	307217.
75.481	2.968E-05	196652.	0.000	2.334E+12	0.000	* This analysis computed pile response using nonlinear moment-curvature relationships.	
-9.7392	4246668.	0.000	0.000	2.334E+12	0.000	Values of total stress due to combined axial and bending stresses are computed only for elastic sections only and do not equal the actual stresses in concrete and steel.	
-18.8863	4280155.	0.000	0.000	2.334E+12	0.000	Stresses in concrete and steel may be interpolated from the output for nonlinear bending properties relative to the magnitude of bending moment developed in the pile.	
-24.3964	4313641.	0.000	0.000	2.334E+12	0.000	Output Summary for Load Case No. 2:	
-27.0366	4347128.	0.000	0.000	2.334E+12	0.000	Pile-head deflection = 1.0000000 inches	
-27.5009	4380615.	0.000	0.000	2.334E+12	0.000	Computed slope at pile head = -0.0046523 radians	
-26.3963	4414101.	0.000	0.000	2.334E+12	0.000	Maximum bending moment = 10363230. inch-lbs	
-24.2337	4447588.	0.000	0.000	2.334E+12	0.000	Maximum shear force = -43091. lbs	
-21.4392	4481075.	0.000	0.000	2.334E+12	0.000	Depth of maximum bending moment = 34.5056000 feet below pile head	
-18.3382	4514561.	0.000	0.000	2.334E+12	0.000	Number of iterations = 17	
-15.1842	4548048.	0.000	0.000	2.334E+12	0.000	Number of zero deflection points = 3	
-12.1578	4581535.	0.000	0.000	2.334E+12	0.000		
-9.3803	4615021.	0.000	0.000	2.334E+12	0.000		
-8.421	1.927E-05	15041.	0.000	2.334E+12	0.000		
-6.9237	4648508.	0.000	0.000	2.334E+12	0.000		
-4.8211	4681995.	0.000	0.000	2.334E+12	0.000		
90.577	8.441E-06	13867.	0.000	2.334E+12	0.000		

Computed Values of Pile Loading and Deflection
for Lateral Loading for Load Case Number 3

Pier 32aff. 1p70										Pier 32aff. 1p70									
Pile-head conditions are Displacement and Moment (Loading Type 4)										Pile-head conditions are Displacement and Moment (Loading Type 4)									
Displacement of pile head = 1.500000 inches										Displacement of pile head = 1.500000 inches									
Moment at pile head = 7818000.0 in-lbs										Moment at pile head = 7818000.0 in-lbs									
Axial load at pile head = 0.0 lbs										Axial load at pile head = 0.0 lbs									
Res. X	Depth	Soil	Deflect.	Bending	Slope	Total	Soil	Force	P	Res. X	Depth	Soil	Deflect.	Bending	Slope	Total	Soil	Force	P
ft	ft	lb/inch	inches	in-lbs	radians	psi*	lb-in^2	lbs	lb/in	ft	ft	lb/inch	inches	in-lbs	radians	psi*	lb-in^2	lbs	lb/in
0.00	0.00	1.5000	7818000.	0.000	-0.006066	0.000	4.180E+11	13628.	-0.006066	0.000	4.180E+11	13628.	-0.006066	0.000	4.180E+11	13628.	-0.006066	0.000	4.180E+11
0.00	1.078	0.000	1.4231	7994345.	-0.005822	0.000	4.180E+11	13628.	-0.005822	0.000	4.180E+11	13628.	-0.005822	0.000	4.180E+11	13628.	-0.005822	0.000	4.180E+11
0.00	2.157	0.000	1.3493	8170691.	-0.005571	0.000	4.178E+11	13628.	-0.005571	0.000	4.178E+11	13628.	-0.005571	0.000	4.178E+11	13628.	-0.005571	0.000	4.178E+11
0.00	3.235	0.000	1.2789	8347036.	-0.005316	0.000	4.177E+11	13628.	-0.005316	0.000	4.177E+11	13628.	-0.005316	0.000	4.177E+11	13628.	-0.005316	0.000	4.177E+11
0.00	4.313	0.000	1.2118	8523382.	-0.005054	0.000	4.176E+11	13628.	-0.005054	0.000	4.176E+11	13628.	-0.005054	0.000	4.176E+11	13628.	-0.005054	0.000	4.176E+11
0.00	5.392	0.000	1.1481	8699727.	-0.004788	0.000	4.175E+11	13628.	-0.004788	0.000	4.175E+11	13628.	-0.004788	0.000	4.175E+11	13628.	-0.004788	0.000	4.175E+11
0.00	6.470	0.000	1.0879	8876073.	-0.004515	0.000	4.174E+11	13628.	-0.004515	0.000	4.174E+11	13628.	-0.004515	0.000	4.174E+11	13628.	-0.004515	0.000	4.174E+11
0.00	7.548	0.000	1.0312	9052418.	-0.004237	0.000	4.173E+11	13628.	-0.004237	0.000	4.173E+11	13628.	-0.004237	0.000	4.173E+11	13628.	-0.004237	0.000	4.173E+11
0.00	8.626	0.000	0.9782	9228764.	-0.003954	0.000	4.172E+11	13628.	-0.003954	0.000	4.172E+11	13628.	-0.003954	0.000	4.172E+11	13628.	-0.003954	0.000	4.172E+11
0.00	9.705	0.000	0.9289	9405109.	-0.003665	0.000	4.171E+11	13628.	-0.003665	0.000	4.171E+11	13628.	-0.003665	0.000	4.171E+11	13628.	-0.003665	0.000	4.171E+11
0.00	10.783	0.000	0.8834	9581454.	-0.003492	0.000	4.170E+11	13628.	-0.003492	0.000	4.170E+11	13628.	-0.003492	0.000	4.170E+11	13628.	-0.003492	0.000	4.170E+11
0.00	11.861	0.000	0.8385	9757800.	-0.003438	0.000	4.170E+11	13628.	-0.003438	0.000	4.170E+11	13628.	-0.003438	0.000	4.170E+11	13628.	-0.003438	0.000	4.170E+11
0.00	12.940	0.000	0.7944	9934145.	-0.003383	0.000	4.170E+11	13628.	-0.003383	0.000	4.170E+11	13628.	-0.003383	0.000	4.170E+11	13628.	-0.003383	0.000	4.170E+11
0.00	14.018	0.000	0.7510	10110491.	-0.003327	0.000	4.170E+11	13628.	-0.003327	0.000	4.170E+11	13628.	-0.003327	0.000	4.170E+11	13628.	-0.003327	0.000	4.170E+11
0.00	15.096	0.000	0.7083	10286836.	-0.003257	0.000	4.170E+11	13628.	-0.003257	0.000	4.170E+11	13628.	-0.003257	0.000	4.170E+11	13628.	-0.003257	0.000	4.170E+11
0.00	16.174	0.000	0.6667	10463182.	-0.003173	0.000	4.170E+11	13628.	-0.003173	0.000	4.170E+11	13628.	-0.003173	0.000	4.170E+11	13628.	-0.003173	0.000	4.170E+11
0.00	17.253	0.000	0.6262	10639527.	-0.003087	0.000	4.170E+11	13628.	-0.003087	0.000	4.170E+11	13628.	-0.003087	0.000	4.170E+11	13628.	-0.003087	0.000	4.170E+11
0.00	18.331	0.000	0.5868	10815873.	-0.002998	0.000	4.170E+11	13628.	-0.002998	0.000	4.170E+11	13628.	-0.002998	0.000	4.170E+11	13628.	-0.002998	0.000	4.170E+11
0.00	19.409	0.000	0.5486	10992218.	-0.002907	0.000	4.170E+11	13628.	-0.002907	0.000	4.170E+11	13628.	-0.002907	0.000	4.170E+11	13628.	-0.002907	0.000	4.170E+11
0.00	20.488	0.000	0.5116	11168563.	-0.002816	0.000	4.170E+11	13628.	-0.002816	0.000	4.170E+11	13628.	-0.002816	0.000	4.170E+11	13628.	-0.002816	0.000	4.170E+11
0.00	21.566	0.000	0.4757	11344909.	-0.002722	0.000	4.170E+11	13628.	-0.002722	0.000	4.170E+11	13628.	-0.002722	0.000	4.170E+11	13628.	-0.002722	0.000	4.170E+11
0.00	22.644	0.000	0.4411	11521254.	-0.002627	0.000	4.170E+11	13628.	-0.002627	0.000	4.170E+11	13628.	-0.002627	0.000	4.170E+11	13628.	-0.002627	0.000	4.170E+11
0.00	23.723	0.000	0.4077	11697600.	-0.002531	0.000	4.170E+11	13628.	-0.002531	0.000	4.170E+11	13628.	-0.002531	0.000	4.170E+11	13628.	-0.002531	0.000	4.170E+11
0.00	24.801	0.000	0.3756	11873945.	-0.002433	0.000	4.170E+11	13628.	-0.002433	0.000	4.170E+11	13628.	-0.002433	0.000	4.170E+11	13628.	-0.002433	0.000	4.170E+11
0.00	25.879	0.000	0.3448	12050291.	-0.002334	0.000	4.170E+11	13628.	-0.002334	0.000	4.170E+11	13628.	-0.002334	0.000	4.170E+11	13628.	-0.002334	0.000	4.170E+11
0.000	0.000	0.000	0.000	0.000	-0.002334	0.000	4.170E+11	13628.	-0.002334	0.000	4.170E+11	13628.	-0.002334	0.000	4.170E+11	13628.	-0.002334	0.000	4.170E+11

X		Y		Pier 32aff.lp7o		Stiffness		Stress		Force		Pier 32aff.lp7o	
Es*	Lat	Lat	Load	Force	S	psi*	lb-in ²	lb/in	lb/in	lb-in ²	lb/in	lb/in	lb/in
feet	inch	inch	in-lbs	lbs	radians								
lb/inch	lb/inch	lb/inch	in-lbs	lbs	radians								
0.000	0.00	0.00	2.0000	7818000.	-0.007437	0.000	4.180E+11	0.000	0.000	0.3092	16377543.	0.000	1.557E+12
0.000	1.078	0.000	1.9053	8113157.	0.007190	0.000	4.180E+11	0.000	0.000	0.2772	16665230.	0.000	1.557E+12
0.000	2.157	0.000	1.8139	8408313.	0.006935	0.000	4.177E+11	0.000	0.000	0.2471	16925946.	0.000	1.556E+12
0.000	3.235	0.000	1.7259	8703470.	0.006669	0.000	4.175E+11	0.000	0.000	0.2188	17139791.	0.000	1.556E+12
0.000	4.313	0.000	1.6413	8998627.	0.006395	0.000	4.174E+11	0.000	0.000	0.1923	17287704.	0.000	1.556E+12
0.000	5.392	0.000	1.5604	9293783.	0.006111	0.000	4.172E+11	0.000	0.000	0.1677	17352784.	0.000	1.556E+12
0.000	6.470	0.000	1.4832	9588940.	0.005819	0.000	4.170E+11	0.000	0.000	0.1450	17321380.	0.000	1.556E+12
0.000	7.548	0.000	1.4098	9884097.	0.005516	0.000	4.168E+11	0.000	0.000	0.1241	17182908.	0.000	1.556E+12
0.000	8.626	0.000	1.3404	10179253.	0.005205	0.000	4.167E+11	0.000	0.000	0.1051	16930783.	0.000	1.556E+12
0.000	9.705	0.000	1.2751	10474410.	0.004884	0.000	4.165E+11	0.000	0.000	0.0879	16563773.	0.000	1.557E+12
0.000	10.783	0.000	1.2140	10769567.	0.004677	0.000	4.160E+12	0.000	0.000	0.0725	16089255.	0.000	1.557E+12
0.000	11.861	0.000	1.1541	11064723.	0.004586	0.000	4.160E+12	0.000	0.000	0.0668	15516669.	0.000	1.558E+12
0.000	12.940	0.000	1.0953	11359880.	0.004493	0.000	4.160E+12	0.000	0.000	0.0633	14856899.	0.000	1.558E+12
0.000	14.018	0.000	1.0378	11655036.	0.004398	0.000	4.160E+12	0.000	0.000	0.0600	14212695.	0.000	1.558E+12
0.000	15.096	0.000	0.9815	11950193.	0.004300	0.000	4.160E+12	0.000	0.000	0.0574	13663976.	0.000	1.559E+12
0.000	16.174	0.000	0.9265	12245350.	0.004199	0.000	4.160E+12	0.000	0.000	0.0550	13123151.	0.000	1.559E+12
0.000	17.253	0.000	0.8728	12540506.	0.004096	0.000	4.160E+12	0.000	0.000	0.0526	12473229.	0.000	1.559E+12
0.000	18.331	0.000	0.8205	12835663.	0.003991	0.000	4.160E+12	0.000	0.000	0.0500	11853339.	0.000	1.559E+12
0.000	19.409	0.000	0.7695	13130820.	0.003883	0.000	4.160E+12	0.000	0.000	0.0476	11284419.	0.000	1.566E+12
0.000	20.488	0.000	0.7200	13425976.	0.003773	0.000	4.160E+12	0.000	0.000	0.0451	10724877.	0.000	2.317E+12
0.000	21.566	0.000	0.6719	13721133.	0.003660	0.000	4.160E+12	0.000	0.000	0.0426	10172487.	0.000	2.319E+12
0.000	22.644	0.000	0.6253	14016290.	0.003545	0.000	4.160E+12	0.000	0.000	0.0400	9724877.	0.000	2.321E+12
0.000	23.723	0.000	0.5802	14311446.	0.003428	0.000	4.160E+12	0.000	0.000	0.0375	9281204.	0.000	2.323E+12
0.000	24.801	0.000	0.5366	14606603.	0.003307	0.000	4.160E+12	0.000	0.000	0.0350	8838708.	0.000	2.325E+12
0.000	25.879	0.000	0.4946	14901760.	0.003185	0.000	4.160E+12	0.000	0.000	0.0325	8396194.	0.000	2.327E+12
0.000	26.957	0.000	0.4541	15196916.	0.003060	0.000	4.160E+12	0.000	0.000	0.0300	7953700.	0.000	2.329E+12
0.000	28.036	0.000	0.4154	15492073.	0.002932	0.000	4.160E+12	0.000	0.000	0.0275	7511206.	0.000	2.331E+12
0.000	29.114	0.000	0.3783	15787230.	0.002802	0.000	4.160E+12	0.000	0.000	0.0250	7068712.	0.000	2.333E+12
0.000	30.192	0.000	0.3428	16082386.	0.002670	0.000	4.160E+12	0.000	0.000	0.0225	6626218.	0.000	2.334E+12

STR-III
 A=2.0
 LATERAL
 RESISTANCE
 = 22.817213
 FK

Pier 32aff.lp7o															
0.000	0.000	0.000	0.2518	0.000	5260728.	4861.7547	-0.001114	0.000	2.326E+12						
0.000	15.096	0.000	0.000	0.000	5260728.	4861.7547	-0.001114	0.000	2.326E+12						
0.000	16.174	0.2376	0.000	0.000	5323637.	4861.7547	-0.001084	0.000	2.326E+12						
0.000	17.253	0.000	0.000	0.000	5386547.	4861.7547	-0.001055	0.000	2.326E+12						
0.000	18.331	0.2103	0.000	0.000	5449456.	4861.7547	-0.001024	0.000	2.326E+12						
0.000	19.409	0.1972	0.000	0.000	5512365.	4861.7547	-0.000994	0.000	2.326E+12						
0.000	20.488	0.1846	0.000	0.000	5575274.	4861.7547	-0.000963	0.000	2.326E+12						
0.000	21.566	0.1723	0.000	0.000	5638183.	4861.7547	-0.000932	0.000	2.326E+12						
0.000	22.644	0.1604	0.000	0.000	5701092.	4861.7547	-0.000900	0.000	2.326E+12						
0.000	23.723	0.1490	0.000	0.000	5764002.	4861.7547	-0.000868	0.000	2.326E+12						
0.000	24.801	0.1380	0.000	0.000	5826911.	4861.7547	-0.000836	0.000	2.326E+12						
0.000	25.879	0.1274	0.000	0.000	5889820.	4861.7547	-0.000804	0.000	2.326E+12						
0.000	26.957	0.1172	0.000	0.000	5952729.	4861.7547	-0.000771	0.000	2.326E+12						
0.000	28.036	0.1074	0.000	0.000	6015638.	4861.7547	-0.000737	0.000	2.326E+12						
0.000	29.114	0.1000	0.000	0.000	6078547.	4861.7547	-0.000704	0.000	2.326E+12						
0.000	30.192	0.0892	0.000	0.000	6141456.	4861.7547	-0.000670	0.000	2.326E+12						
0.000	31.271	0.0808	0.000	0.000	6204365.	4695.9727	-0.000635	0.000	2.326E+12						
-25.3249	105.7868	0.000	0.000	0.000	6267274.	4015.3595	-0.000601	0.000	2.326E+12						
-79.3749	145.6652	0.000	0.000	0.000	6330184.	2711.5249	-0.000566	0.000	2.326E+12						
-121.3548	241.9857	0.000	0.000	0.000	6393093.	927.3672	-0.000530	0.000	2.326E+12						
-153.8134	342.0411	0.000	0.000	0.000	6456002.	-1207.9587	-0.000495	0.000	2.326E+12						
-176.3284	442.9000	0.000	0.000	0.000	6518911.	-3579.0604	-0.000460	0.000	2.326E+12						
-190.3662	543.3662	0.000	0.000	0.000	6581820.	-6084.2232	-0.000425	0.000	2.326E+12						
-196.9509	643.8222	0.000	0.000	0.000	6644729.	-8635.2100	-0.000391	0.000	2.326E+12						
-197.3406	744.2887	0.000	0.000	0.000	6707638.	-11157.	-0.000357	0.000	2.326E+12						
-192.4288	844.7441	0.000	0.000	0.000	6770547.	-13587.	-0.000324	0.000	2.326E+12						
-183.1785	945.2000	0.000	0.000	0.000	6833456.	-15875.	-0.000292	0.000	2.326E+12						
-170.5049	1045.6666	0.000	0.000	0.000	6896365.	-17983.	-0.000261	0.000	2.326E+12						
-155.2679	1146.1322	0.000	0.000	0.000	6959274.	-19882.	-0.000231	0.000	2.326E+12						
-138.2643	1246.5887	0.000	0.000	0.000	7022183.	-21554.	-0.000203	0.000	2.326E+12						
-120.2223	1347.0441	0.000	0.000	0.000	7085092.	-22991.	-0.000176	0.000	2.326E+12						
-101.7960	1447.5000	0.000	0.000	0.000	7147901.	-24190.	-0.000151	0.000	2.326E+12						
-83.5620	1547.9559	0.000	0.000	0.000	7210810.	0.000	0.000	0.000	2.326E+12						

Pier 32aff.lp7o															
86.2640	2.0000000	17405485.	-74206.	0.000	0.0000000	17405485.	-74206.	0.000	0.5000000 inches						
80.8725	2.0000000	17348862.	-73362.	0.000	0.0000000	17348862.	-73362.	0.000	4380000.0 in-lbs						
75.4810	2.0000000	17350072.	-73015.	0.000	0.0000000	17350072.	-73015.	0.000	0.0 lbs						
70.0895	2.0000000	17357343.	-72897.	0.000	0.0000000	17357343.	-72897.	0.000							
64.6980	2.0000000	17216182.	-78947.	0.000	0.0000000	17216182.	-78947.	0.000							
59.3065	2.0000000	15738755.	-87995.	0.000	0.0000000	15738755.	-87995.	0.000							
53.9150	2.0000000	10950672.	-78793.	0.000	0.0000000	10950672.	-78793.	0.000							
48.5235	2.0000000	7818000.	-57106.	0.000	0.0000000	7818000.	-57106.	0.000							
43.1320	2.0000000	7818000.	-34729.	0.000	0.0000000	7818000.	-34729.	0.000							
37.7405	0.0000000	41389480186.	-4569525710.	0.000	0.0000000	41389480186.	-4569525710.	0.000							
37.7405	0.0000000	41389480186.	-4569525710.	0.000	0.0000000	41389480186.	-4569525710.	0.000							
37.7405	0.0000000	41389480186.	-4569525710.	0.000	0.0000000	41389480186.	-4569525710.	0.000							
37.7405	0.0000000	41389480186.	-4569525710.	0.000	0.0000000	41389480186.	-4569525710.	0.000							

Computed Values of Pile Loading and Deflection for Lateral Loading for Load Case Number 5

Pile-head conditions are Displacement and Moment (Loading Type 4)															
Displacement of pile head = 0.500000 inches															
Moment at pile head = 4380000.0 in-lbs															
Axial load at pile head = 0.0 lbs															
Depth	Deflect.	Bending	Shear	Slope	Total	Bending	Soil								
X	y	Moment	Force	S	Stress	stiffness	P								
feet	inches	in-lbs	Tbs	radians	psi*	lb-in/2	lb/in								
lb/inch	lb/inch	lb/inch													
0.00	0.000	4380000.	4861.7547	-0.001671	0.000	1.341E+12	0.000	1.341E+12							
0.00	0.4787	4442909.	4861.7547	-0.001629	0.000	1.341E+12	0.000	1.341E+12							
0.00	2.157	4505818.	4861.7547	-0.001585	0.000	1.341E+12	0.000	1.341E+12							
0.00	3.235	4568727.	4861.7547	-0.001542	0.000	1.340E+12	0.000	1.340E+12							
0.00	4.313	4631637.	4861.7547	-0.001497	0.000	1.340E+12	0.000	1.340E+12							
0.00	5.392	4694546.	4861.7547	-0.001452	0.000	1.340E+12	0.000	1.340E+12							
0.00	6.470	4757455.	4861.7547	-0.001406	0.000	1.340E+12	0.000	1.340E+12							
0.00	7.548	4820364.	4861.7547	-0.001360	0.000	1.340E+12	0.000	1.340E+12							
0.00	8.626	4883273.	4861.7547	-0.001313	0.000	1.339E+12	0.000	1.339E+12							
0.00	9.705	4946182.	4861.7547	-0.001266	0.000	1.339E+12	0.000	1.339E+12							
0.00	10.783	5009092.	4861.7547	-0.001228	0.000	2.327E+12	0.000	2.327E+12							
0.00	11.861	5072001.	4861.7547	-0.001200	0.000	2.326E+12	0.000	2.326E+12							
0.00	12.940	5134910.	4861.7547	-0.001172	0.000	2.326E+12	0.000	2.326E+12							
0.00	14.018	5197819.	4861.7547	-0.001143	0.000	2.326E+12	0.000	2.326E+12							

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48.524	0.005182	4015345.	0.000	2.329E+12	0.000	2.329E+12	0.000	2.329E+12
-66.0163	164842.	0.000	0.000	0.000	0.000	0.000	0.000	0.000
-49.5733	174888.	3684286.	0.000	0.000	0.000	0.000	0.000	0.000
-34.5642	184534.	3344927.	0.000	0.000	0.000	0.000	0.000	0.000
-21.2372	194380.	2999781.	0.000	0.000	0.000	0.000	0.000	0.000
-9.7579	205026.	2651079.	0.000	0.000	0.000	0.000	0.000	0.000
-0.2111	215072.	2300743.	0.000	0.000	0.000	0.000	0.000	0.000
7.3979	225118.	1950372.	0.000	0.000	0.000	0.000	0.000	0.000
56.072	-0.000723	1601239.	0.000	0.000	0.000	0.000	0.000	0.000
173.1261	3097805.	0.000	0.000	0.000	0.000	0.000	0.000	0.000
193.7090	2766035.	1281094.	0.000	0.000	0.000	0.000	0.000	0.000
203.1741	2636120.	9933382.	0.000	0.000	0.000	0.000	0.000	0.000
205.1681	2610031.	739688.	0.000	0.000	0.000	0.000	0.000	0.000
201.7841	2653626.	520345.	0.000	0.000	0.000	0.000	0.000	0.000
194.4166	2754192.	334789.	0.000	0.000	0.000	0.000	0.000	0.000
184.0825	2908941.	181784.	0.000	0.000	0.000	0.000	0.000	0.000
171.5685	3121352.	59600.	0.000	0.000	0.000	0.000	0.000	0.000
157.5054	3400369.	-33857.	0.000	0.000	0.000	0.000	0.000	0.000
142.4081	3761259.	-100942.	0.000	0.000	0.000	0.000	0.000	0.000
119.2168	3978775.	-144184.	0.000	0.000	0.000	0.000	0.000	0.000
91.7361	4012262.	-167465.	0.000	0.000	0.000	0.000	0.000	0.000
67.5363	4045748.	-175386.	0.000	0.000	0.000	0.000	0.000	0.000
46.8898	4079235.	-171999.	0.000	0.000	0.000	0.000	0.000	0.000
29.8170	4112722.	-160761.	0.000	0.000	0.000	0.000	0.000	0.000
16.1555	4146208.	-144531.	0.000	0.000	0.000	0.000	0.000	0.000
5.6186	4179695.	-125596.	0.000	0.000	0.000	0.000	0.000	0.000
-2.1555	4213182.	-105721.	0.000	0.000	0.000	0.000	0.000	0.000
-7.5647	4246668.	-86206.	0.000	0.000	0.000	0.000	0.000	0.000
-11.0152	4280155.	-67958.	0.000	0.000	0.000	0.000	0.000	0.000
-12.8895	4313641.	-51553.	0.000	0.000	0.000	0.000	0.000	0.000
-13.7816	4347128.	-37307.	0.000	0.000	0.000	0.000	0.000	0.000
-13.3153	4380615.	-25350.	0.000	0.000	0.000	0.000	0.000	0.000
-12.4544	4414101.	-15382.	0.000	0.000	0.000	0.000	0.000	0.000
81.9511	5.257E-05	-7919.8539	0.000	2.334E+12	0.000	2.334E+12	0.000	2.334E+12

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-11.1946	4447588.	0.000	0.000	0.000	0.000	0.000	0.000	0.000	2.334E+12	
-9.7176	4481075.	-2131.6733	0.000	0.000	0.000	0.000	0.000	0.000	0.000	2.334E+12
-8.1640	4514561.	2029.4311	0.000	0.000	0.000	0.000	0.000	0.000	0.000	2.334E+12
-6.6374	4548048.	4823.6075	0.000	0.000	0.000	0.000	0.000	0.000	0.000	2.334E+12
-5.2100	4581535.	6506.4555	0.000	0.000	0.000	0.000	0.000	0.000	0.000	2.334E+12
-3.9275	4615021.	7316.9730	0.000	0.000	0.000	0.000	0.000	0.000	0.000	2.334E+12
-2.8144	4648508.	7469.8972	0.000	0.000	0.000	0.000	0.000	0.000	0.000	2.334E+12
-1.8787	4681995.	7151.6003	0.000	0.000	0.000	0.000	0.000	0.000	0.000	2.334E+12
-1.1164	4715481.	6518.7422	0.000	0.000	0.000	0.000	0.000	0.000	0.000	2.334E+12
-0.5146	4748968.	5698.9677	0.000	0.000	0.000	0.000	0.000	0.000	0.000	2.334E+12
-0.0554	4782455.	4793.0291	0.000	0.000	0.000	0.000	0.000	0.000	0.000	2.334E+12
0.2824	4815941.	3877.8177	0.000	0.000	0.000	0.000	0.000	0.000	0.000	2.334E+12
0.5205	4849428.	3009.8825	0.000	0.000	0.000	0.000	0.000	0.000	0.000	2.334E+12
0.6805	4882915.	2229.1031	0.000	0.000	0.000	0.000	0.000	0.000	0.000	2.334E+12
0.7818	4916401.	1562.2624	0.000	0.000	0.000	0.000	0.000	0.000	0.000	2.334E+12
0.8416	4949888.	1026.3291	0.000	0.000	0.000	0.000	0.000	0.000	0.000	2.334E+12
0.8738	4983374.	651.3139	0.000	0.000	0.000	0.000	0.000	0.000	0.000	2.334E+12
0.8888	5016861.	382.6030	0.000	0.000	0.000	0.000	0.000	0.000	0.000	2.334E+12
0.8865	4888539.	282.7023	0.000	0.000	0.000	0.000	0.000	0.000	0.000	2.334E+12
0.8892	509788.	157.2769	0.000	0.000	0.000	0.000	0.000	0.000	0.000	2.334E+12
0.0913	530717.	126.7864	0.000	0.000	0.000	0.000	0.000	0.000	0.000	2.334E+12
0.0929	551647.	71.5801	0.000	0.000	0.000	0.000	0.000	0.000	0.000	2.334E+12
0.0941	572576.	51.9214	0.000	0.000	0.000	0.000	0.000	0.000	0.000	2.334E+12
0.0950	593503.	8.0102	0.000	0.000	0.000	0.000	0.000	0.000	0.000	2.334E+12
0.0957	507217.	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	2.334E+12

* This analysis computed pile response using nonlinear moment-curvature

relationships.

Values of total stress due to combined axial and bending stresses are computed

only for elastic sections only and do not equal the actual stresses in concrete and

steel.

Stresses in concrete and steel may be interpolated from the output for nonlinear

bending properties relative to the magnitude of bending moment developed in the

pile.

Output Summary for Load Case No. 5:

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 Pile-head deflection = 0.5000000 inches
 Computed slope at pile head = -0.0016711 radians
 Maximum bending moment = 6333157.7 inch-lbs
 Maximum shear force = -27076.6 lbs
 Depth of maximum bending moment = 34.5056000 feet below pile head
 Depth of maximum shear force = 53.9150000 feet below pile head
 Number of iterations = 6
 Number of zero deflection points = 3

 Computed Values of Pile Loading and Deflection
 For Lateral Loading for Load Case Number 6

 Pile-head conditions are Displacement and Moment (Loading Type 4)
 Displacement of pile head = 1.0000000 inches
 Moment at pile head = 4380000.0 in-lbs
 Axial load at pile head = 0.0 lbs

Depth Res. X feet	Deflect. Y inches	Bending Distrib. Moment in-lbs	Shear Force lbs	Slope S radians	Total Stress psi*	Bending Stiffness lb-in ²	Soil P lb/in
0.000	1.0000	4380000.0	15799.	-0.003088	0.000	1.341E+12	0.000
0.000	0.9603	4584431.	15799.	-0.003045	0.000	1.341E+12	0.000
0.000	0.9212	4788862.	15799.	-0.002999	0.000	1.340E+12	0.000
0.000	0.8827	4993293.	15799.	-0.002952	0.000	1.339E+12	0.000
0.000	0.8448	5197724.	15799.	-0.002903	0.000	1.338E+12	0.000
0.000	0.8076	5402155.	15799.	-0.002852	0.000	1.338E+12	0.000
0.000	0.7710	5606587.	15799.	-0.002798	0.000	1.337E+12	0.000
0.000	0.7351	5811018.	15799.	-0.002743	0.000	1.336E+12	0.000
0.000	0.7000	6015449.	15799.	-0.002622	0.000	4.193E+11	0.000
0.000	0.6673	6219880.	15799.	-0.002433	0.000	4.189E+11	0.000
0.000	0.6370	6424311.	15799.	-0.002319	0.000	2.324E+12	0.000
0.000	0.6073	6628742.	15799.	-0.002283	0.000	2.323E+12	0.000
0.000	0.5780	6833173.	15799.	-0.002246	0.000	2.323E+12	0.000
0.000	0.5491	7037604.	15799.	-0.002207	0.000	2.323E+12	0.000
0.000	0.5208	7242035.	15799.	-0.002167	0.000	2.322E+12	0.000
0.000	0.4931	7446466.	15799.	-0.002126	0.000	2.322E+12	0.000
0.000	0.4658	7650897.	15799.	-0.002084	0.000	2.321E+12	0.000
0.000	0.4391	7855328.	15799.	-0.002041	0.000	2.321E+12	0.000
0.000	0.4130	8059760.	15799.	-0.001997	0.000	2.321E+12	0.000
0.000	0.3875	8264191.	15799.	-0.001951	0.000	2.320E+12	0.000
0.000	0.3625	8468622.	15799.	-0.001904	0.000	2.320E+12	0.000
0.000	0.3382	8673053.	15799.	-0.001857	0.000	2.319E+12	0.000
0.000	0.3145	8877484.	15799.	-0.001808	0.000	2.319E+12	0.000
0.000	0.2914	9081915.	15799.	-0.001758	0.000	2.319E+12	0.000
0.000	0.2690	9286346.	15799.	-0.001706	0.000	2.318E+12	0.000
0.000	0.2472	9490777.	15799.	-0.001654	0.000	2.318E+12	0.000
0.000	0.2262	9695208.	15799.	-0.001600	0.000	2.317E+12	0.000
0.000	0.2058	9899639.	15799.	-0.001546	0.000	2.317E+12	0.000
0.000	0.1862	10104070.	15799.	-0.001488	0.000	2.203E+12	0.000
0.000	0.1673	10308502.	15553.	-0.001417	0.000	1.602E+12	0.000
0.000	0.1495	10506576.	14429.	-0.001332	0.000	1.581E+12	0.000
0.000	0.1328	10681911.	12034.	-0.001245	0.000	1.564E+12	0.000
0.000	0.1173	10818019.	8510.6053	-0.001156	0.000	1.560E+12	0.000
0.000	0.1029	10902159.	4223.6850	-0.001066	0.000	1.560E+12	0.000
0.000	0.0897	10927325.	-491.9678	-0.000975	0.000	1.560E+12	0.000
0.000	0.0777	10889427.	-5428.7687	-0.000885	0.000	1.560E+12	0.000
0.000	0.0668	10786833.	-10414.	-0.000795	0.000	1.560E+12	0.000
0.000	0.0571	10619911.	-15311.	-0.000707	0.000	1.570E+12	0.000
0.000	0.0485	10390592.	-20015.	-0.000621	0.000	1.593E+12	0.000
0.000	0.0410	10101944.	-24452.	-0.000549	0.000	2.242E+12	0.000
0.000	0.0343	9757787.	-28563.	-0.000493	0.000	2.317E+12	0.000
0.000	0.0283	9362769.	-32290.	-0.000439	0.000	2.318E+12	0.000
0.000	0.0229	8921149.	-35596.	-0.000388	0.000	2.319E+12	0.000
0.000	0.0182	8441575.	-38458.	-0.000340	0.000	2.320E+12	0.000
0.000	0.0141	7926679.	-40870.	-0.000294	0.000	2.321E+12	0.000
0.000	0.0106	7383894.	-42837.	-0.000252	0.000	2.322E+12	0.000
0.000	0.0082	6818299.	-44376.	-0.000212	0.000	2.323E+12	0.000
0.000	0.0065	6335484.	-45514.	-0.000176	0.000	2.324E+12	0.000
0.000	0.0051	5849310.	-46285.	-0.000143	0.000	2.325E+12	0.000
0.000	0.0030	5640440.	-46285.	-0.000143	0.000	2.325E+12	0.000

SCR-1
 Δ=1.0
 LATERAL
 RESISTANCE
 = 15.79

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-46.1169	194980.	0.000	0.000	2.327E+12	86.264	4.457E-05	7076.0640	182.4804	-7.255E-07	0.000	2.334E+12
52.837	0.001417	5037673.	0.000	2.327E+12	-15.7798	4.581535.	0.000	282.4804	-6.732E-07	0.000	2.334E+12
-22.4466	205026.	0.000	0.000	2.328E+12	87.342	3.543E-05	11789.	137.6280	-6.007E-07	0.000	2.334E+12
53.915	0.000135	4431149.	0.000	2.329E+12	-12.6374	4.615021.	0.000	27.9790	-5.182E-07	0.000	2.334E+12
-2.2498	215027.	0.000	0.000	2.330E+12	88.421	2.714E-05	14386.	-50.9589	-4.338E-07	0.000	2.334E+12
54.993	-0.000827	3824248.	0.000	2.331E+12	-9.7516	4.648508.	0.000	-103.9070	-3.530E-07	0.000	2.334E+12
14.3918	225118.	0.000	0.000	2.332E+12	89.499	1.989E-05	15351.	-135.4706	-2.797E-07	0.000	2.334E+12
56.072	-0.001515	3219757.	0.000	2.333E+12	-7.1963	4.681995.	0.000	-149.8968	-2.160E-07	0.000	2.334E+12
250.0184	2135574.	2657127.	0.000	2.334E+12	90.577	1.373E-05	15111.	-150.9200	-1.632E-07	0.000	2.334E+12
285.2111	1872244.	0.000	0.000	2.335E+12	91.656	8.662E-06	14032.	-141.6802	-1.212E-07	0.000	2.334E+12
57.150	-0.001971	2657127.	0.000	2.336E+12	-3.1792	4.748968.	0.000	4875.6930	-8.929E-08	0.000	2.334E+12
285.2228	0.002237	2142251.	0.000	2.337E+12	92.734	4.598E-06	12421.	3393.4482	-6.636E-08	0.000	2.334E+12
303.8171	175676.	1678244.	0.000	2.338E+12	-1.6994	4.782455.	0.000	2238.4277	-5.075E-08	0.000	2.334E+12
311.3133	1715413.	0.000	0.000	2.339E+12	93.812	1.475E-06	10526.	4875.6930	-8.929E-08	0.000	2.334E+12
59.306	-0.002348	1266361.	0.000	2.340E+12	-0.5303	4.815941.	0.000	6620.5766	-1.212E-07	0.000	2.334E+12
60.385	0.002339	1266361.	0.000	2.341E+12	94.890	-9.931E-07	8542.2631	101.9068	-6.636E-08	0.000	2.334E+12
310.7345	1718655.	0.000	0.000	2.342E+12	0.3722	4.849428.	0.000	-74.6963	-5.075E-08	0.000	2.334E+12
304.0492	1756485.	9065505.	0.000	2.343E+12	1.0560	4.882915.	0.000	-44.0202	-4.050E-08	0.000	2.334E+12
292.6625	1824865.	597558.	0.000	2.344E+12	1.5686	4.916401.	0.000	26.2251	-3.340E-08	0.000	2.334E+12
277.6455	1923606.	337611.	0.000	2.345E+12	1.9544	4.949888.	0.000	-22.6827	-2.819E-08	0.000	2.334E+12
259.8513	2055376.	124152.	0.000	2.346E+12	2.2514	4.983374.	0.000	18.8024	-2.460E-08	0.000	2.334E+12
239.9799	2225620.	-45799.	0.000	2.347E+12	2.4900	5.016861.	0.000	-14.5940	-2.236E-08	0.000	2.334E+12
218.6168	2443166.	-175570.	0.000	2.348E+12	100.282	-6.422E-06	1460.3682	-10.0604	-2.117E-08	0.000	2.334E+12
66.855	-0.001158	-175570.	0.000	2.349E+12	101.360	-6.894E-06	1099.2210	-5.1983	-2.070E-08	0.000	2.334E+12
67.933	-0.000933	-268737.	0.000	2.350E+12	0.2605	4.888859.	0.000	0.000	-2.061E-08	0.000	2.334E+12
196.2544	2721628.	-329044.	0.000	2.351E+12	0.2871	5.09788.	0.000	0.000	0.000	0.000	2.334E+12
69.011	-0.000728	-329044.	0.000	2.352E+12	103.517	7.623E-06	512.2104	0.000	0.000	0.000	2.334E+12
173.3025	3082173.	0.000	0.000	2.353E+12	0.3127	5.30717.	0.000	0.000	0.000	0.000	2.334E+12
70.090	-0.000546	-360335.	0.000	2.354E+12	104.595	7.923E-06	295.0906	0.000	0.000	0.000	2.334E+12
150.0860	3559085.	-366497.	0.000	2.355E+12	0.3378	5.51647.	0.000	0.000	0.000	0.000	2.334E+12
71.168	-0.000390	-366497.	0.000	2.356E+12	105.673	8.202E-06	134.3286	0.000	0.000	0.000	2.334E+12
123.8343	4112722.	-351924.	0.000	2.357E+12	0.3629	5.72576.	0.000	0.000	0.000	0.000	2.334E+12
72.246	-0.000260	-351924.	0.000	2.358E+12	106.752	9.6471E-06	84.7357	0.000	0.000	0.000	2.334E+12
83.2652	4146208.	-323410.	0.000	2.359E+12	0.3886	5.93503.	0.000	0.000	0.000	0.000	2.334E+12
73.324	-0.000155	-323410.	0.000	2.360E+12	107.830	9.738E-06	0.000	0.000	0.000	0.000	2.334E+12
50.1797	4179695.	-286495.	0.000	2.361E+12	0.4149	5.07217.	0.000	0.000	0.000	0.000	2.334E+12
74.403	-7.404E-05	-286495.	0.000	2.362E+12							
24.1078	4213182.	0.000	0.000	2.363E+12							
75.481	-1.329E-05	-245543.	0.000	2.364E+12							
4.3604	4246668.	0.000	0.000	2.365E+12							
76.559	2.985E-05	-203861.	0.000	2.366E+12							
-9.8747	4280155.	-163832.	0.000	2.367E+12							
77.638	5.837E-05	-163832.	0.000	2.368E+12							
-19.4576	4313641.	-127061.	0.000	2.369E+12							
78.716	7.513E-05	-127061.	0.000	2.370E+12							
-25.2395	4347128.	-94516.	0.000	2.371E+12							
79.794	8.277E-05	-94516.	0.000	2.372E+12							
-28.0222	4380615.	-66663.	0.000	2.373E+12							
80.873	8.364E-05	-66663.	0.000	2.374E+12							
-28.5314	4414101.	-43387.	0.000	2.375E+12							
81.951	7.972E-05	-43387.	0.000	2.376E+12							
-27.4013	4447588.	-25099.	0.000	2.377E+12							
83.029	7.126E-05	-25099.	0.000	2.378E+12							
-25.3680	4483875.	10825.	0.000	2.379E+12							
22.94107	451382E-05	-10825.	0.000	2.380E+12							
-22.90186	454421E-05	-279.1522	0.000	2.381E+12							
-19.0534	4548048.	0.000	0.000	2.382E+12							

* This analysis computed pile response using nonlinear moment-curvature relationships.

Values of total stress due to combined axial and bending stresses are computed only for elastic sections only and do not equal the actual stresses in concrete and steel.

Stresses in concrete and steel may be interpolated from the output for nonlinear bending properties relative to the magnitude of bending moment developed in the pile.

Output Summary for Load Case No. 6:

Pile-head deflection	=	1.0000000 inches
Computed slope at pile head	=	-0.0030829 radians
Maximum bending moment	=	10927325 inch-lbs
Maximum shear force	=	-46888 lbs
Depth of maximum bending moment	=	36.6622000 feet below pile head
Depth of maximum shear force	=	53.9150000 feet below pile head
Number of iterations	=	55

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23338. -0.004596

Number of zero deflection points = 3

Pile-head Deflection vs. Pile Length for Load Case 6

Boundary Condition Type 4, Deflection and Moment

Deflection = 1.00000 in
Moment = 4380000. in-lb
Axial Load = 0. lb

Pile Length feet	Pile Head Deflection inches	Maximum Moment in-lb	Maximum Shear lbs
107.8300	1.0000000	10927325.	-46888.
102.4385	1.0000000	10901757.	-46579.
97.0470	1.0000000	10882998.	-46499.
91.6555	1.0000000	10940233.	-47007.
86.2640	1.0000000	10928176.	-46841.
80.8725	1.0000000	10877120.	-46234.
75.4810	1.0000000	10880881.	-46623.
70.0895	1.0000000	10900250.	-46250.
64.6980	1.0000000	10864859.	-49725.
59.3065	1.0000000	10479996.	-56731.
53.9150	1.0000000	4380000.	-51939.
48.5235	1.0000000	4380000.	-36352.
43.1320	1.0000000	4380000.	-21193.
37.7405	1.0000000	4380000.	-10810.
37.7405	0.0000000	66239071156.	-7312996861.
37.7405	0.0000000	66239071156.	-7312996861.
37.7405	0.0000000	66239071156.	-7312996861.
37.7405	0.0000000	66239071156.	-7312996861.
37.7405	0.0000000	66239071156.	-7312996861.

Computed Values of Pile Loading and Deflection for Lateral Loading for Load Case Number 7

Pile-head conditions are Displacement and Moment (Loading Type 4)
Displacement of pile head = 1.500000 inches
Moment at pile head = 4380000.0 in-lb
Axial load at pile head = 0.0 lbs

Depth Res. x feet	Soil Spr. y inches	Deflect. Lat. Load lb/inch	Bending Moment in-lb	Total Stress psi*	Slope radians	Shear Force lbs	Bending Stiffness lb-in^2	Soil Stress P lb/in
0.00	1.5000	4380000.	23338.	-0.004687	0.000	1.341E+12		
0.000	0.000	0.000	23338.	-0.004643	0.000	1.341E+12		
0.000	1.078	1.4396	4681982.					
0.000	0.000	0.000						

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2.157	1.3798	4983964.	0.000	1.339E+12				
0.000	0.000	0.000	23338.	-0.004596	0.000	1.338E+12		
3.235	1.3207	5285946.	0.000	1.338E+12				
0.000	0.000	0.000	23338.	-0.004494	0.000	1.337E+12		
4.313	1.2622	5587928.	0.000	4.238E+11				
0.000	0.000	0.000	23338.	-0.004377	0.000	4.190E+11		
5.392	1.2044	5889909.	0.000	4.188E+11				
0.000	0.000	0.000	23338.	-0.003995	0.000	4.186E+11		
6.470	1.1489	6191891.	0.000	4.184E+11				
0.000	0.000	0.000	23338.	-0.003790	0.000	4.184E+11		
7.548	1.0959	6493873.	0.000	4.184E+11				
0.000	0.000	0.000	23338.	-0.003575	0.000	4.184E+11		
8.626	1.0455	6795855.	0.000	4.184E+11				
0.000	0.000	0.000	23338.	-0.003445	0.000	4.184E+11		
9.705	0.9978	7097837.	0.000	4.184E+11				
0.000	0.000	0.000	23338.	-0.003403	0.000	4.184E+11		
10.783	0.9530	7399819.	0.000	4.184E+11				
0.000	0.000	0.000	23338.	-0.003359	0.000	4.184E+11		
11.861	0.9087	7701801.	0.000	4.184E+11				
0.000	0.000	0.000	23338.	-0.003314	0.000	4.184E+11		
12.940	0.8649	8003783.	0.000	4.184E+11				
0.000	0.000	0.000	23338.	-0.003266	0.000	4.184E+11		
14.018	0.8218	8305765.	0.000	4.184E+11				
0.000	0.000	0.000	23338.	-0.003218	0.000	4.184E+11		
15.096	0.7792	8607746.	0.000	4.184E+11				
0.000	0.000	0.000	23338.	-0.003167	0.000	4.184E+11		
16.174	0.7372	8909728.	0.000	4.184E+11				
0.000	0.000	0.000	23338.	-0.003115	0.000	4.184E+11		
17.253	0.6959	9211710.	0.000	4.184E+11				
0.000	0.000	0.000	23338.	-0.003061	0.000	4.184E+11		
18.331	0.6553	9513692.	0.000	4.184E+11				
0.000	0.000	0.000	23338.	-0.002995	0.000	4.184E+11		
19.409	0.6153	9815674.	0.000	4.184E+11				
0.000	0.000	0.000	23338.	-0.002914	0.000	4.184E+11		
20.488	0.5760	10117656.	0.000	4.184E+11				
0.000	0.000	0.000	23338.	-0.002827	0.000	4.184E+11		
21.566	0.5378	10419638.	0.000	4.184E+11				
0.000	0.000	0.000	23338.	-0.002737	0.000	4.184E+11		
22.644	0.5006	10721620.	0.000	4.184E+11				
0.000	0.000	0.000	23338.	-0.002645	0.000	4.184E+11		
23.723	0.4646	11023601.	0.000	4.184E+11				
0.000	0.000	0.000	23338.	-0.002549	0.000	4.184E+11		
24.801	0.4298	11325583.	0.000	4.184E+11				
0.000	0.000	0.000	23338.	-0.002452	0.000	4.184E+11		
25.879	0.3962	11627565.	0.000	4.184E+11				
0.000	0.000	0.000	23338.	-0.002351	0.000	4.184E+11		
26.957	0.3638	11929547.	0.000	4.184E+11				
0.000	0.000	0.000	23338.	-0.002248	0.000	4.184E+11		
28.036	0.3327	12231529.	0.000	4.184E+11				
0.000	0.000	0.000	23338.	-0.002143	0.000	4.184E+11		
29.114	0.3030	12533511.	0.000	4.184E+11				
0.000	0.000	0.000	23066.	-0.002035	0.000	4.184E+11		
30.192	0.2745	12835493.	0.000	4.184E+11				
0.000	0.000	0.000	21813.	-0.001925	0.000	4.184E+11		
31.271	0.2475	13137475.	0.000	4.184E+11				
-42.077	0.2199	8195190.	0.000	4.184E+11				
32.349	0.1939	8537219.	0.000	4.184E+11				
-151.373	0.1687	88837397.	0.000	4.184E+11				
33.427	0.1437	92357687.	0.000	4.184E+11				
-262.362	0.1187	95877977.	0.000	4.184E+11				
34.505	0.0937	99398267.	0.000	4.184E+11				
-368.810	0.0687	102918157.	0.000	4.184E+11				
35.583	0.0437	106438047.	0.000	4.184E+11				
9670.0323	0.0187	14091455.	0.000	4.184E+11				

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Pier 32aff.1p7o		Pier 32aff.1p7o	
39.897	0.1233	17827409.	0.000
-739.3724	77562.	0.000	1.556E+12
40.975	0.1041	17546887.	0.000
-740.4139	92077.	0.000	1.556E+12
42.054	0.0866	17142395.	0.000
-700.1489	104566.	0.000	1.556E+12
43.132	0.0711	16620676.	0.000
-629.5423	114612.	0.000	1.557E+12
44.210	0.0573	13993549.	0.000
-551.9893	124658.	0.000	1.557E+12
-470.9479	134704.	0.000	1.557E+12
-389.5538	144750.	0.000	1.558E+12
-304.7766	151893.	0.000	1.558E+12
48.524	0.0260	13611978.	0.000
-169.3930	0.0186	12697324.	0.000
-236.5222	164842.	0.000	1.559E+12
-169.3930	174888.	0.000	1.559E+12
-110.9184	184934.	0.000	1.560E+12
-62.4396	194980.	0.000	2.317E+12
-19.5180	205026.	0.000	2.319E+12
17.4286	215072.	0.000	2.321E+12
48.2120	225118.	0.000	2.323E+12
406.7509	1312699.	0.000	2.325E+12
446.7156	1195253.	0.000	2.327E+12
58.228	-0.005319	3919953.	0.000
468.4752	1139731.	0.000	2.329E+12
477.2353	1118807.	0.000	2.330E+12
476.1688	1121310.	0.000	2.332E+12
61.463	-0.005295	1811738.	0.000
467.4456	1142232.	0.000	2.333E+12
62.541	-0.004966	1267052.	0.000
452.6681	1179517.	0.000	2.334E+12
63.620	-0.004545	798157.	0.000
433.0829	1232855.	0.000	2.334E+12
64.698	-0.004068	401774.	0.000
409.6955	1303228.	0.000	2.334E+12
65.776	-0.003561	73989.	0.000
383.3416	1392818.	0.000	2.334E+12
354.7284	1505160.	0.000	2.334E+12
324.4612	1645362.	0.000	2.334E+12
293.0594	1821877.	0.000	2.334E+12
260.9638	2045935.	0.000	2.334E+12
228.5352	2336230.	0.000	2.334E+12
196.0400	2723451.	0.000	2.334E+12
73.324	-0.000649	-706528.	0.000
163.6090	3263253.	0.000	2.334E+12
74.403	-0.000417	-665167.	0.000
131.1322	4071352.	0.000	2.334E+12
75.481	-0.000232	-601850.	0.000
76.3045	4246668.	0.000	2.334E+12
76.559	-9.141E-05	-525758.	0.000
30.2369	4280155.	0.000	2.334E+12
77.638	1.196E-05	-444602.	0.000
-3.9871	4313641.	0.000	2.334E+12
78.716	8.344E-05	-364115.	0.000
-28.0304	4347128.	0.000	2.334E+12
79.794	0.000129	-288320.	0.000
-43.6005	4380615.	0.000	2.334E+12
-52.3493	4414101.	0.000	2.334E+12
-80.873	0.000153	-219826.	0.000
-81.951	0.000162	-160096.	0.000
-55.8052	4447588.	0.000	2.334E+12
-55.3297	4481075.	-109711.	0.000
84.107	0.000149	0.000	2.334E+12
-52.0948	4514561.	0.000	2.334E+12
-47.0762	4548048.	0.000	2.334E+12
-41.0589	4581535.	0.000	2.334E+12
-34.6498	4615021.	-11673.	0.000
87.342	9.715E-05	5970.0227	0.000
88.421	7.877E-05	17811.	0.000
-28.2972	4648508.	0.000	2.334E+12
-22.3118	4681995.	24914.	0.000
-16.8893	4715481.	28282.	0.000
-12.1321	4748968.	28821.	0.000
92.734	2.184E-05	27329.	0.000
-8.0703	4782455.	0.000	2.334E+12
93.812	1.257E-05	24486.	0.000
-4.6801	4815941.	20860.	0.000
-1.9004	4849428.	0.000	2.334E+12
0.3535	4882915.	16915.	0.000
2.1774	4916401.	13029.	0.000
3.6686	4949688.	9508.4234	0.000
4.9170	4983374.	6601.6485	0.000
5.9982	5016861.	4518.1370	0.000
101.360	-1.785E-05	3438.9230	0.000
0.6744	4888393.	9.000	2.334E+12
0.7873	509786.	9.000	2.334E+12
0.8998	5307194E-05	1638.1364	0.000
1.0459	55367376E-05	984.3052	0.000
1.1036	55164355E-05	400.1878	0.000
1.1304	673575355E-05	0.000	2.334E+12
1.1306	75257728E-05	115.3316	0.000
1.2514	5953505.	0.000	2.334E+12

107.830 -2.901E-05 0.000 0.000 -1.337E-07 0.000 2.334E+12
 1.3776 307217. 0.000

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* This analysis computed pile response using nonlinear moment-curvature relationships. Values of total stress due to combined axial and bending stresses are computed only for elastic sections only and do not equal the actual stresses in concrete and steel. Stresses in concrete and steel may be interpolated from the output for nonlinear bending properties relative to the magnitude of bending moment developed in the pile.

Output Summary for Load Case No. 8:
 Pile-head deflection = 2.0000000 inches
 Computed slope at pile head = -0.0061147 radians
 Maximum bending moment = 18021438. inch-lbs
 Maximum shear force = -78322. lbs
 Depth of maximum bending moment = 37.7405000 feet below pile head
 Depth of maximum shear force = 53.9150000 feet below pile head
 Number of iterations = 35
 Number of zero deflection points = 3

Computed Values of Pile Loading and Deflection
 for Lateral Loading for Load Case Number 9

Pile-head conditions are Shear and Moment (Loading Type 1)

Res. X	Soil Spr. y	Deflect. Lat. Load lb/inch	Bending Moment in-lbs	Shear Force lbs	Slope radians	Total Stress psi*	Bending Stiffness lb-in^2	Soil P lb/in
0.000	0.000	1.9216	7818000.	21300.	-0.007232	0.000	4.180E+11	
0.000	1.078	1.8296	8093613.	21300.	-0.006986	0.000	4.180E+11	
0.000	2.157	1.7408	8389227.	21300.	-0.006731	0.000	4.177E+11	
0.000	3.235	1.6554	8644840.	21300.	-0.006467	0.000	4.176E+11	
0.000	4.313	1.5734	8920454.	21300.	-0.006195	0.000	4.174E+11	
0.000	5.392	1.4951	9196067.	21300.	-0.005914	0.000	4.172E+11	
0.000	6.470	1.4204	9471681.	21300.	-0.005624	0.000	4.171E+11	
0.000	7.548	1.3495	9747294.	21300.	-0.005326	0.000	4.169E+11	
0.000	8.626	1.2825	10022908.	21300.	-0.005019	0.000	4.168E+11	

0.000	9.705	0.000	1.2196	10298521.	21300.	-0.004704	0.000	4.166E+11
0.000	10.783	0.000	1.1608	10574135.	21300.	-0.004501	0.000	4.157E+11
0.000	11.861	0.000	1.1031	10849748.	21300.	-0.004412	0.000	4.1560E+11
0.000	12.940	0.000	1.0466	11125362.	21300.	-0.004321	0.000	4.1560E+11
0.000	14.018	0.000	0.9913	11400975.	21300.	-0.004227	0.000	4.1559E+11
0.000	15.096	0.000	0.9372	11676589.	21300.	-0.004132	0.000	4.1559E+11
0.000	16.174	0.000	0.8844	11952202.	21300.	-0.004034	0.000	4.1559E+11
0.000	17.253	0.000	0.8328	12227816.	21300.	-0.003933	0.000	4.1559E+11
0.000	18.331	0.000	0.7826	12503429.	21300.	-0.003831	0.000	4.1559E+11
0.000	19.409	0.000	0.7337	12779043.	21300.	-0.003726	0.000	4.1559E+11
0.000	20.488	0.000	0.6862	13054656.	21300.	-0.003618	0.000	4.1558E+11
0.000	21.566	0.000	0.6401	13330270.	21300.	-0.003509	0.000	4.1558E+11
0.000	22.644	0.000	0.5954	13605883.	21300.	-0.003397	0.000	4.1558E+11
0.000	23.723	0.000	0.5522	13881497.	21300.	-0.003283	0.000	4.1558E+11
0.000	24.801	0.000	0.5104	14157110.	21300.	-0.003166	0.000	4.1558E+11
0.000	25.879	0.000	0.4702	14432724.	21300.	-0.003048	0.000	4.1558E+11
0.000	26.957	0.000	0.4315	14708337.	21300.	-0.002927	0.000	4.1558E+11
0.000	28.036	0.000	0.3945	14983950.	21300.	-0.002803	0.000	4.1557E+11
0.000	29.114	0.000	0.3590	15259564.	21300.	-0.002678	0.000	4.1557E+11
0.000	30.192	0.000	0.3252	15535177.	21300.	-0.002550	0.000	4.1557E+11
0.000	31.271	0.2930	15810791.	15810791.	21015.	-0.002420	0.000	4.1557E+11
-43.9866	1942.4730	0.000	16079040.	16079040.	19704.	-0.002287	0.000	4.1557E+11
-158.6868	7820.6307	0.000	16320719.	16320719.	16895.	-0.002152	0.000	4.1557E+11
-275.5418	15248.	0.000	16516263.	16516263.	12606.	-0.002016	0.000	4.1557E+11
-387.3567	24231.	0.000	16646951.	16646951.	6953.2797	-0.001878	0.000	4.1557E+11
-486.3466	34643.	0.000	16696208.	16696208.	144.2605	-0.001739	0.000	4.1557E+11
-566.0846	46287.	0.000	16850684.	16850684.	-7578.9636	-0.001601	0.000	4.1557E+11
-627.6500	59438.	0.000	16900071.	16900071.	-15946.	-0.001463	0.000	4.1557E+11
-665.5677	73722.	0.000	16938019.	16938019.	-24424.	-0.001327	0.000	4.1557E+11
-644.8526	84474.	0.000	15868001.	15868001.	-32494.	-0.001194	0.000	4.1557E+11
-602.4657	94520.	0.000	15397110.	15397110.	-39941.	-0.001064	0.000	4.1557E+11
-548.5815	104366.	0.000						

Pier 32aff.lp7o			Pier 32aff.lp7o			
31.271	0.1205	8507732.	0.000	2.320E+12	0.000	2.334E+12
-34.8238	3739.3251	0.000	0.000	2.319E+12	-0.000	2.334E+12
32.349	0.1089	8644237.	0.000	2.319E+12	0.000	2.334E+12
-119.0626	14152	0.000	0.000	2.319E+12	-0.000	2.334E+12
33.427	0.0978	8760807.	0.000	2.319E+12	0.000	2.334E+12
-182.9810	24198	0.000	0.000	2.319E+12	-0.000	2.334E+12
34.506	0.0875	8846740.	0.000	2.319E+12	0.000	2.334E+12
-231.4677	34244	0.000	0.000	2.319E+12	-0.000	2.334E+12
35.584	0.0777	8893917.	0.000	2.319E+12	0.000	2.334E+12
-266.0171	44290	0.000	0.000	2.319E+12	-0.000	2.334E+12
36.662	0.0686	8896555.	0.000	2.319E+12	0.000	2.334E+12
-288.1314	54336	0.000	0.000	2.319E+12	-0.000	2.334E+12
37.741	0.0602	8850949.	0.000	2.319E+12	0.000	2.334E+12
-299.3072	64382	0.000	0.000	2.319E+12	-0.000	2.334E+12
38.819	0.0523	8755230.	0.000	2.319E+12	0.000	2.334E+12
-301.0216	74428	0.000	0.000	2.319E+12	-0.000	2.334E+12
39.897	0.0451	8609109.	0.000	2.320E+12	0.000	2.334E+12
-294.7175	84474	0.000	0.000	2.320E+12	-0.000	2.334E+12
40.975	0.0386	8413644.	0.000	2.320E+12	0.000	2.334E+12
-281.7894	94520	0.000	0.000	2.320E+12	-0.000	2.334E+12
42.054	0.0326	8170997.	0.000	2.320E+12	0.000	2.334E+12
-263.5700	104566	0.000	0.000	2.320E+12	-0.000	2.334E+12
43.132	0.0272	7884219.	0.000	2.321E+12	0.000	2.334E+12
-241.3175	114612	0.000	0.000	2.321E+12	-0.000	2.334E+12
44.210	0.0224	7557038.	0.000	2.322E+12	0.000	2.334E+12
-216.2046	124658	0.000	0.000	2.322E+12	-0.000	2.334E+12
45.289	0.0182	7193656.	0.000	2.322E+12	0.000	2.334E+12
-189.3085	134704	0.000	0.000	2.323E+12	-0.000	2.334E+12
46.367	0.0144	6798578.	0.000	2.324E+12	0.000	2.334E+12
-161.6035	144750	0.000	0.000	2.324E+12	-0.000	2.334E+12
47.445	0.0112	6376442.	0.000	2.325E+12	0.000	2.334E+12
-133.9552	154796	0.000	0.000	2.325E+12	-0.000	2.334E+12
48.524	0.008408	5931877.	0.000	2.326E+12	0.000	2.334E+12
-107.1150	164842	0.000	0.000	2.326E+12	-0.000	2.334E+12
49.602	0.006046	5469378.	0.000	2.327E+12	0.000	2.334E+12
-81.7177	174888	0.000	0.000	2.327E+12	-0.000	2.334E+12
50.680	0.004078	4993197.	0.000	2.328E+12	0.000	2.334E+12
-58.2802	184934	0.000	0.000	2.328E+12	-0.000	2.334E+12
51.758	0.002469	4507257.	0.000	2.329E+12	0.000	2.334E+12
-37.2009	194980	0.000	0.000	2.329E+12	-0.000	2.334E+12
52.837	0.001184	4015089.	0.000	2.329E+12	0.000	2.334E+12
-18.7603	205026	0.000	0.000	2.329E+12	-0.000	2.334E+12
53.915	0.000188	3519780.	0.000	2.331E+12	0.000	2.334E+12
-3.1232	215072	0.000	0.000	2.331E+12	-0.000	2.334E+12
54.993	0.000555	3023948.	0.000	2.331E+12	0.000	2.334E+12
9.6592	225118	0.000	0.000	2.331E+12	0.000	2.334E+12
56.072	0.001081	2529733.	0.000	2.332E+12	0.000	2.334E+12
211.6652	2533470.	0.000	0.000	2.332E+12	0.000	2.334E+12
57.150	0.001425	2070958.	0.000	2.332E+12	0.000	2.334E+12
242.9119	2205328.	0.000	0.000	2.333E+12	0.000	2.334E+12
58.228	-0.001621	1652854.	0.000	2.333E+12	0.000	2.334E+12
258.9848	2067618.	0.000	0.000	2.334E+12	0.000	2.334E+12
59.306	0.001698	1278113.	0.000	2.334E+12	0.000	2.334E+12
265.0351	2020070.	0.000	0.000	2.334E+12	0.000	2.334E+12
60.385	-0.001683	947748.	0.000	2.334E+12	0.000	2.334E+12
263.8717	2028874.	0.000	0.000	2.334E+12	0.000	2.334E+12
61.463	-0.001600	661564.	0.000	2.334E+12	0.000	2.334E+12
257.3036	2080719.	0.000	0.000	2.334E+12	0.000	2.334E+12
62.541	-0.001470	418461.	0.000	2.334E+12	0.000	2.334E+12
246.6201	2171033.	0.000	0.000	2.334E+12	0.000	2.334E+12
63.620	-0.001510	216650.	0.000	2.334E+12	0.000	2.334E+12
232.8027	2300183.	0.000	0.000	2.334E+12	0.000	2.334E+12
64.698	-0.001134	53818.	0.000	2.334E+12	0.000	2.334E+12

216.6326	2472293.	0.000	-8494.9791	1.368E-05	0.000	2.334E+12		
65.776	-0.000954	198.7500	2695303.	0.000	-166025.	0.000	2.334E+12	
66.855	-0.000780	179.6881	2981980.	0.000	-229222.	0.000	2.334E+12	
67.933	-0.000617	159.8905	3352212.	0.000	-265649.	0.000	2.334E+12	
69.011	-0.000471	139.7163	3837633.	0.000	-278682.	0.000	2.334E+12	
70.090	-0.000344	108.4653	4079235.	0.000	-273554.	0.000	2.334E+12	
71.168	-0.000237	75.3344	4112722.	0.000	1681.2200	6.046E-06	0.000	2.334E+12
72.246	-0.000150	47.9378	4146208.	0.000	2159.6912	4.700E-06	0.000	2.334E+12
73.324	-8.054E-05	26.0168	4179695.	0.000	2386.9663	3.508E-06	0.000	2.334E+12
74.403	-2.798E-05	9.1119	4213182.	0.000	2424.1925	2.487E-06	0.000	2.334E+12
75.481	1.023E-05	-3.3580	4246668.	0.000	2324.6183	1.640E-06	0.000	2.334E+12
76.559	3.638E-05	-12.0326	4280153.	0.000	2133.1503	9.602E-07	0.000	2.334E+12
77.638	5.268E-05	-17.5615	4313641.	0.000	1886.4520	4.332E-07	0.000	2.334E+12
78.716	6.123E-05	-20.5692	4347128.	0.000	1613.4316	4.162E-08	0.000	2.334E+12
79.794	6.389E-05	-21.6300	4380615.	0.000	1335.9837	-2.343E-07	0.000	2.334E+12
80.873	6.230E-05	-21.2535	4414101.	0.000	1069.8781	-4.143E-07	0.000	2.334E+12
81.951	5.783E-05	-19.8769	4447588.	0.000	825.7087	-5.176E-07	0.000	2.334E+12
83.029	5.158E-05	-17.8630	4481075.	0.000	609.8384	-5.616E-07	0.000	2.334E+12
84.107	4.443E-05	-15.5029	4514561.	0.000	425.2930	-5.619E-07	0.000	2.334E+12
85.186	3.705E-05	-13.0213	4548048.	0.000	272.5729	-5.317E-07	0.000	2.334E+12
86.264	2.989E-05	-10.5838	4581535.	0.000	150.3649	-4.820E-07	0.000	2.334E+12
87.342	2.329E-05	-8.3052	4615021.	0.000	56.1455	-4.214E-07	0.000	2.334E+12
88.421	1.742E-05	-6.2578	4648508.	0.000	-13.3237	-3.568E-07	0.000	2.334E+12
89.499	1.238E-05	-4.4797	4681995.	0.000	-61.6042	-2.932E-07	0.000	2.334E+12
90.577	8.185E-06	-2.9827	4715481.	0.000	-92.2823	-2.340E-07	0.000	2.334E+12
91.656	4.793E-06	-1.7590	4748968.	0.000	-108.7543	-1.814E-07	0.000	2.334E+12
92.734	2.129E-06	-0.7870	4782455.	0.000	-114.0822	-1.366E-07	0.000	2.334E+12
93.812	9.812E-08	-0.0365	4815941.	0.000	-110.9083	-1.000E-07	0.000	2.334E+12
94.890	-1.406E-06	0.5271	4849428.	0.000	-101.4179	-7.138E-08	0.000	2.334E+12
95.969	2.490E-06	0.9398	4882915.	0.000	-87.3393	-5.002E-08	0.000	2.334E+12
97.047	-3.234E-06	1.2363	4916475.	0.000	-69.9737	-3.491E-08	0.000	2.334E+12
98.125	9.855E-06	1.4478	4949868.	0.000				

Pier 32aff.lp7o			
99.204	-4.157E-06	1426.1729	0.000
1.6011	4.983374	0.000	0.000
100.282	-4.427E-06	910.0232	0.000
1.7166	5.016861	0.000	0.000
101.360	-4.632E-06	681.2892	0.000
0.1750	4.88859	0.000	0.000
102.438	-4.788E-06	481.8580	0.000
0.1887	5.09788	0.000	0.000
103.517	-4.910E-06	314.0133	0.000
0.2014	5.30717	0.000	0.000
104.595	-5.009E-06	179.8860	0.000
0.2135	5.51647	0.000	0.000
105.673	-5.095E-06	81.5119	0.000
0.2254	5.72576	0.000	0.000
106.752	-5.175E-06	20.8847	0.000
0.2374	5.93505	0.000	0.000
107.830	-5.254E-06	0.000	0.000
0.2495	3.07217	0.000	0.000

* This analysis computed pile response using nonlinear moment-curvature relationships.
 Values of total stress due to combined axial and bending stresses are computed only for elastic sections only and do not equal the actual stresses in concrete and steel.
 Stresses in concrete and steel may be interpolated from the output for nonlinear bending properties relative to the magnitude of bending moment developed in the pile.

Output Summary for Load Case No. 10:
 Pile-head deflection = 0.6958919 inches
 Computed slope at pile head = -0.0021611 radians
 Maximum bending moment = 8896555. inch-lbs
 Maximum shear force = -38299. lbs
 Depth of maximum bending moment = 36.6622000 feet below pile head
 Depth of maximum shear force = 53.9150000 feet below pile head
 Number of iterations = 7
 Number of zero deflection points = 3

Results of Pile Buckling Analysis
 Computation Pile-head Loading Condition used for Pile Buckling Analyses
 Computations Used Shear and Moment Condition
 Pile-head deflection vs. Pile Length for Load Case 10
 Boundary Condition Type 1, Shear and Moment
 Shear = 11000. lb
 Moment = 4380000. in-lb
 Axial Load = 0. lb

Pier 32aff.lp7o			
Pile Length feet	Pile Head Deflection inches	Maximum Moment In-lbs	Maximum Shear lbs
107.8300	0.6958919	8896555.	-38299.
102.4385	0.6951013	8903139.	-38173.
97.0470	0.6959158	8900401.	-38169.
91.6555	0.6942844	8896698.	-38357.
86.2640	0.6951490	8901199.	-38265.
80.8725	0.6959999	8902508.	-37959.
75.4810	0.6962323	8901952.	-38291.
70.0895	0.6964632	8902254.	-37915.
64.6980	0.7006732	8894894.	-40370.
59.3065	0.7613014	8865442.	-47149.
53.9150	1.3031333	8816877.	-63702.
48.5235	6.1818095	8737712.	-92329.

Summary of Pile Response(s)

Definitions of Pile-head Loading Conditions:
 Load Type 1: Load 1 = Shear, lbs, and Load 2 = Moment, in-lbs
 Load Type 2: Load 1 = Shear, lbs, and Load 2 = Slope, radians
 Load Type 3: Load 1 = Shear, lbs, and Load 2 = Rotational Stiffness, in-lbs/radian
 Load Type 4: Load 1 = Top Deflection, inches, and Load 2 = Moment, in-lbs
 Load Type 5: Load 1 = Top Deflection, inches, and Load 2 = Slope, radians

Load Case No.	Type	Maximum Shear in Pile lbs	Pile-head		Axial Loading lbs	Pile-head Deflection inches	Maximum Moment in Pile in-lbs
			Condition 1 Pile-head v(inches) or Rotation in-lb/rad. radians	Condition 2 Pile-head v(inches) or in-lb, rad., Rotation in-lb/rad. radians			
1	4	y = 0.5000	M = 7818000.		0.0000000	0.5000000	
2	4	y = -20013.	M = -0.00327536		0.0000000	1.0000000	
3	4	y = 1.0000	M = 7818000.		0.0000000	1.5000000	
4	4	y = -43091.	M = -0.00465229		0.0000000	2.0000000	
5	4	y = 1.5000	M = 7818000.		0.0000000	2.5000000	
6	4	y = -56014.	M = -0.00606664		0.0000000	3.0000000	
7	4	y = 2.0000	M = 7818000.		0.0000000	3.5000000	
8	4	y = -73950.	M = -0.00743695		0.0000000	4.0000000	
9	4	y = 0.5000	M = 4380000.		0.0000000	4.5000000	
10	4	y = -27076.	M = -0.00167107		0.0000000	5.0000000	
11	4	y = 1.0000	M = 4380000.		0.0000000	5.5000000	
12	4	y = -46888.	M = -0.00308795		0.0000000	6.0000000	
13	4	y = 1.5000	M = 4380000.		0.0000000	6.5000000	
14	4	y = -60788.	M = -0.00468652		0.0000000	7.0000000	
15	4	y = 2.0000	M = 4380000.		0.0000000	7.5000000	
16	4	y = -78322.	M = -0.00611469		0.0000000	8.0000000	
17	4	y = 2.5000	M = 4380000.		0.0000000	8.5000000	
18	4	y = -96766.	M = -0.00773180		0.0000000	9.0000000	
19	4	y = 3.0000	M = 4380000.		0.0000000	9.5000000	
20	4	y = -115210.	M = -0.00945991		0.0000000	10.0000000	

SAR-1 " < 1.0
 Δ = 0.70 δk

0.69589191

Pier 32aff.lp70
 10 1 V = 11000. M = 4380000. 0.00000000
 8896555. -38299. -0.00216110

Results of Pile Buckling Analysis

Maximum Compression Loading for Pile Buckling Analysis = 698600. lb

Pile-head Condition 0, Shear Force and Moment

Shear = 14000. lb
 Moment = 9502800. in-lb

Trial Thrust Number	Axial Thrust lbs	Pile Head Deflection inches	Maximum Moment in-lbs	Maximum Shear lbs
1	0.0000	1.76670	15227966.	-63426.
2	14257.	1.76925	15250930.	-63527.
3	28514.	1.77181	15273960.	-63628.
4	42771.	1.77438	15297055.	-63729.
5	57029.	1.77695	15320216.	-63830.
6	71286.	1.77953	15343443.	-63932.
7	85543.	1.78212	15366736.	-64034.
8	99800.	1.78472	15390097.	-64137.
9	114057.	1.78732	15413526.	-64240.
10	128314.	1.78994	15437021.	-64343.
11	142571.	1.79255	15460583.	-64446.
12	156829.	1.79518	15484214.	-64549.
13	171086.	1.79782	15507914.	-64653.
14	185343.	1.80046	15531682.	-64757.
15	199600.	1.80311	15555519.	-64862.
16	213857.	1.80577	15579424.	-64968.
17	228114.	1.80843	15603399.	-65074.
18	242371.	1.81111	15627445.	-65180.
19	256629.	1.81379	15651560.	-65287.
20	270886.	1.81645	15675743.	-65393.
21	285143.	1.81911	15699993.	-65500.
22	299400.	1.82178	15724316.	-65607.
23	313657.	1.82446	15748708.	-65714.
24	327914.	1.82714	15773168.	-65822.
25	342171.	1.82983	15797702.	-65930.
26	356429.	1.83253	15822307.	-66038.
27	370686.	1.83524	15846984.	-66146.
28	384943.	1.83795	15871733.	-66255.
29	399200.	1.84067	15896554.	-66364.
30	413457.	1.84340	15921448.	-66474.
31	427714.	1.84614	15946414.	-66583.
32	441971.	1.85001	15971736.	-66718.
33	456229.	1.85548	15997384.	-66890.
34	470486.	1.86096	16023368.	-67061.
35	484743.	1.86613	16049599.	-67227.
36	499000.	1.86898	16075056.	-67340.
37	513257.	1.87183	16100592.	-67453.
38	527514.	1.87470	16126203.	-67567.
39	541771.	1.87756	16151889.	-67681.
40	556029.	1.88044	16177657.	-67795.
41	570286.	1.88333	16203500.	-67910.
42	584543.	1.88623	16229421.	-68025.
43	598800.	1.88913	16255423.	-68140.

Pier 32aff.lp70
 1.89206 16281508. -68256.
 1.89504 16307684. -68373.
 1.89802 16333942. -68491.
 1.90102 16360281. -68608.
 1.90402 16386702. -68726.
 1.90704 16413204. -68844.
 1.91006 16439788. -68963.

Maximum moment is 40.70% of the plastic moment capacity of pile section 1

Hyperbolic Fit of Pile Buckling Behavior: Thrust Force = $[y - y(1)] / (b + a[y - y(1)])$

Pile buckling capacity estimated from hyperbolic curve = 4316155. lb
 Maximum axial thrust from analysis = 698600. lb

Axial Buckling capacity is limited by the axial structural capacity of the pile.

Axial Buckling capacity is limited by the peak axial thrust reached in the buckling analysis.

Fitting parameter a (slope) = 2.3169E-07 lb
 Fitting parameter b (intercept) = 1.7439E-07 lb
 Lateral pile deflection at zero axial thrust, y(1) = 1.76670 in
 R Squared = 0.87777

Note: The axial buckling capacity is a function of pile-head loading, pile-head fixity conditions, pile embedment, pile dimensions and stiffness, and local soil conditions. It is recommended that all analyses of pile buckling be performed using the maximum pile-head loads expected for the structure in order to compute the most conservative estimate of pile buckling capacity.

The pile buckling capacity estimated from the hyperbolic curve fitting method usually over-estimates the pile buckling capacity for nonlinear piles because buckling capacity may be controlled by the development of a plastic hinge in the pile. Please check the magnitude of maximum moment developed in the pile and compare the value to the plastic moment capacity for the pile. If the values are close, report the buckling capacity as the last computed value of axial thrust for which a solution was reported.

The analysis ended normally.

PIER 1

Worst Case	Limit State	Load Case	Column	Top/Bot	M _u (k-ft)	P _u (k)	V _u (k)
Max P _u	STR-I	1/2/3	1	T	540.1	777.5	
	SER-I	1/2/3	1	T	248.8	516.1	
Max V _u	STR-I	26	3	T	458.3		13.6
	SER-I	28	4	T	65.3		9.9

PIER 2

Worst Case	Limit State	Load Case	Column	Top/Bot	M _u (k)	P _u (k)	V _u (k)
Max P _u	STR-I	2	4	T	252.0	689.2	
	SER-I	1/3	1	T	132.4	464.8	
Max V _u	STR-V	28	4	T	115.2		8.8
	SER-I	28	4	T	98.6		8.7

PIER 3

Worst Case	Limit State	Load Case	Column	Top/Bot	M _u (k)	P _u (k)	V _u (k)
Max P _u	STR-I	4	4	T	141.4	688.3	
	SER-I	4	1	T	218.4	500.6	
Max V _u	STR-III	25	2	T	651.5		21.3
	SER-I	26	3	T	365.0		11.0

Handwritten note: R_R = 695 k

PIER 4

Worst Case	Limit State	Load Case	Column	Top/Bot	M _u (k)	P _u (k)	V _u (k)
Max P _u	STR-I	1/2/3	1	T	377.0	709.1	
	SER-I	1/2/3	1	T	185.3	475.0	
Max V _u	STR-I	26	4	T	316.1		9.8
	SER-I	26	4	T	270.7		8.4

PIER 3
 4' φ, 3/4" STEEL CASING @ EL -1.0
 DEFLECTION
 STR III (lbs)
 SER-2 (lbs)

0.5	-6580	4,862
1.0	6374	15,799 ←
1.5	13,628	23,338
2.0	22,810	32,016

PIER 3 ↑

~~4' φ, 3/4" STEEL CASING @ EL -1.0
 DEFLECTION
 STR III (lbs)
 SER-1 (lbs)~~

0.5	-5902	7,173
1.0	6973	18,443 ←
1.5	14,286	26,371
2.0	23,443 ←	34,639

↑ CONTROLS

GEOTECHNICAL AXIAL CAPACITY
 = 695^k > 688^k OK

LATERAL CAPACITY 2" DEFLECTION (STR III)
 22.81^k > 21.3^k OK ← CONTROLS

LATERAL CAPACITY 1" DEFLECTION (SER-2)
 15.79^k > 11.0^k

PIER 4

Boring No. JS-7

By: SJM

Chk: *AT*
OG Elev. =

11.00

Sample No.	Depth of SS run (ft)	N-Values Field	q' _v (ksf)	C _N	N _{CORR}
2	4	55	0.190	1.788	98
3	6	4	0.286	1.653	7
4	8	5	0.381	1.556	8
5	10	3	0.476	1.482	4
6	12	16	0.571	1.421	23
7	14	4	0.666	1.369	5
8	16	8	0.762	1.325	11
9	18	5	0.857	1.285	6
11	22	9	1.047	1.218	11
12	24	9	1.142	1.189	11
13	26	13	1.238	1.162	15
14	28	24	1.333	1.138	27
15	30	34	1.428	1.114	38
16	32	20	1.523	1.093	22
17	34	23	1.618	1.073	25
18	36	22	1.714	1.053	23
19	38	20	1.809	1.035	21
20	40	40	1.904	1.018	41
21	43	42	2.047	0.994	42
22	48	21	2.286	0.957	20
23	53	11	2.523	0.924	10
24	58	14	2.761	0.894	13
25	63	48	2.999	0.866	42
26	68	62	3.237	0.841	52
27	73	95	3.475	0.817	78
28	78	75	3.713	0.795	60
29	83	49	3.951	0.774	38
30	88	55	4.189	0.755	42
31	93	40	4.427	0.736	29
32	98	94	4.665	0.719	68

GWT= 5.0
γ = 110 lb/ft³
γ' = 47.6 lb/ft³

N_{avg} (Below BFE) = 27
(Ref. AASHTO Eqn 10.4.6.2.4-1)

C_N = 0.77xlog(40/q'_v)
N_{CORR} = N_{Field} x C_N

LAGER

Boring No. JS-8

By: SJM

Chk: *AT*
OG Elev. =

1.00

Sample No.	Depth of SS run (ft)	N-Values Field	q' _v (ksf)	C _N	N _{CORR}
2	2	8	0.095	2.020	16
3	4	2	0.190	1.788	4
4	6	3	0.286	1.653	5
5	8	21	0.381	1.556	33
6	10	15	0.476	1.482	22
7	12	17	0.571	1.421	24
8	14	16	0.666	1.369	22
9	16	15	0.762	1.325	20
10	18	11	0.857	1.285	14
11	23	16	1.095	1.203	19
12	28	10	1.333	1.138	11
13	33	22	1.571	1.083	24
14	38	28	1.809	1.035	29
15	43	28	2.047	0.994	28
16	48	27	2.286	0.957	26
17	53	27	2.523	0.924	25
18	58	28	2.761	0.894	25
19	63	47	2.999	0.866	41
20	68	42	3.237	0.841	35
21	73	0	3.475	0.817	0
22	78	79	3.713	0.795	63
23	83	85	3.951	0.774	66
24	88	50	4.189	0.755	38
25	93	50	4.427	0.736	37
26	98	50	4.665	0.719	36

GWT= 5.0

①

②

③

④

⑤

⑥

IGNORE

N_{avg} (Below BFE) = 28
(Ref. AASHTO Eqn 10.4.6.2.4-1)

C_N = 0.77xlog(40/q'_v)
N_{CORR} = N_{Field} x C_N

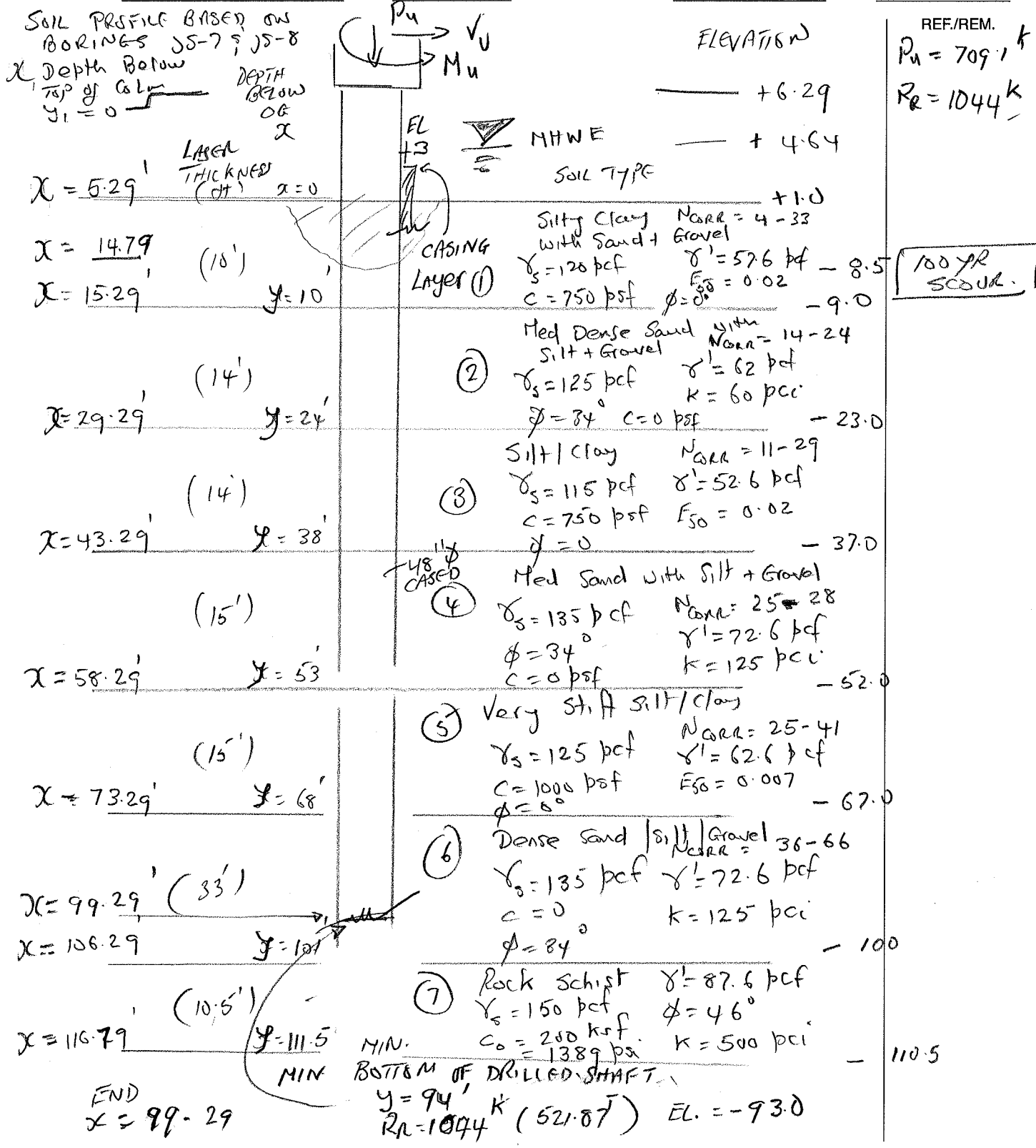
PROJECT BR1-159 JOB NO. _____ SHEET NO. 1 OF 1

LOCATION PIER 4

SUBJECT SOIL PROFILE (JS-7 & JS-8) (AXIAL & LATERAL CAPACITIES)

DESIGNED BY SJM DATE 7/14 CHECKED BY AT DATE 8/14

REVISED BY _____ DATE _____ BACK CHECKED BY _____ DATE _____



AXIAL CAPACITY

Pier 41.sfo
 STRENGTH REDUCTION FACTOR-ALPHA = 0.550E+00
 END BEARING COEFFICIENT-NC = 0.800E+01
 UNDRAINED SHEAR STRENGTH, LB/SQ FT = 0.750E+03
 INTERNAL FRICTION ANGLE, DEG. = 0.000E+00
 BLOWS PER FOOT FROM STANDARD PENETRATION TEST = 0.120E+03
 SOIL UNIT WEIGHT, LB/CU FT = 0.100E+11
 MAXIMUM LOAD TRANSFER FOR SOIL, LB/SQ FT DEPTH, FT = 0.100E+02

LRFD RESISTANCE FACTOR (SIDE FRICTION) = 0.450E+00
 LRFD RESISTANCE FACTOR (TIP RESISTANCE) = 0.400E+00

LAYER NO 2----SAND
 AT THE TOP
 SKIN FRICTION COEFFICIENT- BETA = 0.107E+01
 UNDRAINED SHEAR STRENGTH, LB/SQ FT = 0.000E+00
 INTERNAL FRICTION ANGLE, DEG. = 0.340E+02
 BLOWS PER FOOT FROM STANDARD PENETRATION TEST = 0.000E+00
 SOIL UNIT WEIGHT, LB/CU FT = 0.125E+03
 MAXIMUM LOAD TRANSFER FOR SOIL, LB/SQ FT DEPTH, FT = 0.100E+11

AT THE BOTTOM
 SKIN FRICTION COEFFICIENT- BETA = 0.839E+00
 UNDRAINED SHEAR STRENGTH, LB/SQ FT = 0.000E+00
 INTERNAL FRICTION ANGLE, DEG. = 0.340E+02
 BLOWS PER FOOT FROM STANDARD PENETRATION TEST = 0.000E+00
 SOIL UNIT WEIGHT, LB/CU FT = 0.125E+03
 MAXIMUM LOAD TRANSFER FOR SOIL, LB/SQ FT DEPTH, FT = 0.240E+02

LRFD RESISTANCE FACTOR (SIDE FRICTION) = 0.550E+00
 LRFD RESISTANCE FACTOR (TIP RESISTANCE) = 0.500E+00

LAYER NO 3----CLAY
 AT THE TOP
 STRENGTH REDUCTION FACTOR-ALPHA = 0.550E+00
 END BEARING COEFFICIENT-NC = 0.800E+01
 UNDRAINED SHEAR STRENGTH, LB/SQ FT = 0.750E+03
 INTERNAL FRICTION ANGLE, DEG. = 0.000E+00
 BLOWS PER FOOT FROM STANDARD PENETRATION TEST = 0.000E+00
 SOIL UNIT WEIGHT, LB/CU FT = 0.115E+03
 MAXIMUM LOAD TRANSFER FOR SOIL, LB/SQ FT DEPTH, FT = 0.240E+02

AT THE BOTTOM
 STRENGTH REDUCTION FACTOR-ALPHA = 0.550E+00
 END BEARING COEFFICIENT-NC = 0.800E+01
 UNDRAINED SHEAR STRENGTH, LB/SQ FT = 0.750E+03
 INTERNAL FRICTION ANGLE, DEG. = 0.000E+00
 BLOWS PER FOOT FROM STANDARD PENETRATION TEST = 0.000E+00

Pier 41.sfo
 SHAFT for Windows, Version 2012.7.11
 Serial Number : 228741384
 VERTICALLY LOADED DRILLED SHAFT ANALYSIS
 (C) Copyright ENSOFT, Inc., 1987-2012
 All Rights Reserved

Path to file locations : Y:\bridges\DELDOT\BRI-159_JAMES ST
 BRIDGE\FOUNDATION REPORT\SHAFT Output : pier 41.sfd
 Name of input data file : pier 41.sfo
 Name of output file : pier 41.sfo
 Name of plot output file : pier 41.sfp
 Name of runtime file : Pier 41.sff

Time and date of Analysis
 Date: October 24, 2014 Time: 14:02:15

BRI-159 Pier 4
 PROPOSED DEPTH = 100.0 FT

NUMBER OF LAYERS = 7

WATER TABLE DEPTH = 0.0 FT.

SOIL INFORMATION
 LAYER NO 1----CLAY

AT THE TOP
 STRENGTH REDUCTION FACTOR-ALPHA = 0.550E+00
 END BEARING COEFFICIENT-NC = 0.800E+01
 UNDRAINED SHEAR STRENGTH, LB/SQ FT = 0.750E+03
 INTERNAL FRICTION ANGLE, DEG. = 0.000E+00
 BLOWS PER FOOT FROM STANDARD PENETRATION TEST = 0.120E+03
 SOIL UNIT WEIGHT, LB/CU FT = 0.100E+11
 MAXIMUM LOAD TRANSFER FOR SOIL, LB/SQ FT DEPTH, FT = 0.100E+02

AT THE BOTTOM
 STRENGTH REDUCTION FACTOR-ALPHA = 0.550E+00
 END BEARING COEFFICIENT-NC = 0.800E+01
 UNDRAINED SHEAR STRENGTH, LB/SQ FT = 0.750E+03
 INTERNAL FRICTION ANGLE, DEG. = 0.000E+00
 BLOWS PER FOOT FROM STANDARD PENETRATION TEST = 0.000E+00

Pier 41.sfo
LRFD RESISTANCE FACTOR (SIDE FRICTION)
LRFD RESISTANCE FACTOR (TIP RESISTANCE)

= 0.450E+00
= 0.400E+00

LAYER NO 6----SAND

AT THE TOP

SKIN FRICTION COEFFICIENT- BETA
UNDRAINED SHEAR STRENGTH, LB/SQ FT
INTERNAL FRICTION ANGLE, DEG.
BLOWS PER FOOT FROM STANDARD PENETRATION TEST
SOIL UNIT WEIGHT, LB/CU FT
MAXIMUM LOAD TRANSFER FOR SOIL, LB/SQ FT
DEPTH, FT

= 0.387E+00
= 0.000E+00
= 0.340E+02
= 0.000E+00
= 0.135E+03
= 0.100E+11
= 0.680E+02

AT THE BOTTOM

SKIN FRICTION COEFFICIENT- BETA
UNDRAINED SHEAR STRENGTH, LB/SQ FT
INTERNAL FRICTION ANGLE, DEG.
BLOWS PER FOOT FROM STANDARD PENETRATION TEST
SOIL UNIT WEIGHT, LB/CU FT
MAXIMUM LOAD TRANSFER FOR SOIL, LB/SQ FT
DEPTH, FT

= 0.250E+00
= 0.000E+00
= 0.340E+02
= 0.000E+00
= 0.135E+03
= 0.100E+11
= 0.101E+03

LRFD RESISTANCE FACTOR (SIDE FRICTION)
LRFD RESISTANCE FACTOR (TIP RESISTANCE)

= 0.550E+00
= 0.500E+00

LAYER NO 7----WEAK ROCK

AT THE TOP

DIAMETER OF SOCKET, FT
SLUMP OF CONCRETE, IN
ANGLE OF INTERFACE FRICTION, DEG.
UNIAXIAL COMPRESSION STRENGTH OF ROCK, LB/SQ FT
ELASTIC MODULUS FOR THE INTACT ROCK, LB/SQ IN.
ROCK QUALITY DESIGNATION (RQD) %
DEPTH, FT

= 0.350E+01
= 0.000E+00
= 0.000E+00
= 0.200E+06
= 0.497E+07
= 0.580E+02
= 0.101E+03

AT THE BOTTOM

DIAMETER OF SOCKET, FT
SLUMP OF CONCRETE, IN
ANGLE OF INTERFACE FRICTION, DEG.
UNIAXIAL COMPRESSION STRENGTH OF ROCK, LB/SQ FT
ELASTIC MODULUS FOR THE INTACT ROCK, LB/SQ IN.
ROCK QUALITY DESIGNATION (RQD) %
DEPTH, FT

= 0.350E+01
= 0.000E+00
= 0.000E+00
= 0.200E+06
= 0.497E+07
= 0.580E+02
= 0.112E+03

LRFD RESISTANCE FACTOR (SIDE FRICTION)
LRFD RESISTANCE FACTOR (TIP RESISTANCE)

= 0.550E+00
= 0.500E+00

Pier 41.sfo
SOIL UNIT WEIGHT, LB/CU FT
MAXIMUM LOAD TRANSFER FOR SOIL, LB/SQ FT
DEPTH, FT

= 0.115E+03
= 0.100E+11
= 0.380E+02

LRFD RESISTANCE FACTOR (SIDE FRICTION)
LRFD RESISTANCE FACTOR (TIP RESISTANCE)

= 0.450E+00
= 0.400E+00

LAYER NO 4----SAND

AT THE TOP

SKIN FRICTION COEFFICIENT- BETA
UNDRAINED SHEAR STRENGTH, LB/SQ FT
INTERNAL FRICTION ANGLE, DEG.
BLOWS PER FOOT FROM STANDARD PENETRATION TEST
SOIL UNIT WEIGHT, LB/CU FT
MAXIMUM LOAD TRANSFER FOR SOIL, LB/SQ FT
DEPTH, FT

= 0.668E+00
= 0.000E+00
= 0.340E+02
= 0.000E+00
= 0.135E+03
= 0.100E+11
= 0.380E+02

AT THE BOTTOM

SKIN FRICTION COEFFICIENT- BETA
UNDRAINED SHEAR STRENGTH, LB/SQ FT
INTERNAL FRICTION ANGLE, DEG.
BLOWS PER FOOT FROM STANDARD PENETRATION TEST
SOIL UNIT WEIGHT, LB/CU FT
MAXIMUM LOAD TRANSFER FOR SOIL, LB/SQ FT
DEPTH, FT

= 0.517E+00
= 0.000E+00
= 0.340E+02
= 0.000E+00
= 0.135E+03
= 0.100E+11
= 0.530E+02

LRFD RESISTANCE FACTOR (SIDE FRICTION)
LRFD RESISTANCE FACTOR (TIP RESISTANCE)

= 0.550E+00
= 0.500E+00

LAYER NO 5----CLAY

AT THE TOP

STRENGTH REDUCTION FACTOR-ALPHA
END BEARING COEFFICIENT-NC
UNDRAINED SHEAR STRENGTH, LB/SQ FT
INTERNAL FRICTION ANGLE, DEG.
BLOWS PER FOOT FROM STANDARD PENETRATION TEST
SOIL UNIT WEIGHT, LB/CU FT
MAXIMUM LOAD TRANSFER FOR SOIL, LB/SQ FT
DEPTH, FT

= 0.550E+00
= 0.800E+01
= 0.100E+04
= 0.000E+00
= 0.000E+00
= 0.125E+03
= 0.100E+11
= 0.530E+02

AT THE BOTTOM

STRENGTH REDUCTION FACTOR-ALPHA
END BEARING COEFFICIENT-NC
UNDRAINED SHEAR STRENGTH, LB/SQ FT
INTERNAL FRICTION ANGLE, DEG.
BLOWS PER FOOT FROM STANDARD PENETRATION TEST
SOIL UNIT WEIGHT, LB/CU FT
MAXIMUM LOAD TRANSFER FOR SOIL, LB/SQ FT
DEPTH, FT

= 0.550E+00
= 0.800E+01
= 0.100E+04
= 0.000E+00
= 0.000E+00
= 0.125E+03
= 0.100E+11
= 0.680E+02

Pier 41.sfo
LRFD RESISTANCE FACTOR (SIDE FRICTION)
LRFD RESISTANCE FACTOR (TIP RESISTANCE)

= 0.450E+00
= 0.400E+00

LAYER NO 6----SAND

AT THE TOP

SKIN FRICTION COEFFICIENT- BETA
UNDRAINED SHEAR STRENGTH, LB/SQ FT
INTERNAL FRICTION ANGLE, DEG.
BLOWS PER FOOT FROM STANDARD PENETRATION TEST
SOIL UNIT WEIGHT, LB/CU FT
MAXIMUM LOAD TRANSFER FOR SOIL, LB/SQ FT
DEPTH, FT

= 0.387E+00
= 0.000E+00
= 0.340E+02
= 0.000E+00
= 0.135E+03
= 0.100E+11
= 0.680E+02

AT THE BOTTOM

SKIN FRICTION COEFFICIENT- BETA
UNDRAINED SHEAR STRENGTH, LB/SQ FT
INTERNAL FRICTION ANGLE, DEG.
BLOWS PER FOOT FROM STANDARD PENETRATION TEST
SOIL UNIT WEIGHT, LB/CU FT
MAXIMUM LOAD TRANSFER FOR SOIL, LB/SQ FT
DEPTH, FT

= 0.250E+00
= 0.000E+00
= 0.340E+02
= 0.000E+00
= 0.135E+03
= 0.100E+11
= 0.101E+03

LRFD RESISTANCE FACTOR (SIDE FRICTION)
LRFD RESISTANCE FACTOR (TIP RESISTANCE)

= 0.550E+00
= 0.500E+00

LAYER NO 7----WEAK ROCK

AT THE TOP

DIAMETER OF SOCKET, FT
SLUMP OF CONCRETE, IN
ANGLE OF INTERFACE FRICTION, DEG.
UNIAXIAL COMPRESSION STRENGTH OF ROCK, LB/SQ FT
ELASTIC MODULUS FOR THE INTACT ROCK, LB/SQ IN.
ROCK QUALITY DESIGNATION (RQD) %
DEPTH, FT

= 0.350E+01
= 0.000E+00
= 0.000E+00
= 0.200E+06
= 0.497E+07
= 0.580E+02
= 0.101E+03

AT THE BOTTOM

DIAMETER OF SOCKET, FT
SLUMP OF CONCRETE, IN
ANGLE OF INTERFACE FRICTION, DEG.
UNIAXIAL COMPRESSION STRENGTH OF ROCK, LB/SQ FT
ELASTIC MODULUS FOR THE INTACT ROCK, LB/SQ IN.
ROCK QUALITY DESIGNATION (RQD) %
DEPTH, FT

= 0.350E+01
= 0.000E+00
= 0.000E+00
= 0.200E+06
= 0.497E+07
= 0.580E+02
= 0.112E+03

LRFD RESISTANCE FACTOR (SIDE FRICTION)
LRFD RESISTANCE FACTOR (TIP RESISTANCE)

= 0.550E+00
= 0.500E+00

Pier 41.sfo

DIAMETER OF STEM = 4.000 FT.
 DIAMETER OF BASE = 4.000 FT.
 ANGLE OF STEM TO BASE = 0.000 FT.
 ANGLE OF BELL = 0.000 DEG.
 IGNORED TOP PORTION = 2.500 FT.
 IGNORED BOTTOM PORTION = 2.500 FT.
 AREA OF ONE PERCENT STEEL = 18.098 SQ. IN.
 ELASTIC MODULUS, EC = 0.312E+07 LB/SQ. IN.
 VOLUME OF UNDERREAM = 0.000 CU. YDS.

PREDICTED RESULTS

OS = ULTIMATE SIDE RESISTANCE;
 QB = ULTIMATE BASE RESISTANCE;
 QU = WEIGHT OF DRILLED SHAFT (UPLIFT CAPACITY ONLY);
 LU = TOTAL ULTIMATE RESISTANCE;
 LRFQ QS = TOTAL SIDE FRICTION USING LRFQ RESISTANCE FACTOR
 TO THE ULTIMATE SIDE RESISTANCE;
 LRFQ QB = TOTAL BASE BEARING USING LRFQ RESISTANCE FACTOR
 TO THE ULTIMATE BASE RESISTANCE;
 LRFQ QU = TOTAL CAPACITY WITH LRFQ RESISTANCE FACTOR.

LENGTH (FEET)	VOLUME (CU. YDS)	OS (TONS)	QB (TONS)	QU (TONS)	LRFQ QS (TONS)	LRFQ QB (TONS)	LRFQ QU (TONS)
14.0	6.52	2.27	134.08	136.34	0.99	67.04	68.02
15.0	6.98	6.80	134.08	140.87	3.48	67.04	70.52
16.0	7.45	16.33	134.08	145.41	5.97	67.04	73.01
17.0	7.91	16.18	119.62	135.80	8.64	59.81	68.45
18.0	8.38	21.33	103.56	124.89	11.47	51.78	62.25
19.0	8.84	26.77	85.89	112.66	14.47	42.94	57.41
20.0	9.31	32.50	66.62	99.11	17.61	33.31	50.92
21.0	9.78	38.50	52.16	90.66	20.91	26.08	46.99
22.0	10.24	44.76	42.52	87.28	24.36	21.26	45.62
23.0	10.71	51.27	37.70	88.97	27.94	18.85	46.74
24.0	11.17	58.02	37.70	95.73	31.65	15.08	50.58
25.0	11.64	65.01	37.70	102.72	35.50	15.08	54.55
26.0	12.10	72.23	37.70	109.93	39.47	15.08	58.64
27.0	12.57	79.66	37.70	117.37	43.55	15.08	62.84
28.0	13.03	87.30	37.70	125.01	47.76	15.08	64.01
29.0	13.50	95.15	37.70	132.84	52.09	15.08	65.17
30.0	13.96	103.20	37.70	140.87	56.62	15.08	66.33
31.0	14.43	111.45	37.70	149.10	61.34	15.08	67.49
32.0	14.90	119.90	37.70	157.53	66.25	15.08	68.65
33.0	15.36	128.55	37.70	166.16	71.36	15.08	69.81
34.0	15.83	137.40	37.70	175.00	76.66	15.08	71.00
35.0	16.29	146.45	37.70	184.05	82.15	15.08	72.21
36.0	16.76	155.70	37.70	193.30	87.92	15.08	73.44
37.0	17.22	165.15	37.70	202.75	93.87	15.08	74.69
38.0	17.69	174.80	37.70	212.40	100.00	15.08	75.96
39.0	18.15	184.65	37.70	222.25	106.31	15.08	77.25
40.0	18.62	194.80	37.70	232.30	112.80	15.08	78.56
41.0	19.08	205.25	37.70	242.55	119.47	15.08	79.89
42.0	19.55	216.00	37.70	253.00	126.31	15.08	81.24
43.0	20.02	227.05	37.70	264.05	133.32	15.08	82.61
44.0	20.48	238.40	37.70	275.40	140.50	15.08	84.00
45.0	20.95	250.05	37.70	287.05	147.84	15.08	85.41
46.0	21.41	262.00	37.70	299.00	155.34	15.08	86.84

Page 5

47.0	21.88	171.46	107.54	181.40	90.42	53.77	144.19
48.0	22.34	181.40	92.17	191.45	95.88	46.09	141.97
49.0	22.81	191.45	75.41	201.50	101.41	37.71	139.12
50.0	23.27	201.50	62.84	211.55	106.99	31.42	138.81
51.0	23.74	211.55	54.46	221.60	112.62	27.23	139.85
52.0	24.21	221.60	50.27	231.65	118.29	25.14	143.43
53.0	24.67	231.65	50.27	241.70	124.01	25.11	144.12
54.0	25.14	241.70	50.27	251.75	129.76	20.11	149.87
55.0	25.60	251.75	50.27	261.80	135.55	20.11	155.66
56.0	26.07	261.80	50.27	271.85	141.37	20.11	161.48
57.0	26.53	271.85	50.27	281.90	147.21	20.11	167.32
58.0	27.00	281.90	50.27	291.95	153.06	20.11	173.18
59.0	27.46	291.95	50.27	302.00	158.92	20.11	179.05
60.0	27.93	302.00	50.27	312.05	164.79	20.11	184.92
61.0	28.39	312.05	50.27	322.10	170.65	20.11	190.79
62.0	28.86	322.10	50.27	332.15	176.51	20.11	196.66
63.0	29.33	332.15	50.27	342.20	182.37	20.11	202.53
64.0	29.79	342.20	50.27	352.25	188.23	20.11	208.40
65.0	30.26	352.25	50.27	362.30	194.09	20.11	214.27
66.0	30.72	362.30	50.27	372.35	199.95	20.11	220.14
67.0	31.19	372.35	50.27	382.40	205.81	20.11	226.01
68.0	31.65	382.40	50.27	392.45	211.67	20.11	231.88
69.0	32.12	392.45	50.27	402.50	217.53	20.11	237.75
70.0	32.58	402.50	50.27	412.55	223.39	20.11	243.62
71.0	33.05	412.55	50.27	422.60	229.25	20.11	249.49
72.0	33.51	422.60	50.27	432.65	235.11	20.11	255.36
73.0	33.98	432.65	50.27	442.70	240.97	20.11	261.23
74.0	34.45	442.70	50.27	452.75	246.83	20.11	267.10
75.0	34.91	452.75	50.27	462.80	252.69	20.11	272.97
76.0	35.38	462.80	50.27	472.85	258.55	20.11	278.84
77.0	35.84	472.85	50.27	482.90	264.41	20.11	284.71
78.0	36.31	482.90	50.27	492.95	270.27	20.11	290.58
79.0	36.77	492.95	50.27	503.00	276.13	20.11	296.45
80.0	37.24	503.00	50.27	513.05	281.99	20.11	302.32
81.0	37.70	513.05	50.27	523.10	287.85	20.11	308.19
82.0	38.17	523.10	50.27	533.15	293.71	20.11	314.06
83.0	38.63	533.15	50.27	543.20	299.57	20.11	319.93
84.0	39.10	543.20	50.27	553.25	305.43	20.11	325.80
85.0	39.57	553.25	50.27	563.30	311.29	20.11	331.67
86.0	40.03	563.30	50.27	573.35	317.15	20.11	337.54
87.0	40.50	573.35	50.27	583.40	323.01	20.11	343.41
88.0	40.96	583.40	50.27	593.45	328.87	20.11	349.28
89.0	41.43	593.45	50.27	603.50	334.73	20.11	355.15
90.0	41.89	603.50	50.27	613.55	340.59	20.11	361.02
91.0	42.36	613.55	50.27	623.60	346.45	20.11	366.89
92.0	42.82	623.60	50.27	633.65	352.31	20.11	372.76
93.0	43.29	633.65	50.27	643.70	358.17	20.11	378.63
94.0	43.76	643.70	50.27	653.75	364.03	20.11	384.50
95.0	44.22	653.75	50.27	663.80	369.89	20.11	390.37
96.0	44.69	663.80	50.27	673.85	375.75	20.11	396.24
97.0	45.15	673.85	50.27	683.90	381.61	20.11	402.11
98.0	45.62	683.90	50.27	693.95	387.47	20.11	407.98
99.0	46.08	693.95	50.27	704.00	393.33	20.11	413.85
100.0	46.55	704.00	50.27	714.05	399.19	20.11	419.72

RESULT FROM TREND (AVERAGED) LINE

TOP LOAD	TOP MOVEMENT	TIP LOAD	TIP MOVEMENT
0.1404E+00	0.4644E-04	0.3959E-01	0.1000E-04
0.7019E+00	0.2322E-03	0.1797E+00	0.5000E-04

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R_R = 1044 K

y = 94

Pier 41_sfo

0.1404E+01	0.4644E-03	0.3859E+00	0.1000E-03
0.7046E+02	0.2326E-01	0.1979E+02	0.5000E-02
0.1059E+03	0.3494E-01	0.2969E+02	0.7500E-02
0.1415E+03	0.4665E-01	0.3859E+02	0.1000E-01
0.3284E+03	0.1141E+00	0.9897E+02	0.2500E-01
0.5229E+03	0.2111E+00	0.1979E+03	0.5000E-01
0.7262E+03	0.2985E+00	0.2969E+03	0.7500E-01
0.8654E+03	0.3769E+00	0.3859E+03	0.1000E+00
0.1514E+04	0.7942E+00	0.9666E+03	0.2500E+00
0.1921E+04	0.1220E+01	0.1375E+04	0.5000E+00
0.2092E+04	0.1418E+01	0.1550E+04	0.6250E+00
0.2620E+04	0.2217E+01	0.2081E+04	0.1200E+01
0.2871E+04	0.3524E+01	0.2333E+04	0.2400E+01

RESULT FROM UPPER-BOUND LINE

TOP LOAD ton	TOP MOVEMENT IN.	TIP LOAD ton	TIP MOVEMENT IN.
0.2396E+00	0.6836E-04	0.5913E-01	0.1000E-04
0.1198E+01	0.3418E-03	0.2956E+00	0.5000E-04
0.2396E+01	0.6836E-03	0.5913E+00	0.1000E-03
0.1208E+03	0.3434E-01	0.2956E+02	0.5000E-02
0.1816E+03	0.5161E-01	0.4435E+02	0.7500E-02
0.2389E+03	0.6870E-01	0.5913E+02	0.1000E-01
0.4962E+03	0.1398E+00	0.1478E+03	0.2500E-01
0.7662E+03	0.2812E+00	0.2956E+03	0.5000E-01
0.9718E+03	0.3871E+00	0.4435E+03	0.7500E-01
0.1248E+04	0.4841E+00	0.5913E+03	0.1000E+00
0.2016E+04	0.1003E+01	0.1652E+04	0.2500E+00
0.2399E+04	0.1417E+01	0.1826E+04	0.5000E+00
0.2535E+04	0.1600E+01	0.1966E+04	0.6250E+00
0.2880E+04	0.2322E+01	0.2303E+04	0.1200E+01
0.2964E+04	0.3537E+01	0.2333E+04	0.2400E+01

RESULT FROM LOWER-BOUND LINE

TOP LOAD ton	TOP MOVEMENT IN.	TIP LOAD ton	TIP MOVEMENT IN.
0.6632E-01	0.2825E-04	0.2004E-01	0.1000E-04
0.3317E+00	0.1413E-03	0.1002E+00	0.5000E-04
0.6632E+00	0.2825E-03	0.2004E+00	0.1000E-03
0.3317E+00	0.1413E-01	0.1002E+02	0.5000E-02
0.4979E+02	0.2119E-01	0.1503E+02	0.7500E-02
0.6649E+02	0.2827E-01	0.2004E+02	0.1000E-01
0.1654E+03	0.7071E-01	0.5011E+02	0.2500E-01
0.3170E+03	0.1383E+00	0.1002E+03	0.5000E-01
0.4380E+03	0.2023E+00	0.1503E+03	0.7500E-01
0.5437E+03	0.2626E+00	0.2004E+03	0.1000E+00
0.1001E+04	0.5823E+00	0.4981E+03	0.2500E+00
0.1443E+04	0.1022E+01	0.9240E+03	0.5000E+00
0.1649E+04	0.1336E+01	0.1137E+04	0.6250E+00
0.2360E+04	0.2118E+01	0.1852E+04	0.1200E+01
0.2766E+04	0.3488E+01	0.2261E+04	0.2400E+01

PIER 4 LATERAL CAPACITY

Pier 4laf.lp7o

Pier 4laf.lp7o

Description: Pier 4 Lateral Capacity

LPile Plus for Windows, Version 2013-07.007

Analysis of Individual Piles and Drilled Shafts
Subjected to Lateral Loading Using the p-y Method

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Program Options and Settings

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Files Used for Analysis

Path to file locations: Y:\Bridges\DELDOT\BRL-159_JAMES ST BRIDGE\FOUNDATION
REPORT\LPile output\ Pier 4laf.lp7d
Name of input data file: Pier 4laf.lp7o
Name of output report file: Pier 4laf.lp7p
Name of plot output file: Pier 4laf.lp7p
Name of runtime message file: Pier 4laf.lp7r

Date and Time of Analysis

Date: October 24, 2014 Time: 15:21:24

Problem Title

Project Name: BRL-159 Pier 4

Job Number:

Client: DeIDOT

Engineer: SJM

Page 1

Engineering Units of Input Data and Computations:
- Engineering units are US Customary Units (pounds, feet, inches)

Analysis Control Options:
- Maximum number of iterations allowed = 100
- Deflection tolerance for convergence = 1.0000E-05 in
- Maximum allowable deflection = 100.0000 in
- Number of pile increments = 100

Loading Type and Number of Cycles of Loading:
- Static loading specified

Computational Options:
- Use unfactored loads in computations (conventional analysis)
- Compute pile response under loading and nonlinear bending properties of pile
(only if nonlinear pile properties are input)
- Use of p-y modification factors for p-y curves not selected
- Loading by lateral soil movements acting on pile not selected
- Input of shear resistance at the pile tip not selected
- Computation of pile-head foundation stiffness matrix not selected
- Push-over analysis of pile not selected
- Buckling analysis of pile not selected

Output Options:
- No p-y curves to be computed and reported for user-specified depths
- Values of pile-head deflection, bending moment, shear force, and
soil reaction are printed for full length of pile.
- Printing increment (nodal spacing of output points) = 1

Pile Structural Properties and Geometry

Total number of pile sections = 2

Total length of pile = 99.29 ft

Depth of ground surface below top of pile = 14.79 ft

Pile diameter values used for p-y curve computations are defined using 4 points.

p-y curves are computed using pile diameter values interpolated with depth over
the length of the pile.

Point	Depth X ft	Pile Diameter D in
1	0.00000	48.0000000
2	3.29000	48.0000000
3	3.29000	49.0000000

Page 2

4 99.290000 49.000000 Pier 41af.1p7o

Input structural Properties:

 Pile Section No. 1:

Section Type = Drilled shaft (Bored pile)
 Section Length = 3.29000 ft
 Section Diameter = 48.00000 in

Pile Section No. 2:
 Section Type = Drilled shaft with
 Permanent casing
 Section Length = 96.00000 ft
 Section Diameter = 49.00000 in

 Ground Slope and Pile Batter Angles

Ground Slope Angle = 0.000 degrees
 = 0.000 radians
 Pile Batter Angle = 0.000 degrees
 = 0.000 radians

 Soil and Rock Layering Information

The soil profile is modelled using 7 layers

Layer 1 is soft clay, p-y criteria by Matlock, 1970
 Distance from top of pile to top of layer = 14.79000 ft
 Distance from top of pile to bottom of layer = 15.29000 ft
 Effective unit weight at top of layer = 42.60000 pcf
 Effective unit weight at bottom of layer = 62.60000 pcf
 Undrained cohesion at top of layer = 750.00000 psf
 Undrained cohesion at bottom of layer = 750.00000 psf
 Epsilon-50 at top of layer = 0.02000
 Epsilon-50 at bottom of layer = 0.02000

Layer 2 is sand, p-y criteria by Reese et al., 1974
 Distance from top of pile to top of layer = 15.29000 ft
 Distance from top of pile to bottom of layer = 29.29000 ft
 Effective unit weight at top of layer = 62.60000 pcf
 Effective unit weight at bottom of layer = 87.60000 pcf
 Friction angle at top of layer = 34.00000 deg.
 Friction angle at bottom of layer = 34.00000 deg.
 Subgrade k at top of layer = 60.00000 pci
 Subgrade k at bottom of layer = 60.00000 pci

Layer 3 is soft clay, p-y criteria by Matlock, 1970

 Pier 41af.1p7o
 Distance from top of pile to top of layer = 29.29000 ft
 Distance from top of pile to bottom of layer = 43.29000 ft
 Effective unit weight at top of layer = 52.60000 pcf
 Effective unit weight at bottom of layer = 72.60000 pcf
 Undrained cohesion at top of layer = 750.00000 psf
 Undrained cohesion at bottom of layer = 750.00000 psf
 Epsilon-50 at top of layer = 0.02000
 Epsilon-50 at bottom of layer = 0.02000

Layer 4 is sand, p-y criteria by Reese et al., 1974
 Distance from top of pile to top of layer = 43.29000 ft
 Distance from top of pile to bottom of layer = 58.29000 ft
 Effective unit weight at top of layer = 72.60000 pcf
 Effective unit weight at bottom of layer = 72.60000 pcf
 Friction angle at top of layer = 34.00000 deg.
 Friction angle at bottom of layer = 34.00000 deg.
 Subgrade k at top of layer = 125.00000 pci
 Subgrade k at bottom of layer = 125.00000 pci

Layer 5 is stiff clay with water-induced erosion
 Distance from top of pile to top of layer = 58.29000 ft
 Distance from top of pile to bottom of layer = 73.29000 ft
 Effective unit weight at top of layer = 62.60000 pcf
 Effective unit weight at bottom of layer = 62.60000 pcf
 Undrained cohesion at top of layer = 1000.00000 psf
 Undrained cohesion at bottom of layer = 1000.00000 psf
 Epsilon-50 at top of layer = 0.00700
 Epsilon-50 at bottom of layer = 0.00700
 Subgrade k at top of layer = 200.00000 pci
 Subgrade k at bottom of layer = 200.00000 pci

Layer 6 is sand, p-y criteria by Reese et al., 1974
 Distance from top of pile to top of layer = 73.29000 ft
 Distance from top of pile to bottom of layer = 106.29000 ft
 Effective unit weight at top of layer = 72.60000 pcf
 Effective unit weight at bottom of layer = 72.60000 pcf
 Friction angle at top of layer = 34.00000 deg.
 Friction angle at bottom of layer = 34.00000 deg.
 Subgrade k at top of layer = 125.00000 pci
 Subgrade k at bottom of layer = 125.00000 pci

Layer 7 is weak rock, p-y criteria by Reese, 1997
 Distance from top of pile to top of layer = 106.29000 ft
 Distance from top of pile to bottom of layer = 169.29000 ft
 Effective unit weight at top of layer = 87.60000 pcf
 Effective unit weight at bottom of layer = 87.60000 pcf
 Uniaxial compressive strength at top of layer = 1389.00000 psi
 Uniaxial compressive strength at bottom of layer = 1389.00000 psi
 Initial modulus of rock at top of layer = 4970000. psi
 Initial modulus of rock at bottom of layer = 4970000. psi
 RQD of rock at top of layer = 0.0000 %
 RQD of rock at bottom of layer = 0.0000 %
 k rim of rock at top of layer = 0.0000
 k rim of rock at bottom of layer = 0.0000

(Depth of lowest soil layer extends 17.50 ft below pile tip)

Summary of Soil Properties

Layer	Uniaxial qu psi	Soil Type or (p-y Curve Criteria) GSI	RQD %	Strain	Layer Depth kpy	Effective Rock Mass Unit Wt. pcf	Undrained Cohesion Rock Emass krm
1	Soft Clay			0.02000	14.790	42.600	750.000
2	Sand (Reese, et al.)			0.02000	15.290	42.600	750.000
3	Soft Clay			0.02000	29.290	52.600	750.000
4	Sand (Reese, et al.)			0.02000	43.290	52.600	750.000
5	stiff Clay with Free water			0.00700	58.290	62.600	1000.000
6	Sand (Reese, et al.)			0.00700	73.290	62.600	1000.000
7	Weak Rock			0.00700	106.290	87.600	4970000.
0.00					116.790	87.600	4970000.

Loading Type

Static loading criteria were used when computing p-y curves for all analyses.

Pile-head Loading and Pile-head Fixity Conditions

Number of loads specified = 10

Load No.	Load Type	Condition	Condition	Axial Thrust Force, lbs
1	4	y = 0.50000 in	M = 3793200. in-lbs	0.0000000
2	4	y = 1.00000 in	M = 3793200. in-lbs	0.0000000
3	4	y = 1.50000 in	M = 3793200. in-lbs	0.0000000
4	4	y = 2.00000 in	M = 3793200. in-lbs	0.0000000
5	4	y = 0.50000 in	M = 3248400. in-lbs	0.0000000
6	4	y = 1.00000 in	M = 3248400. in-lbs	0.0000000
7	4	y = 1.50000 in	M = 3248400. in-lbs	0.0000000
8	4	y = 2.00000 in	M = 3248400. in-lbs	0.0000000
9	1	V = 9800.00000 lbs	M = 3793200. in-lbs	0.0000000
10	1	V = 8400.00000 lbs	M = 3248400. in-lbs	0.0000000

V = perpendicular shear force applied to pile head
M = bending moment applied to pile head
y = lateral deflection relative to pile axis
S = pile slope relative to original pile batter angle
R = rotational stiffness applied to pile head
Axial thrust is assumed to be acting axially for all pile batter angles.

Computations of Nominal Moment Capacity and Nonlinear Bending Stiffness

Axial thrust force values were determined from pile-head loading conditions

Number of Pile Sections Analyzed = 2

Pile Section No. 1:

Pier 41af.lp7o
 Dimensions and Properties of Drilled Shaft (Bored Pile):

Length of Section = 3.29000 ft
 Shaft Diameter = 48.00000 in
 Concrete Cover Thickness = 4.00000 in
 Number of Reinforcing Bars = 50 bars
 Yield Stress of Reinforcing Bars = 60000. psi
 Modulus of Elasticity of Reinforcing Bars = 29000000. psi
 Gross Area of Shaft = 1809.55737 sq. in.
 Total Area of Reinforcing Steel = 39.50000 sq. in.
 Area Ratio of Steel Reinforcement = 2.18 percent
 Edge-to-Edge Bar Spacing = 0.89438 in
 Maximum Concrete Aggregate Size = 7.72
 Ratio of Bar Spacing to Aggregate Size = 0.37500 in
 Offset of Center of Rebar Cage from Center of Pile = 0.0000 in

Axial Structural Capacities:

Nom. Axial Structural Capacity = 0.85 Fc Ac + Fy As = 9140.470 kips
 Tensile Load for Cracking of Concrete = -911.303 kips
 Nominal Axial Tensile Capacity = -2370.000 kips

Reinforcing Bar Dimensions and Positions Used in Computations:

Bar Number	Bar Diam. inches	Bar Area sq. in.	X inches	Y inches
1	1.00000	0.79000	19.49359	-0.49995
2	1.00000	0.79000	19.49359	0.49995
3	1.00000	0.79000	19.05949	4.36562
4	1.00000	0.79000	18.75683	8.35210
5	1.00000	0.79000	17.32341	8.95300
6	1.00000	0.79000	16.81171	3.87621
7	1.00000	0.79000	14.82788	12.76891
8	1.00000	0.79000	13.10917	13.10917
9	1.00000	0.79000	10.82737	16.72687
10	1.00000	0.79000	10.49933	18.38501
11	1.00000	0.79000	6.44837	18.69400
12	1.00000	0.79000	1.72927	18.82372
13	1.00000	0.79000	1.72927	18.82372
14	1.00000	0.79000	0.72505	18.48662
15	1.00000	0.79000	-3.16184	18.24199
16	1.00000	0.79000	-7.14382	19.65462
17	1.00000	0.79000	-11.84780	17.85119
18	1.00000	0.79000	-16.75233	17.82546
19	1.00000	0.79000	-19.04047	15.38875
20	1.00000	0.79000	-12.81090	14.70139
21	1.00000	0.79000	-15.47629	11.86231
22	1.00000	0.79000	-16.06451	11.05358
23	1.00000	0.79000	-17.94064	7.64091
24	1.00000	0.79000	-18.30872	6.71123
25	1.00000	0.79000	-19.27722	2.83920
26	1.00000	0.79000	-19.40254	1.94719
27	1.00000	0.79000	-19.40254	-1.94719
28	1.00000	0.79000	-19.27722	-2.83920
29	1.00000	0.79000	-18.30872	-6.71123
30	1.00000	0.79000	-17.94064	-7.64091
31	1.00000	0.79000	-16.06451	-11.05358
32	1.00000	0.79000	-15.47679	-11.86231
33	1.00000	0.79000	-12.81090	-14.70139

Pier 41af.lp7o
 34 1.00000 -12.04047 -15.33875
 35 0.79000 -8.75233 -17.42546
 36 0.79000 -7.84760 -17.85119
 37 0.79000 -4.14382 -19.05462
 38 0.79000 -3.16164 -19.24199
 39 0.79000 0.72505 -19.48652
 40 0.79000 1.72927 -19.42373
 41 0.79000 5.54837 -18.69400
 42 0.79000 6.49933 -18.38501
 43 0.79000 10.02307 -16.72687
 44 0.79000 10.86731 -16.19110
 45 0.79000 13.86798 -13.70873
 46 0.79000 14.55245 -12.97984
 47 0.79000 16.84151 -9.82921
 48 0.79000 17.32321 -8.95300
 49 0.79000 18.75683 -5.33210
 50 0.79000 19.00549 -4.36362

NOTE: The positions of the above rebars were computed by LPile

Minimum spacing between any two bars not equal to zero = -0.0001096 inches between Bars 1 and 2

Spacing to aggregate size ratio = -0.0002922

Concrete Properties:

Compressive Strength of Concrete = 4500.00000 psi
 Modulus of Elasticity of Concrete = 3823676. psi
 Modulus of Rupture of Concrete = -503.11528 psi
 Compression Strain at Peak Stress = 0.00200
 Tensile Strain at Fracture of Concrete = -0.0001132
 Maximum Coarse Aggregate Size = 0.37500 in

Number of Axial Thrust Force Values Determined from Pile-head Loadings = 1

Number	Axial Thrust Force Kips
1	0.000

Definitions of Run Messages and Notes:

C = concrete in section has cracked in tension
 Y = stress in reinforcing steel has reached yield stress.
 T = ACI 318-08 criteria for controlled section met, tensile strain in reinforcement exceeds 0.005 while simultaneously compressive strain in concrete is more than 0.003. see ACI 318.08, Section 10.3.4.
 Z = depth of tensile zone in concrete section is less than 10 percent of section depth.
 Bending Stiffness (EI) = Computed Bending Moment / Curvature.
 Position of neutral axis is measured from edge of compression side of pile.
 Compressive stresses and strains are positive in sign.
 Tensile stresses and strains are negative in sign.

Pier 41af.jp7o

Axial Thrust Force = 0.000 kips		Bending		Depth to		Max Comp		Max Tens	
Bending Curvature rad/in. ksi	Max Steel Stress ksi	Run Msg	Stiffness kip-in2	N Axis	in	Strain	in/in	Strain	in/in
0.00000625	845.95144339		135322294.	24.0001518	24.0001510	-0.0000150			
0.0665544	0.4306528								
0.00001250	1688.2814444		1350625155.	24.0001524	-0.0000300				
0.1326129	0.8613055								
0.000001875	2526.9900314		1347728017.	24.0001529	-0.0000450				
0.1981756	1.2919583								
0.000002500	3362.0771951		1344830878.	24.0001534	-0.0000600				
0.2632425	1.7226111								
0.000003125	4193.5429353		1341933739.	24.0001540	-0.0000750				
0.3278135	2.1532639								
0.3918887	2.5839168		1339036601.	24.0001545	-0.0000900				
0.4534681	3.0145696								
0.000005000	5845.6101456		1336139462.	24.0001551	-0.0001050				
0.3080092	-4.8693722								
0.000005625	5845.6101456		1169122029.	14.1767436	-0.0000798				
0.3438573	-5.4774992								
0.000006250	5845.6101456		1039219581.	14.1814610	-0.0002113				
0.3835595	-6.0852532								
0.000006875	5845.6101456		935297623.	14.1861892	-0.0000887				
0.4211155	-6.6928337								
0.000007500	5845.6101456		850270567.	14.1909283	-0.0000976				
0.4585249	-7.3002399								
0.000008125	5845.6101456		779414686.	14.1956783	-0.0001065				
0.4957876	-7.9074715								
0.000008750	5845.6101456		719459710.	14.2004394	-0.0001154				
0.5329033	-8.5143276								
0.000009375	5845.6101456		668069731.	14.2052115	-0.0001243				
0.5698716	-9.1214077								
0.000010000	5845.6101456		623531749.	14.2099947	-0.0001332				
0.6066924	-9.7281112								
0.000010600	5845.6101456		584561015.	14.2147891	-0.0001421				
0.6433633	-10.346374								
0.000011300	5845.6101456		550175073.	14.2195946	-0.0001511				
0.6796902	-10.9408657								
0.7166866	5845.6101456		519609791.	14.2244115	-0.0001600				
0.7524843	-11.543143								
0.000013100	5845.6101456		492261907.	14.2292396	-0.0001690				
0.7885732	-12.14077								
0.000013800	5845.6101456		467648812.	14.2340792	-0.0001779				
0.8245038	-12.743877								
0.000014400	5845.6101456		445379821.	14.2389301	-0.0001869				
0.8602829	-13.348877								
0.000015000	5845.6101456		425135283.	14.2437926	-0.0001959				
0.8959132	-13.950371								
0.000015600	5845.6101456		419046578.	14.2486666	-0.0002048				
0.9313934	-14.553048								
0.000016300	5845.6101456		418901006.	14.2535522	-0.0002138				
0.9667234	-15.150491								
0.000016900	5845.6101456		418755135.	14.2584494	-0.0002228				
			418608964.	14.2633583	-0.0002318				
			418462492.	14.2682790	-0.0002408				
			70611.5545606						

Pier 41af.jp7o

1.0019026	-16.3900109	C	418315718.	14.2732116	0.0002498	-0.0005902
0.0000175	7320.5250670	C				
1.0369310	-16.9945451	C	418168640.	14.2781560	0.0002588	-0.0006112
0.0000181	7579.3065976	C				
1.0718081	-17.5988942	C	418021256.	14.2831123	0.0002678	-0.0006322
0.0000188	7837.8985565	C				
1.1065338	-18.2030577	C	417873566.	14.2880807	0.0002768	-0.0006532
0.0000194	8096.3003444	C				
1.1411076	-18.8070346	C	417725568.	14.2930611	0.0002859	-0.0006741
0.0000200	8354.5113583	C				
1.1755294	-19.4108245	C	417577260.	14.2980536	0.0002949	-0.0006951
0.0000206	8612.5309914	C				
1.2097888	-20.0144267	C	417428642.	14.3030584	0.0003039	-0.0007161
0.0000213	8870.3586334	C				
1.2439155	-20.6178403	C	417279711.	14.3080753	0.0003130	-0.0007370
0.0000219	9127.9936698	C				
1.2778793	-21.2210647	C	417130466.	14.3131046	0.0003220	-0.0007580
0.0000225	9385.4354826	C				
1.3116898	-21.8240993	C	416980906.	14.3181462	0.0003311	-0.0007789
0.0000231	9642.6834500	C				
1.3453467	-22.4269432	C	416831029.	14.3232002	0.0003402	-0.0007998
0.0000238	9899.7369459	C				
1.3788497	-23.0295958	C	416680834.	14.3282668	0.0003493	-0.0008207
0.0000244	10157.	C				
1.4121886	-23.6320564	C	4165379475.	14.3384375	0.0003674	-0.0008626
0.0000256	10670.	C				
1.4784325	-24.8363989	C	416076834.	14.3486590	0.0003856	-0.0009044
0.0000269	11182.	C				
1.5440460	-26.0399864	C	415772890.	14.3589318	0.0004038	-0.0009462
0.0000281	11694.	C				
1.6090366	-27.2427466	C	415467630.	14.3692563	0.0004221	-0.0009879
0.0000294	12204.	C				
1.6734018	-28.4447402	C	415161043.	14.3796331	0.0004404	-0.0010296
0.0000306	12714.	C				
1.7371390	-29.6459388	C	414853116.	14.3900627	0.0004587	-0.0010713
0.0000319	13223.	C				
1.8002456	-30.8463362	C	414543834.	14.4005458	0.0004770	-0.0011130
0.0000331	13732.	C				
1.8627191	-32.0459262	C	414233186.	14.4110828	0.0004954	-0.0011546
0.0000344	14239.	C				
1.9245367	-33.2447024	C	413921159.	14.4216743	0.0005138	-0.0011962
0.0000356	14746.	C				
1.9857359	-34.4426584	C	413607737.	14.4323209	0.0005322	-0.0012378
0.0000369	15252.	C				
2.0463138	-35.6397875	C	413292908.	14.4430232	0.0005506	-0.0012794
0.0000381	15757.	C				
2.1062279	-36.8360832	C	412976658.	14.4537818	0.0005691	-0.0013209
0.0000394	16261.	C				
2.1634952	-38.0313587	C	412658972.	14.4645973	0.0005876	-0.0013624
0.0000406	16764.	C				
2.2241131	-39.2261717	C	412339835.	14.4754703	0.0006062	-0.0014038
0.0000419	17269.	C				
2.2807819	-40.4137268	C	412019235.	14.4864015	0.0006247	-0.0014453
0.0000431	17774.	C				
2.3383890	-41.6127020	C	411697154.	14.4973914	0.0006433	-0.0014867
0.0000444	18279.	C				
2.3960414	-42.8001826	C	411373579.	14.5084408	0.0006619	-0.0015281
0.0000456	18784.	C				
2.4530326	-43.9950769	C	411048519.	14.5195502	0.0006806	-0.0015694
0.0000469	19289.	C				
2.5072609	-45.1862362	C	410721909.	14.5307205	0.0006993	-0.0016107
0.0000481	19794.	C				
2.5620203	-46.3756131	C				

Pier 41af. 1p7o				Pier 41af. 1p7o			
0.0000494	20263.	410393756.	0.0007180	-0.0016520	4.4193369	-60.0000000	0.0018187
2.6160105	-47.5640922	14.5419521	0.0007368	-0.0016932	0.0001344	37263.	-0.0046313
0.0000506	20759.	410064046.	0.0007555	-0.0017345	4.4484203	-60.0000000	-0.0018731
2.6683276	-48.7516657	14.5532459	0.0007744	-0.0017556	0.0001394	37535.	-0.0048169
0.0000519	21255.	409732761.	0.0007932	-0.0018168	4.47088379	-60.0000000	-0.0019270
2.7219685	-49.9383259	14.5646025	0.0008121	-0.0018579	0.0001444	37783.	-0.0050030
0.0000531	21749.	409399885.	0.0008310	-0.0018990	4.48686079	-60.0000000	-0.0019810
2.7739299	-51.1240649	14.5760227	0.0008499	-0.0019401	0.0001494	38022.	-0.0051890
0.0000544	22243.	409065400.	0.0008689	-0.0020221	4.48653333	-60.0000000	-0.0020345
2.8252088	-52.3088745	14.5875072	0.0008879	-0.0020631	0.0001544	38238.	-0.0053755
0.0000556	22736.	408729291.	0.0009069	-0.0021040	4.4989879	-60.0000000	-0.0020872
2.8758017	-53.4927466	14.6106719	0.0009260	-0.0021449	0.0001594	38435.	-0.0055628
0.0000569	23227.	408391538.	0.0009451	-0.0021858	4.4991008	-60.0000000	-0.0021396
2.9257055	-54.6756728	14.6223538	0.0009642	-0.0022267	0.0001644	38613.	-0.0057504
0.0000581	23718.	408052124.	0.0009833	-0.0022675	4.4961694	60.0000000	-0.0021918
2.9749169	-55.8576448	14.6341029	0.0010025	-0.0023083	4.4988350	60.0000000	-0.0059382
0.0000594	24208.	407711031.	0.0010217	-0.0023490	4.4998572	60.0000000	-0.0061256
3.0234323	-57.0386538	407368552.	0.0010410	-0.0023898	4.4971745	60.0000000	-0.0022444
0.0000606	24697.	407368552.	0.0010602	-0.0024311	4.4972710	60.0000000	-0.0022966
3.0712187	-58.2190319	14.6572221	0.0010789	-0.0024730	0.0001794	39093.	-0.0063134
0.0000619	25185.	406729201.	0.0010970	-0.0025156	4.4996672	60.0000000	-0.0065012
3.1182718	-59.3987969	14.6687831	0.00111664	-0.0025585	4.4996672	60.0000000	-0.0066897
0.0000631	25672.	406679201.	0.0011357	-0.0026000	4.4971451	60.0000000	-0.0068784
3.1646176	-60.0000000	406331998.	0.0011564	-0.0026436	4.4999003	60.0000000	-0.0070675
0.0000644	26158.	406331998.	0.0011749	-0.0026879	4.4999003	60.0000000	-0.0072564
3.2102527	-60.0000000	405983085.	0.0011936	-0.0027306	4.4956386	60.0000000	-0.0074451
0.0000656	26643.	405983085.	0.001212326	-0.0027739	4.4956386	60.0000000	-0.0076340
3.2551736	-60.0000000	405632443.	0.0012294	-0.0028174	4.4932210	60.0000000	-0.0078229
0.0000669	27127.	405632443.	0.0012494	-0.0028606	4.4932210	60.0000000	-0.0080120
3.2995766	-60.0000000	405280053.	0.0012684	-0.0029036	4.4932210	60.0000000	-0.0082012
0.0000681	27610.	405280053.	0.0012879	-0.0029469	4.4932210	60.0000000	-0.0083911
3.3428584	-60.0000000	404925896.	0.0013069	-0.0029902	4.4932210	60.0000000	-0.0085812
0.0000694	28092.	404925896.	0.0013259	-0.0030335	4.4932210	60.0000000	-0.0087715
3.3856151	-60.0000000	404569952.	0.0013449	-0.0030768	4.4932210	60.0000000	-0.0089617
0.0000706	28573.	404569952.	0.0013639	-0.0031201	4.4932210	60.0000000	-0.0091518
3.4276432	-60.0000000	404091673.	0.0013829	-0.0031634	4.4932210	60.0000000	-0.0093417
0.0000719	29044.	404091673.	0.0014019	-0.0032067	4.4932210	60.0000000	-0.0095318
3.4687035	-60.0000000	40372266.	0.0014209	-0.0032500	4.4932210	60.0000000	-0.0097217
0.0000731	29475.	40372266.	0.0014399	-0.0032933	4.4932210	60.0000000	-0.0099115
3.5079550	-60.0000000	401455043.	0.0014589	-0.0033366	4.4932210	60.0000000	-0.0101049
0.0000744	29858.	401455043.	0.0014779	-0.0033800	4.4932210	60.0000000	-0.0103044
3.5452601	-60.0000000	392246336.	0.0014969	-0.0034233	4.4932210	60.0000000	-0.0105039
0.0000757	31133.	392246336.	0.0015159	-0.0034666	4.4932210	60.0000000	-0.0107034
3.6813494	-60.0000000	381149774.	0.0015349	-0.0035100	4.4932210	60.0000000	-0.0109029
0.0000770	31660.	381149774.	0.0015539	-0.0035533	4.4932210	60.0000000	-0.0111024
3.7013683	-60.0000000	369362560.	0.0015729	-0.0035966	4.4932210	60.0000000	-0.0113019
0.0000783	32010.	369362560.	0.0015919	-0.0036400	4.4932210	60.0000000	-0.0115014
3.7979394	-60.0000000	357505362.	0.0016109	-0.0036833	4.4932210	60.0000000	-0.0117009
0.0000796	32370.	357505362.	0.0016299	-0.0037266	4.4932210	60.0000000	-0.0119004
3.8070144	-60.0000000	345931693.	0.0016489	-0.0037700	4.4932210	60.0000000	-0.0121000
0.0000809	32740.	345931693.	0.0016679	-0.0038133	4.4932210	60.0000000	-0.0123000
3.8882438	-60.0000000	334703122.	0.0016869	-0.0038566	4.4932210	60.0000000	-0.0125000
0.0000822	32933.	334703122.	0.0017059	-0.0039000	4.4932210	60.0000000	-0.0127000
3.9070144	-60.0000000	323940666.	0.0017249	-0.0039433	4.4932210	60.0000000	-0.0129000
4.0882438	35431.	323940666.	0.0017439	-0.0039866	4.4932210	60.0000000	-0.0131000
0.0001044	35871.	313627073.	0.0017629	-0.0040300	4.4932210	60.0000000	-0.0133000
4.1641357	-60.0000000	313627073.	0.0017819	-0.0040733	4.4932210	60.0000000	-0.0135000
4.2307884	-60.0000000	303860741.	0.0018009	-0.0041166	4.4932210	60.0000000	-0.0137000
4.2891684	-60.0000000	2945530941.	0.0018199	-0.0041600	4.4932210	60.0000000	-0.0139000
4.3399744	-60.0000000	285688006.	0.0018389	-0.0042033	4.4932210	60.0000000	-0.0141000
4.3832660	-60.0000000	285688006.	0.0018579	-0.0042466	4.4932210	60.0000000	-0.0143000
0.0001244	36961.	13.6338565	0.0018769	-0.0042900	4.4867102	60.0000000	-0.0145000
4.3832660	36961.	13.6338565	0.0018959	-0.0043333	4.4867102	60.0000000	-0.0147000
0.0001294	36961.	13.6338565	0.0019149	-0.0043766	4.4867102	60.0000000	-0.0149000
4.3832660	36961.	13.6338565	0.0019339	-0.0044200	4.4867102	60.0000000	-0.0151000
0.0001344	36961.	13.6338565	0.0019529	-0.0044633	4.4867102	60.0000000	-0.0153000
4.3832660	36961.	13.6338565	0.0019719	-0.0045066	4.4867102	60.0000000	-0.0155000
0.0001394	36961.	13.6338565	0.0019909	-0.0045500	4.4867102	60.0000000	-0.0157000
4.3832660	36961.	13.6338565	0.0020099	-0.0045933	4.4867102	60.0000000	-0.0159000
0.0001444	36961.	13.6338565	0.0020289	-0.0046366	4.4867102	60.0000000	-0.0161000
4.3832660	36961.	13.6338565	0.0020479	-0.0046800	4.4867102	60.0000000	-0.0163000
0.0001494	36961.	13.6338565	0.0020669	-0.0047233	4.4867102	60.0000000	-0.0165000
4.3832660	36961.	13.6338565	0.0020859	-0.0047666	4.4867102	60.0000000	-0.0167000
0.0001544	36961.	13.6338565	0.0021049	-0.0048100	4.4867102	60.0000000	-0.0169000
4.3832660	36961.	13.6338565	0.0021239	-0.0048533	4.4867102	60.0000000	-0.0171000
0.0001594	36961.	13.6338565	0.0021429	-0.0048966	4.4867102	60.0000000	-0.0173000
4.3832660	36961.	13.6338565	0.0021619	-0.0049400	4.4867102	60.0000000	-0.0175000
0.0001644	36961.	13.6338565	0.0021809	-0.0049833	4.4867102	60.0000000	-0.0177000
4.3832660	36961.	13.6338565	0.0021999	-0.0050266	4.4867102	60.0000000	-0.0179000
0.0001694	36961.	13.6338565	0.0022189	-0.0050700	4.4867102	60.0000000	-0.0181000
4.3832660	36961.	13.6338565	0.0022379	-0.0051133	4.4867102	60.0000000	-0.0183000
0.0001744	36961.	13.6338565	0.0022569	-0.0051566	4.4867102	60.0000000	-0.0185000
4.3832660	36961.	13.6338565	0.0022759	-0.0052000	4.4867102	60.0000000	-0.0187000
0.0001794	36961.	13.6338565	0.0022949	-0.0052433	4.4867102	60.0000000	-0.0189000
4.3832660	36961.	13.6338565	0.0023139	-0.0052866	4.4867102	60.0000000	-0.0191000
0.0001844	36961.	13.6338565	0.0023329	-0.0053300	4.4867102	60.0000000	-0.0193000
4.3832660	36961.	13.6338565	0.0023519	-0.0053733	4.4867102	60.0000000	-0.0195000
0.0001894	36961.	13.6338565	0.0023709	-0.0054166	4.4867102	60.0000000	-0.0197000
4.3832660	36961.	13.6338565	0.0023899	-0.0054600	4.4867102	60.0000000	-0.0199000
0.0001944	36961.	13.6338565	0.0024089	-0.0055033	4.4867102	60.0000000	-0.0201000
4.3832660	36961.	13.6338565	0.0024279	-0.0055466	4.4867102	60.0000000	-0.0203000
0.0001994	36961.	13.6338565	0.0024469	-0.0055900	4.4867102	60.0000000	-0.0205000
4.3832660	36961.	13.6338565	0.0024659	-0.0056333	4.4867102	60.0000000	-0.0207000
0.0002044	36961.	13.6338565	0.0024849	-0.0056766	4.4867102	60.0000000	-0.0209000
4.3832660	36961.	13.6338565	0.0025039	-0.0057200	4.4867102	60.0000000	-0.0211000
0.0002094	36961.	13.6338565	0.0025229	-0.0057633	4.4867102	60.0000000	-0.0213000
4.3832660	36961.	13.6338565	0.0025419	-0.0058066	4.4867102	60.0000000	-0.0215000
0.0002144	36961.	13.6338565	0.0025609	-0.0058500	4.4867102	60.0000000	-0.0217000
4.3832660	36961.	13.6338565	0.0025799	-0.0058933	4.4867102	60.0000000	-0.0219000
0.0002194	36961.	13.6338565	0.0025989	-0.0059366	4.4867102	60.0000000	-0.0221000
4.3832660	36961.	13.6338565	0.0026179	-0.0059800	4.4867102	60.0000000	-0.0223000
0.0002244	36961.	13.6338565	0.0026369	-0.0060233	4.4867102	60.0000000	-0.0225000
4.3832660	36961.	13.6338565	0.0026559	-0.0060666	4.4867102	60.0000000	-0.0227000
0.0002294	36961.	13.6338565	0.0026749	-0.0			

Summary of Results for Nominal (Unfactored) Moment Capacity for Section 1

Moment values interpolated at maximum compressive strain = 0.003 or maximum developed moment if pile fails at smaller strains.

Load No.	Axial Thrust kips	Nominal Mom. Cap. in-kip	Max. Comp. Strain
1	0.000	40395.232	0.00300000

Note note that the values of moment capacity in the table above are not factored by a strength reduction factor (ϕ -factor).

In ACI 318-08, the value of the strength reduction factor depends on whether the transverse reinforcing steel bars are tied hoops (0.65) or spirals (0.70).

The above values should be multiplied by the appropriate strength reduction factor to compute ultimate moment capacity according to ACI 318-08, section 9.3.2.2 or the value required by the design standard being followed.

The following table presents factored moment capacities and corresponding bending stiffnesses computed for common resistance factor values used for reinforced concrete sections.

Axial Load Capacity in-kip	Resistance Factor at Ult. Mom. Cap. for Moment	Nominal Bending Stiffness at Ult. Mom. Cap. kip-in ²	Nominal Moment Capacity at Ult. Mom. Cap. in-kip	Ultimate (Factored) Axial Thrust kips	Ultimate Moment
26236.900	0.65	406260579.288	40395.232	0.000	
28276.662	0.70	404789053.314	40395.232	0.000	
30296.424	0.75	398293409.577	40395.232	0.000	

Pile Section No. 2:

Dimensions and Properties of Drilled Shaft (Bored Pile) with Permanent Casing:

Length of Section	=	96.00000 ft
Outer Diameter of Concrete Core	=	49.0000 in
Casing Wall Thickness	=	4.0000 in
Moment of Inertia of Steel Casing	=	22403. in ⁴
Elastic Modulus of Steel	=	290000000. psi
Area of Steel Reinforcing Bars	=	0.79000 sq. in.
Edge-to-Edge Bar Spacing	=	2.76901 in
Maximum Concrete Aggregate Size	=	0.37500 in

Ratio of Bar Spacing to Aggregate Size = 7.38
 Offset of Center of Rebar Cage from Center of Pile = 0.0000 in
 Yield Stress of Reinforcing Bars = 60000. psi
 Modulus of Elasticity of Reinforcing Bars = 29000000. psi
 Gross Area of Pile = 1885.74099 sq. in.
 Area of Concrete = 1770.05737 sq. in.
 Cross-sectional Area of Steel Casing = 76.18362 sq. in.
 Area of All Steel (Casing and Bars) = 115.68362 sq. in.
 Area Ratio of All Steel to Gross Area of Pile = 6.13 percent

Axial Structural Capacities:

Nom. Axial Structural Capacity = 0.85 Fc Ac + Fy As = 11883.080 kips
 Tensile Load for Cracking of Concrete = -1165.721 kips
 Nominal Axial Tensile Capacity = -5112.610 kips

Reinforcing Bar Dimensions and Positions Used in Computations:

Bar Number	Bar Diam. inches	Bar Area sq. in.	X inches	Y inches
1	1.00000	0.79000	18.99342	-0.49994
2	1.00000	0.79000	18.99342	0.49994
3	1.00000	0.79000	18.52104	4.23924
4	1.00000	0.79000	18.27238	5.20771
5	1.00000	0.79000	16.88491	8.71205
6	1.00000	0.79000	16.40321	9.58825
7	1.00000	0.79000	14.18784	12.63745
8	1.00000	0.79000	13.50337	13.36653
9	1.00000	0.79000	10.59950	13.76879
10	1.00000	0.79000	9.75507	16.30456
11	1.00000	0.79000	6.34476	17.90953
12	1.00000	0.79000	5.39382	18.21831
13	1.00000	0.79000	1.69136	18.52455
14	1.00000	0.79000	0.69355	18.98733
15	1.00000	0.79000	-3.06793	18.75068
16	1.00000	0.79000	-7.63464	18.36332
17	1.00000	0.79000	-8.53927	17.39863
18	1.00000	0.79000	-11.72165	16.37290
19	1.00000	0.79000	-12.49207	14.31601
20	1.00000	0.79000	-15.07214	11.36851
21	1.00000	0.79000	-17.47560	10.72959
22	1.00000	0.79000	-17.84368	7.45978
23	1.00000	0.79000	-18.78039	6.37711
24	1.00000	0.79000	-18.90631	2.86621
25	1.00000	0.79000	-18.90631	1.86431
26	1.00000	0.79000	-18.90631	-1.87451
27	1.00000	0.79000	-17.87368	-2.57971
28	1.00000	0.79000	-17.87368	-5.35678
29	1.00000	0.79000	-15.45986	-10.75969
30	1.00000	0.79000	-13.07294	-14.16881
31	1.00000	0.79000	-11.49207	-14.31601
32	1.00000	0.79000	-11.72165	-14.36336
33	1.00000	0.79000	-8.13937	-16.97290
34	1.00000	0.79000	-9.63464	-19.39633
35	1.00000	0.79000	-4.05010	-18.56332
36	1.00000	0.79000	-3.06793	-18.25068
37	1.00000	0.79000	0.69355	-18.68733
38	1.00000	0.79000	1.69136	-18.92455
39	1.00000	0.79000	5.39382	-18.92455
40	1.00000	0.79000	9.75507	-18.92455

Pier 41af.lp7o
 1.00000 5.39382 -18.21831
 0.79000 6.34476 -17.90933
 0.79000 9.75507 -16.30456
 1.00000 10.59930 -15.76879
 0.79000 13.50337 -13.36633
 1.00000 14.18784 -12.63745
 0.79000 16.40321 -9.58625
 0.79000 16.88491 -8.71205
 0.79000 18.27238 -5.20771
 0.79000 18.52104 -4.23924

NOTE: The positions of the above rebars were computed by LPile
 Minimum spacing between any two bars not equal to zero = -0.0001154 inches between
 Bars 1 and 2

Spacing to aggregate size ratio = -0.0003078

Concrete Properties:
 Compressive Strength of Concrete = 4500.00000 psi
 Modulus of Elasticity of Concrete = 3823676. psi
 Modulus of Rupture of Concrete = -503.11528 psi
 Compression Strain at Peak Stress = 0.00200
 Tensile Strain at Fracture of Concrete = -0.0001152
 Maximum Coarse Aggregate Size = 0.37500 in

Number of Axial Thrust Force Values Determined from Pile-head Loadings = 1

Number Axial Thrust Force
 kips

 1 0.000

Definitions of Run Messages and Notes:

 C = concrete in section has cracked in tension.
 Y = stress in reinforcing steel has reached yield stress.
 T = ACI 318-08 criteria for tension-controlled section met, tensile strain in
 reinforcement exceeds 0.005 while simultaneously compressive strain in
 concrete more than 0.003. See ACI 318-08, Section 10.3.4.
 Z = depth of tensile zone in concrete section is less than 10 percent of section
 depth.

Bending Stiffness (EI) = Computed Bending Moment / Curvature.
 Position of neutral axis is measured from edge of compression side of pile.
 Compressive stresses and strains are positive in sign.
 Tensile stresses and strains are negative in sign.

Axial Thrust Force = 0.000 kips
 Bending Moment Max Steel Bending Max Comp Max Tens
 Curvature Max Steel Moment Run N Axis
 Stress Stress Stress
 in-kip in in/in in/in in/in

ksi	ksi	ksi	Pier 41af.lp7o	ksi	ksi
0.00000625	1246.1877906	1993900465.	24.5001275	0.0000153	-0.0000153
0.0679356	0.4396242	0.4396242		0.0000306	-0.0000306
0.00001250	2488.7459054	1990996724.	24.5001279	0.0000459	-0.0000459
0.1353544	0.8792484	0.8792484		0.0000612	-0.0000612
0.00001875	3727.6743445	1988092984.	24.5001283	0.0000766	-0.0000766
0.2022566	1.3188726	1.3188726		0.0000919	-0.0000919
0.00002500	4962.9731077	1985189243.	24.5001286	0.0001072	-0.0001072
0.2686421	1.7584968	1.7584968		0.0001524	-0.0001524
0.00003125	6194.6421952	1982285502.	24.5001290	0.0001715	-0.0001715
0.3345108	2.1981210	2.1981210		0.0001905	-0.0001905
0.00003750	7422.6816068	1979381762.	24.5001294	0.0002095	-0.0002095
0.3998628	2.6377453	2.6377453		0.0002285	-0.0002285
0.00004375	8647.0913427	1976478021.	24.5001298	0.0002475	-0.0002475
0.4646981	3.0773696	3.0773696		0.0002665	-0.0002665
0.00005000	8647.0913427	1729418269.	18.5144499	0.0002854	-0.0002854
0.4015395	-4.3848797	-4.3848797		0.0003044	-0.0003044
0.00005625	8647.0913427	1537260683.	18.5199878	0.0003234	-0.0003234
0.4505457	-4.9320864	-4.9320864		0.0003423	-0.0003423
0.00006250	8647.0913427	1383534615.	18.5255374	0.0003613	-0.0003613
0.4992868	-5.4790901	-5.4790901		0.0003802	-0.0003802
0.00006875	8647.0913427	1257758741.	18.5310987	0.0003992	-0.0003992
0.5477623	-6.0258903	-6.0258903		0.0004181	-0.0004181
0.00007500	8894.9772711	1185996969.	18.5366719	0.0004370	-0.0004370
0.5959719	-6.5724864	-6.5724864		0.0004559	-0.0004559
0.00008125	9632.8701085	1185584013.	18.5422569	0.0004748	-0.0004748
0.6439151	-7.1188776	-7.1188776		0.0004937	-0.0004937
0.00008750	10370.	1185170297.	18.5478538	0.0005126	-0.0005126
0.6915914	-7.6650633	-7.6650633		0.0005315	-0.0005315
0.00009375	11107.	1184753819.	18.5534628	0.0005504	-0.0005504
0.7390003	-8.2110429	-8.2110429		0.0005693	-0.0005693
0.0001000	11843.	1184340574.	18.5590837	0.0005882	-0.0005882
0.7861415	-8.7568157	-8.7568157		0.0006071	-0.0006071
0.000106	12579.	118324560.	18.5647167	0.0006260	-0.0006260
0.8330144	-9.3023810	-9.3023810		0.0006449	-0.0006449
0.000113	13314.	1183507775.	18.5703619	0.0006638	-0.0006638
0.8796186	-9.8477382	-9.8477382		0.0006827	-0.0006827
0.000119	14049.	1183090214.	18.5760192	0.0007016	-0.0007016
0.9259536	-10.3928865	-10.3928865		0.0007205	-0.0007205
0.000125	14783.	1182671874.	18.5816888	0.0007394	-0.0007394
0.9720190	-10.9378253	-10.9378253		0.0007583	-0.0007583
0.000131	15517.	118252753.	18.5873707	0.0007772	-0.0007772
1.0178143	-11.4825539	-11.4825539		0.0007961	-0.0007961
0.000138	16250.	1181832847.	18.5930649	0.0008150	-0.0008150
1.0633390	-12.0270716	-12.0270716		0.0008339	-0.0008339
0.000144	16993.	1181412154.	18.5987715	0.0008528	-0.0008528
1.1083926	-12.5713777	-12.5713777		0.0008717	-0.0008717
0.000150	17713.	1180990669.	18.6044906	0.0008906	-0.0008906
1.1535747	-13.1154716	-13.1154716		0.0009095	-0.0009095
0.000156	18446.	1180568590.	18.6102222	0.0009284	-0.0009284
1.1962848	-13.6593524	-13.6593524		0.0009473	-0.0009473
0.000163	19172.	1180143512.	18.6159664	0.0009662	-0.0009662
1.2427224	-14.2030196	-14.2030196		0.0009851	-0.0009851
0.000169	19908.	1179724794.	18.6217231	0.0009999	-0.0009999
1.2868879	-14.7495653	-14.7495653		0.0010147	-0.0010147
0.000175	20657.	1179307322.	18.6274926	0.0010295	-0.0010295
1.3309787	-15.2897307	-15.2897307		0.0010443	-0.0010443
0.000181	21407.	1178897160.	18.6332748	0.0010591	-0.0010591
1.3739581	-15.8327316	-15.8327316		0.0010739	-0.0010739
0.000188	22157.	1178444660.	18.6390698	0.0010887	-0.0010887
1.4177383	-16.3755370	-16.3755370		0.0011035	-0.0011035

Pier 41af.jp7o		Pier 41af.jp7o	
0.0000194	22824.	1178017845.	18.6448776
1.4608062	-16.9181250	C	18.6506984
0.0000200	23552.	1175589911.	18.6565321
1.5035986	-17.4604949	C	18.6623788
0.0000206	24279.	1177161157.	18.6682387
1.5461152	-18.0026461	C	18.6741116
0.0000213	25006.	1176731577.	18.6799978
1.5883554	-18.5445778	C	18.6858973
0.0000219	25732.	1176301169.	18.6918101
1.6303186	-19.0862892	C	18.7036758
1.6720045	26457.	1175627796.	18.7155957
0.0000225	27182.	1175437855.	18.7275700
1.7134124	-20.1690483	C	18.7395995
1.7545419	28630.	117500945.	18.7516845
1.7953924	-21.2509174	C	18.7638256
0.0000244	30076.	1173701123.	18.7760234
1.8762546	-22.3318905	C	18.7882783
0.0000269	31520.	1172827657.	18.8005910
1.9559948	32961.	1171950748.	18.8129619
2.0346089	-24.4911229	C	18.8253917
2.1120926	34400.	1171070367.	18.8378808
0.0000306	35837.	1170186484.	18.8504300
2.1884416	-26.6466950	C	18.8589255
2.2636516	37271.	1169290688.	18.8705441
2.3377183	-27.7230922	C	18.88228946
0.0000344	38704.	1168406088.	18.8908550
2.4824038	40133.	1167313512.	18.9008353
2.5530137	-29.8730762	C	18.91425698
2.6224624	41561.	1166615309.	18.92405278
2.6907451	42986.	1165713445.	18.9329698
2.7578573	-30.9466494	C	18.9425698
2.8232113	44408.	1164807888.	18.9520000
2.8876274	45829.	1163986066.	18.961114
2.9443974	-32.0192676	C	18.9707739
3.0034056	47246.	1163132423.	18.9801194
3.0566932	48633.	1162363563.	18.9893985
3.1102262	-34.1615112	C	18.9987393
3.1622450	49971.	1161567545.	18.0000000
3.2127711	51397.	1160709000.	18.0000000
3.2619595	-36.3050439	C	18.0000000
0.0000331	52717.	1159410080.	18.0000000
	54197.	1158263473.	18.0000000
	55628.	1157142569.	18.0000000
	57078.	1156033301.	18.0000000
	58527.	115493301.	18.0000000
	59977.	115383430.	18.0000000
	61427.	115274052.	18.0000000
	62877.	115164646.	18.0000000
	64327.	115055472.	18.0000000
	65777.	114946452.	18.0000000
	67227.	114837329.	18.0000000
	68677.	114728210.	18.0000000
	70127.	114619078.	18.0000000
	71577.	114510000.	18.0000000
	73027.	114400923.	18.0000000
	74477.	114291846.	18.0000000
	75927.	114182769.	18.0000000
	77377.	114073692.	18.0000000
	78827.	113964615.	18.0000000
	80277.	113855538.	18.0000000
	81727.	113746461.	18.0000000
	83177.	113637384.	18.0000000
	84627.	113528307.	18.0000000
	86077.	113419230.	18.0000000
	87527.	113310153.	18.0000000
	88977.	113201076.	18.0000000
	90427.	113091999.	18.0000000
	91877.	112982922.	18.0000000
	93327.	112873845.	18.0000000
	94777.	112764768.	18.0000000
	96227.	112655691.	18.0000000
	97677.	112546614.	18.0000000
	99127.	112437537.	18.0000000
	100577.	112328460.	18.0000000
	102027.	112219383.	18.0000000
	103477.	112110306.	18.0000000
	104927.	112001229.	18.0000000
	106377.	111892152.	18.0000000
	107827.	111783075.	18.0000000
	109277.	111673998.	18.0000000
	110727.	111564921.	18.0000000
	112177.	111455844.	18.0000000
	113627.	111346767.	18.0000000
	115077.	111237690.	18.0000000
	116527.	111128613.	18.0000000
	117977.	111019536.	18.0000000
	119427.	110910459.	18.0000000
	120877.	110801382.	18.0000000
	122327.	110692305.	18.0000000
	123777.	110583228.	18.0000000
	125227.	110474151.	18.0000000
	126677.	110365074.	18.0000000
	128127.	110255997.	18.0000000
	129577.	110146920.	18.0000000
	131027.	110037843.	18.0000000
	132477.	109928766.	18.0000000
	133927.	109819689.	18.0000000
	135377.	109710612.	18.0000000
	136827.	109601535.	18.0000000
	138277.	109492458.	18.0000000
	139727.	109383381.	18.0000000
	141177.	109274304.	18.0000000
	142627.	109165227.	18.0000000
	144077.	109056150.	18.0000000
	145527.	108947073.	18.0000000
	146977.	108837996.	18.0000000
	148427.	108728919.	18.0000000
	149877.	108619842.	18.0000000
	151327.	108510765.	18.0000000
	152777.	108401688.	18.0000000
	154227.	108292611.	18.0000000
	155677.	108183534.	18.0000000
	157127.	108074457.	18.0000000
	158577.	107965380.	18.0000000
	160027.	107856303.	18.0000000
	161477.	107747226.	18.0000000
	162927.	107638149.	18.0000000
	164377.	107529072.	18.0000000
	165827.	107419995.	18.0000000
	167277.	107310918.	18.0000000
	168727.	107201841.	18.0000000
	170177.	107092764.	18.0000000
	171627.	106983687.	18.0000000
	173077.	106874610.	18.0000000
	174527.	106765533.	18.0000000
	175977.	106656456.	18.0000000
	177427.	106547379.	18.0000000
	178877.	106438302.	18.0000000
	180327.	106329225.	18.0000000
	181777.	106220148.	18.0000000
	183227.	106111071.	18.0000000
	184677.	106001994.	18.0000000
	186127.	105892917.	18.0000000
	187577.	105783840.	18.0000000
	189027.	105674763.	18.0000000
	190477.	105565686.	18.0000000
	191927.	105456609.	18.0000000
	193377.	105347532.	18.0000000
	194827.	105238455.	18.0000000
	196277.	105129378.	18.0000000
	197727.	105020301.	18.0000000
	199177.	104911224.	18.0000000
	200627.	104802147.	18.0000000
	202077.	104693070.	18.0000000
	203527.	104583993.	18.0000000
	204977.	104474916.	18.0000000
	206427.	104365839.	18.0000000
	207877.	104256762.	18.0000000
	209327.	104147685.	18.0000000
	210777.	104038608.	18.0000000
	212227.	103929531.	18.0000000
	213677.	103820454.	18.0000000
	215127.	103711377.	18.0000000
	216577.	103602300.	18.0000000
	218027.	103493223.	18.0000000
	219477.	103384146.	18.0000000
	220927.	103275069.	18.0000000
	222377.	103165992.	18.0000000
	223827.	103056915.	18.0000000
	225277.	102947838.	18.0000000
	226727.	102838761.	18.0000000
	228177.	102729684.	18.0000000
	229627.	102620607.	18.0000000
	231077.	102511530.	18.0000000
	232527.	102402453.	18.0000000
	233977.	102293376.	18.0000000
	235427.	102184299.	18.0000000
	236877.	102075222.	18.0000000
	238327.	101966145.	18.0000000
	239777.	101857068.	18.0000000
	241227.	101747991.	18.0000000
	242677.	101638914.	18.0000000
	244127.	101529837.	18.0000000
	245577.	101420760.	18.0000000
	247027.	101311683.	18.0000000
	248477.	101202606.	18.0000000
	249927.	101093529.	18.0000000
	251377.	100984452.	18.0000000
	252827.	100875375.	18.0000000
	254277.	100766298.	18.0000000
	255727.	100657221.	18.0000000
	257177.	100548144.	18.0000000
	258627.	100439067.	18.0000000
	260077.	100329990.	18.0000000
	261527.	100220913.	18.0000000
	262977.	100111836.	18.0000000
	264427.	100002759.	18.0000000
	265877.	99899502.	18.0000000
	267327.	99778725.	18.0000000
	268777.	99657948.	18.0000000
	270227.	99537171.	18.0000000
	271677.	99416394.	18.0000000
	273127.	99295617.	18.0000000
	274577.	99174840.	18.0000000
	276027.	99054063.	18.0000000
	277477.	98933286.	18.0000000
	278927.	98812509.	18.0000000
	280377.	98691732.	18.0000000
	281827.	98570955.	18.0000000
	283277.	98450178.	18.0000000
	284727.	98329401.	18.0000000
	286177.	98208624.	18.0000000
	287627.	98087847.	18.0000000
	289077.	97967070.	18.0000000
	290527.	97846293.	18.0000000
	291977.	97725516.	18.0000000
	293427.	97604739.	18.0000000
	294877.	97483962.	18.0000000
	296327.	97363185.	18.0000000
	297777.	97242408.	18.0000000
	299227.	97121631.	18.0000000
	300677.	97000854.	18.0000000
	302127.	96880077.	18.0000000
	303577.	96759300.	18.0000000
	305027.	96638523.	18.0000000
	306477.	96517746.	18.0000000
	307927.	96396969.	18.0000000
	309377.	96276192.	18.0000000
	310827.	96155415.	18.0000000
	312277.	96034638.	18.0000000
	313727.	95913861.	18.0000000
	315177.	95793084.	18.0000000
	316627.	95672307.	18.0000000
	318077.	95551530.	18.0000000
	319527.	95430753.	18.0000000
	320977.	95310000.	18.0000000
	322427.	95189223.	18.0000000
	323877.	95068446.	18.0000000
	325327.	94947669.	18.0000000
	326777.	94826892.	18.0000000
	328227.	94706115.	18.0000000
	329677.	94585338.	18.0000000
	331127.	94464561.	18.0000000
	332577.	94343784.	18.0000000
	334027.	94223007.	18.0000000
	335477.	94102230.	18.0000000
	336927.	93981453.	18.0000000
	338377.	93860676.	18.0000000
	339827.	93739899.	18.0000000
	341277.	93619122.	18.0000000
	342727.	93498345.	18.0000000
	344177.	93377568.	18.0000000
	345627.	93256791.	18.0000000
	347077.	93136014.	18.0000000
	348527.	93015237.	18.0000000
	349977.	92894460.	18.0000000

Pier 41af.1p7o

Load No.	Axial Thrust kips	Nominal Mem. Cap. in-kip	Max. Comp. Strain
0.0001494	83870.		
4.4967207	60.0000000	561472182.	0.0024224
0.0001544	84197.	16.2171924	-0.0048969
4.4959984	60.0000000	36.0000000	0.0024912
0.0001594	84492.	16.1373405	-0.0050732
4.4952081	60.0000000	36.0000000	0.0025599
0.0001644	84764.	16.0618326	-0.0052495
4.4963383	60.0000000	36.0000000	0.0026282
0.0001694	85016.	15.9893153	-0.0054261
4.4958938	60.0000000	36.0000000	0.0026964
0.0001744	85250.	15.9198154	-0.0056030
4.4973913	60.0000000	36.0000000	0.0027642
0.0001794	85470.	15.8522568	-0.0057801
4.4959838	60.0000000	36.0000000	0.0028319
0.0001844	85672.	15.7875418	-0.0059575
4.4971898	60.0000000	36.0000000	0.0028993
0.0001894	85863.	15.7250435	-0.0061351
4.4992099	60.0000000	36.0000000	0.0029666
0.0001944	86039.	15.6654328	-0.0063127
4.4956681	60.0000000	36.0000000	0.0030339
0.0001994	86203.	15.6085953	-0.0064905
4.4939379	60.0000000	36.0000000	0.0031010
0.0002044	86354.	15.5537463	-0.0066683
4.4940147	60.0000000	36.0000000	0.0031683
0.0002094	86502.	15.5023858	-0.0068461
4.4974792	60.0000000	36.0000000	0.0032358
0.0002144	86628.	15.4543831	-0.0070236
4.4927456	60.0000000	36.0000000	0.0033035
0.0002194	86741.	15.4101001	-0.0072008
4.4976689	60.0000000	36.0000000	0.0033715
0.0002244	86847.	15.3687912	-0.0073778
4.4922294	60.0000000	36.0000000	0.0034394
0.0002344	87016.	15.3287878	-0.0075550
4.4910346	60.0000000	36.0000000	0.0035080
0.0002394	87093.	15.2937898	-0.0077314
4.4964573	60.0000000	36.0000000	0.0035766
0.0002444	87157.	15.2602682	-0.0079077
4.4994370	60.0000000	36.0000000	0.0036453
0.0002494	87214.	15.2284729	-0.0080841
4.4957504	60.0000000	36.0000000	0.0037146
0.0002544	87270.	15.2004065	-0.0082598
4.4929161	60.0000000	36.0000000	0.0037838
		343075082.	-0.0084355
		36.0000000	0.0038533
			-0.0086111

Summary of Results for Nominal (Unfactored) Moment Capacity for Section 2

Moment values interpolated at maximum compressive strain = 0.003 or maximum developed moment if pile fails at smaller strains.

Load No.	Axial Thrust kips	Nominal Mem. Cap. in-kip	Max. Comp. Strain
1	0.000	85950.433	0.00300000

Note that the values of moment capacity in the table above are not factored by a strength reduction factor (phi-factor).

In ACI 318-08, the value of the strength reduction factor depends on whether the transverse reinforcing steel bars are tied hoops (0.65) or spirals (0.70).

The above values should be multiplied by the appropriate strength reduction factor to compute ultimate moment capacity according to ACI 318-08, Section 9.3.2.2 or the value required by the design standard being followed.

The following table presents factored moment capacities and corresponding bending stiffnesses computed for common resistance factor values used for reinforced concrete sections.

Axial Load Capacity in-kip	Resistance Factor at Ult. Mom. Cap. for Moment	Bending Stiffness at Ult. Mom. Cap. kip-in ²	Nominal Moment Capacity in-kip	Ultimate (Factored) Axial Thrust kips	Ultimate Moment
55867.779	0.65	1105241617.673	85950.433	0.000	
60165.302	0.70	1056639830.845	85950.433	0.000	
64462.825	0.75	1006420922.590	85950.433	0.000	

Computed Values of Pile Loading and Deflection for Lateral Loading for Load Case Number 1

Pile-head conditions are Displacement and Moment (Loading Type 4)
 Displacement of pile head = 0.500000 inches
 Moment at pile head = 3793200.0 in-lbs
 Axial load at pile head = 0.0 lbs

Depth res. feet	Soil X Es ² h ³ lb/inch	Deflect. Lat. Load in-lbs	Bending Moment in-lbs	Shear Force lbs	Slope S radians	Total stress psi*	Bending Stiffness lb-in ²
0.000	0.00	0.000	3793200.	23022.	-0.002030	0.000	1.343E+12
0.000	0.993	0.000	4760 0.000	23022.	-0.001995	0.000	1.343E+12
0.000	1.986	0.000	4525 4341804.	23022.	-0.001958	0.000	1.341E+12
0.000	2.979	0.000	4294 4616107.	23022.	-0.001918	0.000	1.340E+12
0.000	3.972	0.000	4067 4890409.	23022.	-0.001883	0.000	1.985E+12
0.000	4.965	0.000	3845 5164711.	23022.	-0.001853	0.000	1.985E+12
0.000	5.957	0.000	3626 5439013.	23022.	-0.001821	0.000	1.984E+12
0.000	6.950	0.000	3411 5713315.	23022.	-0.001787	0.000	1.983E+12

Pier 4laf.lp7o			Pier 4laf.lp7o		
0.000	7.943	0.3200	0.000	1.983E+12	0.000
0.000	8.936	0.2993	0.000	1.982E+12	0.000
0.000	9.929	0.2791	0.000	1.981E+12	0.000
0.000	10.922	0.2594	0.000	1.981E+12	0.000
0.000	11.915	0.2401	0.000	1.980E+12	0.000
0.000	12.908	0.2214	0.000	1.980E+12	0.000
0.000	13.901	0.2031	0.000	1.979E+12	0.000
0.000	14.893	0.1855	0.000	1.978E+12	0.000
-162.9463	10468.	0.0000	0.000	1.978E+12	0.000
15.886	8158903.	0.1684	0.000	1.978E+12	0.000
-53.4715	3784.1319	0.0000	0.000	1.978E+12	0.000
-160.5122	12595.	0.1518	0.000	1.977E+12	0.000
-252.7019	22152.	0.1359	0.000	1.977E+12	0.000
-310.1623	30670.	0.1207	0.000	1.977E+12	0.000
-350.1920	39187.	0.1065	0.000	1.977E+12	0.000
-373.7190	47705.	0.0933	0.000	1.977E+12	0.000
-383.5722	56223.	0.0813	0.000	1.977E+12	0.000
-387.0975	64741.	0.0703	0.000	1.977E+12	0.000
-371.6133	73258.	0.0604	0.000	1.977E+12	0.000
-354.3980	81776.	0.0516	0.000	1.977E+12	0.000
-332.3636	90294.	0.0439	0.000	1.977E+12	0.000
-307.8606	98637.	0.0371	0.000	1.977E+12	0.000
-279.7871	107323.	0.0310	0.000	1.977E+12	0.000
-247.3179	115845.	0.0254	0.000	1.977E+12	0.000
-157.20987	124376.	0.0204	0.000	1.977E+12	0.000
-149.3179	132906.	0.0160	0.000	1.977E+12	0.000
-139.9456	141436.	0.0120	0.000	1.977E+12	0.000
-128.7800	149966.	0.008594	0.000	1.977E+12	0.000
-114.9212	158496.	0.00509	0.000	1.977E+12	0.000
-96.4579	167026.	0.003053	0.000	1.977E+12	0.000
-65.8223	175556.	0.001895	0.000	1.977E+12	0.000
67.6298	184086.	-0.000898	0.000	1.977E+12	0.000
95.7251	192616.	-0.002358	0.000	1.977E+12	0.000
38.723	201146.	-0.003518	0.000	1.977E+12	0.000
112.1388	379740.	0.0000	0.000	1.983E+12	0.000
123.8784	334668.	0.004410	0.000	1.982E+12	0.000
132.8256	312334.	0.005064	0.000	1.981E+12	0.000
139.7961	302420.	0.005508	0.000	1.981E+12	0.000
145.2257	299897.	0.005770	0.000	1.980E+12	0.000
167.3823	339402.	0.005876	0.000	1.980E+12	0.000
180.8347	368249.	0.005851	0.000	1.979E+12	0.000
190.4262	396829.	0.005718	0.000	1.978E+12	0.000
191.2517	414574.	0.005497	0.000	1.978E+12	0.000
188.9634	432319.	0.005208	0.000	1.977E+12	0.000
183.8734	450064.	0.004868	0.000	1.978E+12	0.000
176.3613	467810.	0.004492	0.000	1.978E+12	0.000
166.8113	485555.	0.004093	0.000	1.978E+12	0.000
155.6123	503300.	0.003684	0.000	1.978E+12	0.000
143.1481	521046.	0.003273	0.000	1.978E+12	0.000
129.7905	538791.	0.002870	0.000	1.978E+12	0.000
115.8935	556536.	0.002467	0.000	1.978E+12	0.000
101.7885	574282.	0.002064	0.000	1.978E+12	0.000
87.7821	592027.	0.001661	0.000	1.978E+12	0.000
74.1345	609772.	0.001258	0.000	1.978E+12	0.000
108.8993	1117300.	0.001161	0.000	1.978E+12	0.000
96.1478	1265535.	0.001095	0.000	1.978E+12	0.000
83.4238	1458760.	0.001060	0.000	1.978E+12	0.000
70.7246	1720400.	0.001029	0.000	1.978E+12	0.000
57.9533	2098600.	0.000997	0.000	1.978E+12	0.000
44.8262	2719978.	0.000970	0.000	1.978E+12	0.000
30.5763	3986733.	0.000943	0.000	1.978E+12	0.000
9.6319	5312642.	0.000916	0.000	1.978E+12	0.000
66.524	57255.	0.000895	0.000	1.978E+12	0.000
-23.2302	5237431.	0.000870	0.000	1.978E+12	0.000
-31.6185	3848194.	0.000845	0.000	1.978E+12	0.000
-68.510	0.000129	0.000820	0.000	1.978E+12	0.000
-36.3215	3349883.	0.000795	0.000	1.978E+12	0.000
-69.503	0.000149	0.000770	0.000	1.978E+12	0.000
-39.0733	3114087.	0.000745	0.000	1.978E+12	0.000
3339332.	0.000	-34612.	-6.485E-05	0.000	1.989E+12
2935727.	0.000	-33083.	-4.605E-05	0.000	1.990E+12
2550979.	0.000	-31459.	-2.963E-05	0.000	1.991E+12
2186077.	0.000	-29761.	-1.546E-05	0.000	1.991E+12
1841791.	0.000	-27898.	-3.407E-06	0.000	1.992E+12
1521267.	0.000	-25824.	6.649E-06	0.000	1.993E+12
1228415.	0.000	-23612.	1.486E-05	0.000	1.994E+12
958596.	0.000	-21338.	2.139E-05	0.000	1.994E+12
717929.	0.000	-19073.	2.640E-05	0.000	1.994E+12
504088.	0.000	-16852.	3.005E-05	0.000	1.994E+12
316551.	0.000	-14706.	3.250E-05	0.000	1.994E+12
153649.	0.000	-12662.	3.390E-05	0.000	1.994E+12
14629.	0.000	-10741.	3.441E-05	0.000	1.994E+12
-102300.	0.000	-8960.9847	3.415E-05	0.000	1.994E+12
-198908.	0.000	-7334.9804	3.325E-05	0.000	1.994E+12
-277090.	0.000	-5871.3426	3.182E-05	0.000	1.994E+12
-338819.	0.000	-4574.5242	2.998E-05	0.000	1.994E+12
-386099.	0.000	-3445.1766	2.782E-05	0.000	1.994E+12
-420917.	0.000	-2480.4566	2.541E-05	0.000	1.994E+12
-443207.	0.000	-1389.9331	2.282E-05	0.000	1.994E+12
-50058.	0.000	-168.3859	2.013E-05	0.000	1.994E+12
-109220.	0.000	901.4060	1.743E-05	0.000	1.994E+12
-432558.	0.000	1819.7419	1.480E-05	0.000	1.994E+12
-405856.	0.000	2586.3274	1.229E-05	0.000	1.994E+12
-370927.	0.000	3198.6854	9.972E-06	0.000	1.994E+12
-329633.	0.000	3647.6341	7.879E-06	0.000	1.994E+12
-284005.	0.000	3886.8568	6.046E-06	0.000	1.994E+12
-237010.	0.000	3805.8463	4.489E-06	0.000	1.994E+12
-193313.	0.000	3479.0907	3.203E-06	0.000	1.994E+12
-154105.	0.000	3074.3450	2.165E-06	0.000	1.994E+12
-120053.	0.000	2625.1877	1.346E-06	0.000	1.994E+12

Pier 41af.lp7o

70.496	0.000161	-91548.	2150.6486	7.141E-07	1.994E+12	0.000
-40.5821	2998335.	0.000	1663.2176	2.350E-07	1.994E+12	0.000
-1.171	2950707.	0.000	1171.6242	-1.257E-07	1.994E+12	0.000
-41.2373	2950707.	0.000	875.1525	-4.030E-07	1.994E+12	0.000
-41.2808	2947616.	0.000	774.5999	-6.179E-07	1.994E+12	0.000
-8.4845	618227.	0.000	675.9586	-7.777E-07	1.994E+12	0.000
-8.3941	635972.	0.000	580.7490	-8.894E-07	1.994E+12	0.000
-8.1637	653717.	0.000	490.2027	-9.598E-07	1.994E+12	0.000
-7.8181	672462.	0.000	405.2787	-9.952E-07	1.994E+12	0.000
-7.3809	689208.	0.000	326.6835	-1.002E-06	1.994E+12	0.000
-6.8743	706953.	0.000	254.8940	-9.851E-07	1.994E+12	0.000
-6.3186	724698.	0.000	190.1831	-9.502E-07	1.994E+12	0.000
-5.7319	742444.	0.000	132.6476	-9.019E-07	1.994E+12	0.000
-5.1303	760189.	0.000	82.2350	-8.440E-07	1.994E+12	0.000
-4.5275	777934.	0.000	38.7722	-7.804E-07	1.994E+12	0.000
-3.9347	795680.	0.000	1.9918	-7.139E-07	1.994E+12	0.000
-3.3609	813423.	0.000	-28.4411	-6.473E-07	1.994E+12	0.000
-2.8130	831170.	0.000	-52.9050	-5.828E-07	1.994E+12	0.000
-2.2734	848916.	0.000	-71.7994	-5.220E-07	1.994E+12	0.000
-1.7375	866653.	0.000	-85.5246	-4.663E-07	1.994E+12	0.000
-1.2006	884406.	0.000	-94.4639	-4.167E-07	1.994E+12	0.000
-0.6633	902156.	0.000	-98.9684	-3.739E-07	1.994E+12	0.000
-0.1271	919897.	0.000	-99.3450	-3.381E-07	1.994E+12	0.000
0.4157	937643.	0.000	-95.8465	-3.093E-07	1.994E+12	0.000
0.9333	955387.	0.000	-88.6658	-2.874E-07	1.994E+12	0.000
1.4515	973133.	0.000	-77.9330	-2.718E-07	1.994E+12	0.000
1.9738	990878.	0.000	-63.7152	-2.618E-07	1.994E+12	0.000
2.5018	1008623.	0.000	-46.0212	-2.563E-07	1.994E+12	0.000
3.0308	1028369.	0.000	-24.8095	-2.540E-07	1.994E+12	0.000
3.5608	1048114.	0.000	0.000	-2.535E-07	1.994E+12	0.000
4.0908	1067859.	0.000				
4.6208	1087604.	0.000				
5.1508	1107349.	0.000				
5.6808	1127094.	0.000				
6.2108	1146839.	0.000				
6.7408	1166584.	0.000				
7.2708	1186329.	0.000				
7.8008	1206074.	0.000				
8.3308	1225819.	0.000				
8.8608	1245564.	0.000				
9.3908	1265309.	0.000				
9.9208	1285054.	0.000				
10.4508	1304799.	0.000				
10.9808	1324544.	0.000				
11.5108	1344289.	0.000				
12.0408	1364034.	0.000				
12.5708	1383779.	0.000				
13.1008	1403524.	0.000				
13.6308	1423269.	0.000				
14.1608	1443014.	0.000				
14.6908	1462759.	0.000				
15.2208	1482504.	0.000				
15.7508	1502249.	0.000				
16.2808	1521994.	0.000				
16.8108	1541739.	0.000				
17.3408	1561484.	0.000				
17.8708	1581229.	0.000				
18.4008	1600974.	0.000				
18.9308	1620719.	0.000				
19.4608	1640464.	0.000				
19.9908	1660209.	0.000				
20.5208	1679954.	0.000				
21.0508	1699699.	0.000				
21.5808	1719444.	0.000				
22.1108	1739189.	0.000				
22.6408	1758934.	0.000				
23.1708	1778679.	0.000				
23.7008	1798424.	0.000				
24.2308	1818169.	0.000				
24.7608	1837914.	0.000				
25.2908	1857659.	0.000				
25.8208	1877404.	0.000				
26.3508	1897149.	0.000				
26.8808	1916894.	0.000				
27.4108	1936639.	0.000				
27.9408	1956384.	0.000				
28.4708	1976129.	0.000				
29.0008	1995874.	0.000				
29.5308	2015619.	0.000				
30.0608	2035364.	0.000				
30.5908	2055109.	0.000				
31.1208	2074854.	0.000				
31.6508	2094599.	0.000				
32.1808	2114344.	0.000				
32.7108	2134089.	0.000				
33.2408	2153834.	0.000				
33.7708	2173579.	0.000				
34.3008	2193324.	0.000				
34.8308	2213069.	0.000				
35.3608	2232814.	0.000				
35.8908	2252559.	0.000				
36.4208	2272304.	0.000				
36.9508	2292049.	0.000				
37.4808	2311794.	0.000				
38.0108	2331539.	0.000				
38.5408	2351284.	0.000				
39.0708	2371029.	0.000				
39.6008	2390774.	0.000				
40.1308	2410519.	0.000				
40.6608	2430264.	0.000				
41.1908	2450009.	0.000				
41.7208	2469754.	0.000				
42.2508	2489499.	0.000				
42.7808	2509244.	0.000				
43.3108	2528989.	0.000				
43.8408	2548734.	0.000				
44.3708	2568479.	0.000				
44.9008	2588224.	0.000				
45.4308	2607969.	0.000				
45.9608	2627714.	0.000				
46.4908	2647459.	0.000				
47.0208	2667204.	0.000				
47.5508	2686949.	0.000				
48.0808	2706694.	0.000				
48.6108	2726439.	0.000				
49.1408	2746184.	0.000				
49.6708	2765929.	0.000				
50.2008	2785674.	0.000				
50.7308	2805419.	0.000				
51.2608	2825164.	0.000				
51.7908	2844909.	0.000				
52.3208	2864654.	0.000				
52.8508	2884399.	0.000				
53.3808	2904144.	0.000				
53.9108	2923889.	0.000				
54.4408	2943634.	0.000				
54.9708	2963379.	0.000				
55.5008	2983124.	0.000				
56.0308	3002869.	0.000				
56.5608	3022614.	0.000				
57.0908	3042359.	0.000				
57.6208	3062104.	0.000				
58.1508	3081849.	0.000				
58.6808	3101594.	0.000				
59.2108	3121339.	0.000				
59.7408	3141084.	0.000				
60.2708	3160829.	0.000				
60.8008	3180574.	0.000				
61.3308	3200319.	0.000				
61.8608	3220064.	0.000				
62.3908	3239809.	0.000				
62.9208	3259554.	0.000				
63.4508	3279299.	0.000				
63.9808	3299044.	0.000				
64.5108	3318789.	0.000				
65.0408	3338534.	0.000				
65.5708	3358279.	0.000				
66.1008	3378024.	0.000				
66.6308	3397769.	0.000				
67.1608	3417514.	0.000				
67.6908	3437259.	0.000				
68.2208	3457004.	0.000				
68.7508	3476749.	0.000				
69.2808	3496494.	0.000				
69.8108	3516239.	0.000				
70.3408	3535984.	0.000				
70.8708	3555729.	0.000				
71.4008	3575474.	0.000				
71.9308	3595219.	0.000				
72.4608	3614964.	0.000				
72.9908	3634709.	0.000				
73.5208	3654454.	0.000				
74.0508	3674199.	0.000				
74.5808	3693944.	0.000				
75.1108	3713689.	0.000				
75.6408	3733434.	0.000				
76.1708	3753179.	0.000				
76.7008	3772924.	0.000				
77.2308	3792669.	0.000				
77.7608	3812414.	0.000				
78.2908	3832159.	0.000				
78.8208	3851904.	0.000				
79.3508	3871649.	0.000				
79.8808	3891394.	0.000				
80.4108	3911139.	0.000				
80.9408	3930884.	0.000				
81.4708	3950629.	0.000				

Pier 41af.lp7o

-17.0575	618227.	0.000	0.000	1.994E+12	0.000	1.994E+12
74.468	0.000318	-69598.	1630.3063	-1.072E-06	0.000	1.994E+12
-16.9977	635972.	0.000	1429.9416	-1.433E-06	0.000	1.994E+12
75.460	0.000303	-51380.	1235.3932	-1.693E-06	0.000	1.994E+12
-16.6353	653717.	0.000	1049.3670	-1.865E-06	0.000	1.994E+12
76.453	0.000284	-35523.	874.0028	-1.962E-06	0.000	1.994E+12
-16.0213	671462.	0.000	710.9125	-1.996E-06	0.000	1.994E+12
77.446	0.000263	-21941.	561.2264	-1.981E-06	0.000	1.994E+12
-15.2047	689208.	0.000	425.6444	-1.925E-06	0.000	1.994E+12
78.439	0.000240	-10517.	304.4907	-1.839E-06	0.000	1.994E+12
-14.2316	706953.	0.000	197.7703	-1.731E-06	0.000	1.994E+12
79.432	0.000216	-1113.9276	105.2263	-1.609E-06	0.000	1.994E+12
-13.1445	724698.	0.000	26.3960	-1.480E-06	0.000	1.994E+12
80.425	0.000192	6423.4422	-39.3355	-1.348E-06	0.000	1.994E+12
-11.9816	742444.	0.000	-92.6841	-1.220E-06	0.000	1.994E+12
81.418	0.000169	12260.	-134.4194	-1.098E-06	0.000	1.994E+12
-10.7770	760189.	0.000	-165.3221	-9.857E-07	0.000	1.994E+12
82.411	0.000146	16566.	-186.1463	-8.852E-07	0.000	1.994E+12
-9.5597	777934.	0.000	-197.5867	-7.979E-07	0.000	1.994E+12
83.404	0.000125	19516.	-200.2525	-7.247E-07	0.000	1.994E+12
-8.3542	795680.	0.000	-194.6465	-6.658E-07	0.000	1.994E+12
84.396	0.000105	21279.	-181.1511	-6.207E-07	0.000	1.994E+12
-7.1801	813425.	0.000	-160.0211	-5.885E-07	0.000	1.994E+12
85.389	8.676E-05	22023.	-131.3835	-5.677E-07	0.000	1.994E+12
-6.0523	831170.	0.000	-95.2453	-5.563E-07	0.000	1.994E+12
86.382	6.991E-05	21908.	-51.5095	-5.516E-07	0.000	1.994E+12
-4.9813	848916.	0.000	0.000	-5.506E-07	0.000	1.994E+12
87.375	5.463E-05	21086.	0.000	0.000	0.000	1.994E+12
-3.9737	866661.	0.000	0.000	0.000	0.000	1.994E+12
88.368	4.085E-05	19700.	0.000	0.000	0.000	1.994E+12
-3.0319	884406.	0.000	0.000	0.000	0.000	1.994E+12
89.361	2.847E-05	17883.	0.000	0.000	0.000	1.994E+12
-2.1553	902151.	0.000	0.000	0.000	0.000	1.994E+12
90.354	1.736E-05	15760.	0.000	0.000	0.000	1.994E+12
-1.3402	919897.	0.000	0.000	0.000	0.000	1.994E+12
91.347	7.373E-06	13447.	0.000	0.000	0.000	1.994E+12
-0.5802	937642.	0.000	0.000	0.000	0.000	1.994E+12
92.340	-1.655E-06	11052.	0.000	0.000	0.000	1.994E+12
0.1327	955387.	0.000	0.000	0.000	0.000	1.994E+12
93.333	-9.896E-06	8675.0247	0.000	0.000	0.000	1.994E+12
0.8083	973133.	0.000	0.000	0.000	0.000	1.994E+12
94.325	-1.752E-05	6413.2235	0.000	0.000	0.000	1.994E+12
1.4570	990878.	0.000	0.000	0.000	0.000	1.994E+12
2.0898	1008623.	0.000	0.000	0.000	0.000	1.994E+12
2.7172	1026369.	0.000	0.000	0.000	0.000	1.994E+12
3.3489	1044114.	0.000	0.000	0.000	0.000	1.994E+12
3.9926	1061859.	0.000	0.000	0.000	0.000	1.994E+12
4.6537	539802.	0.000	0.000	0.000	0.000	1.994E+12

* This analysis computed pile response using nonlinear moment-curvature relationships.
 Values of total stress due to combined axial and bending stresses are computed only for elastic sections only and do not equal the actual stresses in concrete and steel.
 Stresses in concrete and steel may be interpolated from the output for nonlinear bending properties relative to the magnitude of bending moment developed in the pile.

Pier 41af.lp7o

Output Summary for Load Case No. 2:

Pile-head deflection = 1.000000 inches
 Computed slope at pile head = -0.0038805 radians
 Maximum bending moment = 14522309.1 inch-lbs
 Maximum shear force = -59840. lbs
 Depth of maximum bending moment = 22.8367000 feet below pile head
 Depth of maximum shear force = 35.7444000 feet below pile head
 Number of iterations = 70
 Number of zero deflection points = 3

Computed Values of Pile Loading and Deflection for Lateral Loading for Load Case Number 3

Pile-head conditions are Displacement and Moment (Loading Type 4)
 Displacement of pile head = 1.500000 inches
 Moment at pile head = 3793200.0 in-lbs
 Axial load at pile head = 0.0 lbs

Res. X	Depth	Deflect.	Bending	Shear	Slope	Total	Bending
Soil	Soil	spr.	Distrib.	Force	S	Stress	Stiffness
				lbs	radians	psi*	lb-in ²
							lb/in
0.00	0.00	1.5000	3793200.	64823.	-0.005697	0.000	1.343E+12
0.000	0.993	0.000	0.000	64823.	-0.005660	0.000	1.343E+12
0.000	1.986	0.000	4565551.	64823.	-0.005616	0.000	1.338E+12
0.000	2.979	0.000	0.000	64823.	-0.005505	0.000	4.190E+11
0.000	3.972	0.000	6110253.	64823.	-0.005398	0.000	1.981E+12
0.000	4.965	0.000	6882604.	64823.	-0.005354	0.000	1.979E+12
0.000	5.957	0.000	7654955.	64823.	-0.005305	0.000	1.977E+12
0.000	6.950	0.000	8427306.	64823.	-0.005234	0.000	1.186E+12
0.000	7.943	0.000	9199657.	64823.	-0.005137	0.000	1.185E+12
0.000	8.936	0.000	9972008.	64823.	-0.005033	0.000	1.185E+12
0.000	9.929	0.000	10744359.	64823.	-0.004921	0.000	1.185E+12
0.000	10.922	0.000	11516710.	64823.	-0.004802	0.000	1.184E+12
0.000	11.915	0.000	12289061.	64823.	-0.004674	0.000	1.184E+12
0.000	12.908	0.000	13061412.	64823.	-0.004539	0.000	1.183E+12
0.000	13.901	0.000	13833763.	64823.	-0.004395	0.000	1.183E+12
0.000	14.894	0.000	14606114.	64823.	-0.004250	0.000	1.182E+12

Pier 41af.jp7o	Pier 41af.jp7o			Pier 41af.jp7o
14.893	0.5876	15378465.	0.000	1.182E+12
-239.3203	4852.4148	0.000	0.000	1.182E+12
15.886	0.5380	16116841.	0.000	1.182E+12
-72.7275	1610.6911	0.000	0.000	1.182E+12
16.879	0.4903	16844893.	0.000	1.181E+12
-222.2336	5400.7641	0.000	0.000	1.181E+12
17.872	0.4446	17541396.	0.000	1.181E+12
-382.0481	10239.	0.000	0.000	1.181E+12
18.865	0.4010	18183663.	0.000	1.180E+12
-539.9012	16042.	0.000	0.000	1.180E+12
19.858	0.3596	18749284.	0.000	1.180E+12
-685.6145	22716.	0.000	0.000	1.180E+12
20.851	0.3205	19217573.	0.000	1.180E+12
-811.5757	30173.	0.000	0.000	1.180E+12
21.844	0.2837	19570649.	0.000	1.180E+12
-914.8156	38427.	0.000	0.000	1.180E+12
22.837	0.2492	19793856.	0.000	1.180E+12
-995.5391	47603.	0.000	0.000	1.180E+12
23.830	0.2171	19875733.	0.000	1.180E+12
-1047.6715	57500.	0.000	0.000	1.180E+12
24.823	0.1874	19808881.	0.000	1.180E+12
-1077.1040	68484.	0.000	0.000	1.180E+12
25.815	0.1601	19589120.	0.000	1.180E+12
-1071.6414	79763.	0.000	0.000	1.180E+12
26.808	0.1351	19217226.	0.000	1.180E+12
-1030.8295	90897.	0.000	0.000	1.180E+12
27.801	0.1125	18698993.	0.000	1.180E+12
-959.7802	101672.	0.000	0.000	1.180E+12
28.794	0.0921	18044508.	0.000	1.181E+12
-882.3364	114173.	0.000	0.000	1.181E+12
29.787	0.0739	17264764.	0.000	1.181E+12
-840.9899	38880.	0.000	0.000	1.182E+12
30.780	0.0577	16450808.	0.000	1.182E+12
-828.9521	47279.	0.000	0.000	1.182E+12
31.773	0.0435	15604349.	0.000	1.183E+12
-817.5585	58801.	0.000	0.000	1.183E+12
32.766	0.0312	14727400.	0.000	1.183E+12
-807.9689	75556.	0.000	0.000	1.183E+12
33.759	0.0207	13822347.	0.000	1.184E+12
-805.511	102281.	0.000	0.000	1.184E+12
34.752	0.0118	12892086.	0.000	1.184E+12
-805.511	152800.	0.000	0.000	1.184E+12
35.744	0.004477	11940330.	0.000	1.184E+12
-807.531	239678.	0.000	0.000	1.185E+12
36.737	0.001422	10972366.	0.000	1.185E+12
-807.531	659686.	0.000	0.000	1.185E+12
37.730	0.006006	10016022.	0.000	1.185E+12
-807.531	2392703	0.000	0.000	1.186E+12
38.723	0.009391	9078012.	0.000	1.186E+12
-807.531	197323	0.000	0.000	1.186E+12
39.716	0.0117	8162081.	0.000	1.186E+12
-807.531	174724.	0.000	0.000	1.186E+12
40.709	0.0134	7270484.	0.000	1.186E+12
-807.531	163321	0.000	0.000	1.186E+12
41.702	0.0146	6404067.	0.000	1.186E+12
-807.531	157934	0.000	0.000	1.186E+12
42.695	0.0153	5566907.	0.000	1.186E+12
-807.531	156361	0.000	0.000	1.186E+12
43.688	0.0157	4757396.	0.000	1.186E+12
-807.531	156361	0.000	0.000	1.186E+12
44.680	0.0157	3990395.	0.000	1.186E+12
-807.531	250391	0.000	0.000	1.186E+12
45.673	-0.0154	3271084.	0.000	1.186E+12
-807.531	671462.	0.000	0.000	1.186E+12
356.1792	276309.	0.000	0.000	1.182E+12
46.666	-0.0148	2601838.	0.000	1.182E+12
380.5040	305630.	0.000	0.000	1.182E+12
47.659	-0.0141	1986609.	0.000	1.182E+12
401.5266	338747.	0.000	0.000	1.181E+12
48.652	-0.0133	1428382.	0.000	1.181E+12
418.9493	376147.	0.000	0.000	1.181E+12
49.645	-0.0123	929629.	0.000	1.181E+12
432.5312	418424.	0.000	0.000	1.181E+12
50.638	-0.0113	492280.	0.000	1.180E+12
442.0896	466298.	0.000	0.000	1.180E+12
51.631	-0.0102	117692.	0.000	1.180E+12
432.5923	503300.	0.000	0.000	1.180E+12
52.624	-0.009177	195485.	0.000	1.180E+12
401.3278	521046.	0.000	0.000	1.180E+12
53.617	-0.008127	451689.	0.000	1.180E+12
367.5242	538791.	0.000	0.000	1.180E+12
54.609	-0.007110	655718.	0.000	1.180E+12
332.0957	556536.	0.000	0.000	1.180E+12
55.602	-0.006139	812602.	0.000	1.180E+12
295.8863	574282.	0.000	0.000	1.180E+12
56.595	-0.005226	927481.	0.000	1.180E+12
259.6595	592027.	0.000	0.000	1.180E+12
57.588	-0.004379	1005498.	0.000	1.180E+12
224.0924	609772.	0.000	0.000	1.180E+12
58.581	-0.003603	1051702.	0.000	1.180E+12
191.8227	634297.	0.000	0.000	1.180E+12
59.574	-0.002903	1070675.	0.000	1.180E+12
172.1685	706713.	0.000	0.000	1.181E+12
60.567	-0.002278	1065206.	0.000	1.181E+12
152.5333	797695.	0.000	0.000	1.181E+12
61.560	-0.001730	1038084.	0.000	1.181E+12
132.9106	915479.	0.000	0.000	1.182E+12
113.2200	1074717.	0.000	0.000	1.182E+12
62.553	-0.001255	992093.	0.000	1.182E+12
63.546	-0.000851	930029.	0.000	1.182E+12
64.538	-0.000513	854728.	0.000	1.183E+12
65.531	-0.000237	789147.	0.000	1.183E+12
66.524	1.447E-05	7475.6556	2.094E-05	1.184E+12
67.517	0.000159	7841.1549	1.662E-05	1.184E+12
68.510	3014286.	7673.4067	1.286E-05	1.185E+12
69.503	2227379.	7107.7740	9.645E-06	1.185E+12
70.496	1929308.	6406.8978	6.937E-06	1.185E+12
71.489	1780423.	5624.2137	4.684E-06	1.185E+12
72.482	170100725	4791.0659	2.831E-06	1.185E+12
73.475	16200332	3928.9101	1.320E-06	1.185E+12
74.468	16820032	3328.2530	8.883E-08	1.185E+12
75.461	16820032	2996.1421	-9.057E-07	1.185E+12
76.454	16820032	2661.6377	-1.687E-06	1.185E+12
77.447	16820032	2331.2792	-2.279E-06	1.185E+12
78.440	16820032	2000.0048	0.000	1.185E+12
79.433	16820032	1674.62	0.000	1.185E+12
80.426	16820032	1349.24	0.000	1.185E+12
81.419	16820032	1023.86	0.000	1.185E+12
82.412	16820032	698.48	0.000	1.185E+12
83.405	16820032	373.10	0.000	1.185E+12
84.398	16820032	46.66	0.000	1.185E+12
85.391	16820032	0.00	0.000	1.185E+12

Pier 41af.jp7o	Pier 41af.jp7o			Pier 41af.jp7o
14.893	0.5876	15378465.	0.000	1.182E+12
-239.3203	4852.4148	0.000	0.000	1.182E+12
15.886	0.5380	16116841.	0.000	1.182E+12
-72.7275	1610.6911	0.000	0.000	1.182E+12
16.879	0.4903	16844893.	0.000	1.181E+12
-222.2336	5400.7641	0.000	0.000	1.181E+12
17.872	0.4446	17541396.	0.000	1.181E+12
-382.0481	10239.	0.000	0.000	1.181E+12
18.865	0.4010	18183663.	0.000	1.181E+12
-539.9012	16042.	0.000	0.000	1.181E+12
19.858	0.3596	18749284.	0.000	1.180E+12
-685.6145	22716.	0.000	0.000	1.180E+12
20.851	0.3205	19217573.	0.000	1.180E+12
-811.5757	30173.	0.000	0.000	1.180E+12
21.844	0.2837	19570649.	0.000	1.180E+12
-914.8156	38427.	0.000	0.000	1.180E+12
22.837	0.2492	19793856.	0.000	1.180E+12
-995.5391	47603.	0.000	0.000	1.180E+12
23.830	0.2171	19875733.	0.000	1.180E+12
-1047.6715	57500.	0.000	0.000	1.180E+12
24.823	0.1874	19808881.	0.000	1.180E+12
-1077.1040	68484.	0.000	0.000	1.180E+12
25.815	0.1601	19589120.	0.000	1.180E+12
-1071.6414	79763.	0.000	0.000	1.180E+12
26.808	0.1351	19217226.	0.000	1.180E+12
-1030.8295	90897.	0.000	0.000	1.180E+12
27.801	0.1125	18698993.	0.000	1.180E+12
-959.7802	101672.	0.000	0.000	1.180E+12
28.794	0.0921	18044508.	0.000	1.180E+12
-882.3364	114173.	0.000	0.000	1.180E+12
29.787	0.0739	17264764.	0.000	1.180E+12
-840.9899	38880.	0.000	0.000	1.180E+12
30.780	0.0577	16450808.	0.000	1.180E+12
-828.9521	47279.	0.000	0.000	1.180E+12
31.773	0.0435	15604349.	0.000	1.180E+12
-817.5585	58801.	0.000	0.000	1.180E+12
32.766	0.0312	14727400.	0.000	1.180E+12
-807.9689	75556.	0.000	0.000	1.180E+12
33.759	0.0207	13822347.	0.000	1.180E+12
-805.511	102281.	0.000	0.000	1.180E+12
34.752	0.0118	12892086.	0.000	1.180E+12
-805.511	152800.	0.000	0.000	1.180E+12
35.744	0.004477	11940330.	0.000	1.180E+12
-807.531	239678.	0.000	0.000	1.180E+12
36.737	0.001422	10972366.	0.000	1.180E+12
-807.531	659686.	0.000	0.000	1.180E+12
37.730	0.006006	10016022.	0.000	1.180E+12
-807.531	2392703	0.000	0.000	1.180E+12
38.723	0.009391	9078012.	0.000	1.180E+12
-807.531	197323	0.000	0.000	1.180E+12
39.716	0.0117	8162081.	0.000	1.180E+12
-807.531	174724.	0.000	0.000	1.180E+12
40.709	0.0134	7270484.	0.000	1.180E+12
-807.531	163321	0.000	0.000	1.180E+12
41.702	0.0146	6404067.	0.000	1.180E+12
-807.531	157934	0.000	0.000	1.180E+12
42.695	0.0153	5566907.	0.000	1.180E+12
-807.531	156361	0.000	0.000	1.180E+12
43.688	0.0157	4757396.	0.000	1.180E+12
-807.531	156361	0.000	0.000	1.180E+12
44.680	0.0157	3990395.	0.000	1.180E+12
-807.531	250391	0.000	0.000	1.180E+12
45.673	-0.0154	3271084.	0.000	1.180E+12
-807.531	671462.	0.000	0.000	1.180E+12

Pier 4laf.lpZo		Pier 4laf.lpZo	
Maximum shear force	= -80753. lbs	2010.5666	-2.704E-06
Depth of maximum bending moment	= 23.8296000 feet below pile head	0.000	0.000
Depth of maximum shear force	= 36.7373000 feet below pile head	-36242.	1703.9959
Number of iterations	= 25	0.000	-2.987E-06
Number of zero deflection points	= 3	-17717.	1415.1135
		0.000	-3.148E-06
		0.000	1146.5855
		0.000	-3.208E-06
		0.000	900.2797
		0.000	-3.187E-06
		0.000	677.3548
		0.000	-3.102E-06
		0.000	478.3564
		0.000	-2.968E-06
		0.000	303.3143
		0.000	-2.801E-06
		0.000	151.8407
		0.000	-2.612E-06
		0.000	23.2260
		0.000	-2.412E-06
		0.000	-83.4692
		0.000	-2.210E-06
		0.000	-169.3283
		0.000	-2.015E-06
		0.000	-235.4986
		0.000	-1.831E-06
		0.000	-283.1207
		0.000	-1.664E-06
		0.000	-313.2655
		0.000	-1.517E-06
		0.000	-326.8827
		0.000	-1.393E-06
		0.000	-324.7583
		0.000	-1.292E-06
		0.000	-307.4853
		0.000	-1.214E-06
		0.000	-275.4450
		0.000	-1.158E-06
		0.000	-228.8031
		0.000	-1.121E-06
		0.000	-167.5192
		0.000	-1.101E-06
		0.000	-91.3717
		0.000	-1.093E-06
		0.000	0.000
		0.000	-1.091E-06
		0.000	0.000

* This analysis computed pile response using nonlinear moment-curvature relationships. Values of total stress due to combined axial and bending stresses are computed for elastic sections only and do not equal the actual stresses in concrete and steel. Stresses in concrete and steel may be interpolated from the output for nonlinear bending properties relative to the magnitude of bending moment developed in the pile.

Output Summary for Load Case No. 3:
 Pile-head deflection = 1.5000000 inches
 Computed slope at pile head = -0.0056969 radians
 Maximum bending moment = 19875733. inch-lbs
 Page 31

Pier 4laf.lpZo
 = -80753. lbs
 = 23.8296000 feet below pile head
 = 36.7373000 feet below pile head
 = 25
 = 3

 Computed Values of Pile Loading and Deflection
 for Lateral Loading for Load Case Number 4

Pile-head conditions are Displacement and Moment (Loading Type 4)
 Displacement of pile head = 2.000000 inches
 Moment at pile head = 3793200.0 in-lbs
 Axial load at pile head = 0.0 lbs

Depth, X	Soil Spr.	Deflect. inches	Bending Moment in-lbs	Shear Force lbs	Slope radians	Total Stress psi*	Bending Stiffness lb-in ²
0.000	0.000	2.0000	3793200.	81307.	-0.007274	0.000	1.343E+12
0.000	0.993	0.9135	4761952.	81307.	-0.007236	0.000	1.343E+12
0.000	1.986	1.8276	5730703.	81307.	-0.007190	0.000	1.336E+12
0.000	2.979	1.7422	6699455.	81307.	-0.007069	0.000	4.187E+11
0.000	3.972	1.6591	7668207.	81307.	-0.006950	0.000	1.979E+12
0.000	4.965	1.5766	8636959.	81307.	-0.006888	0.000	1.328E+12
0.000	5.957	1.4950	9605710.	81307.	-0.006801	0.000	1.186E+12
0.000	6.950	1.4145	10574462.	81307.	-0.006700	0.000	1.185E+12
0.000	7.943	1.3353	11543214.	81307.	-0.006589	0.000	1.185E+12
0.000	8.936	1.2575	12511966.	81307.	-0.006468	0.000	1.184E+12
0.000	9.929	1.1812	13480717.	81307.	-0.006337	0.000	1.183E+12
0.000	10.922	1.1065	14449469.	81307.	-0.006196	0.000	1.183E+12
0.000	11.915	1.0335	15418221.	81307.	-0.006046	0.000	1.182E+12
0.000	12.908	0.9624	16386973.	81307.	-0.005886	0.000	1.182E+12
0.000	13.901	0.8933	17355724.	81307.	-0.005715	0.000	1.181E+12
0.000	14.893	0.8262	18324476.	79709.	-0.005535	0.000	1.181E+12
-268.1067	3866.3353	0.000	19255167.	77637.	-0.005346	0.000	1.180E+12
-79.7319	1247.7438	0.000	20174539.	75701.	-0.005147	0.000	1.180E+12
-245.2116	4180.7710	0.000	21059099.	71715.	-0.004938	0.000	1.179E+12
17.872	0.6387	21059099.					

STR-1
 D = 2"
 LATERAL RESISTANCE = 8131

Pier 41af.jp70		Pier 41af.jp70	
-423.9029	7907.5402	49.645	-0.0154
18.865	21883482.	495.0243	383563.
-601.8395	12339.	50.638	-0.0144
19.858	22622426.	512.4546	423949.
-768.1652	17393.	51.631	-0.0133
20.851	23252319.	525.1616	489612.
-914.3620	22984.	52.624	-0.0122
21.844	23752408.	532.7504	521046.
-1037.5366	29115.	53.617	-0.0110
22.837	24105205.	497.9172	538791.
-1138.1018	35869.	54.609	-0.009838
23.830	24296434.	459.5360	556536.
-1208.3089	43051.	55.602	-0.008688
24.823	24316129.	418.7345	574282.
-1253.7406	50860.	56.595	-0.007578
25.815	24157839.	376.5500	592027.
-1263.3831	58816.	333.9156	609772.
-1239.2853	66732.	237.8009	511654.
-1182.6497	74536.	217.3172	559882.
-1121.8561	83593.	196.7542	618397.
-293.5231	26207.	176.1671	690666.
30.780	20901947.	61.560	-0.003039
-283.5571	30820.	62.553	-0.002370
-271.9011	36686.	155.5748	782088.
32.766	20694.	63.546	-0.001783
-258.3542	44357.	64.538	-0.001276
33.759	18020032.	114.1304	1066103.
-242.6094	54772.	65.531	-0.000844
-224.1623	69697.	92.8153	1310952.
35.744	15923414.	66.524	-0.000482
-202.0964	92944.	70.1738	1733926.
36.737	14830504.	67.517	-0.000186
-174.4539	134919.	43.5317	2795469.
37.730	2006685.	68.510	5.312E-05
-135.4901	241479.	69.503	0.000241
38.723	12575918.	-49.5896	2453009
39.716	1642114.	70.496	0.000384
136.9337	273821.	-62.6577	1941729.
167.4877	196523.	71.489	0.000490
186.6537	169609.	72.482	0.000564
199.5134	8191213.	-75.7094	1602800.
45.688	158873.	-31.7127	618227635
309.3740	22735.	33.9104	63597635
345.5444	242534.	35.1550	63370641
41.680	101170.	-35.5249	61450631
352.6329	26384.	-35.5249	61450631
46.966	268320172	-35.1064	689208
416.37659	316213.	-34.2458	70695377
446.78452	316213.	-32.7942	734698
473.0523	347823.	80.425	0.000497
2070253.		2070253.	
0.000		0.000	
1446337.		1446337.	
0.000		0.000	
895170.		895170.	
0.000		0.000	
418556.		418556.	
0.000		0.000	
17573.		17573.	
0.000		0.000	
-312724.		-312724.	
0.000		0.000	
-577785.		-577785.	
0.000		0.000	
-783401.		-783401.	
0.000		0.000	
-935561.		-935561.	
0.000		0.000	
-1040318.		-1040318.	
0.000		0.000	
-1111316.		-1111316.	
0.000		0.000	
-1151463.		-1151463.	
0.000		0.000	
-1163678.		-1163678.	
0.000		0.000	
-1150884.		-1150884.	
0.000		0.000	
-1116004.		-1116004.	
0.000		0.000	
-1061968.		-1061968.	
0.000		0.000	
-991730.		-991730.	
0.000		0.000	
-908315.		-908315.	
0.000		0.000	
-814938.		-814938.	
0.000		0.000	
-715381.		-715381.	
0.000		0.000	
-619130.		-619130.	
0.000		0.000	
-529518.		-529518.	
0.000		0.000	
-449602.		-449602.	
0.000		0.000	
-379531.		-379531.	
0.000		0.000	
-264644.		-264644.	
0.000		0.000	
-214666.		-214666.	
0.000		0.000	
-164677.		-164677.	
0.000		0.000	
-158477.		-158477.	
0.000		0.000	
-129332.		-129332.	
0.000		0.000	
-94385.		-94385.	
0.000		0.000	
63898.		63898.	
0.000		0.000	
1966.8088		1966.8088	
-3.685E-06		-3.685E-06	

Pier 41af.jp70		Pier 41af.jp70	
65604.	-0.004721	0.000	1.179E+12
57443.	-0.004496	0.000	1.178E+12
47419.	-0.004264	0.000	1.178E+12
35791.	-0.004027	0.000	1.177E+12
22830.	-0.003784	0.000	1.177E+12
8851.3482	-0.003539	0.000	1.177E+12
-5816.0656	-0.003293	0.000	1.177E+12
-20812.	-0.003048	0.000	1.177E+12
-35721.	-0.002805	0.000	1.177E+12
-50151.	-0.002567	0.000	1.178E+12
-63881.	-0.002335	0.000	1.178E+12
-72313.	-0.002110	0.000	1.179E+12
-75751.	-0.001894	0.000	1.179E+12
-79060.	-0.001688	0.000	1.180E+12
-82219.	-0.001491	0.000	1.180E+12
-85203.	-0.001304	0.000	1.181E+12
-87984.	-0.001128	0.000	1.181E+12
-90523.	-0.000962	0.000	1.182E+12
-92766.	-0.000807	0.000	1.183E+12
-94613.	-0.000663	0.000	1.183E+12
-95099.	-0.000531	0.000	1.184E+12
-93963.	-0.000410	0.000	1.185E+12
-92149.	-0.000300	0.000	1.185E+12
-90040.	-0.000202	0.000	1.186E+12
-87739.	-0.000131	0.000	1.197E+12
-84706.	-8.440E-05	0.000	1.980E+12
-80803.	-4.431E-05	0.000	1.982E+12
-76465.	-1.0004E-05	0.000	1.984E+12
-71704.	1.872E-05	0.000	1.986E+12
-66561.	4.233E-05	0.000	1.988E+12
-61081.	6.117E-05	0.000	1.990E+12

Pier 4laf.lp7o

-30.9458	742444.	0.000	0.000	1.994E+12	0.000	1.994E+12	
81.418	0.000451	-17030.	1610.8974	-3.851E-06	0.000	1.994E+12	
-28.7969	760189.	0.000	1281.8651	-3.901E-06	0.000	1.994E+12	
82.411	0.000405	119.4952	981.8083	-3.860E-06	0.000	1.994E+12	
-26.4340	777934.	0.000	711.9819	-3.750E-06	0.000	1.994E+12	
83.404	0.000358	13516.	472.9312	-3.588E-06	0.000	1.994E+12	
-23.9331	795680.	0.000	264.6249	-3.393E-06	0.000	1.994E+12	
84.396	0.000313	23516.	86.5860	-3.180E-06	0.000	1.994E+12	
-21.3595	813425.	0.000	-61.9820	-2.960E-06	0.000	1.994E+12	
85.389	0.000269	30483.	-182.0762	-2.744E-06	0.000	1.994E+12	
-18.7672	831170.	0.000	-274.7850	-2.541E-06	0.000	1.994E+12	
-16.1988	848916.	0.000	-341.1894	-2.358E-06	0.000	1.994E+12	
-13.6865	866661.	0.000	-382.2784	-2.200E-06	0.000	1.994E+12	
-11.2519	884406.	0.000	-398.8774	-2.068E-06	0.000	1.994E+12	
-8.9070	902151.	0.000	-391.5942	-1.965E-06	0.000	1.994E+12	
-6.6550	919897.	0.000	-360.7818	-1.890E-06	0.000	1.994E+12	
-4.4916	937642.	0.000	6277.0806	-306.5205	-1.840E-06	0.000	1.994E+12
92.340	3.000E-05	24379.	3018.1397	-228.6218	-1.812E-06	0.000	1.994E+12
-2.4056	955387.	0.000	829.1148	-126.6551	-1.801E-06	0.000	1.994E+12
93.333	4.661E-06	19654.	0.000	-1.798E-06	0.000	1.994E+12	
-0.3807	973133.	0.000	0.000	0.000	0.000	1.994E+12	
94.325	-1.928E-05	14874.	0.000	0.000	0.000	1.994E+12	
1.6033	990878.	0.000	0.000	0.000	0.000	1.994E+12	
95.318	-4.216E-05	10322.	0.000	0.000	0.000	1.994E+12	
3.5689	1008623.	0.000	0.000	0.000	0.000	1.994E+12	
96.311	-6.430E-05	6277.0806	0.000	0.000	0.000	1.994E+12	
5.5393	1026369.	0.000	0.000	0.000	0.000	1.994E+12	
97.304	-8.600E-05	3018.1397	0.000	0.000	0.000	1.994E+12	
7.5366	1044114.	0.000	0.000	0.000	0.000	1.994E+12	
98.297	-0.000107	829.1148	0.000	0.000	0.000	1.994E+12	
9.5794	1061859.	0.000	0.000	0.000	0.000	1.994E+12	
99.290	-0.000129	0.000	0.000	0.000	0.000	1.994E+12	
11.6808	539802.	0.000	0.000	0.000	0.000	1.994E+12	

* This analysis computed pile response using non-linear moment-curvature relationships.
 Values of total stress due to combined axial and bending stresses are computed only for elastic sections only and do not equal the actual stresses in concrete and steel.
 Stresses in concrete and steel may be interpolated from the output for non-linear bending properties relative to the magnitude of bending moment developed in the pile.

Output Summary for Load Case No. 4:

Pile-head deflection	=	2.0000000	inches
Computed slope at pile head	=	-0.0072742	radians
Maximum bending moment	=	24316129.	in-lb
Maximum shear force	=	950999.	lbs
Depth of maximum bending moment	=	24.8225000	feet below pile head
Depth of maximum shear force	=	38.7231000	feet below pile head
Number of iterations	=	34	
Number of zero deflection points	=	3	

Pier 4laf.lp7o

Pile-head Deflection vs. Pile Length for Load Case 4

Boundary Condition Type 4, Deflection and Moment

Deflection = 2.00000 in
 Moment = 3793200. in-lb
 Axial Load = 0. lb

Pile Length feet	Pile Head Deflection inches	Maximum Moment In-lbs	Maximum Shear lbs
99.2900	2.0000000	24316129.	-950999.
94.3255	2.0000000	24504975.	-96727.
89.3610	2.0000000	24213305.	-94256.
84.3965	2.0000000	24239414.	-94583.
79.4320	2.0000000	24150574.	-94044.
74.4675	2.0000000	24343237.	-95428.
69.5030	2.0000000	24345289.	-95426.
64.5385	2.0000000	24303128.	-94434.
59.5740	2.0000000	24348518.	-94824.
54.6095	2.0000000	23971285.	-96823.
49.6450	2.0000000	22353775.	-103165.
44.6805	2.0000000	17016700.	-96258.
39.7160	2.0000000	9445260.	-73026.
34.7515	2.0000000	6214615.	-64898.
29.7870	2.0000000	4592931.	-56652.
24.8225	2.0000000	3793200.	-30756.
19.8580	2.0000000	3793200.	-17460.
14.8935	4.792396E+11	-1.005555E+11	0.000000
9.9290	4.792396E+11	-1.005555E+11	0.000000
5.0000	4.792396E+11	-1.005555E+11	0.000000

Computed Values of Pile Loading and Deflection for Lateral Loading for Load Case Number 5

Pile-head conditions are Displacement and Moment (Loading Type 4)
 Displacement of pile head = 0.500000 inches
 Moment at pile head = 3248400.0 in-lb
 Axial Load at pile head = 0.0 lbs

Res. X	Depth, Soil Spr. y	Deflect. Lat. Load	Bending Moment	Shear Force	Slope	Total Stress	Bending Stiffness
ft	ft	inches	in-lb	lbs	radians	psi*	lb-in ²
0.000	0.00	0.5000	3248400.	25024.	-0.001991	0.000	1.345E+12
0.000	0.993	0.000	0.4764	3546558.	-0.001961	0.000	1.345E+12
0.000	1.986	0.000	0.4533	3844717.	-0.001928	0.000	1.343E+12
0.000	2.979	0.000	0.4305	4142875.	-0.001893	0.000	1.342E+12

Pier 41laf.jp7o		Pier 41laf.jp7o	
0.000	3.972	0.000	0.000
0.000	4.965	0.000	4441033.
0.000	5.957	0.000	0.000
0.000	6.950	0.000	0.000
0.000	7.943	0.000	0.000
0.000	8.936	0.000	0.000
0.000	9.929	0.000	0.000
0.000	10.922	0.000	0.000
0.000	11.915	0.000	0.000
0.000	12.908	0.000	0.000
0.000	13.901	0.000	0.000
0.000	14.893	0.000	0.000
-163.7347	10366.	0.000	0.000
-53.6972	3739.6013	0.000	0.000
-161.2962	12435.	0.000	0.000
-257.7119	22152.	0.000	0.000
-18.865	0.000	0.000	0.000
-317.3530	30670.	0.000	0.000
-358.3712	39187.	0.000	0.000
-383.1463	47705.	0.000	0.000
-394.0299	56223.	0.000	0.000
-393.3676	64741.	0.000	0.000
-383.4833	73258.	0.000	0.000
-366.6552	81776.	0.000	0.000
-345.0818	90294.	0.000	0.000
-320.5212	98812.	0.000	0.000
-291.6277	107329.	0.000	0.000
-259.5180	115847.	0.000	0.000
-159.8215	88271.	0.000	0.000
-152.3773	106686.	0.000	0.000
-143.5712	131062.	0.000	0.000
-132.7829	167028.	0.000	0.000
-119.7127	224760.	0.000	0.000
25024.	-0.001861	0.000	1.986E+12
25024.	-0.001833	0.000	1.986E+12
25024.	-0.001804	0.000	1.985E+12
25024.	-0.001773	0.000	1.984E+12
25024.	-0.001740	0.000	1.983E+12
25024.	-0.001705	0.000	1.983E+12
25024.	-0.001669	0.000	1.982E+12
25024.	-0.001630	0.000	1.981E+12
25024.	-0.001590	0.000	1.981E+12
25024.	-0.001548	0.000	1.980E+12
25024.	-0.001504	0.000	1.979E+12
24049.	-0.001459	0.000	1.979E+12
22753.	-0.001412	0.000	1.978E+12
21473.	-0.001363	0.000	1.977E+12
18976.	-0.001312	0.000	1.977E+12
15551.	-0.001244	0.000	1.236E+12
11525.	-0.001158	0.000	1.190E+12
7107.4696	-0.001068	0.000	1.186E+12
2477.5200	-0.000978	0.000	1.186E+12
-2213.3222	-0.000887	0.000	1.186E+12
-6841.3337	-0.000796	0.000	1.186E+12
-11310.	-0.000706	0.000	1.188E+12
-15550.	-0.000620	0.000	1.239E+12
-19516.	-0.000552	0.000	1.977E+12
-23162.	-0.000502	0.000	1.977E+12
-26446.	-0.000453	0.000	1.978E+12
-28944.	-0.000406	0.000	1.979E+12
-30805.	-0.000361	0.000	1.980E+12
-32567.	-0.000318	0.000	1.980E+12
-34213.	-0.000278	0.000	1.981E+12
-35717.	-0.000240	0.000	1.983E+12
34.752	0.003700	5646417.	0.000
-102.7911	331047.	0.000	0.000
35.744	0.001457	5197769.	0.000
-77.3664	632591.	0.000	0.000
36.737	-0.000413	4738138.	0.000
52.3503	1508890.	0.000	0.000
37.730	-0.001945	4285938.	0.000
89.8115	550119.	3846489.	0.000
38.723	-0.003171	0.000	0.000
108.3345	407094.	3422418.	0.000
39.716	-0.004122	0.000	0.000
121.1242	350153.	3015543.	0.000
40.709	-0.004828	2627228.	0.000
130.7372	322637.	0.000	0.000
41.702	-0.005319	0.000	0.000
138.1854	309520.	2258530.	0.000
42.695	-0.005623	0.000	0.000
143.9846	305077.	1910272.	0.000
43.688	-0.005766	0.000	0.000
165.4798	341930.	1585506.	0.000
44.680	-0.005773	0.000	0.000
179.3624	370180.	1286203.	0.000
45.673	-0.005667	0.000	0.000
188.7385	396829.	1013694.	0.000
46.666	-0.005469	0.000	0.000
190.2978	414574.	768200.	0.000
47.659	-0.005199	0.000	0.000
188.6493	432319.	549486.	0.000
48.652	-0.004875	0.000	0.000
184.1308	450064.	0.000	0.000
49.645	-0.004511	356913.	0.000
177.1093	467810.	189482.	0.000
50.638	-0.004122	0.000	0.000
167.9687	483555.	45897.	0.000
51.631	-0.003719	0.000	0.000
157.0991	503300.	0.000	0.000
52.624	-0.003313	0.000	0.000
144.8873	521046.	0.000	0.000
53.617	-0.002913	0.000	0.000
131.7091	538791.	0.000	0.000
54.609	-0.002525	0.000	0.000
117.9234	556536.	0.000	0.000
55.602	-0.002155	0.000	0.000
103.8677	574282.	0.000	0.000
56.595	-0.001808	0.000	0.000
89.8352	592027.	0.000	0.000
57.588	-0.001488	0.000	0.000
76.1727	609772.	0.000	0.000
58.581	-0.001198	0.000	0.000
110.5836	1100068.	0.000	0.000
97.8760	1242866.	0.000	0.000
60.567	-0.000711	0.000	0.000
85.1227	1427835.	0.000	0.000
72.51560	0.000515	0.000	0.000
59.823	1676959.	0.000	0.000
59.823	5332033.	0.000	0.000
46.828	5462597.	0.000	0.000
32.8468	5383703598.	0.000	0.000
65.531	-2.039E-05	-289033.	0.000

Pier 4laf.lp7o

14.4091	8420898.	0.000	3807.1160	4.712E-06	0.000	1.994E+12
66.524	4.437E-05	-242160.	3497.7206	3.396E-06	0.000	1.994E+12
-21.2368	5718292.	0.000	3102.0897	2.329E-06	0.000	1.994E+12
67.517	9.190E-05	-198311.	2657.8549	1.483E-06	0.000	1.994E+12
-30.6379	3972396.	0.000	2185.4531	8.258E-07	0.000	1.994E+12
68.510	0.000125	-158811.	1698.1167	3.245E-07	0.000	1.994E+12
-35.7721	3401673.	0.000	1205.0497	-5.593E-08	0.000	1.994E+12
69.503	0.000147	-124389.	906.8121	-3.505E-07	0.000	1.994E+12
-38.7865	3136236.	0.000	804.7008	-5.806E-07	0.000	1.994E+12
70.496	0.000161	-95475.	704.1706	-7.533E-07	0.000	1.994E+12
-40.5002	3004145.	0.000	606.8281	-8.760E-07	0.000	1.994E+12
71.489	0.000167	-72311.	513.9833	-9.554E-07	0.000	1.994E+12
-41.3033	2945618.	0.000	426.6650	-9.982E-07	0.000	1.994E+12
72.482	0.000168	-55010.	345.6407	-1.011E-06	0.000	1.994E+12
-41.4621	2934253.	0.000	271.4397	-9.985E-07	0.000	1.994E+12
73.475	0.000166	-43595.	204.3793	-9.670E-07	0.000	1.994E+12
-8.5996	618227.	0.000	144.5923	-9.209E-07	0.000	1.994E+12
74.468	0.000160	-33401.	92.0553	-8.646E-07	0.000	1.994E+12
-8.5407	635972.	0.000	46.6171	-8.017E-07	0.000	1.994E+12
75.460	0.000152	-24419.	8.0268	-7.355E-07	0.000	1.994E+12
-8.3342	653717.	0.000	-24.0392	-6.687E-07	0.000	1.994E+12
76.423	0.000142	-16621.	-49.9527	-6.036E-07	0.000	1.994E+12
-8.0056	671462.	0.000	-70.1094	-5.421E-07	0.000	1.994E+12
77.446	0.000131	-9958.5439	-84.9086	-4.856E-07	0.000	1.994E+12
-7.5792	689208.	0.000	-94.7345	-4.351E-07	0.000	1.994E+12
78.439	0.000119	-4372.5174	-99.9399	-3.914E-07	0.000	1.994E+12
-7.0779	706953.	0.000	-100.8337	-3.547E-07	0.000	1.994E+12
79.432	0.000107	208.7120	-97.6708	-3.253E-07	0.000	1.994E+12
-6.5227	724698.	0.000	-90.6452	-3.028E-07	0.000	1.994E+12
80.425	9.521E-05	3863.9612	-79.8868	-2.868E-07	0.000	1.994E+12
-5.9326	742444.	0.000	-65.4618	-2.764E-07	0.000	1.994E+12
81.418	8.345E-05	6677.0109	-65.4618	-2.764E-07	0.000	1.994E+12
-5.3241	760189.	0.000	-65.4618	-2.764E-07	0.000	1.994E+12
82.411	7.216E-05	8734.2386	-65.4618	-2.764E-07	0.000	1.994E+12
-4.7117	777934.	0.000	-65.4618	-2.764E-07	0.000	1.994E+12
83.404	6.150E-05	10123.	-65.4618	-2.764E-07	0.000	1.994E+12
-4.1071	795680.	0.000	-65.4618	-2.764E-07	0.000	1.994E+12
84.396	5.115E-05	10928.	-65.4618	-2.764E-07	0.000	1.994E+12
-3.5201	813425.	0.000	-65.4618	-2.764E-07	0.000	1.994E+12
85.389	4.240E-05	11233.	-65.4618	-2.764E-07	0.000	1.994E+12
-2.9576	831170.	0.000	-65.4618	-2.764E-07	0.000	1.994E+12
86.382	3.403E-05	11119.	-65.4618	-2.764E-07	0.000	1.994E+12
-2.4249	848916.	0.000	-65.4618	-2.764E-07	0.000	1.994E+12
87.375	2.648E-05	10861.	-65.4618	-2.764E-07	0.000	1.994E+12
-1.9249	866661.	0.000	-65.4618	-2.764E-07	0.000	1.994E+12
88.368	1.965E-05	9928.8032	-65.4618	-2.764E-07	0.000	1.994E+12
-1.4586	884406.	0.000	-65.4618	-2.764E-07	0.000	1.994E+12
89.361	1.3134E-05	8989.9504	-65.4618	-2.764E-07	0.000	1.994E+12
-1.0256	902134.	0.000	-65.4618	-2.764E-07	0.000	1.994E+12
90.354	8.580E-06	7903.4642	-65.4618	-2.764E-07	0.000	1.994E+12
-0.6236	921377.	0.000	-65.4618	-2.764E-07	0.000	1.994E+12
91.347	927472.	6732.0449	-65.4618	-2.764E-07	0.000	1.994E+12
-0.3513	937672.	5520.9361	-65.4618	-2.764E-07	0.000	1.994E+12
92.340	955387.	4329.6179	-65.4618	-2.764E-07	0.000	1.994E+12
0.1002	973153.	3333.9733	-65.4618	-2.764E-07	0.000	1.994E+12
0.4310	992717.	2169.5800	-65.4618	-2.764E-07	0.000	1.994E+12
0.7483	9990378.	3196.4807	-65.4618	-2.764E-07	0.000	1.994E+12
95.318	1.249E-05	2169.5800	-65.4618	-2.764E-07	0.000	1.994E+12
1.0575	1.008623.	0.000	-65.4618	-2.764E-07	0.000	1.994E+12
96.311	-1.583E-05	1292.8096	-65.4618	-2.764E-07	0.000	1.994E+12
1.3638	1026369.	0.000	-65.4618	-2.764E-07	0.000	1.994E+12

Pier 4laf.lp7o

97.304	-1.908E-05	609.6523	-47.3760	-2.708E-07	0.000	1.994E+12
1.6720	1044114.	0.000	-25.5838	-2.684E-07	0.000	1.994E+12
98.297	-2.228E-05	163.8578	0.000	-2.680E-07	0.000	1.994E+12
1.9860	1061859.	0.000	0.000	0.000	0.000	1.994E+12
99.290	-2.548E-05	0.000	0.000	0.000	0.000	1.994E+12
2.3085	539802.	0.000	0.000	0.000	0.000	1.994E+12

* This analysis computed pile response using nonlinear moment-curvature relationships. Values of total stress due to combined axial and bending stresses are computed only for elastic sections only and do not equal the actual stresses in concrete and steel. Stresses in concrete and steel may be interpolated from the output for nonlinear bending properties relative to the magnitude of bending moment developed in the pile.

Output Summary for Load Case No. 5:

Pile-head deflection.	=	0.5000000 inches
Computed slope at pile head	=	-0.0019910 radians
Maximum bending moment	=	9048855. inch-lbs
Maximum shear force	=	-38265. lbs
Depth of maximum bending moment	=	22.8367000 feet below pile head
Depth of maximum shear force	=	36.7373000 feet below pile head
Number of iterations	=	32
Number of zero deflection points	=	3

Computed Values of Pile Loading and Deflection for Lateral Loading for Load Case Number 6

Pile-head conditions are Displacement and Moment (Loading Type 4)
 Displacement of pile head = 1.000000 inches
 Moment at pile head = 3248400.0 in-lbs
 Axial load at pile head = 0.0 lbs

Depth, X	Soil	Deflect.	Bending	Shear	Slope	Total	Bending	
ft/inch	spr.	inches	Moment	Force	S	Stress	Stiffness	
		lb/inch	in-lbs	lbs	radians	psi*	lb-in^2	
0.000	0.000	1.00000	3248400.	46591.	-0.003836	0.000	1.345E+12	
0.000	0.993	0.000	0.9545	3603523.	46591.	-0.003805	0.000	1.345E+12
0.000	1.986	0.000	0.9093	0.4358647.	46591.	-0.003769	0.000	1.341E+12
0.000	2.979	0.000	0.8647	0.4013770.	46591.	-0.003727	0.000	1.339E+12
0.000	3.972	0.000	0.8205	0.5468893.	46591.	-0.003689	0.000	1.984E+12
0.000	4.965	0.000	0.7767	0.6024016.	46591.	-0.003655	0.000	1.983E+12
0.000	5.957	0.000	0.7334	0.6579140.	46591.	-0.003617	0.000	1.981E+12

SEAL 1
 Δ = 1.0"
 LATERAL RESISTANCE = 4659

Pier 41af.lp7o		Pier 41af.lp7o	
6.950	0.6906	125.9269	280137.
0.000	0.000	38.723	-0.007177
0.000	0.6482	236225.	0.000
0.000	7.943	0.000	0.000
0.000	0.6064	39.716	-0.008563
0.000	8.936	0.000	0.000
0.000	0.5652	154.5970	215120.
0.000	0.5251	40.709	-0.009561
0.000	0.4860	164.2153	204644.
0.000	0.4481	171.8093	200354.
0.000	0.4115	42.695	-0.0106
0.000	0.3762	177.7610	200772.
0.000	0.3423	43.688	-0.0107
0.000	0.3099	240.3265	268168.
0.000	0.2789	44.680	-0.0106
0.000	0.2496	259.0192	292133.
0.000	0.2218	45.673	-0.0103
0.000	0.1958	278.9381	323529.
0.000	0.1714	46.666	-0.009838
0.000	0.1488	296.4588	359042.
0.000	0.1279	47.659	-0.009292
0.000	0.1087	311.3269	399183.
0.000	0.0913	48.652	-0.008665
0.000	0.0755	323.3286	444579.
0.000	0.0614	331.4096	467810.
0.000	0.0488	342.52.	-0.007982
0.000	0.0378	342.52.	-0.007266
0.000	0.0283	296.1193	485555.
0.000	0.0202	276.1239	503300.
0.000	0.01536	254.0853	521046.
0.000	0.01118	230.6375	538791.
0.000	0.00987	206.3765	566336.
0.000	0.00862	181.8524	574282.
0.000	0.00743	157.5642	592027.
0.000	0.00630	133.9570	609772.
0.000	0.00523	146.9731	827743.
0.000	0.00424	130.4721	932384.
0.000	0.00331	114.0056	1066985.
0.000	0.00263	97.5467	1246903.
0.000	0.00216	80.9742	1501888.
0.000	0.00173	63.546	-0.000401
0.000	0.001394	63.9823	1900839.
0.000	0.001118	45.6024	2664504.
0.000	0.000987	21.8314	5545066.
0.000	0.000862	-27.7115	4404431.
0.000	0.000743	-41.2851	2949232.
0.000	0.000630	-48.8695	2491746.
0.000	0.000523		
0.000	0.000424		
0.000	0.000331		
0.000	0.000263		
0.000	0.000216		
0.000	0.000173		
0.000	0.000139		
0.000	0.000111		
0.000	0.000087		
0.000	0.000063		
0.000	0.000049		
0.000	0.000036		
0.000	0.000024		
0.000	0.000018		
0.000	0.000013		
0.000	0.000010		
0.000	0.000008		
0.000	0.000006		
0.000	0.000005		
0.000	0.000004		
0.000	0.000003		
0.000	0.000002		
0.000	0.000001		
0.000	0.000000		

Pier 41af.lpf0
 * This analysis computed pile response using nonlinear moment-curvature relationships.
 Values of total stress due to combined axial and bending stresses are computed only for elastic sections only and do not equal the actual stresses in concrete and steel.
 Stresses in concrete and steel may be interpolated from the output for nonlinear bending properties relative to the magnitude of bending moment developed in the pile.

Output Summary for Load Case No. 6:

Pile-head deflection = 1.000000 inches
 Computed slope at pile head = -0.0038361 radians
 Maximum bending moment = 14485099. inch-lbs
 Maximum shear force = -59725. lbs
 Depth of maximum bending moment = 22.8367000 feet below pile head
 Depth of maximum shear force = 35.7444000 feet below pile head
 Number of iterations = 19
 Number of zero deflection points = 3

Pile-head deflection vs. Pile Length for Load Case 6

Boundary Condition Type 4, Deflection and Moment

Deflection = 1.00000 in
 Moment = 3248400. in-lb
 Axial Load = 0. lb

Pile Length Feet	Pile Head Deflection Inches	Maximum Moment In-lbs	Maximum Shear lbs
99.2500	1.0000000	14485099.	-59725.
94.3235	1.0000000	14512574.	-60266.
89.3610	1.0000000	14469042.	-59513.
84.3965	1.0000000	14501442.	-59604.
79.4320	1.0000000	14479766.	-59587.
74.4675	1.0000000	14475799.	-59899.
69.5030	1.0000000	14450612.	-59958.
64.5385	1.0000000	14466042.	-59467.
59.5740	1.0000000	14452129.	-59216.
54.6095	1.0000000	14458558.	-59652.
49.6450	1.0000000	14493902.	-64295.
44.6805	1.0000000	14983217.	-69122.
39.7160	1.0000000	4328669.	-32866.
34.7515	1.0000000	3517142.	-6074.
29.7870	1.0000000	3248400.	-21638.

Computed values of Pile Loading and Deflection for Lateral Loading for Load Case Number 7

Pier 41af.lpf0
 4323.8466 3.167E-06
 3670.5143 1.903E-06
 2992.3703 9.012E-07
 2302.8185 1.122E-07
 1855.2777 -5.129E-07
 1652.7022 -1.006E-06
 1452.1440 -1.381E-06
 1256.9856 -1.653E-06
 1070.0100 -1.835E-06
 893.4290 -1.942E-06
 728.9210 -1.984E-06
 577.6767 -1.975E-06
 440.4495 -1.925E-06
 317.6109 -1.843E-06
 209.2066 -1.738E-06
 115.0145 -1.619E-06
 34.6003 -1.492E-06
 -32.6272 -1.362E-06
 -87.3653 -1.234E-06
 -130.3690 -1.113E-06
 -162.4079 -1.001E-06
 -184.2278 -9.002E-07
 -196.5175 -8.127E-07
 -199.8816 -7.393E-07
 -194.8192 -6.801E-07
 -181.7097 -6.348E-07
 -160.8049 -6.024E-07
 -132.2282 -5.814E-07
 -95.9829 -5.699E-07
 -51.9673 -5.652E-07
 0.000 -5.642E-07

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69.503	0.000280	-235287.	0.000	1.994E+12
-53.4680	2276959.	0.000	0.000	1.994E+12
70.496	0.000309	-187565.	0.000	1.994E+12
-56.1994	2166024.	0.000	0.000	1.994E+12
71.489	0.000325	-147820.	0.000	1.994E+12
-57.6329	2111968.	0.000	0.000	1.994E+12
72.482	0.000331	-116258.	0.000	1.994E+12
-58.1142	2094341.	0.000	0.000	1.994E+12
73.475	0.000328	-92945.	0.000	1.994E+12
-17.0093	618227.	0.000	0.000	1.994E+12
74.468	0.000318	-72047.	0.000	1.994E+12
-16.9947	635972.	0.000	0.000	1.994E+12
75.460	0.000304	-53562.	0.000	1.994E+12
-16.6707	633717.	0.000	0.000	1.994E+12
76.453	0.000285	-37443.	0.000	1.994E+12
-16.0883	671462.	0.000	0.000	1.994E+12
77.446	0.000264	-23608.	0.000	1.994E+12
-15.2971	689208.	0.000	0.000	1.994E+12
78.439	0.000242	-11945.	0.000	1.994E+12
-14.3435	706953.	0.000	0.000	1.994E+12
79.432	0.000218	-2318.4085	0.000	1.994E+12
-13.2705	724698.	0.000	0.000	1.994E+12
80.425	0.000194	5424.5805	0.000	1.994E+12
-12.1171	742444.	0.000	0.000	1.994E+12
81.418	0.000171	11447.	0.000	1.994E+12
-10.9176	760189.	0.000	0.000	1.994E+12
82.411	0.000149	15920.	0.000	1.994E+12
-9.7019	777934.	0.000	0.000	1.994E+12
83.404	0.000127	19016.	0.000	1.994E+12
-8.4947	795680.	0.000	0.000	1.994E+12
84.396	0.000107	20906.	0.000	1.994E+12
-7.3162	813425.	0.000	0.000	1.994E+12
85.389	8.162E-05	21757.	0.000	1.994E+12
-6.1819	831170.	0.000	0.000	1.994E+12
86.382	7.162E-05	21730.	0.000	1.994E+12
-5.1026	848916.	0.000	0.000	1.994E+12
87.375	5.617E-05	20979.	0.000	1.994E+12
-4.0853	866661.	0.000	0.000	1.994E+12
88.368	4.621E-05	19648.	0.000	1.994E+12
-3.1330	884406.	0.000	0.000	1.994E+12
89.361	2.565E-05	17873.	0.000	1.994E+12
-2.2450	902351.	0.000	0.000	1.994E+12
90.354	1.635E-05	15778.	0.000	1.994E+12
-1.4717	919897.	0.000	0.000	1.994E+12
91.347	9.139E-06	13482.	0.000	1.994E+12
-0.6453	937642.	0.000	0.000	1.994E+12
92.340	5.507E-06	11095.	0.000	1.994E+12
-0.0802	955381.	0.000	0.000	1.994E+12
93.333	3.318E-06	8719.3768	0.000	1.994E+12
0.7693	3339731.318E-06	6450.7449	0.000	1.994E+12
62.325	9731731E-05	4389.3064	0.000	1.994E+12
1.4313	1008673.	2620.8291	0.000	1.994E+12
95.318	2.454E-05	1620.8049	0.000	1.994E+12
2.0777	1008673.	-132.2282	0.000	1.994E+12
96.311	3.157E-05	-95.9829	0.000	1.994E+12
2.7191	1026369.	-51.9673	0.000	1.994E+12
97.304	3.840E-05	0.000 -5.642E-07	0.000	1.994E+12
3.3650	1044114.	0.000	0.000	1.994E+12
98.297	4.515E-05	333.5941	0.000	1.994E+12
4.0234	1061859.	0.000	0.000	1.994E+12
99.290	5.187E-05	0.000	0.000	1.994E+12
4.6998	539802.	0.000	0.000	1.994E+12

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Pier 41laf.lp7o											
Displacement of pile head											
Moment at pile head											
Axial load at pile head											
Res. X	Depth	Deflect.	Bending	Shear	Slope	Total	Bending	Soil			
lb/inch	ft	inches	in-lbs	lbs	radians	Stress	Stiffness	p			
						psi*	lb-in ²	lb/in			
0.00	0.00	1.5000	3248400.	66691.	-0.005538	0.000	1.345E+12	0.000	1.80E+12	0.000	1.180E+12
0.000	0.000	0.000	0.000	66691.	-0.005506	0.000	1.345E+12	0.000	1.80E+12	0.000	1.180E+12
0.000	0.000	1.4342	4043012.	66691.	-0.005466	0.000	1.340E+12	0.000	1.80E+12	0.000	1.180E+12
0.000	1.986	1.3688	4837623.	66691.	-0.005420	0.000	1.337E+12	0.000	1.80E+12	0.000	1.180E+12
0.000	2.979	1.3039	5652235.	66691.	-0.005375	0.000	1.334E+12	0.000	1.80E+12	0.000	1.180E+12
0.000	3.972	1.2397	6426847.	66691.	-0.005334	0.000	1.329E+12	0.000	1.80E+12	0.000	1.180E+12
0.000	4.965	1.1758	7221459.	66691.	-0.005288	0.000	1.324E+12	0.000	1.80E+12	0.000	1.180E+12
0.000	5.957	1.1125	8016070.	66691.	-0.005221	0.000	1.319E+12	0.000	1.80E+12	0.000	1.180E+12
0.000	6.950	1.0498	8810682.	66691.	-0.005129	0.000	1.314E+12	0.000	1.80E+12	0.000	1.180E+12
0.000	7.943	0.9881	9605294.	66691.	-0.005028	0.000	1.309E+12	0.000	1.80E+12	0.000	1.180E+12
0.000	8.936	0.9276	10399906.	66691.	-0.004920	0.000	1.304E+12	0.000	1.80E+12	0.000	1.180E+12
0.000	9.929	0.8683	11194517.	66691.	-0.004803	0.000	1.299E+12	0.000	1.80E+12	0.000	1.180E+12
0.000	10.922	0.8104	11989129.	66691.	-0.004679	0.000	1.294E+12	0.000	1.80E+12	0.000	1.180E+12
0.000	11.915	0.7539	12783741.	66691.	-0.004546	0.000	1.289E+12	0.000	1.80E+12	0.000	1.180E+12
0.000	12.908	0.6989	13578353.	66691.	-0.004405	0.000	1.284E+12	0.000	1.80E+12	0.000	1.180E+12
0.000	13.901	0.6455	14372964.	66691.	-0.004256	0.000	1.279E+12	0.000	1.80E+12	0.000	1.180E+12
0.000	14.893	0.5939	15167576.	66691.	-0.004100	0.000	1.274E+12	0.000	1.80E+12	0.000	1.180E+12
-240	15.881	0.5432	15962188.	63395.	-0.003935	0.000	1.269E+12	0.000	1.80E+12	0.000	1.180E+12
-72	16.866	0.4924	16756800.	61632.	-0.003763	0.000	1.264E+12	0.000	1.80E+12	0.000	1.180E+12
-222	17.851	0.4417	17551412.	58019.	-0.003585	0.000	1.259E+12	0.000	1.80E+12	0.000	1.180E+12
-383	18.835	0.3910	18345924.	52506.	-0.003399	0.000	1.254E+12	0.000	1.80E+12	0.000	1.180E+12
-542	19.819	0.3403	19140436.	45174.	-0.003209	0.000	1.249E+12	0.000	1.80E+12	0.000	1.180E+12
-688	20.803	0.2896	19934948.	36214.	-0.003014	0.000	1.244E+12	0.000	1.80E+12	0.000	1.180E+12
-815	21.787	0.2389	20729460.	25877.	-0.002815	0.000	1.239E+12	0.000	1.80E+12	0.000	1.180E+12
-919	22.771	0.1882	21523972.	14434.	-0.002615	0.000	1.234E+12	0.000	1.80E+12	0.000	1.180E+12
-1001	23.755	0.1375	22318484.	2186.9494	-0.002415	0.000	1.229E+12	0.000	1.80E+12	0.000	1.180E+12
-1054	24.739	0.0868	23112996.	-10557.	-0.002215	0.000	1.224E+12	0.000	1.80E+12	0.000	1.180E+12
-24.823		0.1914	19806075.								

Pier 41af.jp7o		Pier 41af.jp7o	
res. X	Deflect. Bending Moment	Shear Force	Slope
56.595	-0.005281	-888078.	-8593.1871
262.3824	592027.	0.000	7.337E-05
57.588	-0.004438	0.000	6.781E-05
227.1248	609772.	0.000	6.185E-05
58.581	-0.003665	0.000	5.567E-05
193.4482	628970.	0.000	4.941E-05
59.574	-0.002964	0.000	4.322E-05
173.9786	699361.	0.000	3.723E-05
60.567	-0.002338	0.000	3.153E-05
154.5197	787439.	0.000	2.622E-05
61.560	-0.001787	0.000	2.137E-05
135.0748	900805.	0.000	1.704E-05
62.553	-0.001308	0.000	1.325E-05
115.5798	1052761.	0.000	1.001E-05
63.546	-0.000900	0.000	7.269E-06
95.8460	1269545.	0.000	5.452E-06
64.538	-0.000557	0.000	4.192E-06
75.4069	1613723.	0.000	3.153E-06
65.531	-0.000275	0.000	2.422E-06
52.9694	2297527.	0.000	1.704E-06
66.524	-4.746E-05	0.000	1.325E-06
22.0269	5530345.	0.000	1.001E-06
67.517	0.000131	0.000	7.269E-07
-36.6191	3321328.	0.000	5.452E-07
68.510	0.000268	0.000	4.192E-07
-52.3486	2323860.	0.000	3.153E-07
69.503	0.000370	0.000	2.422E-07
-61.4572	1979563.	0.000	1.704E-07
70.496	0.000442	0.000	1.325E-07
-67.1514	1811757.	0.000	1.001E-07
71.489	0.000489	0.000	7.269E-08
-70.6365	1722398.	0.000	5.452E-08
72.542	0.000515	0.000	4.192E-08
-72.5416	1677093.	0.000	3.153E-08
73.475	0.000526	0.000	2.422E-08
-27.2729	618227.	0.000	1.704E-08
74.468	0.000522	0.000	1.325E-08
-27.8777	635972.	0.000	1.001E-08
75.460	0.000508	0.000	7.269E-09
-27.8774	637117.	0.000	5.452E-09
76.453	0.000485	0.000	4.192E-09
-27.5602	671462.	0.000	3.153E-09
77.446	0.000457	0.000	2.422E-09
-26.4125	689208.	0.000	1.704E-09
78.439	0.000423	0.000	1.325E-09
-25.1171	706953.	0.000	1.001E-09
79.432	0.000387	0.000	7.269E-10
-23.5517	724638.	0.000	5.452E-10
80.425	0.000350	0.000	4.192E-10
-21.7873	742444.	0.000	3.153E-10
81.418	0.000312	0.000	2.422E-10
-19.8890	760180.	0.000	1.704E-10
82.411	0.000274	0.000	1.325E-10
-17.9174	777927.	0.000	1.001E-10
83.404	0.000238	0.000	7.269E-11
-15.9067	795680.	0.000	5.452E-11
84.396	0.000204	0.000	4.192E-11
-13.9104	813425.	0.000	3.153E-11
85.389	0.000171	0.000	2.422E-11
-11.9568	831170.	0.000	1.704E-11
86.382	0.000141	0.000	1.325E-11
-10.0694	848916.	0.000	1.001E-11
87.375	0.000114	0.000	7.269E-12

* This analysis computed pile response using nonlinear moment-curvature relationships.
 Values of total stress due to combined axial and bending stresses are computed only for elastic sections only and do not equal the actual stresses in concrete and steel.
 Stresses in concrete and steel may be interpolated from the output for nonlinear bending properties relative to the magnitude of bending moment developed in the pile.

Output Summary for Load Case No. 7:
 Pile-head deflection. = 1.500000 inches
 Computed slope at pile head = -0.0033379 radians
 Maximum bending moment = 19854861. in-lb
 Maximum shear force = -80481. lb
 Depth of maximum bending moment = 23.8296000 feet below pile head
 Depth of maximum shear force = 36.7373000 feet below pile head
 Number of iterations = 31
 Number of zero deflection points = 3

 Computed Values of Pile Loading and Deflection
 For Lateral Loading for Load Case Number 8

 Pile-head conditions are Displacement and Moment (Loading Type 4)
 Displacement of pile head = 2.00000 inches
 Moment at pile head = 3248400.0 in-lb
 Axial load at pile head = 0.0 lb

Pier 4laf.lp7o												
Est'h	Lat. Load	in-lbs	lbs	radians	psi*	lb-in^2	lb/in	28.794	0.1625	22648701.	Pier 4laf.lp7o	0.000
feet	inches	lb/inch						-1129.8152	82834.	82834.	-62726.	1.178E+12
lb/inch	lb/inch							29.787	0.1358	21821141.	-71215.	1.179E+12
								-295.2664	25901.	0.000	-74675.	1.179E+12
								30.780	0.1118	20951665.	-78007.	1.180E+12
								-285.4113	0.0902	20041671.	-81190.	1.180E+12
								31.773	0.0711	19092796.	-84201.	1.181E+12
								-273.8807	0.0543	18106943.	-87011.	1.181E+12
								32.766	0.0396	17086319.	-89583.	1.182E+12
								-260.4820	0.0270	16033510.	-91865.	1.183E+12
								-244.9223	0.0164	14951593.	-93765.	1.183E+12
								33.759	0.0128	13844397.	-94896.	1.184E+12
								-226.7248	0.0160	12717209.	-94399.	1.184E+12
								34.752	0.0168	11583055.	-92627.	1.185E+12
								-205.0349	0.0172	10467710.	-90543.	1.186E+12
								35.744	0.0171	9333421.	-88261.	1.186E+12
								-178.0669	0.0162	8310100.	-85251.	1.188E+12
								36.737	0.0154	7272558.	-81375.	1.188E+12
								-140.8317	0.0144	6278604.	-77058.	1.188E+12
								37.730	0.0134	5333421.	-72312.	1.188E+12
								-132.4895	0.0123	4442347.	-67178.	1.188E+12
								38.723	0.0111	3610264.	-61701.	1.188E+12
								-49.0647	0.0102	2841533.	-55931.	1.188E+12
								39.716	0.0092	2139954.	-49921.	1.188E+12
								132.4895	0.0082	1508713.	-43726.	1.188E+12
								164.9431	0.0072	950352.	-37403.	1.188E+12
								184.9030	0.0063	4667741.	-31229.	1.188E+12
								198.2115	0.0055	59061.	-25481.	1.188E+12
								307.0382	0.0049	197435.	-20202.	1.188E+12
								343.5451	0.0043	548146.	-15414.	1.188E+12
								381.1567	0.0038	758833.	-11131.	1.188E+12
								415.5286	0.0033	913466.	-8583E-05	1.188E+12
								446.2691	0.0029	107663.	-6889E-05	1.188E+12
								473.0200	0.0025	126068.	-5303E-05	1.188E+12
								495.4719	0.0022	146366.	-4003E-05	1.188E+12
								513.3753	0.0019	166877.	-2957E-05	1.188E+12
								526.5463	0.0017	188277.	-2103E-05	1.188E+12
								534.8670	0.0016	210674.	-1503E-05	1.188E+12
								501.4333	0.0015	233071.	-9957E-05	1.188E+12
								463.3897	0.0014	255466.	-7269E-05	1.188E+12
								422.8190	0.0013	278863.	-5303E-05	1.188E+12
								380.7519	0.0012	302277.	-3889E-05	1.188E+12
								338.1661	0.0011	326608.	-2803E-05	1.188E+12
								239.5306	0.0010	351518.	-1929E-05	1.188E+12
								59.5174	0.0009	376741.	-1098E-05	1.188E+12

219.0908	555327.	0.000	0.000	1.994E+12	0.000	1.994E+12
60.567	-1142232.	-2469.5618	6.700E-05	0.000	1.994E+12	0.000
198.587	612688.	0.000	0.000	1.994E+12	0.000	1.994E+12
61.560	-0.003104	-225.8449	6.012E-05	0.000	1.994E+12	0.000
178.0442	683382.	0.000	0.000	1.994E+12	0.000	1.994E+12
62.553	-0.002429	1773.1172	5.324E-05	0.000	1.994E+12	0.000
157.4986	772552.	-1147614.	0.000	0.000	1.994E+12	0.000
136.9164	888724.	-1115308.	0.000	0.000	1.994E+12	0.000
116.1773	1047437.	-1063566.	0.000	0.000	1.994E+12	0.000
94.9811	1281318.	-995330.	0.000	0.000	1.994E+12	0.000
66.524	-0.000516	7291.0836	2.811E-05	0.000	1.994E+12	0.000
72.5892	1676923.	8001.7532	2.293E-05	0.000	1.994E+12	0.000
46.7027	2608215.	-821586.	0.000	0.000	1.994E+12	0.000
17.5971	6858789.	-722932.	0.000	0.000	1.994E+12	0.000
69.503	0.000223	-626776.	0.000	0.000	1.994E+12	0.000
-47.6955	2548205.	-537391.	0.000	0.000	1.994E+12	0.000
-61.5176	1976561.	0.000	0.000	0.000	1.994E+12	0.000
-70.0236	1736756.	6351.9040	7.830E-06	0.000	1.994E+12	0.000
-75.4330	1612355.	-386027.	0.000	0.000	1.994E+12	0.000
-31.4945	618227.	4848.3516	3.185E-06	0.000	1.994E+12	0.000
-33.8045	635972.	-270493.	0.000	0.000	1.994E+12	0.000
-35.1363	653717.	-219760.	0.000	0.000	1.994E+12	0.000
-35.6075	671482.	-174016.	0.000	0.000	1.994E+12	0.000
-35.3364	689208.	-133326.	0.000	0.000	1.994E+12	0.000
-34.4397	706953.	2788.8562	-2.847E-06	0.000	1.994E+12	0.000
-33.0295	724698.	-66869.	0.000	0.000	1.994E+12	0.000
-31.2111	742444.	-40774.	0.000	0.000	1.994E+12	0.000
-29.0820	760189.	-19109.	0.000	0.000	1.994E+12	0.000
-26.9246	777934.	-1573.4721	0.000	0.000	1.994E+12	0.000
-24.8348	795680.	12168.	0.000	0.000	1.994E+12	0.000
-21.8243	813435.	22469.	0.000	0.000	1.994E+12	0.000
-19.0252	831170.	27696.	0.000	0.000	1.994E+12	0.000
-16.9700	848973.	34918.	0.000	0.000	1.994E+12	0.000
-13.9308	866631.	36402.	0.000	0.000	1.994E+12	0.000
-11.4842	884406.	36608.	0.000	0.000	1.994E+12	0.000
-9.1159	902153.	35382.	0.000	0.000	1.994E+12	0.000
-6.8388	919897.	32463.	0.000	0.000	1.994E+12	0.000
		-268.9626	-2.573E-06	0.000	1.994E+12	0.000

91.347	5.907E-05	28773.	0.000	1.994E+12	0.000	1.994E+12
-4.6489	937642.	0.000	0.000	1.994E+12	0.000	1.994E+12
92.340	3.162E-05	24423.	0.000	1.994E+12	0.000	1.994E+12
-2.5353	955387.	0.000	0.000	1.994E+12	0.000	1.994E+12
93.333	5.901E-06	19713.	0.000	1.994E+12	0.000	1.994E+12
-0.4820	973133.	0.000	0.000	1.994E+12	0.000	1.994E+12
94.325	-1.841E-05	14935.	0.000	1.994E+12	0.000	1.994E+12
1.5312	990878.	0.000	0.000	1.994E+12	0.000	1.994E+12
95.318	-4.166E-05	10374.	0.000	1.994E+12	0.000	1.994E+12
3.5269	1008623.	0.000	0.000	1.994E+12	0.000	1.994E+12
96.311	-6.417E-05	6313.5023	0.000	1.994E+12	0.000	1.994E+12
5.5281	1026369.	0.000	0.000	1.994E+12	0.000	1.994E+12
97.304	-8.624E-05	3037.9768	0.000	1.994E+12	0.000	1.994E+12
7.5570	1044114.	0.000	0.000	1.994E+12	0.000	1.994E+12
98.297	-0.000108	835.2682	0.000	1.994E+12	0.000	1.994E+12
9.6324	1061859.	0.000	0.000	1.994E+12	0.000	1.994E+12
99.290	-0.000130	0.000	0.000	1.994E+12	0.000	1.994E+12
11.7675	539802.	0.000	0.000	1.994E+12	0.000	1.994E+12

* This analysis computed pile response using nonlinear moment-curvature relationships. Values of total stress due to combined axial and bending stresses are computed only for elastic sections only and do not equal the actual stresses in concrete and steel. Stresses in concrete and steel may be interpolated from the output for nonlinear bending properties relative to the magnitude of bending moment developed in the pile.

Output Summary for Load Case No. 8:
 Pile-head deflection = 2.000000 inches
 Computed slope at pile head = -0.0071912 radians
 Maximum bending moment = 24276701. inch-lbs
 Maximum shear force = -94896. lbs
 Depth of maximum bending moment = 24.8225000 feet below pile head
 Depth of maximum shear force = 38.7231000 feet below pile head
 Number of iterations = 16
 Number of zero deflection points = 3

 Computed Values of Pile Loading and Deflection
 for Lateral Loading for Load Case Number 9

Pile-head conditions are Shear and Moment (Loading Type 1)
 Shear force at pile head = 9800.0 lbs
 Applied moment at pile head = 3793200.0 in.-lbs
 Axial Thrust load on pile head = 0.0 lbs
 Depth Deflect. Bending Shear Slope Total Bending Soil
 X Spr. y Distrib. Force S stress stiffness p
 feet in.-lbs lbs radians psi* lb-in*2 lb/in
 lb/inch lb/inch

 0.00 0.2690 3793200. 9800.0000 -0.001199 0.000 1.343E+12

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Pier 41af.jp7o		Pier 41af.jp7o	
0.000	0.000	0.000	0.000
0.000	0.2549	0.000	0.000
0.000	0.000	3909965.	4238155.
0.000	0.2413	4026730.	3959670.
0.000	0.2280	4143495.	0.000
0.000	0.2152	4260260.	3667106.
0.000	0.2027	4377025.	3362520.
0.000	0.1905	4493790.	3049079.
0.000	0.1787	4610555.	2742494.
0.000	0.1671	4727320.	2446812.
0.000	0.1560	4844085.	2164164.
0.000	0.1451	4960850.	1896041.
0.000	0.1346	5077615.	1643570.
0.000	0.1245	5194380.	1407628.
0.000	0.1147	5311146.	1188903.
0.000	0.1053	5427911.	987925.
0.000	0.0963	5544676.	789925.
0.000	0.0877	5662846.	633942.
0.000	0.0796	5781016.	481554.
0.000	0.0718	5899186.	345504.
0.000	0.0644	6017356.	225424.
0.000	0.0575	6135526.	120726.
0.000	0.0509	6253696.	30637.
0.000	0.0448	6371866.	-45774.
0.000	0.0392	6490036.	-109556.
0.000	0.0339	6608206.	-161850.
0.000	0.0291	6726376.	-203853.
0.000	0.0246	6844546.	-236791.
0.000	0.0206	6962716.	-261891.
0.000	0.0170	7080886.	-280354.
0.000	0.0137	7199056.	-293331.
0.000	0.0107	7317226.	-295272.
0.000	0.0081	7435396.	-267626.
0.000	0.0057	7553566.	0.000
0.000	0.0035	7671736.	0.000
0.000	0.0020	7789906.	0.000
0.000	0.0015	7908076.	0.000
0.000	0.0010	8026246.	0.000
0.000	0.0007	8144416.	0.000
0.000	0.0005	8262586.	0.000
0.000	0.0003	8380756.	0.000
0.000	0.0002	8498926.	0.000
0.000	0.0001	8617096.	0.000
0.000	0.0000	8735266.	0.000
0.000	0.0000	8853436.	0.000
0.000	0.0000	8971606.	0.000
0.000	0.0000	9089776.	0.000
0.000	0.0000	9207946.	0.000
0.000	0.0000	9326116.	0.000
0.000	0.0000	9444286.	0.000
0.000	0.0000	9562456.	0.000
0.000	0.0000	9680626.	0.000
0.000	0.0000	9798796.	0.000
0.000	0.0000	9916966.	0.000
0.000	0.0000	1003533.	0.000
0.000	0.0000	1010100.	0.000
0.000	0.0000	1016667.	0.000
0.000	0.0000	1023234.	0.000
0.000	0.0000	1029801.	0.000
0.000	0.0000	1036368.	0.000
0.000	0.0000	1042935.	0.000
0.000	0.0000	1049502.	0.000
0.000	0.0000	1056069.	0.000
0.000	0.0000	1062636.	0.000
0.000	0.0000	1069203.	0.000
0.000	0.0000	1075770.	0.000
0.000	0.0000	1082337.	0.000
0.000	0.0000	1088904.	0.000
0.000	0.0000	1095471.	0.000
0.000	0.0000	1102038.	0.000
0.000	0.0000	1108605.	0.000
0.000	0.0000	1115172.	0.000
0.000	0.0000	1121739.	0.000
0.000	0.0000	1128306.	0.000
0.000	0.0000	1134873.	0.000
0.000	0.0000	1141440.	0.000
0.000	0.0000	1148007.	0.000
0.000	0.0000	1154574.	0.000
0.000	0.0000	1161141.	0.000
0.000	0.0000	1167708.	0.000
0.000	0.0000	1174275.	0.000
0.000	0.0000	1180842.	0.000
0.000	0.0000	1187409.	0.000
0.000	0.0000	1193976.	0.000
0.000	0.0000	1200543.	0.000
0.000	0.0000	1207110.	0.000
0.000	0.0000	1213677.	0.000
0.000	0.0000	1220244.	0.000
0.000	0.0000	1226811.	0.000
0.000	0.0000	1233378.	0.000
0.000	0.0000	1239945.	0.000
0.000	0.0000	1246512.	0.000
0.000	0.0000	1253079.	0.000
0.000	0.0000	1259646.	0.000
0.000	0.0000	1266213.	0.000
0.000	0.0000	1272780.	0.000
0.000	0.0000	1279347.	0.000
0.000	0.0000	1285914.	0.000
0.000	0.0000	1292481.	0.000
0.000	0.0000	1299048.	0.000
0.000	0.0000	1305615.	0.000
0.000	0.0000	1312182.	0.000
0.000	0.0000	1318749.	0.000
0.000	0.0000	1325316.	0.000
0.000	0.0000	1331883.	0.000
0.000	0.0000	1338450.	0.000
0.000	0.0000	1345017.	0.000
0.000	0.0000	1351584.	0.000
0.000	0.0000	1358151.	0.000
0.000	0.0000	1364718.	0.000
0.000	0.0000	1371285.	0.000
0.000	0.0000	1377852.	0.000
0.000	0.0000	1384419.	0.000
0.000	0.0000	1390986.	0.000
0.000	0.0000	1397553.	0.000
0.000	0.0000	1404120.	0.000
0.000	0.0000	1410687.	0.000
0.000	0.0000	1417254.	0.000
0.000	0.0000	1423821.	0.000
0.000	0.0000	1430388.	0.000
0.000	0.0000	1436955.	0.000
0.000	0.0000	1443522.	0.000
0.000	0.0000	1450089.	0.000
0.000	0.0000	1456656.	0.000
0.000	0.0000	1463223.	0.000
0.000	0.0000	1469790.	0.000
0.000	0.0000	1476357.	0.000
0.000	0.0000	1482924.	0.000
0.000	0.0000	1489491.	0.000
0.000	0.0000	1496058.	0.000
0.000	0.0000	1502625.	0.000
0.000	0.0000	1509192.	0.000
0.000	0.0000	1515759.	0.000
0.000	0.0000	1522326.	0.000
0.000	0.0000	1528893.	0.000
0.000	0.0000	1535460.	0.000
0.000	0.0000	1542027.	0.000
0.000	0.0000	1548594.	0.000
0.000	0.0000	1555161.	0.000
0.000	0.0000	1561728.	0.000
0.000	0.0000	1568295.	0.000
0.000	0.0000	1574862.	0.000
0.000	0.0000	1581429.	0.000
0.000	0.0000	1587996.	0.000
0.000	0.0000	1594563.	0.000
0.000	0.0000	1601130.	0.000
0.000	0.0000	1607697.	0.000
0.000	0.0000	1614264.	0.000
0.000	0.0000	1620831.	0.000
0.000	0.0000	1627398.	0.000
0.000	0.0000	1633965.	0.000
0.000	0.0000	1640532.	0.000
0.000	0.0000	1647099.	0.000
0.000	0.0000	1653666.	0.000
0.000	0.0000	1660233.	0.000
0.000	0.0000	1666800.	0.000
0.000	0.0000	1673367.	0.000
0.000	0.0000	1679934.	0.000
0.000	0.0000	1686501.	0.000
0.000	0.0000	1693068.	0.000
0.000	0.0000	1699635.	0.000
0.000	0.0000	1706202.	0.000
0.000	0.0000	1712769.	0.000
0.000	0.0000	1719336.	0.000
0.000	0.0000	1725903.	0.000
0.000	0.0000	1732470.	0.000
0.000	0.0000	1739037.	0.000
0.000	0.0000	1745604.	0.000
0.000	0.0000	1752171.	0.000
0.000	0.0000	1758738.	0.000
0.000	0.0000	1765305.	0.000
0.000	0.0000	1771872.	0.000
0.000	0.0000	1778439.	0.000
0.000	0.0000	1785006.	0.000
0.000	0.0000	1791573.	0.000
0.000	0.0000	1798140.	0.000
0.000	0.0000	1804707.	0.000
0.000	0.0000	1811274.	0.000
0.000	0.0000	1817841.	0.000
0.000	0.0000	1824408.	0.000
0.000	0.0000	1830975.	0.000
0.000	0.0000	1837542.	0.000
0.000	0.0000	1844109.	0.000
0.000	0.0000	1850676.	0.000
0.000	0.0000	1857243.	0.000
0.000	0.0000	1863810.	0.000
0.000	0.0000	1870377.	0.000
0.000	0.0000	1876944.	0.000
0.000	0.0000	1883511.	0.000
0.000	0.0000	1890078.	0.000
0.000	0.0000	1896645.	0.000
0.000	0.0000	1903212.	0.000
0.000	0.0000	1909779.	0.000
0.000	0.0000	1916346.	0.000
0.000	0.0000	1922913.	0.000
0.000	0.0000	1929480.	0.000
0.000	0.0000	1936047.	0.000
0.000	0.0000	1942614.	0.000
0.000	0.0000	1949181.	0.000
0.000	0.0000	1955748.	0.000
0.000	0.0000	1962315.	0.000
0.000	0.0000	1968882.	0.000
0.000	0.0000	1975449.	0.000
0.000	0.0000	1982016.	0.000
0.000	0.0000	1988583.	0.000
0.000	0.0000	1995150.	0.000
0.000	0.0000	2001717.	0.000
0.000	0.0000	2008284.	0.000
0.000	0.0000	2014851.	0.000
0.000	0.0000	2021418.	0.000
0.000	0.0000	2027985.	0.000
0.000	0.0000	2034552.	0.000
0.000	0.0000	2041119.	0.000
0.000	0.0000	2047686.	0.000
0.000	0.0000	2054253.	0.000
0.000	0.0000	2060820.	0.000
0.000	0.0000	2067387.	0.000
0.000	0.0000	2073954.	0.000
0.000	0.0000	2080521.	0.000
0.000	0.0000	2087088.	0.000
0.000	0.0000	2093655.	0.000
0.000	0.0000	2100222.	0.000
0.000	0.0000	2106789.	0.000
0.000	0.0000	2113356.	0.000
0.000	0.0000	2119923.	0.000
0.000	0.0000	2126490.	0.000
0.000	0.0000	2133057.	0.000
0.000	0.0000	2139624.	0.000
0.000	0.0000	2146191.	0.000
0.000	0.0000	2152758.	0.000
0.000	0.0000	2159325.	0.000
0.000	0.0000	2165892.	0.000
0.000	0.0000	2172459.	0.000
0.000	0.0000	2179026.	0.000
0.000	0.0000	2185593.	0.000
0.000	0.0000	2192160.	0.000
0.000	0.0000	2198727.	0.000
0.000	0.0000	2205294.	0.000
0.000	0.0000	2211861.	0.000
0.000	0.0000	2218428.	0.000
0.000	0.0000	2224995.	0.000
0.000	0.0000	2231562.	0.000
0.000	0.0000	2238129.	0.000
0.000	0.0000	2244696.	0.000
0.000	0.0000	2251263.	0.000
0.000	0.0000	2257830.	0.000
0.000	0.0000	2264397.	0.000
0.000	0.0000	2270964.	0.000
0.000	0.0000	2277531.	0.000
0.000	0.0000	2284098.	0.000
0.000	0.0000	2290665.	0.000
0.000	0.0000	2297232.	0.000
0.000	0.0000	2303799.	0.000
0.000	0.0000	2310366.	0.000
0.000	0.0000	2316933.	0.000
0.000	0.0000		

MEMBER FIXITY
 @ 65.531, EL. -59.24

Pier 41af.1p70	0.000	2486.3644	4.921E-06	0.000	1.994E+12	94.325	-4.725E-06	1265.5196	0.000	1.994E+12
37.0325	3346504.	-0.000	-2211569.	0.000	1.994E+12	0.3930	990878.	0.000	0.000	1.994E+12
63.546	-6.533E-05	0.000	0.000	0.000	1.994E+12	95.318	-5.768E-06	847.2985	0.000	1.994E+12
26.7639	4789802.	0.000	-190080.	0.000	1.994E+12	0.4883	1008623.	0.000	0.000	1.994E+12
64.598	-1.459E-05	0.000	0.000	0.000	1.994E+12	96.311	-6.750E-06	498.3951	0.000	1.994E+12
13.0526	10658455.	0.000	156738.	0.000	1.994E+12	0.5815	1026369.	0.000	0.000	1.994E+12
65.531	2.262E-05	0.000	0.000	0.000	1.994E+12	97.304	-7.697E-06	232.0415	0.000	1.994E+12
14.7268	7757851.	0.000	-125487.	0.000	1.994E+12	0.6745	1044114.	0.000	0.000	1.994E+12
66.524	4.867E-05	0.000	0.000	0.000	1.994E+12	98.297	-8.627E-06	61.4440	0.000	1.994E+12
-22.0486	5398014.	0.000	-97367.	0.000	1.994E+12	0.7689	1061859.	0.000	0.000	1.994E+12
67.517	6.578E-05	0.000	0.000	0.000	1.994E+12	99.290	-9.553E-06	0.000	0.000	1.994E+12
-25.7822	4669859.	0.000	-72906.	0.000	1.994E+12	0.8656	539802.	0.000	0.000	1.994E+12
-27.7934	4359371.	0.000	0.000	0.000	1.994E+12	* This analysis computed pile response using nonlinear moment-curvature relationships.				
69.503	8.095E-05	0.000	-52390.	0.000	1.994E+12	Values of total stress due to combined axial and bending stresses are computed only for elastic sections only and do not equal the actual stresses in concrete and steel.				
-28.7568	4232383.	0.000	0.000	0.000	1.994E+12	Stresses in concrete and steel may be interpolated from the output for nonlinear bending properties relative to the magnitude of bending moment developed in the pile.				
70.496	8.222E-05	0.000	-35958.	0.000	1.994E+12	Output Summary for Load Case No. 9:				
-29.0331	4207508.	0.000	0.000	0.000	1.994E+12	Pile-head deflection = 0.2690203 inches				
71.489	8.092E-05	0.000	-23646.	0.000	1.994E+12	Computed slope at pile head = -0.0011985 radians				
-28.8484	4247844.	0.000	0.000	0.000	1.994E+12	Maximum bending moment = 5924522. inch-lbs				
72.482	7.793E-05	0.000	-15430.	0.000	1.994E+12	Maximum shear force = -26019. lbs				
-28.3509	4334344.	0.000	0.000	0.000	1.994E+12	Depth of maximum bending moment = 20.8509000 feet below pile head				
73.475	7.385E-05	0.000	-11239.	0.000	1.994E+12	Depth of maximum shear force = 35.7444000 feet below pile head				
-3.8321	616227.	0.000	0.000	0.000	1.994E+12	Number of iterations = 7				
74.468	6.897E-05	0.000	-7592.3349	0.000	1.994E+12	Number of zero deflection points = 3				
-3.6815	635972.	0.000	0.000	0.000	1.994E+12	Pile-head Deflection vs. Pile Length for Load Case 9				
75.460	6.355E-05	0.000	-4467.8902	0.000	1.994E+12	Boundary Condition Type 1, Shear and Moment				
-3.4867	653717.	0.000	0.000	0.000	1.994E+12	Shear = 9800. lb				
76.453	5.781E-05	0.000	-1838.4319	0.000	1.994E+12	Moment = 3793200. in-lb				
-3.2579	671462.	0.000	0.000	0.000	1.994E+12	AXIAL Load = 0. lb				
77.446	5.194E-05	0.000	328.5257	0.000	1.994E+12	Pile Length				
-3.0044	689208.	0.000	0.000	0.000	1.994E+12	Pile Head Deflection				
78.439	4.609E-05	0.000	2068.9703	0.000	1.994E+12	Pile Head Moment				
-2.7348	706953.	0.000	0.000	0.000	1.994E+12	Pile Head Shear				
79.432	4.039E-05	0.000	3421.1751	0.000	1.994E+12	Pile Length				
-2.4567	724698.	0.000	0.000	0.000	1.994E+12	Pile Head Deflection				
80.425	3.493E-05	0.000	4424.6141	0.000	1.994E+12	Pile Head Moment				
-2.1769	742444.	0.000	0.000	0.000	1.994E+12	Pile Head Shear				
81.418	2.979E-05	0.000	5119.0169	0.000	1.994E+12	Pile Length				
-1.9009	760189.	0.000	0.000	0.000	1.994E+12	Pile Head Deflection				
82.411	2.502E-05	0.000	5543.5674	0.000	1.994E+12	Pile Head Moment				
-1.6333	779934.	0.000	0.000	0.000	1.994E+12	Pile Head Shear				
83.404	2.063E-05	0.000	5736.2452	0.000	1.994E+12	Pile Length				
-1.3779	795680.	0.000	0.000	0.000	1.994E+12	Pile Head Deflection				
84.396	1.668E-05	0.000	5733.3084	0.000	1.994E+12	Pile Head Moment				
-1.1374	813423.	0.000	0.000	0.000	1.994E+12	Pile Head Shear				
85.389	1.309E-05	0.000	5568.9097	0.000	1.994E+12	Pile Length				
-0.9134	831170.	0.000	0.000	0.000	1.994E+12	Pile Head Deflection				
86.382	9.924E-06	0.000	5274.8402	0.000	1.994E+12	Pile Head Moment				
-0.7071	848916.	0.000	0.000	0.000	1.994E+12	Pile Head Shear				
87.375	7.131E-06	0.000	4880.3881	0.000	1.994E+12	Pile Length				
-0.5187	866661.	0.000	0.000	0.000	1.994E+12	Pile Head Deflection				
88.368	4.684E-06	0.000	4412.3037	0.000	1.994E+12	Pile Head Moment				
-0.3477	884400.	0.000	0.000	0.000	1.994E+12	Pile Head Shear				
89.361	2.552E-06	0.000	3894.8575	0.000	1.994E+12	Pile Length				
-0.1932	902151.	0.000	0.000	0.000	1.994E+12	Pile Head Deflection				
90.354	6.974E-07	0.000	3549.9772	0.000	1.994E+12	Pile Head Moment				
-0.0358	919891.	0.000	0.000	0.000	1.994E+12	Pile Head Shear				
91.347	7.189E-07	0.000	2797.4532	0.000	1.994E+12	Pile Length				
0.0753	936421.	0.000	0.000	0.000	1.994E+12	Pile Head Deflection				
0.1873	95356E-06	0.000	2253.1952	0.000	1.994E+12	Pile Head Moment				
0.2934	9731333.	0.000	1739.5295	0.000	1.994E+12	Pile Head Shear				

Pier 41af. 1p70
 44.6805 0.3250785 5925240. 5855354. 5855354. 5855354. 5855354. 5855354. 5855354. 5855354.
 39.7160 0.3892194 32523. 32523. 32523. 32523. 32523. 32523. 32523. 32523.
 34.7515 1.6161080 39254. 39254. 39254. 39254. 39254. 39254. 39254. 39254.
 29.7870 4.3278180 59025. 59025. 59025. 59025. 59025. 59025. 59025. 59025.
 76744. -76744. -76744. -76744. -76744. -76744. -76744. -76744. -76744. -76744.

Computed Values of Pile Loading and Deflection
 for Lateral Loading for Load Case Number 10

Pile-head conditions are Shear and Moment (Loading Type 1)
 = 8400.0 lbs
 = 3248400.0 in-lbs
 = 0.0 lbs

Shear force at pile head
 Applied moment at pile head
 Axial thrust load on pile head

Res. X	Soil Spr.	Depth	Deflect.	Bending	Shear	Slope	Total	Bending	Soil
feet	inches	inches	inches	inches	lbs	radians	Stress	Stiffness	p
lb/inch	lb/inch	lb/inch	lb/inch	lb/inch	psi*	lb-in ²	lb/in ²	lb/in ²	lb/in
0.000	0.000	0.2292	0.3248400	8400.0000	0.001023	0.0000	1.345E+12	0.000	1.985E+12
0.000	0.993	0.2172	0.358484	8400.0000	-0.000994	0.0000	1.345E+12	0.000	1.985E+12
0.000	1.986	0.2055	0.3448569	8400.0000	-0.000964	0.0000	1.344E+12	0.000	1.985E+12
0.000	2.979	0.1942	0.3586653	8400.0000	-0.000933	0.0000	1.344E+12	0.000	1.985E+12
0.000	3.972	0.1833	0.368737	8400.0000	-0.000906	0.0000	1.988E+12	0.000	1.990E+12
0.000	4.965	0.1726	0.3748822	8400.0000	-0.000884	0.0000	1.988E+12	0.000	1.991E+12
0.000	5.957	0.1622	0.384906	8400.0000	-0.000861	0.0000	1.988E+12	0.000	1.991E+12
0.000	6.950	0.1521	0.3948990	8400.0000	-0.000838	0.0000	1.987E+12	0.000	1.992E+12
0.000	7.943	0.1422	0.4049075	8400.0000	-0.000814	0.0000	1.987E+12	0.000	1.992E+12
0.000	8.936	0.1327	0.4149159	8400.0000	-0.000789	0.0000	1.987E+12	0.000	1.993E+12
0.000	9.929	0.1234	0.4249243	8400.0000	-0.000764	0.0000	1.986E+12	0.000	1.994E+12
0.000	10.922	0.1145	0.4349328	8400.0000	-0.000738	0.0000	1.986E+12	0.000	1.994E+12
0.000	11.915	0.1059	0.4449412	8400.0000	-0.000712	0.0000	1.986E+12	0.000	1.994E+12
0.000	12.908	0.0975	0.4549496	8400.0000	-0.000685	0.0000	1.986E+12	0.000	1.994E+12
0.000	13.901	0.0895	0.4649580	8400.0000	-0.000657	0.0000	1.986E+12	0.000	1.994E+12
0.000	14.893	0.0819	0.4749665	7660.8781	-0.000629	0.0000	1.986E+12	0.000	1.994E+12
-124.0679	18056	0.0745	4832136	6731.0597	-0.000600	0.0000	1.985E+12	0.000	1.994E+12
-32.0100	5116.3104	0.0676	4910063	6079.7680	-0.000571	0.0000	1.985E+12	0.000	1.994E+12
-77.3148	13634	0.0609	4977015	4944.2365	-0.000541	0.0000	1.985E+12	0.000	1.994E+12
-113.2938	22152	0.0547	5027882	49.645	-0.0002179	0.0000	1.985E+12	0.000	1.994E+12
-140.7123	30670	0.0488	5058774	18345.2	-0.000172	0.0000	1.988E+12	0.000	1.988E+12
-160.3457	39187	0.0432	5066903	15847	-0.000150	0.0000	1.988E+12	0.000	1.988E+12
-172.9742	47705	0.0380	5050476	13779.7	-0.000129	0.0000	1.989E+12	0.000	1.989E+12
-179.3764	56223	0.0332	5008585	11584.7	-0.000109	0.0000	1.989E+12	0.000	1.989E+12
-180.3231	64741	0.0287	4941094	9029.4	-0.000084	0.0000	1.988E+12	0.000	1.988E+12
-176.5705	73258	0.0246	4848537	7278.01	-0.000062	0.0000	1.988E+12	0.000	1.988E+12
-168.8534	81776	0.0208	4732009	5817.94	-0.000043	0.0000	1.987E+12	0.000	1.987E+12
-157.8792	90294	0.0174	4593068	4593.068	-0.000027	0.0000	1.986E+12	0.000	1.986E+12
-144.3220	98612	0.0143	4433639	3473.29	-0.000021	0.0000	1.986E+12	0.000	1.986E+12
-128.8176	107329	0.0115	4255922	2863.416	-0.0000196	0.0000	1.987E+12	0.000	1.987E+12
-111.9586	115847	0.009034	4062312	2319.08	-0.000172	0.0000	1.988E+12	0.000	1.988E+12
-119.6394	13779.7	0.00843	3851717	1820.126	-0.000150	0.0000	1.988E+12	0.000	1.988E+12
-112.4995	195890	0.00827	3625152	1420.126	-0.000129	0.0000	1.989E+12	0.000	1.989E+12
-103.9147	251311	0.00812	3383835	1080.126	-0.000109	0.0000	1.990E+12	0.000	1.990E+12
-93.3340	340124	0.00806	3129268	820.126	-0.000084	0.0000	1.988E+12	0.000	1.988E+12
-79.4887	510836	0.00806	2863416	620.126	-0.000062	0.0000	1.988E+12	0.000	1.988E+12
-57.9985	1044214	0.00806	2389331	460.126	-0.000043	0.0000	1.988E+12	0.000	1.988E+12
46.9325	1714471	0.00806	1820126	340.126	-0.000027	0.0000	1.986E+12	0.000	1.986E+12
36.737	2321908	0.00806	1372823	250.126	-0.000021	0.0000	1.986E+12	0.000	1.986E+12
86.9322	2064846	0.00806	98612	180.126	-0.0000196	0.0000	1.987E+12	0.000	1.987E+12
96.7316	1820126	0.00806	620126	130.126	-0.000172	0.0000	1.988E+12	0.000	1.988E+12
104.117	15847	0.00806	4062312	90.126	-0.000150	0.0000	1.988E+12	0.000	1.988E+12
109.8713	13779.7	0.00806	3129268	66.126	-0.000129	0.0000	1.989E+12	0.000	1.989E+12
114.3729	11584.7	0.00806	2389331	49.126	-0.000109	0.0000	1.990E+12	0.000	1.990E+12
117.8442	9029.4	0.00806	1820126	36.126	-0.000084	0.0000	1.988E+12	0.000	1.988E+12
93.3622	7278.01	0.00806	1420126	27.126	-0.000062	0.0000	1.988E+12	0.000	1.988E+12
95.9635	5817.94	0.00806	1080126	20.126	-0.000043	0.0000	1.988E+12	0.000	1.988E+12
96.8000	4593.068	0.00806	820126	15.126	-0.000027	0.0000	1.986E+12	0.000	1.986E+12
96.0088	41574	0.00806	620126	11.126	-0.000021	0.0000	1.986E+12	0.000	1.986E+12
93.7507	432319	0.00806	4062312	8.126	-0.0000196	0.0000	1.987E+12	0.000	1.987E+12
90.2043	450064	0.00806	2389331	6.126	-0.000172	0.0000	1.988E+12	0.000	1.988E+12
49.645	-0.0002179	0.0000	1820126	4.126	-0.000150	0.0000	1.988E+12	0.000	1.988E+12

Pier 41laf.lp70		Pier 41laf.lp70	
85.5587	467810.	0.000	1.994E+12
80.0085	485555.	0.000	1.994E+12
51.631	-0.001746	0.000	1.994E+12
73.7486	503300.	0.000	1.994E+12
52.624	-0.001531	0.000	1.994E+12
66.9707	521046.	0.000	1.994E+12
59.6596	538791.	0.000	1.994E+12
52.5911	556536.	0.000	1.994E+12
45.3305	574282.	0.000	1.994E+12
38.7317	592027.	0.000	1.994E+12
31.4369	609772.	0.000	1.994E+12
69.8882	1748857.	0.000	1.994E+12
59.574	-0.00076	0.000	1.994E+12
60.4617	2024317.	0.000	1.994E+12
51.0863	2400549.	0.000	1.994E+12
41.7353	2942787.	0.000	1.994E+12
61.560	-0.000169	0.000	1.994E+12
62.533	3832068.	0.000	1.994E+12
63.546	-4.697E-05	0.000	1.994E+12
22.2223	5637240.	0.000	1.994E+12
64.538	-6.859E-06	0.000	1.994E+12
9.0919	13793336.	0.000	1.994E+12
65.531	2.198E-05	0.000	1.994E+12
-14.7432	7991464.	0.000	1.994E+12
66.324	4.163E-05	0.000	1.994E+12
-20.3253	5874380.	0.000	1.994E+12
67.117	5.402E-05	0.000	1.994E+12
-23.4771	5178302.	0.000	1.994E+12
68.310	6.087E-05	0.000	1.994E+12
-24.8893	489186.	0.000	1.994E+12
-25.6057	472860.	0.000	1.994E+12
-25.6196	48363E-05	0.000	1.994E+12
-25.6189	48363E-05	0.000	1.994E+12
-25.7108	48363E-05	0.000	1.994E+12
-24.7248	501517.	0.000	1.994E+12
-24.7347	51506E-05	0.000	1.994E+12
-2.8570	618222.	0.000	1.994E+12
-2.7172	618222.	0.000	1.994E+12
-2.7172	635971.	0.000	1.994E+12
-2.5493	64646E-05	0.000	1.994E+12
-2.76453	653711.	0.000	1.994E+12
-2.3605	671462.	0.000	1.994E+12
-2.77446	689208.	0.000	1.994E+12
-2.78439	689208.	0.000	1.994E+12
-1.9462	706953.	0.000	1.994E+12
-1.7321	724698.	0.000	1.994E+12
-1.80425	2.439E-05	0.000	1.994E+12
-1.5197	742444.	0.000	1.994E+12
81.418	2.058E-05	4290.5781	0.000
-1.3129	760189.	0.000	1.994E+12
82.411	1.707E-05	4498.2491	0.000
-1.1146	777934.	0.000	1.994E+12
83.404	1.389E-05	4547.6861	0.000
-0.9273	795680.	0.000	1.994E+12
84.396	1.102E-05	4465.4825	0.000
-0.7526	813425.	0.000	1.994E+12
85.389	8.480E-06	4276.4404	0.000
-0.5915	831170.	0.000	1.994E+12
86.382	6.240E-06	4003.4240	0.000
-0.4446	848916.	0.000	1.994E+12
87.375	4.285E-06	3667.2932	0.000
-0.3117	866661.	0.000	1.994E+12
88.368	2.592E-06	3286.9120	0.000
-0.1924	884406.	0.000	1.994E+12
89.361	1.132E-06	2879.2192	0.000
-0.0857	902151.	0.000	1.994E+12
90.354	-1.221E-07	2459.3544	0.000
0.009424	919897.	0.000	1.994E+12
91.347	-1.201E-06	2040.8275	0.000
0.0945	937642.	0.000	1.994E+12
92.340	-2.135E-06	1635.7226	0.000
0.1712	955387.	0.000	1.994E+12
93.333	-2.953E-06	1254.9262	0.000
0.2412	973133.	0.000	1.994E+12
94.325	-3.681E-06	908.3695	0.000
0.3061	990878.	0.000	1.994E+12
95.318	-4.345E-06	605.2744	0.000
0.3678	1008623.	0.000	1.994E+12
96.311	-4.965E-06	334.3939	0.000
0.4277	1026369.	0.000	1.994E+12
97.304	-5.561E-06	164.2341	0.000
0.4873	1044114.	0.000	1.994E+12
98.297	-6.144E-06	43.2500	0.000
0.5476	1061859.	0.000	1.994E+12
99.290	-6.725E-06	0.000	1.994E+12
0.6093	539802.	0.000	1.994E+12

* This analysis computed pile response using nonlinear moment-curvature relationships.

Values of total stress due to combined axial and bending stresses are computed only for elastic sections only and do not equal the actual stresses in concrete and steel.

Stresses in concrete and steel may be interpolated from the output for nonlinear bending properties relative to the magnitude of bending moment developed in the pile.

Output Summary for Load Case No. 10:

File-head deflection	=	0.2291784 inches
Computed slope at pile head	=	-0.0010230 radians
Maximum bending moment	=	3069593. lbf-in
Maximum shear force	=	20.850660 lbf
Depth of maximum bending moment	=	20.850660 feet below pile head
Depth of maximum shear force	=	33.744400 feet below pile head
Number of iterations	=	7
Number of zero deflection points	=	3

Pier 41af.1p7o

Pile-head Deflection vs. Pile Length for Load Case 10

Boundary Condition Type 1, Shear and Moment

Shear Moment	=	8400. 1b
Axial Load	=	3248400. in- 1b
		0. 1b

Pile Length feet	Pile Head Deflection inches	Maximum Moment in-lbs	Maximum Shear lbs
99.2900	0.2291784	5066903.	-22724.
94.3255	0.2297628	5075797.	-22722.
89.3610	0.2300386	5082277.	-22859.
84.3965	0.2303329	5085583.	-22925.
79.4320	0.2307949	5088648.	-22924.
74.4675	0.2310115	5090253.	-22945.
69.5030	0.2368836	5165562.	-23359.
64.5385	0.23211047	5098661.	-23003.
59.5740	0.2325030	5104450.	-22882.
54.6095	0.2374594	5165143.	-24660.
49.6450	0.2365516	5108226.	-28253.
44.6805	0.2723614	5075565.	-33509.
39.7160	0.4601834	5006097.	-48264.
34.7515	1.1178307	4975222.	-64394.
29.7870	2.8363199	4912651.	

The analysis ended normally.

SER 1

Δ = 0.23 < 1" OK

Summary of Pile Response(s)

Definitions of Pile-head Loading Conditions:

- Load Type 1: Load 1 = Shear, lbs, and Load 2 = Moment, in-lbs
- Load Type 2: Load 1 = Shear, lbs, and Load 2 = Slope, radians
- Load Type 3: Load 1 = Shear, lbs, and Load 2 = Rotational Stiffness, in-lbs/radian
- Load Type 4: Load 1 = Top Deflection, inches, and Load 2 = Moment, in-lbs
- Load Type 5: Load 1 = Top Deflection, inches, and Load 2 = Slope, radians

Case No.	Pile Head Deflection in Pile No.	Pile-head Condition 1 v(lbs) or y(inches)	Pile-head Condition 2 Rotation in-lb/rad. or in-lb/rad. radians	Pile-head	
				Axial Loading lbs	Maximum Moment in-lbs
1	4	y = 0.5000	M = 3793200.	0.0000000	0.50000000
2	4	y = -38241.	M = -0.0020301	0.0000000	1.00000000
3	4	y = -59840.	M = -0.00386053	0.0000000	1.50000000
4	4	y = 1.5000	M = 3793200.	0.0000000	1.50000000
5	4	y = -80753.	M = -0.005696889	0.0000000	1.50000000

PIER 1

Worst Case	Limit State	Load Case	Column	Top/Bot	M _u	P _u	V _u
Max P _u	STR-I	1/2/3	1	T	540.1	777.5	
	SER-I	1/2/3	1	T	248.8	516.1	
Max V _u	STR-I	26	3	T	458.3		13.6
	SER-I	28	4	T	65.3		9.9

PIER 2

Worst Case	Limit State	Load Case	Column	Top/Bot	M _u	P _u	V _u
Max P _u	STR-I	2	4	T	252.0	689.2	
	SER-I	1/3	1	T	132.4	464.8	
Max V _u	STR-V	28	4	T	115.2		8.8
	SER-I	28	4	T	98.6		8.7

PIER 3

Worst Case	Limit State	Load Case	Column	Top/Bot	M _u	P _u	V _u
Max P _u	STR-I	4	4	T	141.4	688.3	
	SER-I	4	1	T	218.4	500.6	
Max V _u	STR-III	25	2	T	651.5		21.3
	SER-I	26	3	T	365.0		11.0

PIER 4

$R_R = 1044 \text{ K}$

Worst Case	Limit State	Load Case	Column	Top/Bot	M _u	P _u	V _u
Max P _u	STR-I	1/2/3	1	T	377.0	709.1	
	SER-I	1/2/3	1	T	185.3	475.0	
Max V _u	STR-I	26	4	T	316.1		9.8
	SER-I	26	4	T	270.7		8.4

PIER 4
 4' Ø, 1/2" STEEL CASING @ EL +3.0

DEFLECTION

STR-I
(lbs)

SER I
(lbs)

0.5

23,822

25,024

1.0

44,719

46,591 ← 5K

1.5

64,823

66,691

2.0

81,307

83,836

8K

GEOTECHNICAL AXIAL CAPACITY

= 1044 K > 709.1 K OK

LATERAL CAPACITY, 2" DEFLECTION (STR-I) →

= 81.81 K > 9.8 K

LATERAL CAPACITY, 1" DEFLECTION (SER-I)

= 46.59 K > 8.4 K

FINAL FOUNDATION REPORT (REV. November 2014)

**BR 1-159 - Newport Bridge
James Street Over Christina River
New Castle County, Delaware**

APPENDIX C-3

Scour Analysis Summary

July 30, 2014

TABLE 12
SCOUR DEPTH SUMMARY – PROPOSED JULY 2014 BRIDGE
Scenario 2: FEMA Flows With Normal Depths as DS Controls

Scour at NORTH ABUTMENT

Discharge Frequency	Scour Depths				Elevation at Total Scour Depth	Bottom of Footing/Pile Cap Elevation
	Long Term (ft.)	Contraction (ft.)	Local (ft.)	Total (ft.)		
50 Year	Negligible	0	0	0	NA	
100 Year	Negligible	0	0	0	NA	
500 Year	Negligible	1.14	8.85	9.99	3.5	

Scour at PIER 4

Discharge Frequency	Scour Depths				Elevation at Total Scour Depth	Bottom of Footing/Pile Cap Elevation
	Long Term (ft.)	Contraction (ft.)	Local (ft.)	Total (ft.)		
50 Year	Negligible	0	6.07	6.07	-8	
100 Year	Negligible	0.1	6.53	6.63	-8.5	
500 Year	Negligible	0	7.20	7.20	-9	

Scour at PIER 3

Discharge Frequency	Scour Depths				Elevation at Total Scour Depth	Bottom of Footing/Pile Cap Elevation
	Long Term (ft.)	Contraction (ft.)	Local (ft.)	Total (ft.)		
50 Year	Negligible	0	6.92	6.92	-22	
100 Year	Negligible	0.1	7.20	7.30	-22	
500 Year	Negligible	0	7.20	7.20	-22	

Scour at PIER 2

Discharge Frequency	Scour Depths				Elevation at Total Scour Depth	Bottom of Footing/Pile Cap Elevation
	Long Term (ft.)	Contraction (ft.)	Local (ft.)	Total (ft.)		
50 Year	Negligible	0	0	0	NA	
100 Year	Negligible	0.1	7.18	7.28	-18	
500 Year	Negligible	0	7.20	7.20	-18	

Scour at PIER 1

Discharge Frequency	Scour Depths				Elevation at Total Scour Depth	Bottom of Footing/Pile Cap Elevation
	Long Term (ft.)	Contraction (ft.)	Local (ft.)	Total (ft.)		
50 Year	Negligible	0	0	0	NA	
100 Year	Negligible	0	0	0	NA	
500 Year	Negligible	0	2.27	2.27	6	

Scour at SOUTH ABUTMENT

Discharge Frequency	Scour Depths				Elevation at Total Scour Depth	Bottom of Footing/Pile Cap Elevation
	Long Term (ft.)	Contraction (ft.)	Local (ft.)	Total (ft.)		
50 Year	Negligible	0	0	0	NA	
100 Year	Negligible	0	0	0	NA	
500 Year	Negligible	0	3.04	3.04	5	

FINAL FOUNDATION REPORT (REV. November 2014)
BR 1-159 - Newport Bridge
James Street Over Christina River
New Castle County, Delaware

APPENDIX D

Special Provisions

SECTION 606 DRILLED SHAFTS

606.01 Description.

- A. Furnish all materials, labor, tools, equipment, services and incidentals necessary to construct the drilled shafts in accordance with the Contract Documents and this Specification.

606.02 Materials.

- A. Provide materials as specified in the following:
1. Steel Casings as per Section **1XXX**
 2. Reinforcing Steel as per Section **1XXX**
 - a. Bundle vertical bars when necessary to maximize clear space between vertical reinforcement bars.
 - b. Use rolled hoops or bundled spirals when necessary to maximize clear space between horizontal reinforcement.
 3. Welding Material as per Section **1XXX**
 4. Portland Cement Concrete, Class A or B, as per Section **1XXX**
 - a. Comply to the following concrete slump requirements:
 - i. Dry placement methods: 5 to 7 inches
 - ii. Casing removal methods: 8 to 10 inches
 - iii. Tremie Placement methods: 8 to 10 inches
 - b. Slump loss to less than 4 inches is not permitted during the period equal to the anticipated pour period plus two hours. Slump life may be extended through the use of retarders and mid-range water reducers with the approval of the Engineer.
 - c. Unless otherwise specified on the Plans or as directed by the engineer, the following mix characteristics must be met:
 - i. A maximum course aggregate size of 3/8" in wet hole pours or shafts with dense reinforcing configurations. Dense reinforcing configuration is defined as cases where the clear spacing between verticals or spiral/hoops is less than 10 times the aggregate size.
 - ii. Use of rounded in lieu of crushed aggregates.
 - iii. Use of fly ash as a cement replacement and as a fluidifier.
 5. Slurry as per Section **1XXX**
 6. Access Tubes for Crosshole Sonic Log Testing as per Section **1XXX**
 7. Grout as per Section **1XXX**

606.03 Construction.

- A. *Submittals, Approvals, and Meetings.* At the time of bid, submit the qualifications of the Contractor (i.e., the drilled shaft specialty contractor) to verify the successful completion by the Contractor of at least three separate foundation projects within the last five years with drilled shafts of similar size (diameter and depth) and similar subsurface geotechnical conditions to those shown in the Plans. Include a brief description of each project and the owner's contact person's name and current phone number for each project listed.
1. *Experience and Personnel.* At least two weeks prior to the start of drilled shaft construction, submit a list identifying the on-site supervisors and drill rig operators assigned to the project to the Engineer for approval. In the list, include a detailed summary of each individual's experience in drilled shaft excavation operations, and placement of assembled reinforcing cages and concrete in drilled shafts.
 - a. On-site supervisors must have a minimum of two years' experience in supervising construction of drilled shaft foundations of similar size (diameter and depth) and difficulty to those shown in the Plans, and similar geotechnical conditions to those described in the geotechnical report. The work experience must be direct supervisory

responsibility for the on-site drilled shaft construction operations. Project management level positions indirectly supervising on-site drilled shaft construction operations are not acceptable for this experience requirement.

- b. Drill rig operators must have a minimum one year experience in construction of drilled shaft foundations.

The Engineer will approve or reject the Contractor's qualifications and field personnel within ten working days after receipt of the submission. Do not start work on any drilled shaft until the Contractor's qualifications and field personnel are approved by the Engineer. The Engineer may suspend the drilled shaft construction if the Contractor substitutes field personnel without prior approval by the Engineer. The Contractor is fully liable for the additional costs resulting from the suspension of work, and no adjustments in contract time resulting from such suspension of work will be allowed.

2. *Drilled Shaft Installation Plan.* At least four weeks prior to the start of drilled shaft construction, submit a Drilled Shaft Installation Plan narrative for acceptance by the Engineer. In preparing the narrative, reference the available subsurface geotechnical data provided in the Contract boring logs and any geotechnical report(s) prepared for this project. In this narrative, provide at a minimum the following information:
 - a. Description of overall construction operation sequence and the sequence of drilled shaft construction when in groups or lines.
 - b. A list, description, and capacities of proposed equipment, including but not limited to cranes, drills, augers, bailing buckets, final cleaning equipment and drilling unit. As appropriate, describe why the equipment was selected, and describe equipment suitability to the anticipated site and subsurface conditions. Include a project history of the drilling equipment demonstrating the successful use of the equipment on shafts of equal or greater size in similar subsurface geotechnical conditions.
 - c. Details of drilled shaft excavation methods, including proposed drilling methods, methods for cleanout of the bottom of the excavation hole, and a disposal plan for excavated material and drilling slurry (if applicable). If appropriate, include a review of method suitability to the anticipated site and subsurface geotechnical conditions including boulders and obstruction removal techniques if such are indicated in the Contract subsurface geotechnical information or Contract Documents.
 - d. Details of the method(s) to be used to ensure drilled shaft hole stability (i.e., prevention of caving, bottom heave, etc. using temporary casing, slurry, or other means) during excavation and concrete placement. Include a review of method suitability to the anticipated site and subsurface geotechnical conditions.
 - e. Provide detailed procedures for mixing, using, maintaining, and disposing of the slurry. Also provide a detailed mix design (including all additives and their specific purpose in the slurry mix) and a discussion of its suitability to the anticipated subsurface geotechnical conditions for the proposed slurry.

In the submittal, include a detailed plan for quality control of the selected slurry, including tests to be performed, test methods to be used, and minimum and/or maximum property requirements which must be met to ensure that the slurry functions as intended, considering the anticipated subsurface conditions and shaft construction methods, in accordance with the slurry manufacturer's recommendations and these Specifications. As a minimum, include the following tests in the slurry quality control plan:

Property	Test Method
Density	Mud Weight (Density), API 13B-1, Section 1

Viscosity	Marsh Funnel and Cup, API 13B-1, Section 2.2
pH	Glass Electrode, pH Meter, or pH Paper
Sand Content	Sand, API 13B-1, Section 5

- f. Reinforcing steel working drawings, details of reinforcement placement including type and location of all splices, reinforcement cage support and centralization methods, type and location of all spacers, crosshole sonic logging tubes and other instrumentation, and procedures for lifting and setting the reinforcement cage.
- g. When casings are proposed or required, provide the following:
 - i. Casing dimensions and detailed procedures for permanent casing installation.
 - ii. Temporary casing installation and removal.
 - iii. Methods of advancing the casing, along with the means to be utilized for excavating the drilled shaft hole in accordance with Subsection 606.03 of this Specification.
- h. When using temporary casing, details of the method to extract the temporary casing and maintaining shaft reinforcement in proper alignment and location, and maintaining the concrete slump to keep concrete workable during casing extraction.
- i. Details of concrete placement, including proposed equipment and procedures for delivering concrete to the drilled shaft, placement of the concrete into the shaft including initial placement and the raising of the tremie or pump line during placement, size of tremie and pump lines, operational procedures for pumping, and a sample uniform yield form to be used by the Contractor for plotting the volume of concrete placed versus the depth of shaft for all shaft concrete placement.
- j. The method to be used to form a horizontal construction joint during concrete placement.
- k. When applicable, include a description of the material to be used to temporarily backfill a drilled shaft excavation hole during a stoppage of the excavation operation, as well as the method used to place and remove the material.
- l. Details of procedures to prevent loss of slurry or concrete into waterways, sewers and other areas to be protected.
- m. Describe the method and materials that will be used to fill or eliminate all voids below the top of shaft between the plan shaft diameter and excavated shaft diameter, or between the shaft casing and surrounding soil, if permanent casing is specified.
- n. Details of any required load tests including equipment, instrumentation, procedures, calibration data for test equipment, calculations and drawings.
- o. Details and procedures for protecting existing structures, utilities, roadways and other facilities during drilled shaft installation.
- p. Other information required by the Plans or specified herein.

The Engineer will evaluate the Drilled Shaft Installation Plan for conformance with the Contract Plans and Specifications within ten working days after receipt of the submission. At the option of the Department, a Shaft Installation Plan Submittal Meeting may be scheduled following review of the Contractor's initial submittal of the Plan. Those attending the Shaft Installation Plan Submittal Meeting, if held, must include the following:

- a. The superintendent, on-site supervisors, and other Contractor personnel involved in the preparation and execution of the Drilled Shaft Installation Plan.
- b. The Project Engineer and Department's personnel involved with the structural, geotechnical, and construction review of the Drilled Shaft Installation Plan together with Department's personnel who will provide inspection and oversight during the drilled shaft construction phase of project.

Submit any significant updates or modifications to the Drilled Shaft Installation Plan whenever such updates or modifications are proposed to the Engineer. The Engineer will evaluate the new information for conformance with the Contract Plans and Specifications within ten working days after receipt of the submission.

3. *Slurry Technical Assistance.* If slurry is used to construct the drilled shafts, provide, or arrange for, technical assistance from the slurry manufacturer as specified in Subsection 606.03(D)(4)(a) of this Specification. Submit the following to the Engineer:
 - a. The name and current phone number of the slurry manufacturer's technical representative assigned to the project.
 - b. The name(s) of the Contractor's personnel assigned to the project and trained by the slurry manufacturer's technical representative in the proper use of the slurry. In the submittal, include a signed training certification letter from the slurry manufacturer for each individual, including the date of the training.
4. *Approvals.* Do not begin work until all the required submittals have been accepted in writing by the Engineer. All procedural acceptances given by the Engineer will be subject to trial in the field and will not relieve the Contractor of the responsibility to satisfactorily complete the work.
5. *Drilled Shaft Preconstruction Conference.* Hold a shaft preconstruction conference at least five working days prior to the Contractor beginning any shaft construction work at the site to discuss investigative boring information, construction procedures, personnel, and equipment to be used, and other elements of the accepted Shaft Installation Plan as specified in Subsection 606.03(A)(2) of this Specification. If slurry is used to construct the shafts, the frequency of scheduled site visits to the project site by the slurry manufacturer's representative will be discussed. Those attending must include:
 - a. The superintendent, on site supervisors, and other key personnel identified by the Contractor as being in charge of excavating the shaft, placing the casing and slurry as applicable, placing the steel reinforcing bars, and placing the concrete. If slurry is used to construct the shafts, the slurry manufacturer's representative and a Contractor's employee trained in the use of the slurry, as identified to the Engineer in accordance with Subsection 606.03(D)(4)(a) of this Specification, must also attend.
 - b. The Project Engineer, key inspection personnel, and appropriate representatives of the Department.

If the Contractor's key personnel change, or if the Contractor proposes a significant revision of the approved Drilled Shaft Installation Plan, an additional conference may be held at the request of the Engineer before any additional shaft construction operations are performed.

6. *Logs of Shaft Construction.* Prepare inspection logs documenting each shaft construction activity, including casing installation, excavation, shaft bottom inspection, reinforcement installation and concrete placement. Fully document the work performed with frequent reference to the date, time and casing/excavation elevation in the logs. In addition, prepare and submit the logs documenting any subsurface investigation borings or rock core holes performed for the Contract at drilled shaft foundation locations.

In the records for temporary and permanent casing, include at least the following information:

- a. Identification number and location of the shaft.
- b. Diameter and wall thickness of the casing.
- c. Dimensions of any casing reinforcement.
- d. Top and bottom elevations of the casing.
- e. Method and equipment used for casing installation.
- f. Any problems encountered during casing installation.
- g. Name of the inspector.

In the shaft excavation log, include at least the following information:

- a. Identification number, location and surface elevation of the shaft.
- b. Description and approximate top and bottom elevation of each soil or rock material encountered.
- c. Seepage or groundwater conditions.
- d. Type and dimensions of tools and equipment used, and any changes to the tools and equipment.
- e. Type of drilling fluid used, if any, and the results of slurry tests.
- f. Any problems encountered.
- g. Elevation of any changes in the shaft diameter.
- h. Method used for bottom cleaning.
- i. Final bottom elevation of the shaft.
- j. Name of the inspector and the date, time and name of any changes in the inspector.

In the concrete placement records, include at least the following information:

- a. Concrete mix used.
- b. Time of start and end of concrete placement.
- c. Volume and start/end time for each truck load placed.
- d. Concrete test results.
- e. Concrete surface elevation and corresponding tremie tip elevation periodically during concrete placement.
- f. Concrete yield curve (volume versus concrete elevation, actual and theoretical).
- g. Name of the inspector.

Submit the logs for each shaft construction activity to the Engineer within 24 hours of the completion of that activity. Submit a full set of shaft inspection logs for an individual drilled shaft to the Engineer within 48 hours of the completion of concrete placement at the shaft.

- B. *Drilled Shaft Excavation.* Excavate the drilled shafts to the required depth as shown in the Plans or as directed by the Engineer. Once the excavation operation has been started, conduct the excavation in a continuous operation until the excavation of the shaft is completed, except for pauses and stops as noted, using approved equipment capable of excavating through the type of material expected. Pauses during this excavation operation, except for casing splicing and removal of obstructions, will not be allowed. Provide temporary casing at the site in sufficient quantities to meet the needs of the anticipated construction method.

Pauses, defined as interruptions of the excavation operation, will be allowed only for casing splicing and removal of obstructions. Drilled shaft excavation operation interruptions not conforming to this definition are considered as stops.

If the drilled shaft excavation is not complete at the end of the shift or series of continuous shifts, the drilled shaft excavation operation may be stopped, provided the Contractor, before the end of the work day, protects the shaft as indicated in Subsection 606.03(C) of this Specification.

If slurry is present in the shaft excavation, conform to the requirements of Subsection 606.03(D)(4)(b) of this Specification regarding the maintenance of the minimum level of drilling slurry throughout the stoppage of the shaft excavation operation, and recondition the slurry to the required slurry properties in accordance with Section 606.02 of this Specification prior to recommencing shaft excavation operations.

Ensure the excavation and drilling equipment have adequate capacity, including power, torque and down thrust to excavate a hole of both the maximum diameter and to a depth of 20 feet, or 20 percent, beyond the maximum shaft length shown on the Plans, whichever is greater.

Blasting will only be permitted if specifically stated on the Plans or authorized in writing by the Engineer.

Perform sidewall overreaming when the time for shaft excavation exceeds 36 hours or as directed by the Engineer (measured from the beginning of excavation below the casing when casing is used) before the start of concrete placement. Also perform sidewall overreaming when the sidewall of the hole is determined by the Engineer to have softened due to the excavation methods, swelled due to delays in the start of concrete placement, or degraded because of slurry cake buildup. Overreaming thickness must be a minimum of 1/2-inch and a maximum of 3 inches. Overreaming may be accomplished with a grooving tool, overreaming bucket, or other equipment approved by the Engineer. If overreaming is required as a result of the excavation time exceeding the time limit specified herein, or as a result of excavation methods not in compliance with the approved Drilled Shaft Installation Plan, the Contractor will bear the costs associated with both sidewall overreaming and additional drilled shaft concrete related to overreaming.

Complete excavation to the foundation cap elevation before drilled shaft construction begins, unless otherwise noted in the Contract Documents or approved by the Engineer. Any disturbance to the foundation cap area caused by shaft installation will be repaired by the Contractor prior to placing the cap concrete.

When drilled shafts are to be installed in conjunction with embankment construction, construct drilled shafts after placement of the embankment fill unless otherwise shown on the Contract Documents or approved by the Engineer. Do not cap the drilled shafts installed prior to the completion of the embankment fill until the fill has been placed to the bottom of cap level.

- C. *Drilled Shaft Excavation Protection.* Do not leave drilled shaft excavations open overnight unless cased full depth or otherwise protected against sidewall instability. An open excavation is defined as a drilled shaft that has not been filled with concrete, or temporarily backfilled with a material approved by the Engineer in accordance with Subsection 606.03(A)(2) of this Specification or protected in accordance with Subsection 606.03(D). The use of slurry to protect a drilled shaft during a drilling stoppage or overnight shutdown may be approved by the Engineer.

Casing of drilled shafts in stable rock formations during stoppages is not required, unless shown on the Plans or specified herein.

- D. *Drilled Shaft Excavation Protection Methods.* The Contractor bears full responsibility for selection and execution of the method(s) of stabilizing and maintaining the drilled shaft excavation. Protect the walls and bottom of the drilled shaft excavation so that side wall caving and bottom heave is prevented from occurring, and so that the soil adjacent to the drilled shaft is not disturbed. The Contractor may excavate the drilled shaft without excavation protection provided the Contractor can demonstrate that the soil/rock is stable and above the water table and zones of seepage. Acceptable protection methods include the use of casing, drilling slurry, or both.
1. *Temporary Casing Construction Method.* In stable soils, conduct casing installation and removal operations and drilled shaft excavation operations such that the adjacent soil outside the casing and drilled shaft excavation for the full height of the drilled shaft is not disturbed. Disturbed soil is defined as soil whose geotechnical properties have been changed from those of the original in-situ soil, and whose altered condition adversely affects the performance of the drilled shaft foundation.

If utilizing casing that is adequately sealed into competent soils such that water cannot enter the excavation, the Contractor may, with the Engineer's approval, continue excavation in soils below the water table provided the water level within the casing do not rise or exhibit flow.

As the temporary casing is withdrawn, a sufficient head of fluid concrete must be maintained to ensure that water or slurry outside the temporary casing will not breach the column of freshly placed concrete.

Extract the casing at a slow, uniform rate with the pull in line with the shaft axis. Avoid excessive rotation of the casing to limit deformation of the reinforcing steel cage.

Remove all temporary casings from the excavation as concrete placement is completed, unless permission has been received from the Engineer to leave specified temporary casings in place.

2. *Permanent Casing Construction Method.* When permanent casing is specified, excavation will conform to the specified outside diameter of the drilled shaft. After the casing has been filled with concrete, fill all void space occurring between the casing and drilled shaft excavation with a material which approximates the geotechnical properties of the in-situ soils, in accordance with the Drilled Shaft Installation Plan specified in Subsection 606.03(A)(2) of this Specification and as approved by the Engineer.

When the shaft extends above ground or through a body of water, the portion exposed above ground or through a body of water may be formed with removable casing except when the permanent casing is specified. Strip the removable casing from the shaft in a manner that will not damage the concrete. Casings can be removed when the concrete has attained sufficient strength provided:

- a. Curing of the concrete is continued for a 72-hour period.
- b. The shaft concrete is not exposed to salt water or moving water for 7 days.
- c. The concrete reaches a compressive strength of at least 2500 psi, as determined from concrete cylinder breaks.

Use of removable casing is permitted only if specified on the Plans or approved by the Engineer. Use removable casing in accordance with the equipment and procedures shown in the approved Drilled Shaft Installation Plan, and comply with all other requirements specified herein.

3. *Alternative Casing Methods.* When approved by the Engineer, installation of casing using rotating, oscillating, or vibrating methods will be permitted. Use this alternative casing method in accordance with the equipment and procedures shown in the approved Drilled Shaft Installation Plan, and comply with all other requirements specified herein.

Equip drilled shaft casing with cutting teeth or a cutting shoe and install by rotating, oscillating, or vibrating the casing.

4. *Slurry.* Use slurry in accordance with Subsection 606.02 of this Specification to maintain a stable excavation during excavation and concrete placement operations once water begins to enter the drilled shaft excavation and remain present.

Use slurry to maintain stability during drilled shaft excavation and concrete placement operations in the event that water begins to enter the drilled shaft excavation at a rate of greater than twelve inches per hour, or if the Contractor is not able to restrict the amount of water in the drilled shaft to less than three inches prior to concrete placement, or to

equilibrate water pressure on the sides and base of the drilled shaft excavation when groundwater is encountered or anticipated based on the available subsurface data.

a. *Slurry Technical Assistance.* If slurry is used, the manufacturer's representative, as identified to the Engineer in accordance with Subsection 606.03(A)(3) of this Specification, must:

- i. Provide technical assistance for the use of the slurry.
- ii. Be present at the site prior to introduction of the slurry into a drilled hole.
- iii. Remain at the site during the construction and completion of a minimum of one drilled shaft to adjust the slurry mix to the specific site conditions.

After the manufacturer's representative is no longer present at the site, the Contractor's employee trained in the use of the slurry, as identified to the Engineer in accordance with Subsection 606.03(A)(3) of this Specification, must be present at the site throughout the remainder of shaft slurry operations for this project to perform the duties specified above.

b. *Minimum Level of Slurry in the Excavation.* When slurry is used to maintain a stable excavation, maintain the slurry level in the excavation to obtain hydrostatic equilibrium throughout the construction operation at a height required to provide and maintain a stable hole, but not less than 5 feet above the water table or surface of surrounding water body if at an offshore location.

Provide casing, or other means, as necessary to meet these requirements.

Maintain the slurry level above all unstable zones a sufficient distance to prevent bottom heave, caving or sloughing of those zones.

Throughout all stops in drilled shaft excavation operations, monitor and maintain the slurry level in the excavation the greater of the following elevations:

- i. No lower than the water level elevation outside the drilled shaft.
- ii. Elevation as required to provide and maintain a stable hole.

c. *Cleaning Slurry.* Clean, re-circulate, de-sand, or replace the slurry, as needed, in order to maintain the required slurry properties. Sand content will only be required to be within specified limits immediately prior to concrete placement.

E. *Obstructions.* When obstructions are encountered, notify the Engineer promptly. An obstruction is defined as a specific object (including, but not limited to, boulders, logs, and man-made objects) encountered during the drilled shaft excavation operation which prevents or hinders the advance of the drilled shaft excavation. When efforts to advance past the obstruction to the design drilled shaft tip elevation result in the rate of advance of the drilled shaft drilling equipment being significantly reduced relative to the rate of advance for the portion of the drilled shaft excavation in the geological unit that contains the obstruction, then remove, bypass or break up the obstruction under force account. Blasting will not be permitted unless approved in writing by the Engineer.

Drilling tools that are lost in the excavation will not be considered obstructions, and will be promptly removed by the Contractor. All costs due to lost tool removal will be borne by the Contractor including, but not limited to, costs associated with the repair of hole degradation due to removal operations or an excessive time that the hole remains open.

F. *Protection of Existing Structures.* Control operations to prevent damage to existing structures, utilities, roadways and other facilities. Include preventive measures, but which are not limited to, selecting construction methods and procedures that will prevent excessive caving of the drilled shaft excavation and monitoring and controlling the vibrations from the driving of casing or sheeting, drilling of the shaft, or from blasting, if permitted by the Engineer.

- G. *Slurry Sampling and Testing.* Mix and thoroughly hydrate mineral slurry and polymer slurry in slurry tanks, lined ponds, or storage areas. Draw sample sets from the slurry storage facility and test the samples for conformance with the appropriate specified material properties before beginning slurry placement in the drilled hole. Conform the slurry to the quality control plan included in the Drilled Shaft Installation Plan in accordance with Subsection 606.03(A)(2) of this Specification and as approved by the Engineer. A sample set must be composed of samples taken at mid-height and within two feet of the bottom of the storage area.

Sample and test all slurry in the presence of the Engineer, unless otherwise approved by the Engineer. Record the date, time, names of the persons sampling and testing the slurry, and the results of the tests. Submit a copy of the recorded slurry test results to the Engineer at the completion of each drilled shaft, and during construction of each drilled shaft when requested by the Engineer.

Take and test sample sets of all slurry, composed of samples taken at mid-height and within two feet of the bottom of the drilled shaft, during drilling as necessary to verify the control of the properties of the slurry. As a minimum, take and test the sample sets of polymer slurry at least once every four hours after beginning its use during each shift.

Take and test sample sets of all slurry, as specified, immediately prior to placing concrete.

Demonstrate to the satisfaction of the Engineer that stable conditions are being maintained. If the Engineer determines that stable conditions are not being maintained, immediately take action to stabilize the shaft. Submit a revised Drilled Shaft Installation Plan which addresses the problem and prevents future instability. Do not continue with drilled shaft construction until the damage which has already occurred is repaired in accordance with the Specifications, and until receiving the Engineer's approval of the revised Drilled Shaft Installation Plan.

- H. *Drilled Shaft Excavation Inspection.* Use appropriate means such as a cleanout bucket, air lift or hydraulic pump to clean the bottom of the excavation of all drilled shafts. The base of the drilled shaft excavation cannot be covered with more than three inches of sediment or loose or disturbed material just prior to placing concrete in soil shafts or more than one-half inch for 50 percent of the shaft area in rock sockets.

The excavated drilled shaft will be inspected and approved by the Engineer prior to proceeding with construction. Sound the bottom of the excavated drilled shaft with an airlift pipe, a tape with a heavy weight attached to the end of the tape, a borehole camera with visual sediment depth measurement gauge, or other means acceptable to the Engineer to determine that the drilled shaft bottom meets the requirements in the Contract.

- I. *Assembly and Placement of Reinforcing Steel.* Prior to and during fabrication of the steel reinforcing cage, support the reinforcing bars off the ground surface, and protect the reinforcing bars from contamination with mud and other deleterious materials.

Rigidly brace the reinforcing cage to retain its configuration during handling and construction. Individual or loose bars will not be permitted. Tie all (100%) intersections of vertical and horizontal bars. Show bracing and any extra reinforcing steel required for fabrication of the cage on the working drawings.

Carefully position and securely fasten the reinforcement to provide the minimum clearances specified or shown on the Plans, and to ensure that no displacement of the reinforcing steel cage occurs during placement of the concrete.

Splicing of the reinforcement cage during placement of the cage in the shaft excavation will not be permitted unless otherwise shown on the Plans or approved by the Engineer.

If the reinforcing cage is spliced during placement of the cage into the drilled shaft excavation, the splice details and location of the splices must be in accordance with the Plans and the approved Drilled Shaft Installation Plan. In addition, perform the work within the time limits specified in Subsection 606.03(A).

Securely hold the steel reinforcing cage in position throughout the concrete placement operation. Tie and support the reinforcing steel in the drilled shaft so that the location of the reinforcing steel will remain within allowable tolerance. Use concrete spacers or other approved non-corrosive spacing devices at sufficient intervals (near the bottom, the top and at intervals not exceeding 10 feet vertically) to ensure concentric spacing for the entire cage length. The number of spacers required at each level will be one spacer for each foot of excavation diameter, with a minimum of four spacers at each level. The spacers must be of adequate dimension to ensure an annular space between the outside of the reinforcing cage and the side of the excavation along the entire length of the drilled shaft as shown in the Plans. Provide acceptable feet made of plastic, or concrete (bottom supports) to ensure that the bottom of the cage is maintained at the proper distance above the base of the excavation unless the cage is suspended from a fixed base during the concrete pour.

Remove bracing steel which constricts the interior of the reinforcing cage after lifting the cage if freefall concrete or wet tremie methods of concrete placement are to be used.

Check the elevation of the top of the steel cage before and after the concrete is placed. If the upward displacement of the rebar cage exceeds 2 inches, or if the downward displacement exceeds 6 inches, the drilled shaft will be considered defective. Make corrections to the satisfaction of the Engineer. Do not construct additional drilled shafts until the rebar cage support has been modified in a manner satisfactory to the Engineer.

- J. *Concrete Placement, Curing and Protection.* Commence the Concrete placement as soon as possible after completion of drilled shaft excavation by the Contractor and inspection by the Engineer. Immediately prior to commencing concrete placement, the drilled shaft excavation and the properties of the slurry (if used) must conform to Subsection 606.02 of this Specification. Continue the concrete placement in one operation to the top of the drilled shaft, or as shown in the Plans.

If water is not present (a dry shaft), deposit the concrete through the center of the reinforcement cage by a method which prevents segregation of aggregates. Place the concrete such that the free-fall is vertical down the center of the drilled shaft without hitting the sides, the steel reinforcing bars, or the steel reinforcing bar cage bracing.

If water exists in amounts greater than three inches in depth or enters at a rate of more than twelve inches per hour then fill the drilled shaft excavation with slurry to at least the level specified in Subsection 606.03(D)(4)(b) and concrete placed by tremie methods.

Do not exceed the time limit for concrete placement as defined in the approved Drilled Shaft Installation Plan and demonstrated by a successful technique shaft or test shaft. Commence the concrete placement time at the mixing of the concrete and extend through to the completion of placement of the concrete in the drilled shaft excavation, including removal of any temporary casing. For wet placement methods, the placement time starts at the batching of the initial load of concrete to be placed in the shaft. Prior to concrete placement, provide test results of both a trial

mix and a slump loss test conducted by an approved testing laboratory using approved methods to demonstrate that the concrete meets this defined placement time limit. Maintain the concrete mix with a slump of 4 inches or greater over the defined placement time limit as demonstrated by trial mix and slump loss tests. Conduct the trial mix and slump loss tests at ambient temperatures appropriate for site conditions. Ambient air temperature at the time of concrete placement is not permitted to be greater than the ambient temperature at the time of the concrete trial tests and slump loss tests.

Do not use admixtures such as water reducers, plasticizers, and retarders in the concrete mix unless permitted in the Contract Documents and detailed in the approved Drilled Shaft Installation Plan. Adjust all admixtures, when approved for use, for the conditions encountered on the job so the concrete remains in a workable plastic state throughout the defined placement time limit.

Throughout the underwater concrete placement operation, the discharge end of the tube must remain submerged in the concrete at least five feet and the tube must always contain enough concrete to prevent water from entering. The concrete placement must be continuous until the work is completed, resulting in a seamless, uniform shaft. If the concrete placement operation is interrupted, the Engineer may require the Contractor to prove by core drilling or other tests that the drilled shaft contains no voids or horizontal joints. If testing reveals voids or joints, repair them or replace the drilled shaft at no expense to the Department. Responsibility for coring and testing costs, and calculation of time extension, will be in accordance with Subsection 606.03(M) of this Specification.

Before placing any fresh concrete against concrete deposited in water or slurry (construction joint), remove all scum, laitance, loose gravel and sediment on the surface of the concrete deposited in water or slurry, and chip off any high spots on the surface of the existing concrete that would prevent any steel reinforcing bar cage from being placed in the position required by the Plans.

Complete a concrete yield plot for each wet shaft poured by tremie methods. This yield plot will be submitted to the Department within twenty four (24) hours of completion of the concrete pour.

Do not perform casing installation or drilled shaft excavation operations within a clear distance of three diameters of a newly poured drilled shaft within twenty (24) hours of the placement of concrete and only when the concrete has reached a minimum compressive strength of 1800 psi.

- K. *Tremies*. When placing concrete underwater, use a concrete pump or gravity tremie. A tremie must have a hopper at the top that empties into a watertight tube at least eight inches in diameter. If a pump is used, a watertight tube must be used with a minimum diameter of four inches. The discharge end of the tube on the tremie or concrete pump line must include a device to seal out water while the tube is first filled with concrete. In lieu of a seal at the discharge end of the pipe, the Contractor may opt to place a "Pig" or "Rabbit" in the hopper prior to concrete placement which moves through the tremie when pushed by the concrete, forcing water or slurry from the tremie pipe.

Do not use hopper and tubes that contain aluminum parts that will have contact with the concrete. The inside and outside surfaces of the tubes must be clean and smooth to allow both flow of concrete and the unimpeded withdrawal of the tube during concrete placement.

- L. *Drilled Shaft Construction Tolerances.* Construct the drilled shafts so that the center of the poured shaft at the top of the drilled shaft or mudline, whichever is lower, is within the following horizontal tolerances:

Drilled Shaft Diameter	Tolerance
Greater than 2'-0" and less than 5'-0"	4"
5'-0" or larger	6"

Drilled shafts in soil must be within 1.5 percent of plumb. Drilled shafts in rock must be within 2.0 percent of plumb. Plumbness will be measured from the top of poured drilled shaft elevation or mudline, whichever is lower.

During drilling or excavation of the drilled shaft, make frequent checks on the plumbness, alignment, and dimensions of the drilled shaft. Any deviation exceeding the allowable tolerances will be corrected with a procedure approved by the Engineer.

Do not allow the drilled shaft steel reinforcing bars to be higher than six inches above or three inches below the plan elevation.

The reinforcing cage must be concentric with the drilled shaft excavation within a tolerance of 1-1/2 inches.

The top elevation of the completed drilled shaft must have a tolerance of plus one inch or minus three inches.

Do not allow the diameter of the drilled shaft to be less than the diameter shown on the Plans.

Ensure that tolerances for casings are in accordance with American Pipe Institute tolerances applicable to regular steel pipe.

Drilled shaft excavations and completed drilled shafts not constructed within the required tolerances will be considered defective. The Contractor is responsible for correcting all defective drilled shafts to the satisfaction of the Engineer. Materials and work necessary, including engineering analysis and redesign, to complete corrections for out-of-tolerance drilled shafts will be furnished without either cost to the Department or an extension of the completion date of the project. Redesign drawings and computations submitted will be signed by a registered Professional Engineer licensed in the State of Delaware.

- M. *Integrity Testing.* Crosshole sonic log (CSL) testing must be performed on all drilled shafts. Accommodate the crosshole sonic log testing by furnishing and installing access tubes in accordance with **Section IXXX** of this Specification.

Install access tubes for crosshole sonic log testing in all drilled shafts, except as otherwise noted herein, to permit access for the crosshole sonic log test probes. If, in the opinion of the Engineer, the condition of the drilled shaft excavation permits drilled shaft construction in the dry, the Engineer may specify that the testing be omitted.

Securely attach the access tubes to the interior of the reinforcement cage of the drilled shaft. Furnish and install one access tube for each foot of drilled shaft diameter, rounded to the nearest whole number, unless otherwise shown in the Plans. A minimum of three tubes will be required. Place the access tubes around the drilled shaft, inside the spiral or hoop reinforcement and three inches clear of the vertical reinforcement, at a uniform spacing measured along the circle passing

through the centers of the access tubes. If these minimums cannot be met due to close spacing of the vertical reinforcement, then bundle the access tubes with the vertical reinforcement.

If trimming the cage is required and access tubes for crosshole sonic log testing are attached to the cage, either shift the access tubes up the cage, or cut the access tubes provided that the cut tube ends are adapted to receive the watertight cap as specified.

Install the access tubes in straight alignment and as near to parallel to the vertical axis of the reinforcement cage as possible. Extend the access tubes from the bottom of the drilled shaft to at least two feet above the top of the drilled shaft. Splice joints in the access tubes, if required to achieve full length access tubes, must be watertight. Clear the access tubes of all debris and extraneous materials before installing the access tubes. Care must be taken to prevent damaging the access tubes during reinforcement cage installation and concrete placement operations in the drilled shaft excavation.

Fill the access tubes with potable water before concrete placement, and reinstall the top watertight threaded caps.

Prior to performing any crosshole sonic log testing operations specified in this subsection, remove the concrete at the top of the drilled shaft down to sound concrete.

The Department will perform crosshole sonic log testing and analysis on all completed drilled shafts designated for testing by the Engineer. The Department will require advance notice from the Contractor to schedule all crosshole sonic log testing. The Contractor will give at least forty eight (48) hours' notice to the Engineer of the time the concrete in each drilled shaft to be sufficiently cured to allow for crosshole sonic log testing.

Perform the testing after the drilled shaft concrete has cured at least ninety six (96) hours. Additional curing time prior to testing may be required if the drilled shaft concrete contains admixtures, such as set retarding admixture or water reducing admixture. The additional curing time prior to testing required under these circumstances will not serve as grounds for additional compensation or extension of time to the Contractor. Do not perform any subsequent construction on the completed drilled shaft until the CSL tests are approved and the drilled shaft accepted by the Engineer.

After placing the drilled shaft concrete and before beginning the crosshole sonic log testing of a drilled shaft, inspect the access tubes. Replace each access tube that the test probe cannot pass through, at the Contractor's expense, with a two inch diameter hole cored through the concrete for the entire length of the drilled shaft. Unless directed otherwise by the Engineer, locate the cored holes approximately six inches inside the reinforcement and do not damage the drilled shaft reinforcement. Log descriptions of inclusions and voids in cored holes and submit a copy of the log to the Engineer. Findings from cored holes must be preserved, identified as to location, and made available for inspection by the Engineer.

The Engineer will determine final acceptance of each drilled shaft, based on the crosshole sonic log test results and analysis for the tested shafts and a review of the visual inspection reports for the subject drilled shaft, and will provide a response to the Contractor within three working days after receiving the test results and analysis submittal.

The Engineer may approve continuing with drilled shaft construction prior to approval and acceptance of the first shaft if the Engineer's observations of the construction of the first shaft are

satisfactory, including, but not limited to, conformance to the Drilled Shaft Installation Plan as approved by the Engineer, and the Engineer's review of Contractor's daily reports and inspector's daily logs concerning excavation, steel reinforcing bar placement, and concrete placement.

If the Engineer determines that the concrete placed under slurry for a given drilled shaft is structurally inadequate, that drilled shaft will be rejected. The placement of concrete under slurry will be suspended until the Contractor submits to the Engineer written changes to the methods of drilled shaft construction needed to prevent future structurally inadequate drilled shafts, and receives the Engineer's written approval of the submittal.

If the Engineer determines that additional investigation is necessary, or if the Contractor requests, the Engineer may direct that additional testing be performed at a drilled shaft. At the Engineer's request, drill a corehole in any questionable quality drilled shaft (as determined from crosshole sonic log testing and analysis or by observation of the Engineer) to explore the drilled shaft condition. The number, locations, diameter and depth of the core holes and lengths of individual core runs will be determined by the Engineer. Coring procedures must minimize abrasion and erosion of the core samples, and must avoid damage to the steel reinforcement. Log descriptions of inclusions and voids in cored holes and submit a copy of the log to the Engineer. Preserve the recovered core in suitably labeled wood core boxes, identified as to location and depth, and made available for inspection by the Engineer. The Engineer may direct water pressure testing in the core holes, and/or unconfined compression testing and other laboratory testing on selected samples from the concrete core.

If subsequent testing at a drilled shaft indicates the presence of a defect(s) in the drilled shaft, the testing costs and the delay costs resulting from the additional testing will be borne by the Contractor. If this additional testing indicates that the drilled shaft has no defect, the testing costs and the delay costs resulting from the additional testing will be paid by the Department, and, if the drilled shaft construction is on the critical path of the Contractor's schedule, a time extension equal to the delay created by the additional testing will be granted.

For all drilled shafts determined to be unacceptable, submit a plan for further investigation or remedial action to the Engineer for approval. All modifications to the dimensions of the drilled shafts, as shown in the Plans, required by the investigation and remedial action plan must be supported by calculations and working drawings. All investigation and remedial correction procedures and designs must be prepared by a registered Professional Engineer licensed in the State of Delaware, and submitted to the Engineer for approval. Do not begin repair operations until receiving the Engineer's written approval of the investigation and remedial action plan.

Prior to beginning coring, submit the method and equipment to be used to drill and remove cores from drilled shaft concrete to the Engineer, and do not begin coring until the Engineer's written approval has been received. The coring method and equipment will include for complete core recovery and will minimize abrasion and erosion of the core.

Dewater all access tubes and cored holes and fill with grout after tests are completed and the drilled shaft is accepted. Fill the access tubes and cored holes using grout tubes that extend to the bottom of the tube or hole or into the grout already placed.

Alternative non-destructive tests such as Gamma-Gamma, Sonic Echo/Impulse Response, or Thermal Integrity Profiling may be specified on the Plans or directed by the Engineer to use alongside, or in lieu of, CSL testing. Comply with all requirements for the alternate test methods in accordance with the Plans or Special Provisions.

- N. *Drilled Shaft Load Tests*. Install test shafts at the locations shown on the Plans unless otherwise directed or approved by the Engineer.

Install test shafts to the same dimensions, details and elevations shown on the Plans, and install using the same equipment and installation procedures proposed for installation of the foundation drilled shafts.

If the equipment or procedures are changed following the completion of load testing, install additional load test shafts, and conduct additional load tests as directed by the Engineer at no additional cost to the Department.

Complete all load testing and have the results evaluated by the Engineer before installing any production drilled shafts, unless otherwise authorized by the Engineer.

1. *Static Load Tests*. Perform static load tests in accordance with the procedures specified in ASTM D 1143.
2. *Force Pulse (Rapid) Load Tests*. Perform force pulse (rapid) load tests in accordance with the procedures specified in ASTM D 7383.
3. *Bi-Directional Load Cell Testing*. Install load cells and load test instrumentation in accordance with the bi-directional load cell supplier recommendations, instructions, and procedure manual(s), as approved by the Engineer.

The bi-directional load cells must be capable of expanding to not less than 6 inches while maintaining the applied test load.

The Contractor must be responsible for coordinating with the load cell supplier to determine and/or verify all required equipment, materials, quantities, procedures, and all other applicable items necessary to complete the load testing shown on the Plans.

Furnish an acceptable pressurized gas source, a hydraulic pump, hydraulic lines, calibrated hydraulic gauge and other equipment and material necessary to perform the load tests. Furnish fresh, potable water from an approved source to form the hydraulic fluid used to pressurize the bi-directional load cells.

Furnish, install and monitor vibrating wire strain gauges as shown on the Plans and as directed by the Engineer. Place the strain gauges in pairs on opposite sides of the reinforcing cage at the elevations shown on the Plans, unless otherwise directed by the Engineer.

Attach two LVDT vibrating wire displacement gauges to each load cell to monitor the expansion and contraction of the load cell. In addition, mount two LVDT gauges on an independent reference beam and set on opposite sides of the top of the test shaft to monitor axial shaft displacement.

Set two telltale rods on the top of each load cell to monitor the displacement of the top of the load cell. The telltale must consist of a 3/8-inch diameter stainless steel rod, greased for reducing friction and corrosion, and placed inside a constant 3/4-inch diameter pipe. Individual sections of telltales must be joint coupled flush so that each rod is of uniform diameter throughout its length.

Furnish a portable computer and electronic logging equipment to simultaneously monitor all instrumentation at time intervals designated by the Engineer.

Assemble the load cells, piping and other attachments in preparation for installation in accordance with the requirements of the bi-directional load cell supplier, unless otherwise specified herein or directed by the Engineer. The following guidelines must be followed.

- a. Weld steel top and bottom bearing plates to the load cells. Provide holes through the bearing plates, as appropriate, to facilitate placement of tremie concrete.
- b. Coat the upper surface of the bottom steel bearing plate with grease prior to installation into the shaft, to prevent concrete bonding with the bottom plate.
- c. Attach the load cells and plate assembly to the reinforcement cage. Securely fasten all hydraulic hoses, telltale casing, slip joints, etc. to the rebar cage. Prior to installation into the drilled shaft excavation, protect the top of any piping to keep dirt, concrete or other deleterious materials from entering the piping.
- d. Limit the deflection of the cage to a maximum of 2 feet between pick points while lifting the cage from the horizontal position to vertical. Provide additional support, bracing, strong backs, etc. to maintain the deflection within the specified tolerance.

For each load test, place the load on the drilled shaft in increments of five percent of the estimated maximum test load shown on the Plans, or until the nominal resistance load (as indicated by the instruments) is approached, or to the maximum capacity of the load cell, whichever occurs first. Unless the maximum capacity of the load cell has been reached, apply increments of 2.5 percent of the estimated maximum test load until the limiting load is attained, or the drilled shaft top displacement reaches 2 inches, or to the maximum extension of the load cell. When the load cell will be used for a subsequent loading stage, the Engineer may interrupt the loading sequence at a load cell opening of approximately 3 inches, or less. Maintain each load increment for a minimum period of 5 minutes, with complete sets of readings obtained and recorded from all gauges and instruments at 1, 2 and 5 minutes after application of the load increment. Apply each increment of load within the minimum length of time practical and take the instrument system readings immediately. It is intended that the addition of a load increment and the completion of the instrument system readings be completed within 5 to 15 minutes. The Engineer may elect to hold the maximum applied load for up to one hour.

Remove the load in decrements of about 10 percent of the maximum test load. Remove each decrement of load within the minimum length of time practical and take the instrument system readings immediately. It is intended that the removal of a load decrement and the completion of the instrument system readings be completed within 5 to 15 minutes. The Engineer may also require a reloading cycle with ten loading increments and five unloading decrements. Record the final recovery of the drilled shaft for a period up to one hour after the last unload interval.

Submit a preliminary test report containing the load displacement curves and other test data to the Engineer within three days of completing each load test. Submit the final report on the load tests to the Engineer within ten days after completion of each load test. Include at least the following items in the test report:

- a. Test shaft identification number and location.
- b. Date(s) of testing.
- c. Description of the test shaft details, instrumentation and test procedures.
- d. Tables presenting all instrumentation data.
- e. Plots of load versus displacement (up and down) for each load cell level, for each stage of the test.
- f. Plots of load along the length of the drilled shaft determined from the strain gauge data for at least ten applied load increments.

- g. Summary of unit side resistance along the length of the drilled shaft and end bearing resistance.
- h. Plots of creep displacement for each load increment.
- i. Plot of equivalent top-of-shaft displacement for the test shaft, developed from the load test data.

After completion of the load test to the satisfaction of the Engineer, and when authorized in writing by the Engineer, flush all hydraulic fluid from the bi-directional load cells and hydraulic lines, and replace with cement grout in accordance with the approved Drilled Shaft Installation Plan. Also grout any voids remaining outside the load cells after completion of the load test.

- O. *Technique Shafts.* Demonstrate the adequacy of its methods, techniques and equipment by successfully constructing a technique shaft or shafts in accordance with the requirements shown on the Plans and these Specifications. Position the technique shaft(s) at the location(s) shown on the Plans or as directed by the Engineer, but not less than a clear distance of three drilled shaft diameters from the closest production shaft. Drill the technique shaft(s) to the maximum diameter and maximum depth of any production drilled shaft shown in the Plans. Unless shown otherwise on the Plans, reinforce the technique shaft(s) with the same reinforcement as the corresponding size production shaft, and also include CSL tubes as specified herein. Technique shaft(s) must be completed and accepted by the Engineer prior to initiating installation of the load test shafts and foundation drilled shafts. Failure by the Contractor to demonstrate to the Engineer the adequacy of methods and equipment will be reason for the Engineer to require alterations in equipment and/or method by the Contractor to eliminate unsatisfactory results. Any additional technique shaft(s) required demonstrating the adequacy of altered methods or construction equipment will be at the Contractor's expense. Once approval has been given by the Engineer to construct production drilled shafts, no changes will be permitted in the methods or equipment used to construct the satisfactory technique shaft(s) without the written approval of the Engineer.

The technique shaft(s) will be used by the Engineer to determine if the Contractor can:

1. Control dimensions and alignment of excavations within tolerance.
2. Install casing and remove temporary casing.
3. Seal the casing into impervious materials.
4. Control the size of the excavation under caving conditions by the use of a mineral or polymer slurry or by other means.
5. Properly clean the completed drilled shaft excavation.
6. Construct drilled shafts in open water areas.
7. Handle and install reinforcing cages.
8. Satisfactorily place concrete meeting the Specification requirements within the prescribed time limit.
9. Satisfactorily execute any other necessary construction operation.

When authorized in writing by the Engineer, cut off the technique shaft(s) not less than 2 feet below finished grade and left in place. Restore the disturbed areas at the sites of the technique shaft(s) as nearly as practical to their original condition.

606.04 Method of Measurement.

- A. The Engineer will measure drilled shafts by the length in ft (m) from the plan top of shaft elevation to the final bottom of shaft elevation. The Engineer will not separately measure excavation, blasting, slurry, reinforcing steel, concrete, grout, integrity testing tubes, or non-destructive testing.

- B. The Engineer will measure technique shafts by the length in ft (m) from the existing ground surface elevation at the center of the trial shaft hole prior to drilling to the authorized bottom elevation of the hole. The Engineer will not separately measure excavation, blasting, slurry, reinforcing steel, concrete, grout, integrity testing tubes, or non-destructive testing.
- C. The Engineer will measure permanent casing by the length in ft (m) of each size casing used, as measured along the casing from the top of the shaft elevation or the top of casing, whichever is lower, to the bottom of the casing.
- D. The Engineer will measure load tests by the number of load tests completed according to the specified loading procedures and to the designated maximum load shown on the plans. Payment will include all costs related to the performance of the load test and for the reporting of procedures and results.
- E. The Engineer will measure exploratory drilling by the length in ft (m) from the ground elevation where the drilling begins to the bottom of the exploration hole.

606.05 Basis of Payment.

- A. The Engineer will pay for accepted quantities at the contract unit price as follows:

Item No.	Item Description	UOM
606000	DRILLED SHAFT, 30"	LF
606001	DRILLED SHAFT, 36"	LF
606002	DRILLED SHAFT, 42"	LF
606003	DRILLED SHAFT, 48"	LF
606004	DRILLED SHAFT, 60"	LF
606005	DRILLED SHAFT, 72"	LF
606010	TECHNIQUE SHAFT, 30"	LF
606011	TECHNIQUE SHAFT, 36"	LF
606012	TECHNIQUE SHAFT, 42"	LF
606013	TECHNIQUE SHAFT, 48"	LF
606014	TECHNIQUE SHAFT, 60"	LF
606015	TECHNIQUE SHAFT, 72"	LF
606020	PERMANENT CASING FOR DRILLED SHAFT, 30" DIAMETER	LF
606021	PERMANENT CASING FOR DRILLED SHAFT, 36" DIAMETER	LF
606022	PERMANENT CASING FOR DRILLED SHAFT, 42" DIAMETER	LF

606023	PERMANENT CASING FOR DRILLED SHAFT, 48" DIAMETER	LF
606024	PERMANENT CASING FOR DRILLED SHAFT, 60" DIAMETER	LF
606025	PERMANENT CASING FOR DRILLED SHAFT, 72" DIAMETER	LF
606030	LOAD TESTING OF DRILLED SHAFTS	EACH
606031	EXPLORATORY DRILLING	LF

- B. Such payment is full compensation for furnishing all materials, equipment, labor, and incidentals to complete the work as specified.

ITEM 302XXX – LIGHTWEIGHT AGGREGATE FILL

Description:

This item consists of furnishing all labor, materials, and equipment required for the installation of lightweight aggregate fill as shown on the drawings or as directed by the Engineer.

Materials:

Lightweight Aggregate Fill shall be a lightweight expanded shale aggregate or approved rotary kiln-produced expanded shale substitute meeting all the requirements of a recently completed (2 years max.) ASTM C 330 certification. No by-product slags, coal derived by-product aggregates (cinders, bottom ash, fly ash) or pumice, scoria, or tuff shall be permitted.

The lightweight aggregate fill shall have a proven record of durability and be non-corrosive (less than 100 ppm chloride when measured by AASHTO T 260), and meet the following physical property requirements:

A. Delivered Gradation:

Sieve Size	Percent by Weight Passing
¾"	100-90
½"	70-50
#4	10-0

B. The dry loose unit weight shall be less than 45 pounds per cubic foot (pcf). The lightweight aggregate fill producer shall submit verification of a compacted density of less than 60 pcf when measured by a one-point compaction ("Proctor") test conducted in accordance with ASTM D698, "Standard Test methods for Laboratory Compaction Characteristics of Soil Using Standard Effort (12,400 ft-lbf /cu ft)" (AASHTO T-99).

C. The lightweight aggregate producer shall submit verification that the angle of internal friction shall be greater than 40° when measured in a triaxial compression test on a laboratory sample with a minimum diameter of 10 inches. (ASTM D 698).

D. The maximum Los Angeles Abrasion loss when tested in accordance with ASTM C 131 Modified (8 grading) shall be <30 percent.

E. The minimum permeability shall be 25cm/sec when tested in accordance with ASTM D 2434.

F. The pH shall be between 6.5 and 9.0

G. Absorption: ASTM C 127 (24 hours)	Maximum:	15%
	Minimum:	9%

H. Soundness: ASTM C 88	Maximum 3% loss using the Magnesium Sulfate method
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Construction Methods:

The lightweight aggregate shall be installed after the respective excavation has been approved by the Engineer. Compaction shall be completed and verified in a manner meeting the recommendations and requirement of the material manufacturer. Any aggregate which has been degraded, or has been contaminated by soil, debris or other deleterious materials shall be removed and replaced at the Contractor's expense.

Method of Measurement:

The quantity of lightweight aggregate fill will be measurement in cubic yards of material actually placed and accepted. Measurement will be computed using the method of average end areas between original cross sections and final cross sections after placement of the lightweight aggregate fill.

Basis of Payment:

Payment shall be made at the contract unit price per cubic yard for lightweight aggregate. This price shall be full compensation for furnishing all materials, for preparing and placing these materials, and for all labor, equipment tools, and incidentals necessary to complete the item.